

CONSORZIO DI BONIFICA STORNARA E TARA

viale Magna Grecia, 240 - 74121 TARANTO

*"RIPRISTINO DEL PONTE TUBO DELL'IMPIANTO IRRIGUO CONSORTILE
SX BRADANO UBICATO IN ATTRAVERSAMENTO DELLA LAMA DI LATERZA"
COMUNE DI CASTELLANETA (TARANTO)*

PROGETTO DEFINITIVO

CIG 7845120DD0



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ELABORATO	DATA	SCALA	ALLEGATO
Verifica strutturale di ripristino dei pulvini	02/2021	-	R.7.s.3

AGGIORNAMENTO	DATA	DESCRIZIONE

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VERIFICA PULVINI (armature effetto piastra):

PARAMETRI GENERALI

CASI DI CARICO:

Nome	Descrizione
1	SLU
2	SLU VENTYOY
6	SLU con SISMAX PRINC
7	SLU con SISMAX PRINC
8	SLU con SISMAZ PRINC
13	SLU Solo Perm.

DATI:

tensione di snervamento acciaio (fyk):	450	N/mm2
coefficiente sicurezza acciaio	: 1.15	
deformazione ultima acciaio	: 1.86	per mille
deformazione ultima cls	: 3.5	per mille
rapporto rottura/snervamento (k):	1	
resistenza cilindrica cls (fck):	24.9	N/mm2
coefficiente sicurezza cls	: 1.5	
coefficiente riduttivo (alfa):	0.85	
copriferro inferiore (asse armatura):	3	cm
copriferro superiore (asse armatura):	3	cm

LEGENDA:

spess	= spessore guscio. Verifica effettuata su sezione BxH, con B=1 cm e H="spess" cm
Af	= area disposta al lembo teso, in cm2 al metro
Afc	= area disposta al lembo compresso, in cm2 al metro
Mom	= momento flettente [kNm/m]
Nor	= sforzo normale [kN]
epsC	= deformazione cls [per mille]
epsF	= deformazione acciaio [per mille]

NOTA:

Per gli elementi non dissipativi la permanenza in campo elastico è ottenuta limitando la deformazione dell'acciaio alla deformazione di snervamento (1.86 per mille) e quella del calcestruzzo al 2 per mille.

MACROGUSCIO: Pulvino1

GUSCI	spess	INFERIORE ORIZZONTALE						INFERIORE VERTICALE							
		Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF		
101	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	3.	0.	0.00	0.02		
102	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	3.	0.	0.00	0.01		
103	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	3.	0.	0.00	0.01		
104	55	20.52	20.52	11.	0.	0.02	0.05	19.99	34.27	4.	0.	0.01	0.02		
105	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00		
106	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00		
107	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00		
108	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00		
109	82	20.52	20.52	5.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00		
110	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00		
111	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00		
112	82	20.52	20.52	5.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00		
113	82	20.52	20.52	5.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00		
114	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00		
115	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00		
116	82	20.52	20.52	5.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00		
117	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00		
118	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00		
119	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00		
120	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00		
121	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	3.	0.	0.00	0.02		
122	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	3.	0.	0.00	0.01		
123	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	3.	0.	0.00	0.01		
124	55	20.52	20.52	11.	0.	0.02	0.05	19.99	34.27	4.	0.	0.01	0.02		
GUSCI	spess	SUPERIORE ORIZZONTALE						SUPERIORE VERTICALE							
		Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF		
101	55	20.52	20.52	20.	0.	0.03	0.10	34.27	19.99	10.	0.	0.01	0.03		
102	55	20.52	20.52	203.	0.	0.33	0.98	34.27	19.99	8.	0.	0.01	0.02		
103	55	20.52	20.52	215.	0.	0.35	1.04	34.27	19.99	8.	0.	0.01	0.02		
104	55	20.52	20.52	21.	0.	0.03	0.10	34.27	19.99	10.	0.	0.01	0.03		
105	55	20.52	20.52	21.	0.	0.03	0.10	34.27	19.99	140.	0.	0.20	0.41		
106	55	20.52	20.52	215.	0.	0.35	1.04	34.27	19.99	135.	0.	0.19	0.40		
107	55	20.52	20.52	219.	0.	0.36	1.06	34.27	19.99	136.	0.	0.19	0.40		
108	55	20.52	20.52	20.	0.	0.03	0.10	34.27	19.99	144.	0.	0.20	0.43		
109	82	20.52	20.52	17.	0.	0.01	0.05	34.27	19.99	731.	0.	0.53	1.40		
110	82	20.52	20.52	224.	0.	0.19	0.70	34.27	19.99	730.	0.	0.53	1.40		
111	82	20.52	20.52	224.	0.	0.19	0.70	34.27	19.99	730.	0.	0.53	1.40		
112	82	20.52	20.52	16.	0.	0.01	0.05	34.27	19.99	731.	0.	0.53	1.40		
113	82	20.52	20.52	20.	0.	0.02	0.06	34.27	19.99	730.	0.	0.53	1.40		
114	82	20.52	20.52	225.	0.	0.19	0.71	34.27	19.99	729.	0.	0.53	1.40		
115	82	20.52	20.52	225.	0.	0.20	0.71	34.27	19.99	729.	0.	0.53	1.40		
116	82	20.52	20.52	19.	0.	0.02	0.06	34.27	19.99	730.	0.	0.53	1.40		
117	55	20.52	20.52	18.	0.	0.03	0.09	34.27	19.99	140.	0.	0.19	0.41		
118	55	20.52	20.52	209.	0.	0.34	1.01	34.27	19.99	134.	0.	0.19	0.40		
119	55	20.52	20.52	225.	0.	0.37	1.09	34.27	19.99	135.	0.	0.19	0.40		
120	55	20.52	20.52	17.	0.	0.03	0.08	34.27	19.99	143.	0.	0.20	0.42		
121	55	20.52	20.52	21.	0.	0.03	0.10	34.27	19.99	10.	0.	0.01	0.03		
122	55	20.52	20.52	203.	0.	0.33	0.98	34.27	19.99	8.	0.	0.01	0.02		
123	55	20.52	20.52	215.	0.	0.35	1.04	34.27	19.99	8.	0.	0.01	0.02		
124	55	20.52	20.52	21.	0.	0.03	0.10	34.27	19.99	10.	0.	0.01	0.03		
***** TAGLIO PERPENDICOLARE															
GUSCI	τx	τy	τt	GUSCI	τx	τy	τt	GUSCI	τx	τy	τt	GUSCI	τx	τy	τt
101	0.5	0.3	0.4	102	0.5	0.4	0.5	103	0.5	0.3	0.5	104	0.5	0.3	0.4
104	0.5	0.3	0.4	105	0.5	1.7	1.6	106	0.5	1.5	1.1	107	0.5	1.6	1.2
107	0.5	1.6	1.2	108	0.5	1.6	1.6	109	0.4	0.8	0.7	110	0.8	0.9	0.9
110	0.8	0.9	0.9	111	0.8	0.9	0.9	112	0.4	0.7	0.7				

113	0.4	0.7	0.7	114	0.8	0.9	0.9	115	0.8	0.9	0.9
116	0.4	0.7	0.7	117	0.5	1.6	1.5	118	0.5	1.5	1.1
119	0.5	1.5	1.1	120	0.5	1.6	1.5	121	0.5	0.3	0.4
122	0.5	0.3	0.5	123	0.5	0.4	0.5	124	0.5	0.3	0.4

VERIFICHE A PUNZONAMENTO

	Norm [kN]	beta	sigT [N/mm2]	Pcrit [cm]	Ro [%]	Acrit [cm2]	VRd,c [kN]	VEd [kN]	A staffe [cm2]	VRd,cs [kN]	si	
A	1	-2800.547	1.54	0.010	621.8	0.26	112174.4	1651.220	3811.610	95.3	-0.010	si

MACROGUSCIO: Pulvino2

GUSCI	spess	INFERIORE ORIZZONTALE						INFERIORE VERTICALE					
		Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
201	55	20.52	20.52	9.	0.	0.01	0.04	19.99	34.27	41.	0.	0.06	0.20
202	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	34.	0.	0.05	0.17
203	55	20.52	20.52	5.	0.	0.01	0.03	19.99	34.27	30.	0.	0.04	0.15
204	55	20.52	20.52	31.	0.	0.05	0.15	19.99	34.27	36.	0.	0.05	0.18
205	55	20.52	20.52	12.	0.	0.02	0.06	19.99	34.27	34.	0.	0.05	0.17
206	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	52.	0.	0.08	0.26
207	55	20.52	20.52	12.	0.	0.02	0.06	19.99	34.27	56.	0.	0.08	0.28
208	55	20.52	20.52	31.	0.	0.05	0.15	19.99	34.27	71.	0.	0.11	0.35
209	82	20.52	20.52	11.	0.	0.01	0.03	19.99	34.27	0.	0.	0.00	0.00
210	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
211	82	20.52	20.52	7.	0.	0.01	0.02	19.99	34.27	0.	0.	0.00	0.00
212	82	20.52	20.52	24.	0.	0.02	0.08	19.99	34.27	0.	0.	0.00	0.00
213	82	20.52	20.52	11.	0.	0.01	0.03	19.99	34.27	0.	0.	0.00	0.00
214	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
215	82	20.52	20.52	7.	0.	0.01	0.02	19.99	34.27	0.	0.	0.00	0.00
216	82	20.52	20.52	24.	0.	0.02	0.08	19.99	34.27	0.	0.	0.00	0.00
217	55	20.52	20.52	12.	0.	0.02	0.06	19.99	34.27	27.	0.	0.04	0.13
218	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	47.	0.	0.07	0.23
219	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	51.	0.	0.08	0.25
220	55	20.52	20.52	31.	0.	0.05	0.15	19.99	34.27	65.	0.	0.10	0.32
221	55	20.52	20.52	9.	0.	0.01	0.04	19.99	34.27	40.	0.	0.06	0.20
222	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	33.	0.	0.05	0.16
223	55	20.52	20.52	6.	0.	0.01	0.03	19.99	34.27	30.	0.	0.04	0.15
224	55	20.52	20.52	30.	0.	0.05	0.15	19.99	34.27	36.	0.	0.05	0.18

GUSCI	spess	SUPERIORE ORIZZONTALE						SUPERIORE VERTICALE					
		Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
201	55	20.52	20.52	24.	0.	0.04	0.11	34.27	19.99	37.	0.	0.05	0.11
202	55	20.52	20.52	211.	0.	0.35	1.02	34.27	19.99	37.	0.	0.05	0.11
203	55	20.52	20.52	288.	0.	0.48	1.39	34.27	19.99	41.	0.	0.06	0.12
204	55	20.52	20.52	65.	0.	0.11	0.31	34.27	19.99	50.	0.	0.07	0.15
205	55	20.52	20.52	22.	0.	0.04	0.11	34.27	19.99	136.	0.	0.19	0.40
206	55	20.52	20.52	224.	0.	0.37	1.08	34.27	19.99	164.	0.	0.23	0.48
207	55	20.52	20.52	311.	0.	0.51	1.50	34.27	19.99	172.	0.	0.24	0.51
208	55	20.52	20.52	66.	0.	0.11	0.32	34.27	19.99	194.	0.	0.27	0.57
209	82	20.52	20.52	22.	0.	0.02	0.07	34.27	19.99	763.	0.	0.55	1.46
210	82	20.52	20.52	202.	0.	0.17	0.63	34.27	19.99	762.	0.	0.55	1.46
211	82	20.52	20.52	281.	0.	0.24	0.88	34.27	19.99	762.	0.	0.55	1.46
212	82	20.52	20.52	32.	0.	0.03	0.10	34.27	19.99	763.	0.	0.55	1.46
213	82	20.52	20.52	21.	0.	0.02	0.07	34.27	19.99	736.	0.	0.53	1.41
214	82	20.52	20.52	206.	0.	0.18	0.65	34.27	19.99	735.	0.	0.53	1.41
215	82	20.52	20.52	264.	0.	0.23	0.83	34.27	19.99	735.	0.	0.53	1.41
216	82	20.52	20.52	31.	0.	0.03	0.10	34.27	19.99	735.	0.	0.53	1.41
217	55	20.52	20.52	21.	0.	0.03	0.10	34.27	19.99	134.	0.	0.19	0.40
218	55	20.52	20.52	217.	0.	0.36	1.05	34.27	19.99	163.	0.	0.23	0.48
219	55	20.52	20.52	288.	0.	0.47	1.39	34.27	19.99	171.	0.	0.24	0.50
220	55	20.52	20.52	63.	0.	0.10	0.30	34.27	19.99	192.	0.	0.27	0.57
221	55	20.52	20.52	23.	0.	0.04	0.11	34.27	19.99	36.	0.	0.05	0.11
222	55	20.52	20.52	210.	0.	0.35	1.02	34.27	19.99	37.	0.	0.05	0.11
223	55	20.52	20.52	284.	0.	0.47	1.37	34.27	19.99	40.	0.	0.06	0.12
224	55	20.52	20.52	62.	0.	0.10	0.30	34.27	19.99	50.	0.	0.07	0.15

***** TAGLIO PERPENDICOLARE

GUSCI	tx	ty	tz	GUSCI	tx	ty	tz	GUSCI	tx	ty	tz
201	0.5	0.3	0.4	202	0.5	0.3	0.5	203	0.5	0.4	0.5
204	0.5	0.3	0.4	205	0.5	1.7	1.6	206	0.5	1.6	1.2
207	0.5	1.5	1.1	208	0.5	1.6	1.6	209	0.4	0.8	0.8
210	0.8	0.9	0.9	211	0.8	0.9	0.9	212	0.4	0.7	0.7
213	0.4	0.7	0.7	214	0.8	0.9	0.9	215	0.8	0.9	0.9
216	0.4	0.7	0.7	217	0.5	1.6	1.5	218	0.5	1.5	1.1
219	0.5	1.5	1.1	220	0.5	1.6	1.5	221	0.5	0.3	0.4
222	0.5	0.4	0.5	223	0.5	0.3	0.5	224	0.5	0.3	0.4

VERIFICHE A PUNZONAMENTO

	Norm [kN]	beta	sigT [N/mm2]	Pcrit [cm]	Ro [%]	Acrit [cm2]	VRd,c [kN]	VEd [kN]	A staffe [cm2]	VRd,cs [kN]	si	
A	2	-2800.416	1.54	0.010	621.8	0.26	112175.1	1651.220	3811.410	95.3	-0.010	si

MACROGUSCIO: Pulvino3

GUSCI	spess	INFERIORE ORIZZONTALE						INFERIORE VERTICALE					
		Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
301	55	20.52	20.52	12.	0.	0.02	0.06	19.99	34.27	5.	0.	0.01	0.03
302	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	4.	0.	0.01	0.02
303	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	3.	0.	0.00	0.02
304	55	20.52	20.52	12.	0.	0.02	0.06	19.99	34.27	4.	0.	0.01	0.02
305	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
306	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
307	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
308	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
309	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
310	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
311	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
312	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00

313	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
314	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
315	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
316	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
317	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
318	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
319	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
320	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
321	55	20.52	20.52	12.	0.	0.02	0.06	19.99	34.27	4.	0.	0.01	0.02
322	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	3.	0.	0.00	0.02
323	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	3.	0.	0.00	0.01
324	55	20.52	20.52	12.	0.	0.02	0.06	19.99	34.27	4.	0.	0.01	0.02

SUPERIORE ORIZZONTALE

SUPERIORE VERTICALE

GUSCI	spess	Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
301	55	20.52	20.52	22.	0.	0.04	0.11	34.27	19.99	12.	0.	0.02	0.04
302	55	20.52	20.52	220.	0.	0.36	1.06	34.27	19.99	10.	0.	0.01	0.03
303	55	20.52	20.52	207.	0.	0.34	1.00	34.27	19.99	7.	0.	0.01	0.02
304	55	20.52	20.52	21.	0.	0.03	0.10	34.27	19.99	9.	0.	0.01	0.03
305	55	20.52	20.52	21.	0.	0.03	0.10	34.27	19.99	143.	0.	0.20	0.42
306	55	20.52	20.52	224.	0.	0.37	1.08	34.27	19.99	134.	0.	0.19	0.40
307	55	20.52	20.52	213.	0.	0.35	1.03	34.27	19.99	133.	0.	0.19	0.39
308	55	20.52	20.52	18.	0.	0.03	0.09	34.27	19.99	140.	0.	0.20	0.41
309	82	20.52	20.52	22.	0.	0.02	0.07	34.27	19.99	738.	0.	0.54	1.41
310	82	20.52	20.52	228.	0.	0.20	0.72	34.27	19.99	737.	0.	0.54	1.41
311	82	20.52	20.52	229.	0.	0.20	0.72	34.27	19.99	737.	0.	0.54	1.41
312	82	20.52	20.52	19.	0.	0.02	0.06	34.27	19.99	737.	0.	0.54	1.41
313	82	20.52	20.52	18.	0.	0.02	0.06	34.27	19.99	742.	0.	0.54	1.42
314	82	20.52	20.52	229.	0.	0.20	0.72	34.27	19.99	742.	0.	0.54	1.42
315	82	20.52	20.52	228.	0.	0.20	0.72	34.27	19.99	742.	0.	0.54	1.42
316	82	20.52	20.52	16.	0.	0.01	0.05	34.27	19.99	743.	0.	0.54	1.42
317	55	20.52	20.52	19.	0.	0.03	0.09	34.27	19.99	142.	0.	0.20	0.42
318	55	20.52	20.52	230.	0.	0.38	1.11	34.27	19.99	134.	0.	0.19	0.40
319	55	20.52	20.52	219.	0.	0.36	1.06	34.27	19.99	133.	0.	0.19	0.39
320	55	20.52	20.52	18.	0.	0.03	0.09	34.27	19.99	139.	0.	0.19	0.41
321	55	20.52	20.52	19.	0.	0.03	0.09	34.27	19.99	12.	0.	0.02	0.03
322	55	20.52	20.52	220.	0.	0.36	1.06	34.27	19.99	9.	0.	0.01	0.03
323	55	20.52	20.52	207.	0.	0.34	1.00	34.27	19.99	6.	0.	0.01	0.02
324	55	20.52	20.52	19.	0.	0.03	0.09	34.27	19.99	9.	0.	0.01	0.03

***** TAGLIO PERPENDICOLARE

GUSCI	τx	τy	τt	GUSCI	τx	τy	τt	GUSCI	τx	τy	τt
301	0.5	0.3	0.4	302	0.5	0.4	0.5	303	0.5	0.4	0.5
304	0.5	0.3	0.4	305	0.5	1.7	1.6	306	0.5	1.6	1.2
307	0.5	1.5	1.1	308	0.5	1.6	1.6	309	0.3	0.8	0.7
310	0.8	0.9	0.9	311	0.8	0.9	0.9	312	0.3	0.7	0.7
313	0.3	0.7	0.7	314	0.8	0.9	0.9	315	0.8	0.9	0.9
316	0.4	0.7	0.7	317	0.5	1.6	1.5	318	0.5	1.5	1.1
319	0.5	1.5	1.1	320	0.5	1.6	1.5	321	0.5	0.3	0.4
322	0.5	0.3	0.5	323	0.5	0.3	0.5	324	0.5	0.3	0.4

VERIFICHE A PUNZONAMENTO

A	3	Norm [kN]	beta	sigT [N/mm2]	Pcrit [cm]	Ro [%]	Acrit [cm2]	VRd,c [kN]	VED [kN]	A staffe [cm2]	VRd,cs [kN]	si
		-2800.511	1.54	0.010	621.8	0.26	112175.1	1651.220	3811.470	95.3	-0.010	si

MACROGUSCIO: Pulvino4

INFERIORE ORIZZONTALE								INFERIORE VERTICALE					
GUSCI	spess	Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
401	55	20.52	20.52	12.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01
402	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
403	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
404	55	20.52	20.52	12.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01
405	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
406	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
407	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
408	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
409	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
410	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
411	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
412	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
413	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
414	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
415	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
416	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
417	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
418	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
419	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
420	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
421	55	20.52	20.52	12.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01
422	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
423	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
424	55	20.52	20.52	12.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01

SUPERIORE ORIZZONTALE

SUPERIORE VERTICALE

GUSCI	spess	Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
401	55	20.52	20.52	20.	0.	0.03	0.10	34.27	19.99	11.	0.	0.02	0.03
402	55	20.52	20.52	220.	0.	0.36	1.06	34.27	19.99	9.	0.	0.01	0.03
403	55	20.52	20.52	207.	0.	0.34	1.00	34.27	19.99	8.	0.	0.01	0.02
404	55	20.52	20.52	20.	0.	0.03	0.10	34.27	19.99	11.	0.	0.02	0.03
405	55	20.52	20.52	17.	0.	0.03	0.08	34.27	19.99	143.	0.	0.20	0.42
406	55	20.52	20.52	230.	0.	0.38	1.11	34.27	19.99	135.	0.	0.19	0.40
407	55	20.52	20.52	213.	0.	0.35	1.03	34.27	19.99	134.	0.	0.19	0.39
408	55	20.52	20.52	17.	0.	0.03	0.08	34.27	19.99	140.	0.	0.20	0.41
409	82	20.52	20.52	17.	0.	0.01	0.05	34.27	19.99	730.	0.	0.53	1.40
410	82	20.52	20.52	229.	0.	0.20	0.72	34.27	19.99	730.	0.	0.53	1.40
411	82	20.52	20.52	229.	0.	0.20	0.72	34.27	19.99	730.	0.	0.53	1.40
412	82	20.52	20.52	17.	0.	0.01	0.05	34.27	19.99	731.	0.	0.53	1.40

413	82	20.52	20.52	13.	0.	0.01	0.04	34.27	19.99	730.	0.	0.53	1.40
414	82	20.52	20.52	228.	0.	0.20	0.71	34.27	19.99	730.	0.	0.53	1.40
415	82	20.52	20.52	228.	0.	0.20	0.72	34.27	19.99	730.	0.	0.53	1.40
416	82	20.52	20.52	13.	0.	0.01	0.04	34.27	19.99	730.	0.	0.53	1.40
417	55	20.52	20.52	18.	0.	0.03	0.09	34.27	19.99	143.	0.	0.20	0.42
418	55	20.52	20.52	224.	0.	0.37	1.08	34.27	19.99	134.	0.	0.19	0.40
419	55	20.52	20.52	219.	0.	0.36	1.06	34.27	19.99	133.	0.	0.19	0.39
420	55	20.52	20.52	18.	0.	0.03	0.09	34.27	19.99	140.	0.	0.19	0.41
421	55	20.52	20.52	19.	0.	0.03	0.09	34.27	19.99	11.	0.	0.02	0.03
422	55	20.52	20.52	220.	0.	0.36	1.06	34.27	19.99	9.	0.	0.01	0.03
423	55	20.52	20.52	207.	0.	0.34	1.00	34.27	19.99	8.	0.	0.01	0.02
424	55	20.52	20.52	19.	0.	0.03	0.09	34.27	19.99	11.	0.	0.02	0.03

***** TAGLIO PERPENDICOLARE

GUSCI	τx	τy	τt	GUSCI	τx	τy	τt	GUSCI	τx	τy	τt
401	0.5	0.3	0.4	402	0.5	0.4	0.5	403	0.5	0.4	0.5
404	0.5	0.3	0.4	405	0.5	1.7	1.6	406	0.5	1.6	1.2
407	0.5	1.5	1.1	408	0.5	1.6	1.6	409	0.3	0.8	0.7
410	0.8	0.9	0.9	411	0.8	0.9	0.9	412	0.3	0.7	0.7
413	0.4	0.7	0.7	414	0.8	0.9	0.9	415	0.8	0.9	0.9
416	0.4	0.7	0.7	417	0.5	1.6	1.5	418	0.5	1.5	1.1
419	0.5	1.5	1.1	420	0.5	1.6	1.5	421	0.5	0.3	0.4
422	0.5	0.3	0.5	423	0.5	0.3	0.5	424	0.5	0.3	0.4

VERIFICHE A PUNZONAMENTO

	Norm [kN]	beta	sigT [N/mm2]	Pcrit [cm]	Ro [%]	Acrit [cm2]	VRd,c [kN]	VEd [kN]	A staffe [cm2]	VRd,cs [kN]		
A	4	-2800.553	1.54	0.010	621.8	0.26	112175.1	1651.220	3811.580	95.3	-0.010	si

MACROGUSCIO: Pulvino5

GUSCI	spess	INFERIORE ORIZZONTALE				INFERIORE VERTICALE							
		Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
501	55	20.52	20.52	12.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01
502	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
503	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
504	55	20.52	20.52	12.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01
505	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
506	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
507	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
508	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
509	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
510	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
511	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
512	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
513	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
514	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
515	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
516	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
517	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
518	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
519	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
520	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
521	55	20.52	20.52	12.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01
522	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
523	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
524	55	20.52	20.52	12.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01

SUPERIORE ORIZZONTALE

GUSCI	spess	SUPERIORE ORIZZONTALE				SUPERIORE VERTICALE							
		Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
501	55	20.52	20.52	20.	0.	0.03	0.10	34.27	19.99	11.	0.	0.02	0.03
502	55	20.52	20.52	219.	0.	0.36	1.06	34.27	19.99	9.	0.	0.01	0.03
503	55	20.52	20.52	207.	0.	0.34	1.00	34.27	19.99	8.	0.	0.01	0.02
504	55	20.52	20.52	20.	0.	0.03	0.10	34.27	19.99	10.	0.	0.01	0.03
505	55	20.52	20.52	17.	0.	0.03	0.08	34.27	19.99	143.	0.	0.20	0.42
506	55	20.52	20.52	229.	0.	0.38	1.11	34.27	19.99	135.	0.	0.19	0.40
507	55	20.52	20.52	213.	0.	0.35	1.03	34.27	19.99	134.	0.	0.19	0.39
508	55	20.52	20.52	17.	0.	0.03	0.08	34.27	19.99	140.	0.	0.20	0.41
509	82	20.52	20.52	17.	0.	0.01	0.05	34.27	19.99	730.	0.	0.53	1.40
510	82	20.52	20.52	229.	0.	0.20	0.72	34.27	19.99	730.	0.	0.53	1.40
511	82	20.52	20.52	229.	0.	0.20	0.72	34.27	19.99	730.	0.	0.53	1.40
512	82	20.52	20.52	17.	0.	0.01	0.05	34.27	19.99	731.	0.	0.53	1.40
513	82	20.52	20.52	13.	0.	0.01	0.04	34.27	19.99	730.	0.	0.53	1.40
514	82	20.52	20.52	228.	0.	0.20	0.72	34.27	19.99	730.	0.	0.53	1.40
515	82	20.52	20.52	228.	0.	0.20	0.72	34.27	19.99	730.	0.	0.53	1.40
516	82	20.52	20.52	13.	0.	0.01	0.04	34.27	19.99	730.	0.	0.53	1.40
517	55	20.52	20.52	18.	0.	0.03	0.09	34.27	19.99	143.	0.	0.20	0.42
518	55	20.52	20.52	224.	0.	0.37	1.08	34.27	19.99	134.	0.	0.19	0.40
519	55	20.52	20.52	219.	0.	0.36	1.06	34.27	19.99	133.	0.	0.19	0.39
520	55	20.52	20.52	18.	0.	0.03	0.09	34.27	19.99	139.	0.	0.19	0.41
521	55	20.52	20.52	19.	0.	0.03	0.09	34.27	19.99	11.	0.	0.02	0.03
522	55	20.52	20.52	220.	0.	0.36	1.06	34.27	19.99	9.	0.	0.01	0.03
523	55	20.52	20.52	207.	0.	0.34	1.00	34.27	19.99	8.	0.	0.01	0.02
524	55	20.52	20.52	19.	0.	0.03	0.09	34.27	19.99	11.	0.	0.02	0.03

***** TAGLIO PERPENDICOLARE

GUSCI	τx	τy	τt	GUSCI	τx	τy	τt	GUSCI	τx	τy	τt
501	0.5	0.3	0.4	502	0.5	0.4	0.5	503	0.5	0.4	0.5
504	0.5	0.3	0.4	505	0.5	1.7	1.6	506	0.5	1.6	1.2
507	0.5	1.5	1.1	508	0.5	1.6	1.6	509	0.3	0.8	0.7
510	0.8	0.9	0.9	511	0.8	0.9	0.9	512	0.3	0.7	0.7
513	0.4	0.7	0.7	514	0.8	0.9	0.9	515	0.8	0.9	0.9
516	0.4	0.7	0.7	517	0.5	1.6	1.5	518	0.5	1.5	1.1
519	0.5	1.5	1.1	520	0.5	1.6	1.5	521	0.5	0.3	0.4
522	0.5	0.3	0.5	523	0.5	0.3	0.5	524	0.5	0.3	0.4

VERIFICHE A PUNZONAMENTO

	Norm [kN]	beta	sigT [N/mm2]	Pcrit [cm]	Ro [%]	Acrit [cm2]	VRd,c [kN]	VEd [kN]	A staffe [cm2]	VRd,cs [kN]		
A	5	-2800.568	1.54	0.010	621.8	0.26	112175.1	1651.220	3811.580	95.3	-0.010	si

MACROGUSCIO: Pulvino6

GUSCI	spess	INFERIORE ORIZZONTALE						INFERIORE VERTICALE					
		Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
601	55	20.52	20.52	12.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01
602	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
603	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
604	55	20.52	20.52	12.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01
605	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
606	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
607	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
608	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
609	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
610	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
611	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
612	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
613	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
614	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
615	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
616	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
617	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
618	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
619	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
620	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
621	55	20.52	20.52	12.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01
622	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
623	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
624	55	20.52	20.52	12.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01

GUSCI	spess	SUPERIORE ORIZZONTALE						SUPERIORE VERTICALE					
		Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
601	55	20.52	20.52	20.	0.	0.03	0.10	34.27	19.99	11.	0.	0.02	0.03
602	55	20.52	20.52	220.	0.	0.36	1.06	34.27	19.99	9.	0.	0.01	0.03
603	55	20.52	20.52	207.	0.	0.34	1.00	34.27	19.99	8.	0.	0.01	0.02
604	55	20.52	20.52	20.	0.	0.03	0.10	34.27	19.99	11.	0.	0.02	0.03
605	55	20.52	20.52	17.	0.	0.03	0.08	34.27	19.99	143.	0.	0.20	0.42
606	55	20.52	20.52	230.	0.	0.38	1.11	34.27	19.99	135.	0.	0.19	0.40
607	55	20.52	20.52	213.	0.	0.35	1.03	34.27	19.99	134.	0.	0.19	0.40
608	55	20.52	20.52	17.	0.	0.03	0.08	34.27	19.99	140.	0.	0.20	0.41
609	82	20.52	20.52	17.	0.	0.01	0.05	34.27	19.99	730.	0.	0.53	1.40
610	82	20.52	20.52	229.	0.	0.20	0.72	34.27	19.99	730.	0.	0.53	1.40
611	82	20.52	20.52	229.	0.	0.20	0.72	34.27	19.99	730.	0.	0.53	1.40
612	82	20.52	20.52	17.	0.	0.01	0.05	34.27	19.99	730.	0.	0.53	1.40
613	82	20.52	20.52	13.	0.	0.01	0.04	34.27	19.99	730.	0.	0.53	1.40
614	82	20.52	20.52	228.	0.	0.20	0.72	34.27	19.99	730.	0.	0.53	1.40
615	82	20.52	20.52	228.	0.	0.20	0.72	34.27	19.99	730.	0.	0.53	1.40
616	82	20.52	20.52	13.	0.	0.01	0.04	34.27	19.99	731.	0.	0.53	1.40
617	55	20.52	20.52	18.	0.	0.03	0.09	34.27	19.99	143.	0.	0.20	0.42
618	55	20.52	20.52	224.	0.	0.37	1.08	34.27	19.99	135.	0.	0.19	0.40
619	55	20.52	20.52	219.	0.	0.36	1.06	34.27	19.99	133.	0.	0.19	0.39
620	55	20.52	20.52	18.	0.	0.03	0.09	34.27	19.99	140.	0.	0.19	0.41
621	55	20.52	20.52	19.	0.	0.03	0.09	34.27	19.99	11.	0.	0.02	0.03
622	55	20.52	20.52	220.	0.	0.36	1.06	34.27	19.99	9.	0.	0.01	0.03
623	55	20.52	20.52	207.	0.	0.34	1.00	34.27	19.99	8.	0.	0.01	0.02
624	55	20.52	20.52	19.	0.	0.03	0.09	34.27	19.99	11.	0.	0.02	0.03

***** TAGLIO PERPENDICOLARE

GUSCI	tx	ty	tz	GUSCI	tx	ty	tz	GUSCI	tx	ty	tz
601	0.5	0.3	0.4	602	0.5	0.4	0.5	603	0.5	0.4	0.5
604	0.5	0.4	0.4	605	0.5	1.7	1.6	606	0.5	1.6	1.2
607	0.5	1.5	1.1	608	0.5	1.6	1.6	609	0.3	0.8	0.7
610	0.8	0.9	0.9	611	0.8	0.9	0.9	612	0.3	0.7	0.7
613	0.4	0.7	0.7	614	0.8	0.9	0.9	615	0.8	0.9	0.9
616	0.4	0.7	0.7	617	0.5	1.6	1.5	618	0.5	1.5	1.1
619	0.5	1.5	1.1	620	0.5	1.6	1.5	621	0.5	0.3	0.4
622	0.5	0.3	0.5	623	0.5	0.3	0.5	624	0.5	0.3	0.4

VERIFICHE A PUNZONAMENTO

	Norm [kN]	beta	sigT [N/mm2]	Pcrit [cm]	Ro [%]	Acrit [cm2]	VRd,c [kN]	VEd [kN]	A staffe [cm2]	VRd,cs [kN]	si
A	6	-2800.555	1.54	0.010	621.8	0.26	112175.1	1651.220	3811.610	95.3	-0.010

MACROGUSCIO: Pulvino7

GUSCI	spess	INFERIORE ORIZZONTALE						INFERIORE VERTICALE					
		Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
701	55	20.52	20.52	12.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01
702	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
703	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
704	55	20.52	20.52	12.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.02
705	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
706	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
707	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
708	55	20.52	20.52	11.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
709	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
710	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
711	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
712	82	20.52	20.52	6.	0.	0.01	0.02	19.99	34.27	0.	0.	0.00	0.00
713	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
714	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
715	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
716	82	20.52	20.52	6.	0.	0.01	0.02	19.99	34.27	0.	0.	0.00	0.00
717	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
718	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
719	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
720	55	20.52	20.52	11.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00

721	55	20.52	20.52	12.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01
722	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
723	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
724	55	20.52	20.52	12.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.02
SUPERIORE ORIZZONTALE													
GUSCI	spess	Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
701	55	20.52	20.52	20.	0.	0.03	0.10	34.27	19.99	11.	0.	0.02	0.03
702	55	20.52	20.52	218.	0.	0.36	1.06	34.27	19.99	9.	0.	0.01	0.03
703	55	20.52	20.52	208.	0.	0.34	1.00	34.27	19.99	9.	0.	0.01	0.03
704	55	20.52	20.52	20.	0.	0.03	0.10	34.27	19.99	11.	0.	0.02	0.03
705	55	20.52	20.52	17.	0.	0.03	0.08	34.27	19.99	143.	0.	0.20	0.42
706	55	20.52	20.52	228.	0.	0.38	1.10	34.27	19.99	135.	0.	0.19	0.40
707	55	20.52	20.52	214.	0.	0.35	1.04	34.27	19.99	134.	0.	0.19	0.40
708	55	20.52	20.52	17.	0.	0.03	0.08	34.27	19.99	142.	0.	0.20	0.42
709	82	20.52	20.52	17.	0.	0.01	0.05	34.27	19.99	734.	0.	0.53	1.40
710	82	20.52	20.52	229.	0.	0.20	0.72	34.27	19.99	734.	0.	0.53	1.40
711	82	20.52	20.52	232.	0.	0.20	0.73	34.27	19.99	734.	0.	0.53	1.40
712	82	20.52	20.52	17.	0.	0.01	0.05	34.27	19.99	734.	0.	0.53	1.41
713	82	20.52	20.52	13.	0.	0.01	0.04	34.27	19.99	734.	0.	0.53	1.40
714	82	20.52	20.52	228.	0.	0.20	0.72	34.27	19.99	734.	0.	0.53	1.40
715	82	20.52	20.52	231.	0.	0.20	0.72	34.27	19.99	734.	0.	0.53	1.40
716	82	20.52	20.52	13.	0.	0.01	0.04	34.27	19.99	734.	0.	0.53	1.41
717	55	20.52	20.52	18.	0.	0.03	0.09	34.27	19.99	143.	0.	0.20	0.42
718	55	20.52	20.52	222.	0.	0.37	1.07	34.27	19.99	135.	0.	0.19	0.40
719	55	20.52	20.52	220.	0.	0.36	1.06	34.27	19.99	134.	0.	0.19	0.39
720	55	20.52	20.52	18.	0.	0.03	0.09	34.27	19.99	141.	0.	0.20	0.42
721	55	20.52	20.52	19.	0.	0.03	0.09	34.27	19.99	11.	0.	0.02	0.03
722	55	20.52	20.52	218.	0.	0.36	1.06	34.27	19.99	9.	0.	0.01	0.03
723	55	20.52	20.52	208.	0.	0.34	1.00	34.27	19.99	9.	0.	0.01	0.03
724	55	20.52	20.52	19.	0.	0.03	0.09	34.27	19.99	11.	0.	0.02	0.03

TAGLIO PERPENDICOLARE													
GUSCI	τx	τy	τt	GUSCI	τx	τy	τt	GUSCI	τx	τy	τt		
701	0.5	0.3	0.4	702	0.5	0.4	0.5	703	0.5	0.4	0.5		
704	0.5	0.4	0.4	705	0.5	1.7	1.6	706	0.5	1.6	1.2		
707	0.6	1.5	1.2	708	0.5	1.7	1.6	709	0.3	0.8	0.7		
710	0.8	0.9	0.9	711	0.8	0.9	0.9	712	0.3	0.7	0.7		
713	0.4	0.7	0.7	714	0.8	0.9	0.9	715	0.8	0.9	0.9		
716	0.4	0.7	0.7	717	0.5	1.6	1.5	718	0.5	1.5	1.1		
719	0.5	1.5	1.1	720	0.5	1.6	1.5	721	0.5	0.3	0.4		
722	0.5	0.3	0.5	723	0.5	0.3	0.5	724	0.5	0.3	0.4		
VERIFICHE A PUNZONAMENTO													
		Norm	beta	sigT	Pcrit	Ro	Acrit	VRd,c	VED	A staffe	VRd,cs		
A	7	-2818.	572	1.54	0.010	621.8	0.26	112175.1	1651.220	3839.490	95.3	-0.010	si

MACROGUSCIO: Pulvino8

INFERIORE ORIZZONTALE													
GUSCI	spess	Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
801	55	20.52	20.52	12.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01
802	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
803	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
804	55	20.52	20.52	12.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01
805	55	20.52	20.52	11.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
806	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
807	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
808	55	20.52	20.52	11.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
809	82	20.52	20.52	6.	0.	0.01	0.02	19.99	34.27	0.	0.	0.00	0.00
810	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
811	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
812	82	20.52	20.52	6.	0.	0.01	0.02	19.99	34.27	0.	0.	0.00	0.00
813	82	20.52	20.52	6.	0.	0.01	0.02	19.99	34.27	0.	0.	0.00	0.00
814	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
815	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
816	82	20.52	20.52	6.	0.	0.01	0.02	19.99	34.27	0.	0.	0.00	0.00
817	55	20.52	20.52	11.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
818	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
819	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
820	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
821	55	20.52	20.52	12.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01
822	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
823	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
824	55	20.52	20.52	12.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01
SUPERIORE ORIZZONTALE													
GUSCI	spess	Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
801	55	20.52	20.52	20.	0.	0.03	0.10	34.27	19.99	11.	0.	0.02	0.03
802	55	20.52	20.52	222.	0.	0.37	1.08	34.27	19.99	9.	0.	0.01	0.03
803	55	20.52	20.52	210.	0.	0.35	1.01	34.27	19.99	8.	0.	0.01	0.02
804	55	20.52	20.52	20.	0.	0.03	0.10	34.27	19.99	11.	0.	0.02	0.03
805	55	20.52	20.52	17.	0.	0.03	0.08	34.27	19.99	145.	0.	0.20	0.43
806	55	20.52	20.52	233.	0.	0.38	1.12	34.27	19.99	137.	0.	0.19	0.40
807	55	20.52	20.52	216.	0.	0.36	1.04	34.27	19.99	135.	0.	0.19	0.40
808	55	20.52	20.52	17.	0.	0.03	0.08	34.27	19.99	142.	0.	0.20	0.42
809	82	20.52	20.52	17.	0.	0.01	0.05	34.27	19.99	739.	0.	0.54	1.41
810	82	20.52	20.52	232.	0.	0.20	0.73	34.27	19.99	739.	0.	0.54	1.41
811	82	20.52	20.52	232.	0.	0.20	0.73	34.27	19.99	739.	0.	0.54	1.41
812	82	20.52	20.52	17.	0.	0.01	0.05	34.27	19.99	740.	0.	0.54	1.42
813	82	20.52	20.52	13.	0.	0.01	0.04	34.27	19.99	740.	0.	0.54	1.42
814	82	20.52	20.52	231.	0.	0.20	0.72	34.27	19.99	739.	0.	0.54	1.41
815	82	20.52	20.52	231.	0.	0.20	0.72	34.27	19.99	739.	0.	0.54	1.41
816	82	20.52	20.52	13.	0.	0.01	0.04	34.27	19.99	740.	0.	0.54	1.42
817	55	20.52	20.52	18.	0.	0.03	0.09	34.27	19.99	145.	0.	0.20	0.43
818	55	20.52	20.52	227.	0.	0.37	1.10	34.27	19.99	136.	0.	0.19	0.40
819	55	20.52	20.52	222.	0.	0.37	1.07	34.27	19.99	135.	0.	0.19	0.40
820	55	20.52	20.52	18.	0.	0.03	0.09	34.27	19.99	141.	0.	0.20	0.42

821	55	20.52	20.52	19.	0.	0.03	0.09	34.27	19.99	11.	0.	0.02	0.03
822	55	20.52	20.52	222.	0.	0.37	1.08	34.27	19.99	9.	0.	0.01	0.03
823	55	20.52	20.52	209.	0.	0.35	1.01	34.27	19.99	8.	0.	0.01	0.02
824	55	20.52	20.52	19.	0.	0.03	0.09	34.27	19.99	11.	0.	0.02	0.03

***** TAGLIO PERPENDICOLARE

GUSCI	τx	τy	τt	GUSCI	τx	τy	τt	GUSCI	τx	τy	τt
801	0.5	0.3	0.4	802	0.5	0.4	0.5	803	0.5	0.4	0.5
804	0.5	0.4	0.4	805	0.5	1.7	1.7	806	0.5	1.6	1.2
807	0.6	1.5	1.2	808	0.5	1.7	1.6	809	0.3	0.8	0.8
810	0.8	0.9	0.9	811	0.8	0.9	0.9	812	0.4	0.7	0.7
813	0.4	0.7	0.7	814	0.8	0.9	1.0	815	0.8	0.9	0.9
816	0.4	0.7	0.7	817	0.5	1.6	1.6	818	0.6	1.6	1.2
819	0.5	1.5	1.1	820	0.5	1.6	1.5	821	0.5	0.3	0.4
822	0.5	0.4	0.5	823	0.5	0.3	0.5	824	0.5	0.3	0.4

VERIFICHE A PUNZONAMENTO

	Norm	beta	sigT	Pcrit	Ro	Acrit	VRd,c	VEd	A staffe	VRd,cs		
	[kN]		[N/mm ²]	[cm]	[%]	[cm ²]	[kN]	[kN]	[cm ²]	[kN]		
A	8	-2836.555	1.54	0.010	621.8	0.26	112175.1	1651.220	3866.940	95.3	-0.010	si

MACROGUSCIO: Pulvino9

GUSCI	spess	INFERIORE ORIZZONTALE				INFERIORE VERTICALE							
		Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
901	55	20.52	20.52	12.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.02
902	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
903	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
904	55	20.52	20.52	11.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01
905	55	20.52	20.52	11.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
906	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
907	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
908	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
909	82	20.52	20.52	6.	0.	0.01	0.02	19.99	34.27	0.	0.	0.00	0.00
910	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
911	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
912	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
913	82	20.52	20.52	6.	0.	0.01	0.02	19.99	34.27	0.	0.	0.00	0.00
914	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
915	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
916	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
917	55	20.52	20.52	11.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
918	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
919	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
920	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
921	55	20.52	20.52	12.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.02
922	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
923	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
924	55	20.52	20.52	11.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01

SUPERIORE ORIZZONTALE

GUSCI	spess	SUPERIORE ORIZZONTALE				SUPERIORE VERTICALE							
		Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
901	55	20.52	20.52	20.	0.	0.03	0.10	34.27	19.99	12.	0.	0.02	0.03
902	55	20.52	20.52	223.	0.	0.37	1.08	34.27	19.99	9.	0.	0.01	0.03
903	55	20.52	20.52	209.	0.	0.34	1.01	34.27	19.99	8.	0.	0.01	0.02
904	55	20.52	20.52	20.	0.	0.03	0.10	34.27	19.99	11.	0.	0.01	0.03
905	55	20.52	20.52	17.	0.	0.03	0.08	34.27	19.99	145.	0.	0.20	0.43
906	55	20.52	20.52	233.	0.	0.38	1.13	34.27	19.99	136.	0.	0.19	0.40
907	55	20.52	20.52	214.	0.	0.35	1.04	34.27	19.99	135.	0.	0.19	0.40
908	55	20.52	20.52	17.	0.	0.03	0.08	34.27	19.99	140.	0.	0.20	0.41
909	82	20.52	20.52	17.	0.	0.01	0.05	34.27	19.99	735.	0.	0.53	1.41
910	82	20.52	20.52	232.	0.	0.20	0.73	34.27	19.99	735.	0.	0.53	1.41
911	82	20.52	20.52	229.	0.	0.20	0.72	34.27	19.99	735.	0.	0.53	1.41
912	82	20.52	20.52	17.	0.	0.01	0.05	34.27	19.99	736.	0.	0.53	1.41
913	82	20.52	20.52	13.	0.	0.01	0.04	34.27	19.99	735.	0.	0.53	1.41
914	82	20.52	20.52	230.	0.	0.20	0.72	34.27	19.99	735.	0.	0.53	1.41
915	82	20.52	20.52	228.	0.	0.20	0.72	34.27	19.99	735.	0.	0.53	1.41
916	82	20.52	20.52	13.	0.	0.01	0.04	34.27	19.99	735.	0.	0.53	1.41
917	55	20.52	20.52	18.	0.	0.03	0.09	34.27	19.99	144.	0.	0.20	0.43
918	55	20.52	20.52	227.	0.	0.37	1.10	34.27	19.99	136.	0.	0.19	0.40
919	55	20.52	20.52	220.	0.	0.36	1.07	34.27	19.99	135.	0.	0.19	0.40
920	55	20.52	20.52	18.	0.	0.03	0.09	34.27	19.99	140.	0.	0.20	0.41
921	55	20.52	20.52	19.	0.	0.03	0.09	34.27	19.99	12.	0.	0.02	0.03
922	55	20.52	20.52	223.	0.	0.37	1.08	34.27	19.99	9.	0.	0.01	0.03
923	55	20.52	20.52	209.	0.	0.34	1.01	34.27	19.99	8.	0.	0.01	0.02
924	55	20.52	20.52	19.	0.	0.03	0.09	34.27	19.99	11.	0.	0.01	0.03

***** TAGLIO PERPENDICOLARE

GUSCI	τx	τy	τt	GUSCI	τx	τy	τt	GUSCI	τx	τy	τt
901	0.5	0.3	0.4	902	0.5	0.4	0.5	903	0.5	0.4	0.5
904	0.5	0.3	0.4	905	0.5	1.7	1.7	906	0.5	1.6	1.2
907	0.5	1.5	1.1	908	0.5	1.6	1.6	909	0.3	0.8	0.8
910	0.8	0.9	0.9	911	0.8	0.9	0.9	912	0.4	0.7	0.7
913	0.4	0.7	0.7	914	0.8	0.9	1.0	915	0.8	0.9	0.9
916	0.4	0.7	0.7	917	0.5	1.6	1.6	918	0.6	1.5	1.2
919	0.5	1.5	1.1	920	0.5	1.6	1.5	921	0.5	0.3	0.4
922	0.5	0.3	0.5	923	0.5	0.3	0.5	924	0.5	0.3	0.4

VERIFICHE A PUNZONAMENTO

	Norm	beta	sigT	Pcrit	Ro	Acrit	VRd,c	VEd	A staffe	VRd,cs		
	[kN]		[N/mm ²]	[cm]	[%]	[cm ²]	[kN]	[kN]	[cm ²]	[kN]		
A	9	-2818.567	1.54	0.010	621.8	0.26	112175.1	1651.220	3839.490	95.3	-0.010	si

MACROGUSCIO: Pulvino10

GUSCI	spess	INFERIORE ORIZZONTALE				INFERIORE VERTICALE							
		Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
1001	55	20.52	20.52	12.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01
1002	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01

1003	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
1004	55	20.52	20.52	12.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01
1005	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
1006	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1007	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1008	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
1009	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
1010	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1011	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1012	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
1013	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
1014	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1015	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1016	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
1017	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
1018	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1019	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1020	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
1021	55	20.52	20.52	12.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01
1022	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
1023	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
1024	55	20.52	20.52	12.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01

SUPERIORE ORIZZONTALE								SUPERIORE VERTICALE					
GUSCI	spess	Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
1001	55	20.52	20.52	20.	0.	0.03	0.10	34.27	19.99	11.	0.	0.02	0.03
1002	55	20.52	20.52	219.	0.	0.36	1.06	34.27	19.99	9.	0.	0.01	0.03
1003	55	20.52	20.52	207.	0.	0.34	1.00	34.27	19.99	8.	0.	0.01	0.02
1004	55	20.52	20.52	20.	0.	0.03	0.10	34.27	19.99	11.	0.	0.02	0.03
1005	55	20.52	20.52	17.	0.	0.03	0.08	34.27	19.99	143.	0.	0.20	0.42
1006	55	20.52	20.52	229.	0.	0.38	1.11	34.27	19.99	135.	0.	0.19	0.40
1007	55	20.52	20.52	213.	0.	0.35	1.03	34.27	19.99	134.	0.	0.19	0.40
1008	55	20.52	20.52	17.	0.	0.03	0.08	34.27	19.99	140.	0.	0.20	0.41
1009	82	20.52	20.52	17.	0.	0.01	0.05	34.27	19.99	730.	0.	0.53	1.40
1010	82	20.52	20.52	229.	0.	0.20	0.72	34.27	19.99	729.	0.	0.53	1.40
1011	82	20.52	20.52	229.	0.	0.20	0.72	34.27	19.99	729.	0.	0.53	1.40
1012	82	20.52	20.52	17.	0.	0.01	0.05	34.27	19.99	730.	0.	0.53	1.40
1013	82	20.52	20.52	13.	0.	0.01	0.04	34.27	19.99	730.	0.	0.53	1.40
1014	82	20.52	20.52	228.	0.	0.20	0.71	34.27	19.99	730.	0.	0.53	1.40
1015	82	20.52	20.52	228.	0.	0.20	0.71	34.27	19.99	730.	0.	0.53	1.40
1016	82	20.52	20.52	13.	0.	0.01	0.04	34.27	19.99	730.	0.	0.53	1.40
1017	55	20.52	20.52	18.	0.	0.03	0.09	34.27	19.99	143.	0.	0.20	0.42
1018	55	20.52	20.52	223.	0.	0.37	1.08	34.27	19.99	135.	0.	0.19	0.40
1019	55	20.52	20.52	219.	0.	0.36	1.06	34.27	19.99	133.	0.	0.19	0.39
1020	55	20.52	20.52	18.	0.	0.03	0.09	34.27	19.99	139.	0.	0.19	0.41
1021	55	20.52	20.52	19.	0.	0.03	0.09	34.27	19.99	11.	0.	0.02	0.03
1022	55	20.52	20.52	219.	0.	0.36	1.06	34.27	19.99	9.	0.	0.01	0.03
1023	55	20.52	20.52	207.	0.	0.34	1.00	34.27	19.99	8.	0.	0.01	0.02
1024	55	20.52	20.52	19.	0.	0.03	0.09	34.27	19.99	11.	0.	0.02	0.03

***** TAGLIO PERPENDICOLARE

GUSCI	tx	ty	tz	GUSCI	tx	ty	tz	GUSCI	tx	ty	tz
1001	0.5	0.3	0.4	1002	0.5	0.4	0.5	1003	0.5	0.4	0.5
1004	0.5	0.3	0.4	1005	0.5	1.7	1.6	1006	0.5	1.6	1.2
1007	0.5	1.5	1.1	1008	0.5	1.6	1.6	1009	0.3	0.8	0.7
1010	0.8	0.9	0.9	1011	0.8	0.9	0.9	1012	0.3	0.7	0.7
1013	0.4	0.7	0.7	1014	0.8	0.9	0.9	1015	0.8	0.9	0.9
1016	0.4	0.7	0.7	1017	0.5	1.6	1.5	1018	0.5	1.5	1.1
1019	0.5	1.5	1.1	1020	0.5	1.6	1.5	1021	0.5	0.3	0.4
1022	0.5	0.3	0.5	1023	0.5	0.3	0.5	1024	0.5	0.3	0.4

VERIFICHE A PUNZONAMENTO

A	Norm [kN]	beta	sigT [N/mm2]	Pcrit [cm]	Ro [%]	Acrit [cm2]	VRd,c [kN]	VED [kN]	A staffe [cm2]	VRd,cs [kN]	si	
A	10	-2800.556	1.54	0.010	621.8	0.26	112174.4	1651.220	3811.580	95.3	-0.010	si

MACROGUSCIO: Pulvino11

INFERIORE ORIZZONTALE								INFERIORE VERTICALE					
GUSCI	spess	Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
1101	55	20.52	20.52	12.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01
1102	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
1103	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
1104	55	20.52	20.52	12.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01
1105	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
1106	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1107	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1108	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
1109	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
1110	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1111	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1112	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
1113	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
1114	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1115	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1116	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
1117	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
1118	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1119	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1120	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
1121	55	20.52	20.52	12.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01
1122	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
1123	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
1124	55	20.52	20.52	12.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01

SUPERIORE ORIZZONTALE								SUPERIORE VERTICALE					
GUSCI	spess	Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
1101	55	20.52	20.52	20.	0.	0.03	0.10	34.27	19.99	11.	0.	0.02	0.03
1102	55	20.52	20.52	220.	0.	0.36	1.06	34.27	19.99	9.	0.	0.01	0.03

1103	55	20.52	20.52	207.	0.	0.34	1.00	34.27	19.99	8.	0.	0.01	0.02
1104	55	20.52	20.52	20.	0.	0.03	0.10	34.27	19.99	11.	0.	0.02	0.03
1105	55	20.52	20.52	17.	0.	0.03	0.08	34.27	19.99	143.	0.	0.20	0.42
1106	55	20.52	20.52	229.	0.	0.38	1.11	34.27	19.99	135.	0.	0.19	0.40
1107	55	20.52	20.52	213.	0.	0.35	1.03	34.27	19.99	134.	0.	0.19	0.40
1108	55	20.52	20.52	17.	0.	0.03	0.08	34.27	19.99	140.	0.	0.20	0.41
1109	82	20.52	20.52	17.	0.	0.01	0.05	34.27	19.99	730.	0.	0.53	1.40
1110	82	20.52	20.52	229.	0.	0.20	0.72	34.27	19.99	729.	0.	0.53	1.40
1111	82	20.52	20.52	229.	0.	0.20	0.72	34.27	19.99	729.	0.	0.53	1.40
1112	82	20.52	20.52	17.	0.	0.01	0.05	34.27	19.99	730.	0.	0.53	1.40
1113	82	20.52	20.52	13.	0.	0.01	0.04	34.27	19.99	730.	0.	0.53	1.40
1114	82	20.52	20.52	228.	0.	0.20	0.71	34.27	19.99	730.	0.	0.53	1.40
1115	82	20.52	20.52	228.	0.	0.20	0.71	34.27	19.99	730.	0.	0.53	1.40
1116	82	20.52	20.52	13.	0.	0.01	0.04	34.27	19.99	730.	0.	0.53	1.40
1117	55	20.52	20.52	18.	0.	0.03	0.09	34.27	19.99	143.	0.	0.20	0.42
1118	55	20.52	20.52	224.	0.	0.37	1.08	34.27	19.99	135.	0.	0.19	0.40
1119	55	20.52	20.52	219.	0.	0.36	1.06	34.27	19.99	133.	0.	0.19	0.39
1120	55	20.52	20.52	18.	0.	0.03	0.09	34.27	19.99	140.	0.	0.20	0.41
1121	55	20.52	20.52	19.	0.	0.03	0.09	34.27	19.99	11.	0.	0.02	0.03
1122	55	20.52	20.52	220.	0.	0.36	1.06	34.27	19.99	9.	0.	0.01	0.03
1123	55	20.52	20.52	207.	0.	0.34	1.00	34.27	19.99	8.	0.	0.01	0.02
1124	55	20.52	20.52	19.	0.	0.03	0.09	34.27	19.99	11.	0.	0.02	0.03

***** TAGLIO PERPENDICOLARE

GUSCI	τ_x	τ_y	τ_t	GUSCI	τ_x	τ_y	τ_t	GUSCI	τ_x	τ_y	τ_t
1101	0.5	0.3	0.4	1102	0.5	0.4	0.5	1103	0.5	0.4	0.5
1104	0.5	0.3	0.4	1105	0.5	1.7	1.6	1106	0.5	1.6	1.2
1107	0.5	1.5	1.1	1108	0.5	1.6	1.6	1109	0.3	0.8	0.7
1110	0.8	0.9	0.9	1111	0.8	0.9	0.9	1112	0.3	0.7	0.7
1113	0.4	0.7	0.7	1114	0.8	0.9	0.9	1115	0.8	0.9	0.9
1116	0.4	0.7	0.7	1117	0.5	1.6	1.5	1118	0.5	1.5	1.1
1119	0.5	1.5	1.1	1120	0.5	1.6	1.5	1121	0.5	0.3	0.4
1122	0.5	0.3	0.5	1123	0.5	0.3	0.5	1124	0.5	0.3	0.4

VERIFICHE A PUNZONAMENTO

A	11	Norm [kN]	beta	sigT [N/mm2]	Pcrit [cm]	Ro [%]	Acrit [cm2]	VRd,c [kN]	VED [kN]	A staffe [cm2]	VRd,cs [kN]	si
		-2800.573	1.54	0.010	621.8	0.26	112175.1	1651.220	3811.650	95.3	-0.010	si

MACROGUSCIO: Pulvino12

GUSCI	spess	INFERIORE ORIZZONTALE						INFERIORE VERTICALE					
		Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
1201	55	20.52	20.52	11.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01
1202	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
1203	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
1204	55	20.52	20.52	11.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01
1205	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
1206	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1207	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1208	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
1209	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
1210	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1211	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1212	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
1213	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
1214	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1215	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1216	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
1217	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
1218	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1219	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1220	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
1221	55	20.52	20.52	11.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01
1222	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
1223	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
1224	55	20.52	20.52	11.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01

SUPERIORE ORIZZONTALE

SUPERIORE VERTICALE

GUSCI	spess	SUPERIORE ORIZZONTALE						SUPERIORE VERTICALE					
		Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
1201	55	20.52	20.52	20.	0.	0.03	0.10	34.27	19.99	11.	0.	0.02	0.03
1202	55	20.52	20.52	219.	0.	0.36	1.06	34.27	19.99	9.	0.	0.01	0.03
1203	55	20.52	20.52	206.	0.	0.34	1.00	34.27	19.99	8.	0.	0.01	0.02
1204	55	20.52	20.52	20.	0.	0.03	0.10	34.27	19.99	11.	0.	0.02	0.03
1205	55	20.52	20.52	17.	0.	0.03	0.08	34.27	19.99	143.	0.	0.20	0.42
1206	55	20.52	20.52	229.	0.	0.38	1.11	34.27	19.99	135.	0.	0.19	0.40
1207	55	20.52	20.52	213.	0.	0.35	1.03	34.27	19.99	134.	0.	0.19	0.39
1208	55	20.52	20.52	17.	0.	0.03	0.08	34.27	19.99	140.	0.	0.20	0.41
1209	82	20.52	20.52	17.	0.	0.01	0.05	34.27	19.99	730.	0.	0.53	1.40
1210	82	20.52	20.52	229.	0.	0.20	0.72	34.27	19.99	730.	0.	0.53	1.40
1211	82	20.52	20.52	228.	0.	0.20	0.72	34.27	19.99	730.	0.	0.53	1.40
1212	82	20.52	20.52	17.	0.	0.01	0.05	34.27	19.99	731.	0.	0.53	1.40
1213	82	20.52	20.52	13.	0.	0.01	0.04	34.27	19.99	730.	0.	0.53	1.40
1214	82	20.52	20.52	227.	0.	0.20	0.71	34.27	19.99	729.	0.	0.53	1.40
1215	82	20.52	20.52	227.	0.	0.20	0.71	34.27	19.99	729.	0.	0.53	1.40
1216	82	20.52	20.52	13.	0.	0.01	0.04	34.27	19.99	730.	0.	0.53	1.40
1217	55	20.52	20.52	18.	0.	0.03	0.09	34.27	19.99	143.	0.	0.20	0.42
1218	55	20.52	20.52	223.	0.	0.37	1.08	34.27	19.99	134.	0.	0.19	0.40
1219	55	20.52	20.52	218.	0.	0.36	1.06	34.27	19.99	133.	0.	0.19	0.39
1220	55	20.52	20.52	18.	0.	0.03	0.09	34.27	19.99	140.	0.	0.19	0.41
1221	55	20.52	20.52	19.	0.	0.03	0.09	34.27	19.99	11.	0.	0.02	0.03
1222	55	20.52	20.52	219.	0.	0.36	1.06	34.27	19.99	9.	0.	0.01	0.03
1223	55	20.52	20.52	206.	0.	0.34	1.00	34.27	19.99	8.	0.	0.01	0.02
1224	55	20.52	20.52	19.	0.	0.03	0.09	34.27	19.99	11.	0.	0.02	0.03

***** TAGLIO PERPENDICOLARE

GUSCI	τ_x	τ_y	τ_t	GUSCI	τ_x	τ_y	τ_t	GUSCI	τ_x	τ_y	τ_t
1201	0.5	0.3	0.4	1202	0.5	0.4	0.5	1203	0.5	0.4	0.5
1204	0.5	0.3	0.4	1205	0.5	1.7	1.6	1206	0.5	1.6	1.2

1207	0.5	1.5	1.1	1208	0.5	1.6	1.6	1209	0.3	0.8	0.7
1210	0.8	0.9	0.9	1211	0.8	0.9	0.9	1212	0.4	0.7	0.7
1213	0.4	0.7	0.7	1214	0.8	0.9	0.9	1215	0.8	0.9	0.9
1216	0.4	0.7	0.7	1217	0.5	1.6	1.5	1218	0.5	1.5	1.1
1219	0.5	1.5	1.1	1220	0.5	1.6	1.5	1221	0.5	0.3	0.4
1222	0.5	0.3	0.5	1223	0.5	0.3	0.5	1224	0.5	0.3	0.4

VERIFICHE A PUNZONAMENTO

	Norm	beta	sigT	Pcrit	Ro	Acrit	VRd,c	Ved	A staffe	VRd,cs		
A	12	-2800.557	1.54	0.010	621.8	0.26	112175.1	1651.220	3811.570	95.3	-0.010	si
		[kN]	[N/mm2]	[cm]	[%]	[cm2]	[kN]	[kN]	[cm2]	[kN]		

MACROGUSCIO: Pulvino13

GUSCI	spess	INFERIORE ORIZZONTALE						INFERIORE VERTICALE					
		Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
1301	55	20.52	20.52	11.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01
1302	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
1303	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
1304	55	20.52	20.52	11.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01
1305	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
1306	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1307	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1308	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
1309	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
1310	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1311	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1312	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
1313	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
1314	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1315	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1316	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
1317	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
1318	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1319	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1320	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
1321	55	20.52	20.52	11.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01
1322	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
1323	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
1324	55	20.52	20.52	11.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01

GUSCI	spess	SUPERIORE ORIZZONTALE						SUPERIORE VERTICALE					
		Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
1301	55	20.52	20.52	20.	0.	0.03	0.10	34.27	19.99	11.	0.	0.02	0.03
1302	55	20.52	20.52	219.	0.	0.36	1.06	34.27	19.99	9.	0.	0.01	0.03
1303	55	20.52	20.52	206.	0.	0.34	1.00	34.27	19.99	8.	0.	0.01	0.02
1304	55	20.52	20.52	20.	0.	0.03	0.10	34.27	19.99	11.	0.	0.02	0.03
1305	55	20.52	20.52	17.	0.	0.03	0.08	34.27	19.99	143.	0.	0.20	0.42
1306	55	20.52	20.52	229.	0.	0.38	1.11	34.27	19.99	135.	0.	0.19	0.40
1307	55	20.52	20.52	212.	0.	0.35	1.03	34.27	19.99	134.	0.	0.19	0.40
1308	55	20.52	20.52	17.	0.	0.03	0.08	34.27	19.99	140.	0.	0.20	0.41
1309	82	20.52	20.52	17.	0.	0.01	0.05	34.27	19.99	731.	0.	0.53	1.40
1310	82	20.52	20.52	229.	0.	0.20	0.72	34.27	19.99	730.	0.	0.53	1.40
1311	82	20.52	20.52	228.	0.	0.20	0.72	34.27	19.99	730.	0.	0.53	1.40
1312	82	20.52	20.52	17.	0.	0.01	0.05	34.27	19.99	731.	0.	0.53	1.40
1313	82	20.52	20.52	13.	0.	0.01	0.04	34.27	19.99	730.	0.	0.53	1.40
1314	82	20.52	20.52	227.	0.	0.20	0.71	34.27	19.99	730.	0.	0.53	1.40
1315	82	20.52	20.52	227.	0.	0.20	0.71	34.27	19.99	730.	0.	0.53	1.40
1316	82	20.52	20.52	13.	0.	0.01	0.04	34.27	19.99	730.	0.	0.53	1.40
1317	55	20.52	20.52	18.	0.	0.03	0.09	34.27	19.99	143.	0.	0.20	0.42
1318	55	20.52	20.52	223.	0.	0.37	1.08	34.27	19.99	135.	0.	0.19	0.40
1319	55	20.52	20.52	218.	0.	0.36	1.06	34.27	19.99	133.	0.	0.19	0.39
1320	55	20.52	20.52	18.	0.	0.03	0.09	34.27	19.99	139.	0.	0.19	0.41
1321	55	20.52	20.52	19.	0.	0.03	0.09	34.27	19.99	11.	0.	0.02	0.03
1322	55	20.52	20.52	219.	0.	0.36	1.06	34.27	19.99	9.	0.	0.01	0.03
1323	55	20.52	20.52	206.	0.	0.34	1.00	34.27	19.99	8.	0.	0.01	0.02
1324	55	20.52	20.52	19.	0.	0.03	0.09	34.27	19.99	11.	0.	0.02	0.03

***** TAGLIO PERPENDICOLARE

GUSCI	tx	ty	tz	GUSCI	tx	ty	tz	GUSCI	tx	ty	tz
1301	0.5	0.3	0.4	1302	0.5	0.4	0.5	1303	0.5	0.4	0.5
1304	0.5	0.3	0.4	1305	0.5	1.7	1.6	1306	0.5	1.6	1.2
1307	0.5	1.5	1.1	1308	0.5	1.6	1.6	1309	0.3	0.8	0.7
1310	0.8	0.9	0.9	1311	0.8	0.9	0.9	1312	0.4	0.7	0.7
1313	0.4	0.7	0.7	1314	0.8	0.9	0.9	1315	0.8	0.9	0.9
1316	0.4	0.7	0.7	1317	0.5	1.6	1.5	1318	0.5	1.5	1.1
1319	0.5	1.5	1.1	1320	0.5	1.6	1.5	1321	0.5	0.3	0.4
1322	0.5	0.3	0.5	1323	0.5	0.3	0.5	1324	0.5	0.3	0.4

VERIFICHE A PUNZONAMENTO

	Norm	beta	sigT	Pcrit	Ro	Acrit	VRd,c	Ved	A staffe	VRd,cs		
A	13	-2800.574	1.54	0.010	621.8	0.26	112175.1	1651.220	3811.620	95.3	-0.010	si
		[kN]	[N/mm2]	[cm]	[%]	[cm2]	[kN]	[kN]	[cm2]	[kN]		

MACROGUSCIO: Pulvino14

GUSCI	spess	INFERIORE ORIZZONTALE						INFERIORE VERTICALE					
		Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
1401	55	20.52	20.52	11.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01
1402	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
1403	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
1404	55	20.52	20.52	11.	0.	0.02	0.05	19.99	34.27	3.	0.	0.00	0.01
1405	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
1406	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1407	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1408	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
1409	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
1410	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00

1411	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1412	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
1413	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
1414	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1415	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1416	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
1417	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
1418	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1419	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1420	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
1421	55	20.52	20.52	11.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01
1422	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
1423	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
1424	55	20.52	20.52	11.	0.	0.02	0.05	19.99	34.27	3.	0.	0.00	0.01
SUPERIORE ORIZZONTALE													
GUSCI	spess	Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
1401	55	20.52	20.52	20.	0.	0.03	0.10	34.27	19.99	11.	0.	0.02	0.03
1402	55	20.52	20.52	219.	0.	0.36	1.06	34.27	19.99	9.	0.	0.01	0.03
1403	55	20.52	20.52	206.	0.	0.34	1.00	34.27	19.99	8.	0.	0.01	0.02
1404	55	20.52	20.52	20.	0.	0.03	0.10	34.27	19.99	11.	0.	0.02	0.03
1405	55	20.52	20.52	17.	0.	0.03	0.08	34.27	19.99	143.	0.	0.20	0.42
1406	55	20.52	20.52	229.	0.	0.38	1.11	34.27	19.99	135.	0.	0.19	0.40
1407	55	20.52	20.52	212.	0.	0.35	1.03	34.27	19.99	134.	0.	0.19	0.40
1408	55	20.52	20.52	17.	0.	0.03	0.08	34.27	19.99	140.	0.	0.20	0.41
1409	82	20.52	20.52	17.	0.	0.01	0.05	34.27	19.99	730.	0.	0.53	1.40
1410	82	20.52	20.52	229.	0.	0.20	0.72	34.27	19.99	729.	0.	0.53	1.40
1411	82	20.52	20.52	228.	0.	0.20	0.72	34.27	19.99	729.	0.	0.53	1.40
1412	82	20.52	20.52	17.	0.	0.01	0.05	34.27	19.99	730.	0.	0.53	1.40
1413	82	20.52	20.52	13.	0.	0.01	0.04	34.27	19.99	730.	0.	0.53	1.40
1414	82	20.52	20.52	227.	0.	0.20	0.71	34.27	19.99	730.	0.	0.53	1.40
1415	82	20.52	20.52	227.	0.	0.20	0.71	34.27	19.99	730.	0.	0.53	1.40
1416	82	20.52	20.52	13.	0.	0.01	0.04	34.27	19.99	730.	0.	0.53	1.40
1417	55	20.52	20.52	18.	0.	0.03	0.09	34.27	19.99	143.	0.	0.20	0.42
1418	55	20.52	20.52	223.	0.	0.37	1.08	34.27	19.99	135.	0.	0.19	0.40
1419	55	20.52	20.52	218.	0.	0.36	1.05	34.27	19.99	133.	0.	0.19	0.39
1420	55	20.52	20.52	18.	0.	0.03	0.09	34.27	19.99	139.	0.	0.19	0.41
1421	55	20.52	20.52	19.	0.	0.03	0.09	34.27	19.99	11.	0.	0.02	0.03
1422	55	20.52	20.52	219.	0.	0.36	1.06	34.27	19.99	9.	0.	0.01	0.03
1423	55	20.52	20.52	206.	0.	0.34	1.00	34.27	19.99	8.	0.	0.01	0.02
1424	55	20.52	20.52	19.	0.	0.03	0.09	34.27	19.99	11.	0.	0.02	0.03

***** TAGLIO PERPENDICOLARE

GUSCI	tx	ty	tz	GUSCI	tx	ty	tz	GUSCI	tx	ty	tz
1401	0.5	0.3	0.4	1402	0.5	0.3	0.5	1403	0.5	0.4	0.5
1404	0.5	0.3	0.4	1405	0.5	1.7	1.6	1406	0.5	1.6	1.2
1407	0.5	1.5	1.1	1408	0.5	1.6	1.6	1409	0.3	0.8	0.7
1410	0.8	0.9	0.9	1411	0.8	0.9	0.9	1412	0.4	0.7	0.7
1413	0.4	0.7	0.7	1414	0.8	0.9	0.9	1415	0.8	0.9	0.9
1416	0.4	0.7	0.7	1417	0.5	1.6	1.5	1418	0.5	1.5	1.1
1419	0.5	1.5	1.1	1420	0.5	1.6	1.5	1421	0.5	0.3	0.4
1422	0.5	0.4	0.5	1423	0.5	0.3	0.5	1424	0.5	0.3	0.4

VERIFICHE A PUNZONAMENTO

A	14	Norm [kN]	beta	sigT [N/mm2]	Pcrit [cm]	Ro [%]	Acrit [cm2]	VRd,c [kN]	VED [kN]	A staffe [cm2]	VRd,cs [kN]	si
		-2800.563	1.54	0.010	621.8	0.26	112175.1	1651.220	3811.600	95.3	-0.010	

MACROGUSCIO: Pulvino15

INFERIORE ORIZZONTALE								INFERIORE VERTICALE					
GUSCI	spess	Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
1501	55	20.52	20.52	11.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01
1502	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
1503	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
1504	55	20.52	20.52	11.	0.	0.02	0.05	19.99	34.27	3.	0.	0.00	0.01
1505	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
1506	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1507	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1508	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
1509	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
1510	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1511	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1512	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
1513	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
1514	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1515	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1516	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
1517	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
1518	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1519	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1520	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
1521	55	20.52	20.52	11.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01
1522	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
1523	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
1524	55	20.52	20.52	11.	0.	0.02	0.05	19.99	34.27	3.	0.	0.00	0.01
SUPERIORE ORIZZONTALE								SUPERIORE VERTICALE					
GUSCI	spess	Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
1501	55	20.52	20.52	20.	0.	0.03	0.10	34.27	19.99	11.	0.	0.02	0.03
1502	55	20.52	20.52	218.	0.	0.36	1.06	34.27	19.99	9.	0.	0.01	0.03
1503	55	20.52	20.52	206.	0.	0.34	0.99	34.27	19.99	8.	0.	0.01	0.02
1504	55	20.52	20.52	20.	0.	0.03	0.10	34.27	19.99	11.	0.	0.02	0.03
1505	55	20.52	20.52	17.	0.	0.03	0.08	34.27	19.99	144.	0.	0.20	0.42
1506	55	20.52	20.52	228.	0.	0.38	1.10	34.27	19.99	135.	0.	0.19	0.40
1507	55	20.52	20.52	212.	0.	0.35	1.02	34.27	19.99	134.	0.	0.19	0.40
1508	55	20.52	20.52	17.	0.	0.03	0.08	34.27	19.99	140.	0.	0.20	0.41
1509	82	20.52	20.52	17.	0.	0.01	0.05	34.27	19.99	730.	0.	0.53	1.40
1510	82	20.52	20.52	228.	0.	0.20	0.72	34.27	19.99	729.	0.	0.53	1.40

1511	82	20.52	20.52	228.	0.	0.20	0.71	34.27	19.99	729.	0.	0.53	1.40
1512	82	20.52	20.52	17.	0.	0.01	0.05	34.27	19.99	730.	0.	0.53	1.40
1513	82	20.52	20.52	13.	0.	0.01	0.04	34.27	19.99	730.	0.	0.53	1.40
1514	82	20.52	20.52	227.	0.	0.20	0.71	34.27	19.99	730.	0.	0.53	1.40
1515	82	20.52	20.52	227.	0.	0.20	0.71	34.27	19.99	730.	0.	0.53	1.40
1516	82	20.52	20.52	13.	0.	0.01	0.04	34.27	19.99	730.	0.	0.53	1.40
1517	55	20.52	20.52	18.	0.	0.03	0.09	34.27	19.99	143.	0.	0.20	0.42
1518	55	20.52	20.52	223.	0.	0.37	1.08	34.27	19.99	135.	0.	0.19	0.40
1519	55	20.52	20.52	218.	0.	0.36	1.05	34.27	19.99	134.	0.	0.19	0.39
1520	55	20.52	20.52	18.	0.	0.03	0.09	34.27	19.99	139.	0.	0.19	0.41
1521	55	20.52	20.52	19.	0.	0.03	0.09	34.27	19.99	11.	0.	0.02	0.03
1522	55	20.52	20.52	218.	0.	0.36	1.06	34.27	19.99	9.	0.	0.01	0.03
1523	55	20.52	20.52	206.	0.	0.34	0.99	34.27	19.99	8.	0.	0.01	0.02
1524	55	20.52	20.52	19.	0.	0.03	0.09	34.27	19.99	11.	0.	0.01	0.03

***** TAGLIO PERPENDICOLARE

GUSCI	τ_x	τ_y	τ_t	GUSCI	τ_x	τ_y	τ_t	GUSCI	τ_x	τ_y	τ_t
1501	0.5	0.3	0.4	1502	0.5	0.4	0.5	1503	0.5	0.4	0.5
1504	0.5	0.3	0.4	1505	0.5	1.7	1.6	1506	0.5	1.6	1.2
1507	0.5	1.5	1.1	1508	0.5	1.6	1.6	1509	0.3	0.8	0.7
1510	0.8	0.9	0.9	1511	0.8	0.9	0.9	1512	0.4	0.7	0.7
1513	0.4	0.7	0.7	1514	0.8	0.9	0.9	1515	0.8	0.9	0.9
1516	0.4	0.7	0.7	1517	0.5	1.6	1.5	1518	0.5	1.5	1.1
1519	0.5	1.5	1.1	1520	0.5	1.6	1.5	1521	0.5	0.3	0.4
1522	0.5	0.4	0.5	1523	0.5	0.3	0.5	1524	0.5	0.3	0.4

VERIFICHE A PUNZONAMENTO

	Norm	beta	sigT	Pcrit	Ro	Acrit	VRd,c	VED	A staffe	VRd,cs	
A	[kN]		[N/mm2]	[cm]	[%]	[cm2]	[kN]	[kN]	[cm2]	[kN]	si
A	15	-2800.588	1.54	0.010	621.8	0.26	112175.1	1651.220	3811.640	95.3	-0.010

VERIFICA PULVINI (fessurazione effetto piastra):

PARAMETRI GENERALI

CASI DI CARICO:

Nome	Descrizione
16	Rara (RARA)
17	Rara VentoY (RARA)
18	Frequente (FREQUENTE)
19	Frequente VentoY (FREQUENTE)
20	Quasi Perm (QUASI PERMANENTE)

DATI:

copriferro inferiore (asse armatura):	3	cm
copriferro superiore (asse armatura):	3	cm
Af	= area effettiva tesa (cm ² al metro)	
Afc	= area effettiva compressa (cm ² al metro)	
Mom	= momento flettente [kNm/m]	
Nor	= sforzo normale [kN]	
σc	= tensione calcestruzzo [N/mm ²]	
	valore max per combinazione rara	= 14.9 N/mm ²
	quasi permanente	= 11.2 N/mm ²
σf	= tensione acciaio [N/mm ²]	
	valore max per combinazione rara	= 360 N/mm ²
wkF	= apertura caratteristica per combinazione frequente (mm)	- valore max = 0.4 mm
wkP	= apertura caratteristica per combinazione quasi permanente (mm)	- valore max = 0.3 mm

MACROGUSCIO: Pulvino1

GUSCI	ARMATURA INFERIORE ORIZZONTALE												
	COMBINAZIONE RARA						COMB. FREQUENTE			COMB. QUASI PERMANENTE			
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	wkF	Mom	Nor	σc	wkP
101	20.52	20.52	11.24	0.00	0.26	11.	10.71	0.00	0.004	0.00	0.00	0.00	0.000
102	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
103	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
104	20.52	20.52	11.21	0.00	0.26	11.	10.68	0.00	0.004	0.00	0.00	0.00	0.000
105	20.52	20.52	10.75	0.00	0.25	11.	10.32	0.00	0.004	0.00	0.00	0.00	0.000
106	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
107	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
108	20.52	20.52	10.70	0.00	0.25	11.	10.28	0.00	0.004	0.00	0.00	0.00	0.000
109	20.52	20.52	11.37	0.00	0.14	7.	10.78	0.00	0.003	0.00	0.00	0.00	0.000
110	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
111	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
112	20.52	20.52	11.31	0.00	0.14	7.	10.73	0.00	0.003	0.00	0.00	0.00	0.000
113	20.52	20.52	11.84	0.00	0.14	8.	11.26	0.00	0.003	0.00	0.00	0.00	0.000
114	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
115	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
116	20.52	20.52	11.79	0.00	0.14	8.	11.22	0.00	0.003	0.00	0.00	0.00	0.000
117	20.52	20.52	16.57	0.00	0.38	17.	15.67	0.00	0.006	0.00	0.00	0.00	0.000
118	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
119	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
120	20.52	20.52	16.58	0.00	0.38	17.	15.66	0.00	0.006	0.00	0.00	0.00	0.000
121	20.52	20.52	18.09	0.00	0.42	18.	17.09	0.00	0.007	0.00	0.00	0.00	0.000
122	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
123	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
124	20.52	20.52	18.12	0.00	0.42	18.	17.10	0.00	0.007	0.00	0.00	0.00	0.000
GUSCI	ARMATURA INFERIORE VERTICALE												
	COMBINAZIONE RARA						COMB. FREQUENTE			COMB. QUASI PERMANENTE			
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	wkF	Mom	Nor	σc	wkP
101	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
102	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
103	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
104	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
105	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
106	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
107	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
108	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
109	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
110	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
111	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
112	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
113	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
114	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
115	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
116	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
117	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
118	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
119	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
120	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
121	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
122	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
123	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
124	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
GUSCI	ARMATURA SUPERIORE ORIZZONTALE												
	COMBINAZIONE RARA						COMB. FREQUENTE			COMB. QUASI PERMANENTE			
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	wkF	Mom	Nor	σc	wkP
101	20.52	20.52	0.42	0.00	0.01	0.	0.00	0.00	0.000	6.83	0.00	0.16	0.003
102	20.52	20.52	139.01	0.00	3.22	141.	131.48	0.00	0.061	106.73	0.00	2.47	0.045
103	20.52	20.52	142.28	0.00	3.29	145.	134.59	0.00	0.064	107.07	0.00	2.48	0.046
104	20.52	20.52	0.26	0.00	0.01	0.	0.00	0.00	0.000	6.79	0.00	0.16	0.003
105	20.52	20.52	0.10	0.00	0.00	0.	0.00	0.00	0.000	3.35	0.00	0.08	0.001
106	20.52	20.52	146.82	0.00	3.40	149.	138.91	0.00	0.066	111.30	0.00	2.58	0.048
107	20.52	20.52	143.30	0.00	3.32	146.	135.54	0.00	0.064	111.70	0.00	2.59	0.049
108	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	3.35	0.00	0.08	0.001
109	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.28	0.00	0.06	0.001
110	20.52	20.52	154.61	0.00	1.88	102.	146.46	0.00	0.038	121.53	0.00	1.48	0.031

111	20.52	20.52	150.06	0.00	1.83	99.	142.22	0.00	0.036	121.83	0.00	1.48	0.031
112	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.27	0.00	0.06	0.001
113	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.77	0.00	0.09	0.002
114	20.52	20.52	156.67	0.00	1.91	103.	148.44	0.00	0.039	123.16	0.00	1.50	0.031
115	20.52	20.52	152.43	0.00	1.86	100.	144.47	0.00	0.037	123.47	0.00	1.50	0.031
116	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.79	0.00	0.09	0.002
117	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.80	0.00	0.16	0.003
118	20.52	20.52	143.83	0.00	3.33	146.	136.44	0.00	0.065	122.62	0.00	2.84	0.056
119	20.52	20.52	145.53	0.00	3.37	148.	137.98	0.00	0.066	123.00	0.00	2.85	0.056
120	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.77	0.00	0.16	0.003
121	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	8.86	0.00	0.21	0.003
122	20.52	20.52	135.43	0.00	3.14	138.	128.52	0.00	0.060	113.37	0.00	2.63	0.050
123	20.52	20.52	137.35	0.00	3.18	140.	130.25	0.00	0.061	113.71	0.00	2.63	0.050
124	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	8.80	0.00	0.20	0.003

ARMATURA SUPERIORE VERTICALE

GUSCI	COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE					
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	wkF	Mom	Nor	σc	wkP
101	34.27	19.99	7.56	0.00	0.15	5.	7.18	0.00	0.001	5.93	0.00	0.12	0.001
102	34.27	19.99	4.72	0.00	0.09	3.	4.68	0.00	0.001	2.39	0.00	0.05	0.000
103	34.27	19.99	5.70	0.00	0.11	4.	5.62	0.00	0.001	2.23	0.00	0.04	0.000
104	34.27	19.99	8.90	0.00	0.17	6.	8.46	0.00	0.001	5.70	0.00	0.11	0.001
105	34.27	19.99	88.09	0.00	1.73	55.	82.30	0.00	0.012	68.10	0.00	1.34	0.010
106	34.27	19.99	89.99	0.00	1.77	56.	83.50	0.00	0.013	65.73	0.00	1.29	0.010
107	34.27	19.99	94.88	0.00	1.86	59.	88.33	0.00	0.013	67.49	0.00	1.33	0.010
108	34.27	19.99	95.53	0.00	1.88	59.	88.77	0.00	0.013	75.05	0.00	1.47	0.011
109	34.27	19.99	490.85	0.00	5.02	197.	466.15	0.00	0.066	373.56	0.00	3.82	0.051
110	34.27	19.99	491.03	0.00	5.02	197.	466.31	0.00	0.066	373.44	0.00	3.82	0.051
111	34.27	19.99	491.03	0.00	5.02	197.	466.31	0.00	0.066	373.44	0.00	3.82	0.051
112	34.27	19.99	491.21	0.00	5.02	198.	466.49	0.00	0.066	373.37	0.00	3.82	0.051
113	34.27	19.99	495.22	0.00	5.06	199.	466.98	0.00	0.067	373.56	0.00	3.82	0.051
114	34.27	19.99	495.42	0.00	5.06	199.	467.17	0.00	0.067	373.44	0.00	3.82	0.051
115	34.27	19.99	495.42	0.00	5.06	199.	467.17	0.00	0.067	373.44	0.00	3.82	0.051
116	34.27	19.99	495.61	0.00	5.07	199.	467.35	0.00	0.067	373.37	0.00	3.82	0.051
117	34.27	19.99	81.77	0.00	1.61	51.	81.76	0.00	0.012	68.10	0.00	1.34	0.010
118	34.27	19.99	87.20	0.00	1.71	54.	82.68	0.00	0.012	65.73	0.00	1.29	0.010
119	34.27	19.99	92.65	0.00	1.82	58.	87.62	0.00	0.013	67.49	0.00	1.33	0.010
120	34.27	19.99	93.42	0.00	1.84	58.	87.99	0.00	0.013	75.05	0.00	1.47	0.011
121	34.27	19.99	7.54	0.00	0.15	5.	7.17	0.00	0.001	5.93	0.00	0.12	0.001
122	34.27	19.99	4.72	0.00	0.09	3.	4.68	0.00	0.001	2.39	0.00	0.05	0.000
123	34.27	19.99	5.70	0.00	0.11	4.	5.62	0.00	0.001	2.23	0.00	0.04	0.000
124	34.27	19.99	8.88	0.00	0.17	6.	8.45	0.00	0.001	5.70	0.00	0.11	0.001

MACROGUSCIO: Pulvino2

ARMATURA INFERIORE ORIZZONTALE

GUSCI	COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE					
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	wkF	Mom	Nor	σc	wkP
201	20.52	20.52	11.21	0.00	0.26	11.	10.67	0.00	0.004	0.00	0.00	0.00	0.000
202	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
203	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
204	20.52	20.52	11.07	0.00	0.26	11.	10.55	0.00	0.004	0.00	0.00	0.00	0.000
205	20.52	20.52	10.70	0.00	0.25	11.	10.27	0.00	0.004	0.00	0.00	0.00	0.000
206	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
207	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
208	20.52	20.52	10.51	0.00	0.24	11.	10.11	0.00	0.004	0.00	0.00	0.00	0.000
209	20.52	20.52	11.29	0.00	0.14	7.	10.71	0.00	0.003	0.00	0.00	0.00	0.000
210	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
211	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
212	20.52	20.52	11.17	0.00	0.14	7.	10.60	0.00	0.003	0.00	0.00	0.00	0.000
213	20.52	20.52	11.77	0.00	0.14	8.	11.20	0.00	0.003	0.00	0.00	0.00	0.000
214	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
215	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
216	20.52	20.52	11.57	0.00	0.14	8.	11.01	0.00	0.003	0.00	0.00	0.00	0.000
217	20.52	20.52	16.58	0.00	0.38	17.	15.65	0.00	0.006	0.00	0.00	0.00	0.000
218	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
219	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
220	20.52	20.52	16.55	0.00	0.38	17.	15.57	0.00	0.006	0.00	0.00	0.00	0.000
221	20.52	20.52	18.13	0.00	0.42	18.	17.10	0.00	0.007	0.00	0.00	0.00	0.000
222	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
223	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
224	20.52	20.52	18.08	0.00	0.42	18.	16.99	0.00	0.007	0.00	0.00	0.00	0.000

ARMATURA INFERIORE VERTICALE

GUSCI	COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE					
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	wkF	Mom	Nor	σc	wkP
201	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
202	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
203	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
204	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
205	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
206	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
207	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
208	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
209	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
210	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
211	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
212	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
213	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
214	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
215	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
216	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
217	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
218	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
219	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
220	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
221	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000

222	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
223	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
224	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000

ARMATURA SUPERIORE ORIZZONTALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE						
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	wkF	Mom	Nor	σc	wkP
201	20.52	20.52	0.11	0.00	0.00	0.	0.00	0.00	0.000	6.78	0.00	0.16	0.003
202	20.52	20.52	149.44	0.00	3.46	152.	141.52	0.00	0.068	113.81	0.00	2.64	0.050
203	20.52	20.52	138.59	0.00	3.21	141.	130.93	0.00	0.061	113.66	0.00	2.63	0.050
204	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	8.81	0.00	0.20	0.003
205	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	3.34	0.00	0.08	0.001
206	20.52	20.52	155.59	0.00	3.60	158.	147.31	0.00	0.072	123.06	0.00	2.85	0.056
207	20.52	20.52	146.63	0.00	3.40	149.	138.53	0.00	0.066	122.92	0.00	2.85	0.056
208	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.77	0.00	0.16	0.003
209	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.27	0.00	0.06	0.001
210	20.52	20.52	157.84	0.00	1.92	104.	149.54	0.00	0.039	123.52	0.00	1.50	0.031
211	20.52	20.52	153.16	0.00	1.87	101.	144.89	0.00	0.037	123.44	0.00	1.50	0.031
212	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.78	0.00	0.09	0.002
213	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.79	0.00	0.09	0.002
214	20.52	20.52	156.99	0.00	1.91	104.	148.73	0.00	0.039	121.86	0.00	1.48	0.031
215	20.52	20.52	152.65	0.00	1.86	101.	144.44	0.00	0.037	121.81	0.00	1.48	0.031
216	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.27	0.00	0.06	0.001
217	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.75	0.00	0.16	0.003
218	20.52	20.52	139.13	0.00	3.22	141.	131.87	0.00	0.062	111.76	0.00	2.59	0.049
219	20.52	20.52	140.33	0.00	3.25	143.	132.96	0.00	0.062	111.61	0.00	2.58	0.049
220	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	3.34	0.00	0.08	0.001
221	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	8.78	0.00	0.20	0.003
222	20.52	20.52	129.66	0.00	3.00	132.	122.92	0.00	0.056	107.17	0.00	2.48	0.046
223	20.52	20.52	131.12	0.00	3.04	133.	124.25	0.00	0.057	107.02	0.00	2.48	0.046
224	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.80	0.00	0.16	0.003

ARMATURA SUPERIORE VERTICALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE						
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	wkF	Mom	Nor	σc	wkP
201	34.27	19.99	7.60	0.00	0.15	5.	7.23	0.00	0.001	5.95	0.00	0.12	0.001
202	34.27	19.99	4.55	0.00	0.09	3.	4.59	0.00	0.001	2.44	0.00	0.05	0.000
203	34.27	19.99	5.56	0.00	0.11	3.	5.55	0.00	0.001	2.20	0.00	0.04	0.000
204	34.27	19.99	8.79	0.00	0.17	5.	8.43	0.00	0.001	5.70	0.00	0.11	0.001
205	34.27	19.99	95.68	0.00	1.88	59.	89.39	0.00	0.013	74.95	0.00	1.47	0.011
206	34.27	19.99	89.85	0.00	1.76	56.	83.51	0.00	0.013	67.32	0.00	1.32	0.010
207	34.27	19.99	93.62	0.00	1.84	58.	87.07	0.00	0.013	65.53	0.00	1.29	0.010
208	34.27	19.99	93.47	0.00	1.84	58.	86.66	0.00	0.013	68.27	0.00	1.34	0.010
209	34.27	19.99	490.08	0.00	5.01	197.	465.35	0.00	0.066	373.29	0.00	3.82	0.051
210	34.27	19.99	490.25	0.00	5.01	197.	465.52	0.00	0.066	373.37	0.00	3.82	0.051
211	34.27	19.99	490.25	0.00	5.01	197.	465.52	0.00	0.066	373.37	0.00	3.82	0.051
212	34.27	19.99	490.65	0.00	5.01	197.	465.89	0.00	0.066	373.48	0.00	3.82	0.051
213	34.27	19.99	495.56	0.00	5.06	199.	467.52	0.00	0.067	373.29	0.00	3.82	0.051
214	34.27	19.99	495.77	0.00	5.07	199.	467.72	0.00	0.067	373.37	0.00	3.82	0.051
215	34.27	19.99	495.77	0.00	5.07	199.	467.72	0.00	0.067	373.37	0.00	3.82	0.051
216	34.27	19.99	496.18	0.00	5.07	200.	468.10	0.00	0.067	373.48	0.00	3.82	0.051
217	34.27	19.99	83.61	0.00	1.64	52.	88.82	0.00	0.013	74.95	0.00	1.47	0.011
218	34.27	19.99	79.44	0.00	1.56	49.	82.78	0.00	0.012	67.32	0.00	1.32	0.010
219	34.27	19.99	84.38	0.00	1.66	52.	86.34	0.00	0.013	65.53	0.00	1.29	0.010
220	34.27	19.99	85.75	0.00	1.68	53.	85.82	0.00	0.013	68.27	0.00	1.34	0.010
221	34.27	19.99	7.62	0.00	0.15	5.	7.23	0.00	0.001	5.95	0.00	0.12	0.001
222	34.27	19.99	4.58	0.00	0.09	3.	4.60	0.00	0.001	2.44	0.00	0.05	0.000
223	34.27	19.99	5.59	0.00	0.11	3.	5.56	0.00	0.001	2.20	0.00	0.04	0.000
224	34.27	19.99	8.81	0.00	0.17	5.	8.43	0.00	0.001	5.70	0.00	0.11	0.001

MACROGUSCIO: Pulvino3

ARMATURA INFERIORE ORIZZONTALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE						
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	wkF	Mom	Nor	σc	wkP
301	20.52	20.52	10.87	0.00	0.25	11.	10.29	0.00	0.004	0.00	0.00	0.00	0.000
302	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
303	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
304	20.52	20.52	10.90	0.00	0.25	11.	10.30	0.00	0.004	0.00	0.00	0.00	0.000
305	20.52	20.52	10.32	0.00	0.24	10.	9.78	0.00	0.004	0.00	0.00	0.00	0.000
306	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
307	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
308	20.52	20.52	10.35	0.00	0.24	11.	9.79	0.00	0.004	0.00	0.00	0.00	0.000
309	20.52	20.52	10.72	0.00	0.13	7.	10.12	0.00	0.003	0.00	0.00	0.00	0.000
310	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
311	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
312	20.52	20.52	10.77	0.00	0.13	7.	10.14	0.00	0.003	0.00	0.00	0.00	0.000
313	20.52	20.52	11.18	0.00	0.14	7.	10.59	0.00	0.003	0.00	0.00	0.00	0.000
314	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
315	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
316	20.52	20.52	11.23	0.00	0.14	7.	10.61	0.00	0.003	0.00	0.00	0.00	0.000
317	20.52	20.52	16.27	0.00	0.38	17.	15.43	0.00	0.006	0.00	0.00	0.00	0.000
318	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
319	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
320	20.52	20.52	16.35	0.00	0.38	17.	15.45	0.00	0.006	0.00	0.00	0.00	0.000
321	20.52	20.52	17.94	0.00	0.42	18.	17.01	0.00	0.007	0.00	0.00	0.00	0.000
322	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
323	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
324	20.52	20.52	18.04	0.00	0.42	18.	17.03	0.00	0.007	0.00	0.00	0.00	0.000

ARMATURA INFERIORE VERTICALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE						
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	wkF	Mom	Nor	σc	wkP
301	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
302	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
303	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
304	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
305	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000

306	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
307	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
308	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
309	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
310	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
311	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
312	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
313	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
314	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
315	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
316	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
317	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
318	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
319	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
320	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
321	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
322	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
323	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
324	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000

ARMATURA SUPERIORE ORIZZONTALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE						
	Af	Afc	Mom	Nor	σ_c	σ_f	Mom	Nor	wkF	Mom	Nor	σ_c	wkP
301	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	8.81	0.00	0.20	0.003
302	20.52	20.52	144.49	0.00	3.35	147.	136.92	0.00	0.065	110.57	0.00	2.56	0.048
303	20.52	20.52	140.91	0.00	3.26	143.	133.30	0.00	0.063	117.12	0.00	2.71	0.052
304	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	8.81	0.00	0.20	0.003
305	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.85	0.00	0.16	0.003
306	20.52	20.52	145.55	0.00	3.37	148.	137.85	0.00	0.066	114.95	0.00	2.66	0.051
307	20.52	20.52	148.87	0.00	3.45	151.	140.85	0.00	0.068	126.14	0.00	2.92	0.058
308	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.86	0.00	0.16	0.003
309	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.93	0.00	0.10	0.002
310	20.52	20.52	152.26	0.00	1.85	100.	144.22	0.00	0.037	124.60	0.00	1.52	0.032
311	20.52	20.52	155.26	0.00	1.89	102.	147.04	0.00	0.038	126.34	0.00	1.54	0.032
312	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.92	0.00	0.10	0.002
313	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.21	0.00	0.06	0.001
314	20.52	20.52	154.73	0.00	1.88	102.	146.59	0.00	0.038	126.35	0.00	1.54	0.032
315	20.52	20.52	154.73	0.00	1.88	102.	146.56	0.00	0.038	124.59	0.00	1.52	0.032
316	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.21	0.00	0.06	0.001
317	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	3.67	0.00	0.09	0.001
318	20.52	20.52	147.47	0.00	3.41	150.	139.89	0.00	0.067	126.17	0.00	2.92	0.058
319	20.52	20.52	142.23	0.00	3.29	145.	134.87	0.00	0.064	114.91	0.00	2.66	0.051
320	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	3.67	0.00	0.09	0.001
321	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.94	0.00	0.16	0.003
322	20.52	20.52	139.28	0.00	3.23	142.	132.16	0.00	0.062	117.16	0.00	2.71	0.052
323	20.52	20.52	132.95	0.00	3.08	135.	126.11	0.00	0.058	110.53	0.00	2.56	0.048
324	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.94	0.00	0.16	0.003

ARMATURA SUPERIORE VERTICALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE						
	Af	Afc	Mom	Nor	σ_c	σ_f	Mom	Nor	wkF	Mom	Nor	σ_c	wkP
301	34.27	19.99	8.24	0.00	0.16	5.	7.81	0.00	0.001	6.32	0.00	0.12	0.001
302	34.27	19.99	4.74	0.00	0.09	3.	4.77	0.00	0.001	2.68	0.00	0.05	0.000
303	34.27	19.99	5.73	0.00	0.11	4.	5.70	0.00	0.001	2.27	0.00	0.04	0.000
304	34.27	19.99	9.23	0.00	0.18	6.	8.84	0.00	0.001	5.78	0.00	0.11	0.001
305	34.27	19.99	95.13	0.00	1.87	59.	89.18	0.00	0.013	75.54	0.00	1.48	0.011
306	34.27	19.99	88.87	0.00	1.75	55.	82.86	0.00	0.012	67.34	0.00	1.32	0.010
307	34.27	19.99	92.71	0.00	1.82	58.	86.48	0.00	0.013	65.42	0.00	1.29	0.010
308	34.27	19.99	92.16	0.00	1.81	57.	85.63	0.00	0.013	69.29	0.00	1.36	0.010
309	34.27	19.99	487.30	0.00	4.98	196.	462.62	0.00	0.066	373.39	0.00	3.82	0.051
310	34.27	19.99	487.53	0.00	4.98	196.	462.83	0.00	0.066	373.47	0.00	3.82	0.051
311	34.27	19.99	487.53	0.00	4.98	196.	462.83	0.00	0.066	373.47	0.00	3.82	0.051
312	34.27	19.99	487.71	0.00	4.98	196.	463.00	0.00	0.066	373.58	0.00	3.82	0.051
313	34.27	19.99	501.29	0.00	5.12	202.	473.19	0.00	0.068	373.39	0.00	3.82	0.051
314	34.27	19.99	501.48	0.00	5.13	202.	473.36	0.00	0.068	373.47	0.00	3.82	0.051
315	34.27	19.99	501.48	0.00	5.13	202.	473.36	0.00	0.068	373.47	0.00	3.82	0.051
316	34.27	19.99	501.90	0.00	5.13	202.	473.76	0.00	0.068	373.58	0.00	3.82	0.051
317	34.27	19.99	84.08	0.00	1.65	52.	79.90	0.00	0.012	75.54	0.00	1.48	0.011
318	34.27	19.99	79.31	0.00	1.56	49.	75.77	0.00	0.011	67.34	0.00	1.32	0.010
319	34.27	19.99	84.79	0.00	1.67	53.	81.08	0.00	0.012	65.42	0.00	1.29	0.010
320	34.27	19.99	85.86	0.00	1.69	53.	82.14	0.00	0.012	69.29	0.00	1.36	0.010
321	34.27	19.99	8.27	0.00	0.16	5.	7.82	0.00	0.001	6.32	0.00	0.12	0.001
322	34.27	19.99	4.79	0.00	0.09	3.	4.78	0.00	0.001	2.68	0.00	0.05	0.000
323	34.27	19.99	5.78	0.00	0.11	4.	5.71	0.00	0.001	2.27	0.00	0.04	0.000
324	34.27	19.99	9.29	0.00	0.18	6.	8.85	0.00	0.001	5.78	0.00	0.11	0.001

MACROGUSCIO: Pulvino4

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE						
	Af	Afc	Mom	Nor	σ_c	σ_f	Mom	Nor	wkF	Mom	Nor	σ_c	wkP
401	20.52	20.52	10.89	0.00	0.25	11.	10.30	0.00	0.004	0.00	0.00	0.00	0.000
402	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
403	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
404	20.52	20.52	10.91	0.00	0.25	11.	10.31	0.00	0.004	0.00	0.00	0.00	0.000
405	20.52	20.52	10.34	0.00	0.24	11.	9.79	0.00	0.004	0.00	0.00	0.00	0.000
406	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
407	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
408	20.52	20.52	10.36	0.00	0.24	11.	9.80	0.00	0.004	0.00	0.00	0.00	0.000
409	20.52	20.52	10.76	0.00	0.13	7.	10.13	0.00	0.003	0.00	0.00	0.00	0.000
410	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
411	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
412	20.52	20.52	10.77	0.00	0.13	7.	10.14	0.00	0.003	0.00	0.00	0.00	0.000
413	20.52	20.52	11.22	0.00	0.14	7.	10.59	0.00	0.003	0.00	0.00	0.00	0.000
414	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
415	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
416	20.52	20.52	11.23	0.00	0.14	7.	10.61	0.00	0.003	0.00	0.00	0.00	0.000

417	20.52	20.52	16.35	0.00	0.38	17.	15.44	0.00	0.006	0.00	0.00	0.00	0.000
418	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
419	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
420	20.52	20.52	16.34	0.00	0.38	17.	15.45	0.00	0.006	0.00	0.00	0.00	0.000
421	20.52	20.52	18.04	0.00	0.42	18.	17.03	0.00	0.007	0.00	0.00	0.00	0.000
422	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
423	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
424	20.52	20.52	18.03	0.00	0.42	18.	17.03	0.00	0.007	0.00	0.00	0.00	0.000

ARMATURA INFERIORE VERTICALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE						
	Af	Afc	Mom	Nor	σ_c	σ_f	Mom	Nor	wkF	Mom	Nor	σ_c	wkP
401	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
402	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
403	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
404	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
405	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
406	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
407	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
408	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
409	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
410	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
411	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
412	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
413	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
414	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
415	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
416	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
417	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
418	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
419	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
420	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
421	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
422	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
423	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
424	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000

ARMATURA SUPERIORE ORIZZONTALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE						
	Af	Afc	Mom	Nor	σ_c	σ_f	Mom	Nor	wkF	Mom	Nor	σ_c	wkP
401	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	8.80	0.00	0.20	0.003
402	20.52	20.52	151.81	0.00	3.52	154.	143.81	0.00	0.070	117.17	0.00	2.71	0.052
403	20.52	20.52	140.99	0.00	3.26	143.	133.30	0.00	0.063	117.09	0.00	2.71	0.052
404	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	8.81	0.00	0.20	0.003
405	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.85	0.00	0.16	0.003
406	20.52	20.52	157.93	0.00	3.66	160.	149.56	0.00	0.073	126.18	0.00	2.92	0.058
407	20.52	20.52	148.94	0.00	3.45	151.	140.84	0.00	0.068	126.11	0.00	2.92	0.058
408	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.86	0.00	0.16	0.003
409	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.93	0.00	0.10	0.002
410	20.52	20.52	160.06	0.00	1.95	106.	151.65	0.00	0.040	126.35	0.00	1.54	0.032
411	20.52	20.52	155.29	0.00	1.89	102.	147.03	0.00	0.038	126.32	0.00	1.54	0.032
412	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.92	0.00	0.10	0.002
413	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.22	0.00	0.06	0.001
414	20.52	20.52	159.13	0.00	1.94	105.	150.77	0.00	0.040	124.59	0.00	1.52	0.032
415	20.52	20.52	154.77	0.00	1.88	102.	146.54	0.00	0.038	124.58	0.00	1.52	0.032
416	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.21	0.00	0.06	0.001
417	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	3.67	0.00	0.08	0.001
418	20.52	20.52	141.11	0.00	3.27	143.	133.75	0.00	0.063	114.96	0.00	2.66	0.051
419	20.52	20.52	142.23	0.00	3.29	145.	134.85	0.00	0.064	114.88	0.00	2.66	0.051
420	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	3.67	0.00	0.08	0.001
421	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.93	0.00	0.16	0.003
422	20.52	20.52	131.60	0.00	3.05	134.	124.76	0.00	0.057	110.58	0.00	2.56	0.048
423	20.52	20.52	132.97	0.00	3.08	135.	126.09	0.00	0.058	110.50	0.00	2.56	0.048
424	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.94	0.00	0.16	0.003

ARMATURA SUPERIORE VERTICALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE						
	Af	Afc	Mom	Nor	σ_c	σ_f	Mom	Nor	wkF	Mom	Nor	σ_c	wkP
401	34.27	19.99	8.24	0.00	0.16	5.	7.83	0.00	0.001	6.32	0.00	0.12	0.001
402	34.27	19.99	4.84	0.00	0.09	3.	4.77	0.00	0.001	2.69	0.00	0.05	0.000
403	34.27	19.99	5.81	0.00	0.11	4.	5.71	0.00	0.001	2.25	0.00	0.04	0.000
404	34.27	19.99	9.31	0.00	0.18	6.	8.85	0.00	0.001	5.78	0.00	0.11	0.001
405	34.27	19.99	95.52	0.00	1.88	59.	89.31	0.00	0.013	75.62	0.00	1.49	0.011
406	34.27	19.99	89.18	0.00	1.75	55.	82.97	0.00	0.012	67.41	0.00	1.32	0.010
407	34.27	19.99	92.95	0.00	1.83	58.	86.57	0.00	0.013	65.49	0.00	1.29	0.010
408	34.27	19.99	92.34	0.00	1.81	57.	85.70	0.00	0.013	69.30	0.00	1.36	0.010
409	34.27	19.99	490.76	0.00	5.02	197.	465.99	0.00	0.066	373.45	0.00	3.82	0.051
410	34.27	19.99	490.94	0.00	5.02	197.	466.16	0.00	0.066	373.53	0.00	3.82	0.051
411	34.27	19.99	490.94	0.00	5.02	197.	466.16	0.00	0.066	373.53	0.00	3.82	0.051
412	34.27	19.99	491.32	0.00	5.02	198.	466.53	0.00	0.067	373.63	0.00	3.82	0.051
413	34.27	19.99	494.66	0.00	5.06	199.	466.75	0.00	0.067	373.45	0.00	3.82	0.051
414	34.27	19.99	494.87	0.00	5.06	199.	466.95	0.00	0.067	373.53	0.00	3.82	0.051
415	34.27	19.99	494.87	0.00	5.06	199.	466.95	0.00	0.067	373.53	0.00	3.82	0.051
416	34.27	19.99	495.27	0.00	5.06	199.	467.32	0.00	0.067	373.63	0.00	3.82	0.051
417	34.27	19.99	84.08	0.00	1.65	52.	79.95	0.00	0.012	75.62	0.00	1.49	0.011
418	34.27	19.99	79.33	0.00	1.56	49.	75.81	0.00	0.011	67.41	0.00	1.32	0.010
419	34.27	19.99	84.92	0.00	1.67	53.	81.12	0.00	0.012	65.49	0.00	1.29	0.010
420	34.27	19.99	86.17	0.00	1.69	53.	82.22	0.00	0.012	69.30	0.00	1.36	0.010
421	34.27	19.99	8.26	0.00	0.16	5.	7.83	0.00	0.001	6.32	0.00	0.12	0.001
422	34.27	19.99	4.86	0.00	0.10	3.	4.78	0.00	0.001	2.69	0.00	0.05	0.000
423	34.27	19.99	5.84	0.00	0.11	4.	5.72	0.00	0.001	2.25	0.00	0.04	0.000
424	34.27	19.99	9.33	0.00	0.18	6.	8.86	0.00	0.001	5.78	0.00	0.11	0.001

MACROGUSCIO: Pulvino5

ARMATURA INFERIORE ORIZZONTALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE					
	Af	Afc	Mom	Nor	σ_c	σ_f	Mom	Nor	wkF	Mom	Nor	σ_c

501	20.52	20.52	10.90	0.00	0.25	11.	10.30	0.00	0.004	0.00	0.00	0.00	0.000
502	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
503	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
504	20.52	20.52	10.91	0.00	0.25	11.	10.31	0.00	0.004	0.00	0.00	0.00	0.000
505	20.52	20.52	10.35	0.00	0.24	11.	9.79	0.00	0.004	0.00	0.00	0.00	0.000
506	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
507	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
508	20.52	20.52	10.36	0.00	0.24	11.	9.80	0.00	0.004	0.00	0.00	0.00	0.000
509	20.52	20.52	10.76	0.00	0.13	7.	10.13	0.00	0.003	0.00	0.00	0.00	0.000
510	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
511	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
512	20.52	20.52	10.78	0.00	0.13	7.	10.15	0.00	0.003	0.00	0.00	0.00	0.000
513	20.52	20.52	11.21	0.00	0.14	7.	10.60	0.00	0.003	0.00	0.00	0.00	0.000
514	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
515	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
516	20.52	20.52	11.24	0.00	0.14	7.	10.61	0.00	0.003	0.00	0.00	0.00	0.000
517	20.52	20.52	16.34	0.00	0.38	17.	15.44	0.00	0.006	0.00	0.00	0.00	0.000
518	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
519	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
520	20.52	20.52	16.36	0.00	0.38	17.	15.45	0.00	0.006	0.00	0.00	0.00	0.000
521	20.52	20.52	18.02	0.00	0.42	18.	17.02	0.00	0.007	0.00	0.00	0.00	0.000
522	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
523	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
524	20.52	20.52	18.05	0.00	0.42	18.	17.03	0.00	0.007	0.00	0.00	0.00	0.000

ARMATURA INFERIORE VERTICALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE						
	Af	Afc	Mom	Nor	σ_c	σ_f	Mom	Nor	wkF	Mom	Nor	σ_c	wkP
501	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
502	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
503	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
504	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
505	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
506	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
507	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
508	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
509	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
510	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
511	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
512	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
513	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
514	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
515	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
516	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
517	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
518	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
519	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
520	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
521	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
522	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
523	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
524	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000

ARMATURA SUPERIORE ORIZZONTALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE						
	Af	Afc	Mom	Nor	σ_c	σ_f	Mom	Nor	wkF	Mom	Nor	σ_c	wkP
501	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	8.81	0.00	0.20	0.003
502	20.52	20.52	152.11	0.00	3.52	155.	143.85	0.00	0.070	117.12	0.00	2.71	0.052
503	20.52	20.52	140.67	0.00	3.26	143.	133.23	0.00	0.063	117.07	0.00	2.71	0.052
504	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	8.81	0.00	0.20	0.003
505	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.85	0.00	0.16	0.003
506	20.52	20.52	158.17	0.00	3.66	161.	149.59	0.00	0.073	126.14	0.00	2.92	0.058
507	20.52	20.52	148.67	0.00	3.44	151.	140.78	0.00	0.068	126.09	0.00	2.92	0.058
508	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.86	0.00	0.16	0.003
509	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.93	0.00	0.10	0.002
510	20.52	20.52	160.17	0.00	1.95	106.	151.66	0.00	0.040	126.32	0.00	1.54	0.032
511	20.52	20.52	155.15	0.00	1.89	102.	146.99	0.00	0.038	126.30	0.00	1.54	0.032
512	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.92	0.00	0.10	0.002
513	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.21	0.00	0.06	0.001
514	20.52	20.52	159.24	0.00	1.94	105.	150.79	0.00	0.040	124.57	0.00	1.52	0.032
515	20.52	20.52	154.64	0.00	1.88	102.	146.51	0.00	0.038	124.56	0.00	1.52	0.032
516	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.21	0.00	0.06	0.001
517	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	3.67	0.00	0.08	0.001
518	20.52	20.52	141.06	0.00	3.27	143.	133.74	0.00	0.063	114.92	0.00	2.66	0.051
519	20.52	20.52	142.27	0.00	3.29	145.	134.85	0.00	0.064	114.87	0.00	2.66	0.051
520	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	3.67	0.00	0.08	0.001
521	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.94	0.00	0.16	0.003
522	20.52	20.52	131.54	0.00	3.05	134.	124.74	0.00	0.057	110.53	0.00	2.56	0.048
523	20.52	20.52	133.01	0.00	3.08	135.	126.10	0.00	0.058	110.48	0.00	2.56	0.048
524	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.94	0.00	0.16	0.003

ARMATURA SUPERIORE VERTICALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE						
	Af	Afc	Mom	Nor	σ_c	σ_f	Mom	Nor	wkF	Mom	Nor	σ_c	wkP
501	34.27	19.99	8.20	0.00	0.16	5.	7.80	0.00	0.001	6.31	0.00	0.12	0.001
502	34.27	19.99	4.86	0.00	0.10	3.	4.79	0.00	0.001	2.67	0.00	0.05	0.000
503	34.27	19.99	5.83	0.00	0.11	4.	5.72	0.00	0.001	2.27	0.00	0.04	0.000
504	34.27	19.99	9.30	0.00	0.18	6.	8.85	0.00	0.001	5.78	0.00	0.11	0.001
505	34.27	19.99	95.71	0.00	1.88	59.	89.30	0.00	0.013	75.54	0.00	1.48	0.011
506	34.27	19.99	89.29	0.00	1.75	55.	82.95	0.00	0.012	67.34	0.00	1.32	0.010
507	34.27	19.99	93.07	0.00	1.83	58.	86.56	0.00	0.013	65.43	0.00	1.29	0.010
508	34.27	19.99	92.41	0.00	1.82	57.	85.70	0.00	0.013	69.28	0.00	1.36	0.010
509	34.27	19.99	490.59	0.00	5.01	197.	465.92	0.00	0.066	373.40	0.00	3.82	0.051
510	34.27	19.99	490.77	0.00	5.02	197.	466.08	0.00	0.066	373.47	0.00	3.82	0.051
511	34.27	19.99	490.77	0.00	5.02	197.	466.08	0.00	0.066	373.47	0.00	3.82	0.051
512	34.27	19.99	491.15	0.00	5.02	198.	466.45	0.00	0.066	373.58	0.00	3.82	0.051
513	34.27	19.99	494.85	0.00	5.06	199.	466.74	0.00	0.067	373.40	0.00	3.82	0.051
514	34.27	19.99	495.06	0.00	5.06	199.	466.94	0.00	0.067	373.47	0.00	3.82	0.051
515	34.27	19.99	495.06										

516	34.27	19.99	495.46	0.00	5.06	199.	467.32	0.00	0.067	373.58	0.00	3.82	0.051
517	34.27	19.99	83.88	0.00	1.65	52.	79.86	0.00	0.012	75.54	0.00	1.48	0.011
518	34.27	19.99	79.19	0.00	1.56	49.	75.80	0.00	0.011	67.34	0.00	1.32	0.010
519	34.27	19.99	85.00	0.00	1.67	53.	81.12	0.00	0.012	65.43	0.00	1.29	0.010
520	34.27	19.99	86.17	0.00	1.69	53.	82.20	0.00	0.012	69.28	0.00	1.36	0.010
521	34.27	19.99	8.22	0.00	0.16	5.	7.80	0.00	0.001	6.31	0.00	0.12	0.001
522	34.27	19.99	4.88	0.00	0.10	3.	4.79	0.00	0.001	2.67	0.00	0.05	0.000
523	34.27	19.99	5.86	0.00	0.12	4.	5.73	0.00	0.001	2.27	0.00	0.04	0.000
524	34.27	19.99	9.32	0.00	0.18	6.	8.85	0.00	0.001	5.78	0.00	0.11	0.001

MACROGUSCIO: Pulvino6

GUSCI	ARMATURA INFERIORE ORIZZONTALE						COMB. QUASI PERMANENTE						
	COMBINAZIONE RARA		COMB. FREQUENTE		COMB. QUASI PERMANENTE		Mom	Nor	σc	wkP			
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	wkF	Mom	Nor	σc	wkP
601	20.52	20.52	10.89	0.00	0.25	11.	10.30	0.00	0.004	0.00	0.00	0.00	0.000
602	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
603	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
604	20.52	20.52	10.90	0.00	0.25	11.	10.31	0.00	0.004	0.00	0.00	0.00	0.000
605	20.52	20.52	10.34	0.00	0.24	11.	9.79	0.00	0.004	0.00	0.00	0.00	0.000
606	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
607	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
608	20.52	20.52	10.35	0.00	0.24	11.	9.80	0.00	0.004	0.00	0.00	0.00	0.000
609	20.52	20.52	10.76	0.00	0.13	7.	10.13	0.00	0.003	0.00	0.00	0.00	0.000
610	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
611	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
612	20.52	20.52	10.78	0.00	0.13	7.	10.15	0.00	0.003	0.00	0.00	0.00	0.000
613	20.52	20.52	11.21	0.00	0.14	7.	10.60	0.00	0.003	0.00	0.00	0.00	0.000
614	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
615	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
616	20.52	20.52	11.23	0.00	0.14	7.	10.62	0.00	0.003	0.00	0.00	0.00	0.000
617	20.52	20.52	16.32	0.00	0.38	17.	15.44	0.00	0.006	0.00	0.00	0.00	0.000
618	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
619	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
620	20.52	20.52	16.33	0.00	0.38	17.	15.45	0.00	0.006	0.00	0.00	0.00	0.000
621	20.52	20.52	18.01	0.00	0.42	18.	17.02	0.00	0.007	0.00	0.00	0.00	0.000
622	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
623	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
624	20.52	20.52	18.01	0.00	0.42	18.	17.02	0.00	0.007	0.00	0.00	0.00	0.000

GUSCI	ARMATURA INFERIORE VERTICALE						COMB. QUASI PERMANENTE						
	COMBINAZIONE RARA		COMB. FREQUENTE		COMB. QUASI PERMANENTE		Mom	Nor	σc	wkP			
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	wkF	Mom	Nor	σc	wkP
601	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
602	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
603	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
604	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
605	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
606	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
607	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
608	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
609	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
610	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
611	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
612	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
613	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
614	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
615	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
616	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
617	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
618	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
619	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
620	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
621	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
622	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
623	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
624	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000

GUSCI	ARMATURA SUPERIORE ORIZZONTALE						COMB. QUASI PERMANENTE						
	COMBINAZIONE RARA		COMB. FREQUENTE		COMB. QUASI PERMANENTE		Mom	Nor	σc	wkP			
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	wkF	Mom	Nor	σc	wkP
601	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	8.80	0.00	0.20	0.003
602	20.52	20.52	152.09	0.00	3.52	155.	143.84	0.00	0.070	117.12	0.00	2.71	0.052
603	20.52	20.52	140.57	0.00	3.26	143.	133.18	0.00	0.063	117.02	0.00	2.71	0.052
604	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	8.81	0.00	0.20	0.003
605	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.85	0.00	0.16	0.003
606	20.52	20.52	158.17	0.00	3.66	161.	149.59	0.00	0.073	126.14	0.00	2.92	0.058
607	20.52	20.52	148.60	0.00	3.44	151.	140.73	0.00	0.068	126.04	0.00	2.92	0.058
608	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.85	0.00	0.16	0.003
609	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.93	0.00	0.10	0.002
610	20.52	20.52	160.17	0.00	1.95	106.	151.66	0.00	0.040	126.32	0.00	1.54	0.032
611	20.52	20.52	155.10	0.00	1.89	102.	146.95	0.00	0.038	126.26	0.00	1.54	0.032
612	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.92	0.00	0.10	0.002
613	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.22	0.00	0.06	0.001
614	20.52	20.52	159.23	0.00	1.94	105.	150.78	0.00	0.040	124.55	0.00	1.52	0.032
615	20.52	20.52	154.58	0.00	1.88	102.	146.47	0.00	0.038	124.52	0.00	1.52	0.032
616	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.21	0.00	0.06	0.001
617	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	3.67	0.00	0.08	0.001
618	20.52	20.52	141.03	0.00	3.27	143.	133.72	0.00	0.063	114.92	0.00	2.66	0.051
619	20.52	20.52	142.23	0.00	3.29	145.	134.81	0.00	0.064	114.81	0.00	2.66	0.051
620	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	3.66	0.00	0.08	0.001
621	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.93	0.00	0.16	0.003
622	20.52	20.52	131.51	0.00	3.05	134.	124.72	0.00	0.057	110.53	0.00	2.56	0.048
623	20.52	20.52	132.97	0.00	3.08	135.	126.06	0.00	0.058	110.43	0.00	2.56	0.048
624	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.94	0.00	0.16	0.003

GUSCI	ARMATURA SUPERIORE VERTICALE						COMB. QUASI PERMANENTE			
	COMBINAZIONE RARA		COMB. FREQUENTE		COMB. QUASI PERMANENTE		Mom	Nor	σc	wkP

GUSCI	Af	Afc	Mom	Nor	σ_c	σ_f	Mom	Nor	wkF	Mom	Nor	σ_c	wkP
601	34.27	19.99	8.24	0.00	0.16	5.	7.82	0.00	0.001	6.32	0.00	0.12	0.001
602	34.27	19.99	4.84	0.00	0.10	3.	4.77	0.00	0.001	2.68	0.00	0.05	0.000
603	34.27	19.99	5.82	0.00	0.11	4.	5.71	0.00	0.001	2.25	0.00	0.04	0.000
604	34.27	19.99	9.33	0.00	0.18	6.	8.85	0.00	0.001	5.78	0.00	0.11	0.001
605	34.27	19.99	95.84	0.00	1.88	59.	89.38	0.00	0.013	75.62	0.00	1.49	0.011
606	34.27	19.99	89.48	0.00	1.76	56.	83.04	0.00	0.012	67.41	0.00	1.32	0.010
607	34.27	19.99	93.24	0.00	1.83	58.	86.64	0.00	0.013	65.49	0.00	1.29	0.010
608	34.27	19.99	92.64	0.00	1.82	58.	85.77	0.00	0.013	69.28	0.00	1.36	0.010
609	34.27	19.99	490.50	0.00	5.01	197.	465.94	0.00	0.066	373.45	0.00	3.82	0.051
610	34.27	19.99	490.67	0.00	5.01	197.	466.10	0.00	0.066	373.52	0.00	3.82	0.051
611	34.27	19.99	490.67	0.00	5.01	197.	466.10	0.00	0.066	373.52	0.00	3.82	0.051
612	34.27	19.99	491.06	0.00	5.02	197.	466.48	0.00	0.066	373.63	0.00	3.82	0.051
613	34.27	19.99	495.11	0.00	5.06	199.	466.84	0.00	0.067	373.45	0.00	3.82	0.051
614	34.27	19.99	495.32	0.00	5.06	199.	467.04	0.00	0.067	373.52	0.00	3.82	0.051
615	34.27	19.99	495.32	0.00	5.06	199.	467.04	0.00	0.067	373.52	0.00	3.82	0.051
616	34.27	19.99	495.72	0.00	5.07	199.	467.41	0.00	0.067	373.63	0.00	3.82	0.051
617	34.27	19.99	83.99	0.00	1.65	52.	79.93	0.00	0.012	75.62	0.00	1.49	0.011
618	34.27	19.99	79.00	0.00	1.55	49.	75.79	0.00	0.011	67.41	0.00	1.32	0.010
619	34.27	19.99	84.87	0.00	1.67	53.	81.10	0.00	0.012	65.49	0.00	1.29	0.010
620	34.27	19.99	85.96	0.00	1.69	53.	82.17	0.00	0.012	69.28	0.00	1.36	0.010
621	34.27	19.99	8.24	0.00	0.16	5.	7.82	0.00	0.001	6.32	0.00	0.12	0.001
622	34.27	19.99	4.85	0.00	0.10	3.	4.77	0.00	0.001	2.68	0.00	0.05	0.000
623	34.27	19.99	5.82	0.00	0.11	4.	5.71	0.00	0.001	2.25	0.00	0.04	0.000
624	34.27	19.99	9.32	0.00	0.18	6.	8.85	0.00	0.001	5.78	0.00	0.11	0.001

MACROGUSCIO: Pulvino7

GUSCI	ARMATURA INFERIORE ORIZZONTALE												
	COMBINAZIONE RARA				COMB. FREQUENTE				COMB. QUASI PERMANENTE				
Af	Afc	Mom	Nor	σ_c	σ_f	Mom	Nor	wkF	Mom	Nor	σ_c	wkP	
701	20.52	20.52	11.01	0.00	0.26	11.	10.31	0.00	0.004	0.00	0.00	0.00	0.000
702	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
703	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
704	20.52	20.52	10.93	0.00	0.25	11.	10.31	0.00	0.004	0.00	0.00	0.00	0.000
705	20.52	20.52	10.50	0.00	0.24	11.	9.80	0.00	0.004	0.00	0.00	0.00	0.000
706	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
707	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
708	20.52	20.52	10.34	0.00	0.24	11.	9.81	0.00	0.004	0.00	0.00	0.00	0.000
709	20.52	20.52	10.98	0.00	0.13	7.	10.14	0.00	0.003	0.00	0.00	0.00	0.000
710	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
711	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
712	20.52	20.52	10.71	0.00	0.13	7.	10.16	0.00	0.003	0.00	0.00	0.00	0.000
713	20.52	20.52	11.43	0.00	0.14	8.	10.61	0.00	0.003	0.00	0.00	0.00	0.000
714	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
715	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
716	20.52	20.52	11.18	0.00	0.14	7.	10.62	0.00	0.003	0.00	0.00	0.00	0.000
717	20.52	20.52	16.53	0.00	0.38	17.	15.44	0.00	0.006	0.00	0.00	0.00	0.000
718	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
719	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
720	20.52	20.52	16.34	0.00	0.38	17.	15.45	0.00	0.006	0.00	0.00	0.00	0.000
721	20.52	20.52	18.18	0.00	0.42	18.	17.02	0.00	0.007	0.00	0.00	0.00	0.000
722	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
723	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
724	20.52	20.52	18.08	0.00	0.42	18.	17.02	0.00	0.007	0.00	0.00	0.00	0.000

GUSCI	ARMATURA INFERIORE VERTICALE												
	COMBINAZIONE RARA				COMB. FREQUENTE				COMB. QUASI PERMANENTE				
Af	Afc	Mom	Nor	σ_c	σ_f	Mom	Nor	wkF	Mom	Nor	σ_c	wkP	
701	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
702	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
703	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
704	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
705	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
706	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
707	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
708	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
709	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
710	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
711	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
712	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
713	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
714	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
715	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
716	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
717	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
718	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
719	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
720	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
721	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
722	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
723	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
724	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000

GUSCI	ARMATURA SUPERIORE ORIZZONTALE												
	COMBINAZIONE RARA				COMB. FREQUENTE				COMB. QUASI PERMANENTE				
Af	Afc	Mom	Nor	σ_c	σ_f	Mom	Nor	wkF	Mom	Nor	σ_c	wkP	
701	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	8.80	0.00	0.20	0.003
702	20.52	20.52	150.66	0.00	3.49	153.	143.72	0.00	0.069	117.05	0.00	2.71	0.052
703	20.52	20.52	143.45	0.00	3.32	146.	133.22	0.00	0.063	116.98	0.00	2.71	0.052
704	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	8.81	0.00	0.20	0.003
705	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.85	0.00	0.16	0.003
706	20.52	20.52	156.79	0.00	3.63	159.	149.49	0.00	0.073	126.08	0.00	2.92	0.058
707	20.52	20.52	151.56	0.00	3.51	154.	140.76	0.00	0.068	126.01	0.00	2.92	0.058
708	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.85	0.00	0.16	0.003
709	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.92	0.00	0.10	0.002
710	20.52	20.52	159.04	0.00	1.94	105.	151.59	0.00	0.040	126.26	0.00	1.54	0.032

711	20.52	20.52	157.95	0.00	1.92	104.	146.95	0.00	0.038	126.22	0.00	1.54	0.032
712	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.92	0.00	0.10	0.002
713	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.22	0.00	0.06	0.001
714	20.52	20.52	158.20	0.00	1.93	104.	150.72	0.00	0.040	124.51	0.00	1.52	0.032
715	20.52	20.52	157.32	0.00	1.92	104.	146.47	0.00	0.038	124.48	0.00	1.52	0.032
716	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.21	0.00	0.06	0.001
717	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	3.66	0.00	0.08	0.001
718	20.52	20.52	140.57	0.00	3.26	143.	133.71	0.00	0.063	114.85	0.00	2.66	0.051
719	20.52	20.52	144.32	0.00	3.34	147.	134.78	0.00	0.064	114.78	0.00	2.66	0.051
720	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	3.66	0.00	0.08	0.001
721	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.93	0.00	0.16	0.003
722	20.52	20.52	131.20	0.00	3.04	133.	124.72	0.00	0.057	110.46	0.00	2.56	0.048
723	20.52	20.52	134.81	0.00	3.12	137.	126.03	0.00	0.058	110.39	0.00	2.56	0.048
724	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.93	0.00	0.16	0.003

ARMATURA SUPERIORE VERTICALE

GUSCI	COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE					
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	wkF	Mom	Nor	σc	wkP
701	34.27	19.99	7.96	0.00	0.16	5.	7.79	0.00	0.001	6.30	0.00	0.12	0.001
702	34.27	19.99	5.25	0.00	0.10	3.	4.78	0.00	0.001	2.67	0.00	0.05	0.000
703	34.27	19.99	6.19	0.00	0.12	4.	5.71	0.00	0.001	2.26	0.00	0.04	0.000
704	34.27	19.99	9.65	0.00	0.19	6.	8.84	0.00	0.001	5.78	0.00	0.11	0.001
705	34.27	19.99	95.48	0.00	1.88	59.	89.25	0.00	0.013	75.52	0.00	1.48	0.011
706	34.27	19.99	89.22	0.00	1.75	55.	82.94	0.00	0.012	67.35	0.00	1.32	0.010
707	34.27	19.99	93.05	0.00	1.83	58.	86.55	0.00	0.013	65.44	0.00	1.29	0.010
708	34.27	19.99	92.50	0.00	1.82	57.	85.72	0.00	0.013	69.25	0.00	1.36	0.010
709	34.27	19.99	493.07	0.00	5.04	198.	465.94	0.00	0.066	373.40	0.00	3.82	0.051
710	34.27	19.99	493.25	0.00	5.04	198.	466.10	0.00	0.066	373.47	0.00	3.82	0.051
711	34.27	19.99	493.25	0.00	5.04	198.	466.10	0.00	0.066	373.47	0.00	3.82	0.051
712	34.27	19.99	493.64	0.00	5.04	199.	466.47	0.00	0.066	373.58	0.00	3.82	0.051
713	34.27	19.99	496.85	0.00	5.08	200.	466.70	0.00	0.067	373.40	0.00	3.82	0.051
714	34.27	19.99	497.07	0.00	5.08	200.	466.90	0.00	0.067	373.47	0.00	3.82	0.051
715	34.27	19.99	497.07	0.00	5.08	200.	466.90	0.00	0.067	373.47	0.00	3.82	0.051
716	34.27	19.99	497.48	0.00	5.08	200.	467.27	0.00	0.067	373.58	0.00	3.82	0.051
717	34.27	19.99	84.08	0.00	1.65	52.	79.89	0.00	0.012	75.52	0.00	1.48	0.011
718	34.27	19.99	79.84	0.00	1.57	50.	75.75	0.00	0.011	67.35	0.00	1.32	0.010
719	34.27	19.99	85.74	0.00	1.68	53.	81.06	0.00	0.012	65.44	0.00	1.29	0.010
720	34.27	19.99	87.01	0.00	1.71	54.	82.15	0.00	0.012	69.25	0.00	1.36	0.010
721	34.27	19.99	7.94	0.00	0.16	5.	7.78	0.00	0.001	6.30	0.00	0.12	0.001
722	34.27	19.99	5.25	0.00	0.10	3.	4.78	0.00	0.001	2.67	0.00	0.05	0.000
723	34.27	19.99	6.19	0.00	0.12	4.	5.72	0.00	0.001	2.26	0.00	0.04	0.000
724	34.27	19.99	9.64	0.00	0.19	6.	8.84	0.00	0.001	5.78	0.00	0.11	0.001

MACROGUSCIO: Pulvino8

ARMATURA INFERIORE ORIZZONTALE

GUSCI	COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE					
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	wkF	Mom	Nor	σc	wkP
801	20.52	20.52	11.04	0.00	0.26	11.	10.31	0.00	0.004	0.00	0.00	0.00	0.000
802	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
803	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
804	20.52	20.52	11.05	0.00	0.26	11.	10.32	0.00	0.004	0.00	0.00	0.00	0.000
805	20.52	20.52	10.48	0.00	0.24	11.	9.80	0.00	0.004	0.00	0.00	0.00	0.000
806	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
807	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
808	20.52	20.52	10.50	0.00	0.24	11.	9.81	0.00	0.004	0.00	0.00	0.00	0.000
809	20.52	20.52	10.91	0.00	0.13	7.	10.14	0.00	0.003	0.00	0.00	0.00	0.000
810	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
811	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
812	20.52	20.52	10.94	0.00	0.13	7.	10.17	0.00	0.003	0.00	0.00	0.00	0.000
813	20.52	20.52	11.37	0.00	0.14	7.	10.61	0.00	0.003	0.00	0.00	0.00	0.000
814	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
815	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
816	20.52	20.52	11.39	0.00	0.14	8.	10.63	0.00	0.003	0.00	0.00	0.00	0.000
817	20.52	20.52	16.53	0.00	0.38	17.	15.44	0.00	0.006	0.00	0.00	0.00	0.000
818	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
819	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
820	20.52	20.52	16.55	0.00	0.38	17.	15.45	0.00	0.006	0.00	0.00	0.00	0.000
821	20.52	20.52	18.24	0.00	0.42	19.	17.02	0.00	0.007	0.00	0.00	0.00	0.000
822	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
823	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
824	20.52	20.52	18.24	0.00	0.42	19.	17.02	0.00	0.007	0.00	0.00	0.00	0.000

ARMATURA INFERIORE VERTICALE

GUSCI	COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE					
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	wkF	Mom	Nor	σc	wkP
801	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
802	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
803	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
804	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
805	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
806	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
807	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
808	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
809	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
810	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
811	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
812	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
813	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
814	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
815	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
816	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
817	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
818	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
819	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
820	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
821	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000

822	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
823	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
824	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000

ARMATURA SUPERIORE ORIZZONTALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE						
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	wkF	Mom	Nor	σc	wkP
801	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	8.80	0.00	0.20	0.003
802	20.52	20.52	153.48	0.00	3.55	156.	143.70	0.00	0.069	117.03	0.00	2.71	0.052
803	20.52	20.52	142.53	0.00	3.30	145.	133.17	0.00	0.063	116.92	0.00	2.71	0.052
804	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	8.81	0.00	0.20	0.003
805	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.85	0.00	0.16	0.003
806	20.52	20.52	159.69	0.00	3.70	162.	149.47	0.00	0.073	126.06	0.00	2.92	0.058
807	20.52	20.52	150.59	0.00	3.49	153.	140.72	0.00	0.067	125.95	0.00	2.92	0.058
808	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.85	0.00	0.16	0.003
809	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.92	0.00	0.10	0.002
810	20.52	20.52	161.87	0.00	1.97	107.	151.57	0.00	0.040	126.24	0.00	1.54	0.032
811	20.52	20.52	157.03	0.00	1.91	104.	146.91	0.00	0.038	126.17	0.00	1.54	0.032
812	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.92	0.00	0.10	0.002
813	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.22	0.00	0.06	0.001
814	20.52	20.52	160.93	0.00	1.96	106.	150.69	0.00	0.040	124.48	0.00	1.52	0.032
815	20.52	20.52	156.50	0.00	1.91	103.	146.43	0.00	0.038	124.44	0.00	1.52	0.032
816	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.22	0.00	0.06	0.001
817	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	3.66	0.00	0.08	0.001
818	20.52	20.52	142.71	0.00	3.30	145.	133.68	0.00	0.063	114.83	0.00	2.66	0.051
819	20.52	20.52	143.82	0.00	3.33	146.	134.75	0.00	0.064	114.72	0.00	2.66	0.051
820	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	3.65	0.00	0.08	0.001
821	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.93	0.00	0.16	0.003
822	20.52	20.52	133.09	0.00	3.08	135.	124.69	0.00	0.057	110.44	0.00	2.56	0.048
823	20.52	20.52	134.45	0.00	3.11	137.	125.99	0.00	0.058	110.32	0.00	2.55	0.048
824	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.93	0.00	0.16	0.003

ARMATURA SUPERIORE VERTICALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE						
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	wkF	Mom	Nor	σc	wkP
801	34.27	19.99	8.31	0.00	0.16	5.	7.81	0.00	0.001	6.31	0.00	0.12	0.001
802	34.27	19.99	4.88	0.00	0.10	3.	4.77	0.00	0.001	2.68	0.00	0.05	0.000
803	34.27	19.99	5.87	0.00	0.12	4.	5.71	0.00	0.001	2.25	0.00	0.04	0.000
804	34.27	19.99	9.40	0.00	0.18	6.	8.84	0.00	0.001	5.78	0.00	0.11	0.001
805	34.27	19.99	96.66	0.00	1.90	60.	89.32	0.00	0.013	75.60	0.00	1.49	0.011
806	34.27	19.99	90.29	0.00	1.77	56.	83.00	0.00	0.012	67.41	0.00	1.32	0.010
807	34.27	19.99	94.11	0.00	1.85	58.	86.60	0.00	0.013	65.50	0.00	1.29	0.010
808	34.27	19.99	93.55	0.00	1.84	58.	85.76	0.00	0.013	69.25	0.00	1.36	0.010
809	34.27	19.99	496.76	0.00	5.08	200.	465.99	0.00	0.066	373.45	0.00	3.82	0.051
810	34.27	19.99	496.93	0.00	5.08	200.	466.16	0.00	0.066	373.52	0.00	3.82	0.051
811	34.27	19.99	496.93	0.00	5.08	200.	466.16	0.00	0.066	373.52	0.00	3.82	0.051
812	34.27	19.99	497.33	0.00	5.08	200.	466.53	0.00	0.067	373.63	0.00	3.82	0.051
813	34.27	19.99	500.71	0.00	5.12	201.	466.76	0.00	0.067	373.45	0.00	3.82	0.051
814	34.27	19.99	500.93	0.00	5.12	201.	466.96	0.00	0.067	373.52	0.00	3.82	0.051
815	34.27	19.99	500.93	0.00	5.12	201.	466.96	0.00	0.067	373.52	0.00	3.82	0.051
816	34.27	19.99	501.33	0.00	5.12	202.	467.33	0.00	0.067	373.63	0.00	3.82	0.051
817	34.27	19.99	85.13	0.00	1.67	53.	79.95	0.00	0.012	75.60	0.00	1.49	0.011
818	34.27	19.99	80.02	0.00	1.57	50.	75.82	0.00	0.011	67.41	0.00	1.32	0.010
819	34.27	19.99	85.79	0.00	1.69	53.	81.10	0.00	0.012	65.50	0.00	1.29	0.010
820	34.27	19.99	87.00	0.00	1.71	54.	82.20	0.00	0.012	69.25	0.00	1.36	0.010
821	34.27	19.99	8.30	0.00	0.16	5.	7.80	0.00	0.001	6.31	0.00	0.12	0.001
822	34.27	19.99	4.86	0.00	0.10	3.	4.76	0.00	0.001	2.68	0.00	0.05	0.000
823	34.27	19.99	5.86	0.00	0.12	4.	5.70	0.00	0.001	2.25	0.00	0.04	0.000
824	34.27	19.99	9.37	0.00	0.18	6.	8.83	0.00	0.001	5.78	0.00	0.11	0.001

MACROGUSCIO: Pulvino9

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE						
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	wkF	Mom	Nor	σc	wkP
901	20.52	20.52	10.93	0.00	0.25	11.	10.31	0.00	0.004	0.00	0.00	0.00	0.000
902	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
903	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
904	20.52	20.52	11.04	0.00	0.26	11.	10.32	0.00	0.004	0.00	0.00	0.00	0.000
905	20.52	20.52	10.34	0.00	0.24	11.	9.81	0.00	0.004	0.00	0.00	0.00	0.000
906	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
907	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
908	20.52	20.52	10.53	0.00	0.24	11.	9.82	0.00	0.004	0.00	0.00	0.00	0.000
909	20.52	20.52	10.71	0.00	0.13	7.	10.16	0.00	0.003	0.00	0.00	0.00	0.000
910	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
911	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
912	20.52	20.52	11.02	0.00	0.13	7.	10.18	0.00	0.003	0.00	0.00	0.00	0.000
913	20.52	20.52	11.17	0.00	0.14	7.	10.62	0.00	0.003	0.00	0.00	0.00	0.000
914	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
915	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
916	20.52	20.52	11.47	0.00	0.14	8.	10.64	0.00	0.003	0.00	0.00	0.00	0.000
917	20.52	20.52	16.34	0.00	0.38	17.	15.45	0.00	0.006	0.00	0.00	0.00	0.000
918	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
919	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
920	20.52	20.52	16.55	0.00	0.38	17.	15.45	0.00	0.006	0.00	0.00	0.00	0.000
921	20.52	20.52	18.08	0.00	0.42	18.	17.02	0.00	0.007	0.00	0.00	0.00	0.000
922	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
923	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
924	20.52	20.52	18.19	0.00	0.42	18.	17.02	0.00	0.007	0.00	0.00	0.00	0.000

ARMATURA INFERIORE VERTICALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE						
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	wkF	Mom	Nor	σc	wkP
901	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
902	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
903	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
904	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
905	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000

906	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
907	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
908	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
909	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
910	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
911	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
912	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
913	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
914	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
915	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
916	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
917	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
918	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
919	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
920	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
921	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
922	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
923	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
924	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000

ARMATURA SUPERIORE ORIZZONTALE

GUSCI	COMBINAZIONE RARA						COMB. FREQUENTE			COMB. QUASI PERMANENTE			
	Af	Afc	Mom	Nor	σ_c	σ_f	Mom	Nor	wkF	Mom	Nor	σ_c	wkP
901	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	8.80	0.00	0.20	0.003
902	20.52	20.52	154.06	0.00	3.57	157.	143.66	0.00	0.069	116.95	0.00	2.71	0.052
903	20.52	20.52	139.93	0.00	3.24	142.	133.14	0.00	0.063	116.87	0.00	2.71	0.052
904	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	8.81	0.00	0.20	0.003
905	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.85	0.00	0.16	0.003
906	20.52	20.52	160.36	0.00	3.71	163.	149.42	0.00	0.073	125.98	0.00	2.92	0.058
907	20.52	20.52	147.84	0.00	3.42	150.	140.68	0.00	0.067	125.90	0.00	2.92	0.058
908	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.85	0.00	0.16	0.003
909	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.92	0.00	0.10	0.002
910	20.52	20.52	162.60	0.00	1.98	107.	151.53	0.00	0.040	126.18	0.00	1.54	0.032
911	20.52	20.52	154.24	0.00	1.88	102.	146.88	0.00	0.038	126.12	0.00	1.54	0.032
912	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.91	0.00	0.10	0.002
913	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.22	0.00	0.06	0.001
914	20.52	20.52	161.58	0.00	1.97	107.	150.67	0.00	0.040	124.43	0.00	1.52	0.032
915	20.52	20.52	153.80	0.00	1.87	101.	146.40	0.00	0.038	124.39	0.00	1.51	0.032
916	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.22	0.00	0.06	0.001
917	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	3.65	0.00	0.08	0.001
918	20.52	20.52	143.19	0.00	3.32	145.	133.66	0.00	0.063	114.76	0.00	2.66	0.051
919	20.52	20.52	141.58	0.00	3.28	144.	134.72	0.00	0.064	114.67	0.00	2.66	0.051
920	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	3.65	0.00	0.08	0.001
921	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.93	0.00	0.16	0.003
922	20.52	20.52	133.43	0.00	3.09	136.	124.67	0.00	0.057	110.36	0.00	2.56	0.048
923	20.52	20.52	132.44	0.00	3.07	135.	125.96	0.00	0.058	110.27	0.00	2.55	0.048
924	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.93	0.00	0.16	0.003

ARMATURA SUPERIORE VERTICALE

GUSCI	COMBINAZIONE RARA						COMB. FREQUENTE			COMB. QUASI PERMANENTE			
	Af	Afc	Mom	Nor	σ_c	σ_f	Mom	Nor	wkF	Mom	Nor	σ_c	wkP
901	34.27	19.99	8.50	0.00	0.17	5.	7.77	0.00	0.001	6.29	0.00	0.12	0.001
902	34.27	19.99	4.49	0.00	0.09	3.	4.77	0.00	0.001	2.66	0.00	0.05	0.000
903	34.27	19.99	5.51	0.00	0.11	3.	5.71	0.00	0.001	2.26	0.00	0.04	0.000
904	34.27	19.99	9.07	0.00	0.18	6.	8.83	0.00	0.001	5.77	0.00	0.11	0.001
905	34.27	19.99	96.42	0.00	1.89	60.	89.25	0.00	0.013	75.51	0.00	1.48	0.011
906	34.27	19.99	90.09	0.00	1.77	56.	82.96	0.00	0.012	67.35	0.00	1.32	0.010
907	34.27	19.99	93.86	0.00	1.84	58.	86.57	0.00	0.013	65.44	0.00	1.29	0.010
908	34.27	19.99	93.29	0.00	1.83	58.	85.74	0.00	0.013	69.22	0.00	1.36	0.010
909	34.27	19.99	494.14	0.00	5.05	199.	465.94	0.00	0.066	373.40	0.00	3.82	0.051
910	34.27	19.99	494.30	0.00	5.05	199.	466.11	0.00	0.066	373.47	0.00	3.82	0.051
911	34.27	19.99	494.30	0.00	5.05	199.	466.11	0.00	0.066	373.47	0.00	3.82	0.051
912	34.27	19.99	494.69	0.00	5.06	199.	466.48	0.00	0.066	373.58	0.00	3.82	0.051
913	34.27	19.99	498.23	0.00	5.09	200.	466.71	0.00	0.067	373.40	0.00	3.82	0.051
914	34.27	19.99	498.44	0.00	5.09	200.	466.91	0.00	0.067	373.47	0.00	3.82	0.051
915	34.27	19.99	498.44	0.00	5.09	200.	466.91	0.00	0.067	373.47	0.00	3.82	0.051
916	34.27	19.99	498.84	0.00	5.10	201.	467.28	0.00	0.067	373.58	0.00	3.82	0.051
917	34.27	19.99	84.88	0.00	1.67	53.	88.72	0.00	0.013	75.51	0.00	1.48	0.011
918	34.27	19.99	80.12	0.00	1.57	50.	82.26	0.00	0.012	67.35	0.00	1.32	0.010
919	34.27	19.99	85.02	0.00	1.67	53.	85.89	0.00	0.013	65.44	0.00	1.29	0.010
920	34.27	19.99	86.25	0.00	1.69	54.	84.93	0.00	0.013	69.22	0.00	1.36	0.010
921	34.27	19.99	8.48	0.00	0.17	5.	7.77	0.00	0.001	6.29	0.00	0.12	0.001
922	34.27	19.99	4.48	0.00	0.09	3.	4.77	0.00	0.001	2.66	0.00	0.05	0.000
923	34.27	19.99	5.50	0.00	0.11	3.	5.71	0.00	0.001	2.26	0.00	0.04	0.000
924	34.27	19.99	9.04	0.00	0.18	6.	8.82	0.00	0.001	5.77	0.00	0.11	0.001

MACROGUSCIO: Pulvino10

GUSCI	COMBINAZIONE RARA						COMB. FREQUENTE			COMB. QUASI PERMANENTE			
	Af	Afc	Mom	Nor	σ_c	σ_f	Mom	Nor	wkF	Mom	Nor	σ_c	wkP
1001	20.52	20.52	10.91	0.00	0.25	11.	10.32	0.00	0.004	0.00	0.00	0.00	0.000
1002	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1003	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1004	20.52	20.52	10.92	0.00	0.25	11.	10.33	0.00	0.004	0.00	0.00	0.00	0.000
1005	20.52	20.52	10.37	0.00	0.24	11.	9.81	0.00	0.004	0.00	0.00	0.00	0.000
1006	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1007	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1008	20.52	20.52	10.38	0.00	0.24	11.	9.83	0.00	0.004	0.00	0.00	0.00	0.000
1009	20.52	20.52	10.79	0.00	0.13	7.	10.16	0.00	0.003	0.00	0.00	0.00	0.000
1010	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1011	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1012	20.52	20.52	10.82	0.00	0.13	7.	10.19	0.00	0.003	0.00	0.00	0.00	0.000
1013	20.52	20.52	11.24	0.00	0.14	7.	10.62	0.00	0.003	0.00	0.00	0.00	0.000
1014	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1015	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1016	20.52	20.52	11.27	0.00	0.14	7.	10.65	0.00	0.003	0.00	0.00	0.00	0.000

1017	20.52	20.52	16.34	0.00	0.38	17.	15.45	0.00	0.006	0.00	0.00	0.00	0.000
1018	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1019	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1020	20.52	20.52	16.35	0.00	0.38	17.	15.45	0.00	0.006	0.00	0.00	0.00	0.000
1021	20.52	20.52	18.02	0.00	0.42	18.	17.02	0.00	0.007	0.00	0.00	0.00	0.000
1022	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1023	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1024	20.52	20.52	18.02	0.00	0.42	18.	17.02	0.00	0.007	0.00	0.00	0.00	0.000

ARMATURA INFERIORE VERTICALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE						
	Af	Afc	Mom	Nor	σ_c	σ_f	Mom	Nor	wkF	Mom	Nor	σ_c	wkP
1001	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1002	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1003	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1004	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1005	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1006	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1007	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1008	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1009	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1010	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1011	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1012	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1013	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1014	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1015	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1016	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1017	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1018	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1019	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1020	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1021	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1022	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1023	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1024	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000

ARMATURA SUPERIORE ORIZZONTALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE						
	Af	Afc	Mom	Nor	σ_c	σ_f	Mom	Nor	wkF	Mom	Nor	σ_c	wkP
1001	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	8.80	0.00	0.20	0.003
1002	20.52	20.52	151.93	0.00	3.52	154.	143.69	0.00	0.069	116.92	0.00	2.71	0.052
1003	20.52	20.52	140.40	0.00	3.25	143.	133.01	0.00	0.062	116.79	0.00	2.70	0.052
1004	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	8.81	0.00	0.20	0.003
1005	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.84	0.00	0.16	0.003
1006	20.52	20.52	158.01	0.00	3.66	161.	149.45	0.00	0.073	125.96	0.00	2.92	0.058
1007	20.52	20.52	148.43	0.00	3.44	151.	140.57	0.00	0.067	125.82	0.00	2.91	0.058
1008	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.85	0.00	0.16	0.003
1009	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.92	0.00	0.10	0.002
1010	20.52	20.52	160.04	0.00	1.95	106.	151.53	0.00	0.040	126.15	0.00	1.54	0.032
1011	20.52	20.52	154.94	0.00	1.89	102.	146.80	0.00	0.038	126.06	0.00	1.54	0.032
1012	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.91	0.00	0.10	0.002
1013	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.22	0.00	0.06	0.001
1014	20.52	20.52	159.10	0.00	1.94	105.	150.65	0.00	0.040	124.39	0.00	1.51	0.032
1015	20.52	20.52	154.43	0.00	1.88	102.	146.32	0.00	0.038	124.33	0.00	1.51	0.031
1016	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.22	0.00	0.06	0.001
1017	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	3.65	0.00	0.08	0.001
1018	20.52	20.52	140.93	0.00	3.26	143.	133.61	0.00	0.063	114.73	0.00	2.66	0.051
1019	20.52	20.52	142.10	0.00	3.29	144.	134.68	0.00	0.064	114.59	0.00	2.65	0.051
1020	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	3.64	0.00	0.08	0.001
1021	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.92	0.00	0.16	0.003
1022	20.52	20.52	131.41	0.00	3.04	134.	124.62	0.00	0.057	110.33	0.00	2.55	0.048
1023	20.52	20.52	132.84	0.00	3.08	135.	125.93	0.00	0.058	110.19	0.00	2.55	0.048
1024	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.92	0.00	0.16	0.003

ARMATURA SUPERIORE VERTICALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE						
	Af	Afc	Mom	Nor	σ_c	σ_f	Mom	Nor	wkF	Mom	Nor	σ_c	wkP
1001	34.27	19.99	8.20	0.00	0.16	5.	7.79	0.00	0.001	6.29	0.00	0.12	0.001
1002	34.27	19.99	4.83	0.00	0.09	3.	4.76	0.00	0.001	2.67	0.00	0.05	0.000
1003	34.27	19.99	5.81	0.00	0.11	4.	5.70	0.00	0.001	2.25	0.00	0.04	0.000
1004	34.27	19.99	9.29	0.00	0.18	6.	8.82	0.00	0.001	5.77	0.00	0.11	0.001
1005	34.27	19.99	95.79	0.00	1.88	59.	89.38	0.00	0.013	75.58	0.00	1.48	0.011
1006	34.27	19.99	89.44	0.00	1.76	56.	83.06	0.00	0.012	67.42	0.00	1.32	0.010
1007	34.27	19.99	93.20	0.00	1.83	58.	86.66	0.00	0.013	65.51	0.00	1.29	0.010
1008	34.27	19.99	92.60	0.00	1.82	57.	85.81	0.00	0.013	69.21	0.00	1.36	0.010
1009	34.27	19.99	490.63	0.00	5.01	197.	465.97	0.00	0.066	373.44	0.00	3.82	0.051
1010	34.27	19.99	490.80	0.00	5.02	197.	466.14	0.00	0.066	373.52	0.00	3.82	0.051
1011	34.27	19.99	490.80	0.00	5.02	197.	466.14	0.00	0.066	373.52	0.00	3.82	0.051
1012	34.27	19.99	491.19	0.00	5.02	198.	466.51	0.00	0.067	373.63	0.00	3.82	0.051
1013	34.27	19.99	494.97	0.00	5.06	199.	466.82	0.00	0.067	373.44	0.00	3.82	0.051
1014	34.27	19.99	495.18	0.00	5.06	199.	467.02	0.00	0.067	373.52	0.00	3.82	0.051
1015	34.27	19.99	495.18	0.00	5.06	199.	467.02	0.00	0.067	373.52	0.00	3.82	0.051
1016	34.27	19.99	495.58	0.00	5.06	199.	467.39	0.00	0.067	373.63	0.00	3.82	0.051
1017	34.27	19.99	83.97	0.00	1.65	52.	88.76	0.00	0.013	75.58	0.00	1.48	0.011
1018	34.27	19.99	79.28	0.00	1.56	49.	82.32	0.00	0.012	67.42	0.00	1.32	0.010
1019	34.27	19.99	84.99	0.00	1.67	53.	85.94	0.00	0.013	65.51	0.00	1.29	0.010
1020	34.27	19.99	86.15	0.00	1.69	53.	84.98	0.00	0.013	69.21	0.00	1.36	0.010
1021	34.27	19.99	8.18	0.00	0.16	5.	7.78	0.00	0.001	6.29	0.00	0.12	0.001
1022	34.27	19.99	4.83	0.00	0.09	3.	4.76	0.00	0.001	2.67	0.00	0.05	0.000
1023	34.27	19.99	5.81	0.00	0.11	4.	5.70	0.00	0.001	2.25	0.00	0.04	0.000
1024	34.27	19.99	9.28	0.00	0.18	6.	8.82	0.00	0.001	5.77	0.00	0.11	0.001

MACROGUSCIO: Pulvino11

ARMATURA INFERIORE ORIZZONTALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE					
	Af	Afc	Mom	Nor	σ_c	σ_f	Mom	Nor	wkF	Mom	Nor	σ_c

1101	20.52	20.52	10.92	0.00	0.25	11.	10.32	0.00	0.004	0.00	0.00	0.00	0.000
1102	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1103	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1104	20.52	20.52	10.93	0.00	0.25	11.	10.34	0.00	0.004	0.00	0.00	0.00	0.000
1105	20.52	20.52	10.37	0.00	0.24	11.	9.82	0.00	0.004	0.00	0.00	0.00	0.000
1106	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1107	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1108	20.52	20.52	10.39	0.00	0.24	11.	9.84	0.00	0.004	0.00	0.00	0.00	0.000
1109	20.52	20.52	10.80	0.00	0.13	7.	10.18	0.00	0.003	0.00	0.00	0.00	0.000
1110	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1111	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1112	20.52	20.52	10.83	0.00	0.13	7.	10.20	0.00	0.003	0.00	0.00	0.00	0.000
1113	20.52	20.52	11.25	0.00	0.14	7.	10.64	0.00	0.003	0.00	0.00	0.00	0.000
1114	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1115	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1116	20.52	20.52	11.28	0.00	0.14	7.	10.66	0.00	0.003	0.00	0.00	0.00	0.000
1117	20.52	20.52	16.33	0.00	0.38	17.	15.45	0.00	0.006	0.00	0.00	0.00	0.000
1118	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1119	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1120	20.52	20.52	16.34	0.00	0.38	17.	15.45	0.00	0.006	0.00	0.00	0.00	0.000
1121	20.52	20.52	18.00	0.00	0.42	18.	17.02	0.00	0.007	0.00	0.00	0.00	0.000
1122	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1123	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1124	20.52	20.52	18.00	0.00	0.42	18.	17.02	0.00	0.007	0.00	0.00	0.00	0.000

ARMATURA INFERIORE VERTICALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE						
	Af	Afc	Mom	Nor	σ_c	σ_f	Mom	Nor	wkF	Mom	Nor	σ_c	wkP
1101	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1102	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1103	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1104	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1105	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1106	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1107	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1108	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1109	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1110	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1111	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1112	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1113	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1114	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1115	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1116	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1117	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1118	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1119	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1120	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1121	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1122	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1123	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1124	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000

ARMATURA SUPERIORE ORIZZONTALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE						
	Af	Afc	Mom	Nor	σ_c	σ_f	Mom	Nor	wkF	Mom	Nor	σ_c	wkP
1101	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	8.80	0.00	0.20	0.003
1102	20.52	20.52	151.49	0.00	3.51	154.	143.56	0.00	0.069	116.82	0.00	2.71	0.052
1103	20.52	20.52	140.65	0.00	3.26	143.	132.99	0.00	0.062	116.67	0.00	2.70	0.052
1104	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	8.81	0.00	0.20	0.003
1105	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.84	0.00	0.16	0.003
1106	20.52	20.52	157.66	0.00	3.65	160.	149.33	0.00	0.073	125.87	0.00	2.91	0.058
1107	20.52	20.52	148.62	0.00	3.44	151.	140.53	0.00	0.067	125.72	0.00	2.91	0.058
1108	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.84	0.00	0.16	0.003
1109	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.91	0.00	0.10	0.002
1110	20.52	20.52	159.84	0.00	1.95	105.	151.46	0.00	0.040	126.07	0.00	1.54	0.032
1111	20.52	20.52	154.99	0.00	1.89	102.	146.74	0.00	0.038	125.96	0.00	1.53	0.032
1112	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.91	0.00	0.10	0.002
1113	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.22	0.00	0.06	0.001
1114	20.52	20.52	158.92	0.00	1.94	105.	150.59	0.00	0.040	124.33	0.00	1.51	0.031
1115	20.52	20.52	154.47	0.00	1.88	102.	146.26	0.00	0.038	124.23	0.00	1.51	0.031
1116	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.22	0.00	0.06	0.001
1117	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	3.64	0.00	0.08	0.001
1118	20.52	20.52	140.94	0.00	3.26	143.	133.60	0.00	0.063	114.64	0.00	2.65	0.051
1119	20.52	20.52	141.95	0.00	3.29	144.	134.59	0.00	0.064	114.48	0.00	2.65	0.050
1120	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	3.63	0.00	0.08	0.001
1121	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.92	0.00	0.16	0.003
1122	20.52	20.52	131.43	0.00	3.04	134.	124.60	0.00	0.057	110.23	0.00	2.55	0.048
1123	20.52	20.52	132.69	0.00	3.07	135.	125.84	0.00	0.058	110.08	0.00	2.55	0.048
1124	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.92	0.00	0.16	0.003

ARMATURA SUPERIORE VERTICALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE						
	Af	Afc	Mom	Nor	σ_c	σ_f	Mom	Nor	wkF	Mom	Nor	σ_c	wkP
1101	34.27	19.99	8.16	0.00	0.16	5.	7.75	0.00	0.001	6.27	0.00	0.12	0.001
1102	34.27	19.99	4.83	0.00	0.09	3.	4.76	0.00	0.001	2.65	0.00	0.05	0.000
1103	34.27	19.99	5.80	0.00	0.11	4.	5.70	0.00	0.001	2.26	0.00	0.04	0.000
1104	34.27	19.99	9.29	0.00	0.18	6.	8.81	0.00	0.001	5.77	0.00	0.11	0.001
1105	34.27	19.99	95.49	0.00	1.88	59.	89.27	0.00	0.013	75.49	0.00	1.48	0.011
1106	34.27	19.99	89.29	0.00	1.75	55.	83.01	0.00	0.012	67.36	0.00	1.32	0.010
1107	34.27	19.99	93.06	0.00	1.83	58.	86.61	0.00	0.013	65.46	0.00	1.29	0.010
1108	34.27	19.99	92.59	0.00	1.82	57.	85.81	0.00	0.013	69.16	0.00	1.36	0.010
1109	34.27	19.99	490.60	0.00	5.01	197.	465.93	0.00	0.066	373.39	0.00	3.82	0.051
1110	34.27	19.99	490.77	0.00	5.02	197.	466.09	0.00	0.066	373.47	0.00	3.82	0.051
1111	34.27	19.99	490.77	0.00	5.02	197.	466.09	0.00	0.066	373.47	0.00	3.82	0.051
1112	34.27	19.99	491.16	0.00	5.02	198.	466.47	0.00	0.066	373.57	0.00	3.82	0.051
1113	34.27	19.99	494.76	0.00	5.06	199.	466.74	0.00	0.067	373.39	0.00	3.82	0.051
1114	34.27	19.99	494.97	0.00	5.06	199.	466.94	0.00	0.06				

1116	34.27	19.99	495.37	0.00	5.06	199.	467.31	0.00	0.067	373.57	0.00	3.82	0.051
1117	34.27	19.99	84.05	0.00	1.65	52.	88.72	0.00	0.013	75.49	0.00	1.48	0.011
1118	34.27	19.99	78.99	0.00	1.55	49.	82.22	0.00	0.012	67.36	0.00	1.32	0.010
1119	34.27	19.99	84.69	0.00	1.66	53.	85.85	0.00	0.013	65.46	0.00	1.29	0.010
1120	34.27	19.99	85.90	0.00	1.69	53.	84.87	0.00	0.013	69.16	0.00	1.36	0.010
1121	34.27	19.99	8.16	0.00	0.16	5.	7.74	0.00	0.001	6.27	0.00	0.12	0.001
1122	34.27	19.99	4.83	0.00	0.09	3.	4.76	0.00	0.001	2.65	0.00	0.05	0.000
1123	34.27	19.99	5.81	0.00	0.11	4.	5.70	0.00	0.001	2.26	0.00	0.04	0.000
1124	34.27	19.99	9.28	0.00	0.18	6.	8.81	0.00	0.001	5.77	0.00	0.11	0.001

MACROGUSCIO: Pulvino12

GUSCI	ARMATURA INFERIORE ORIZZONTALE						COMB. QUASI PERMANENTE						
	COMBINAZIONE RARA		COMB. FREQUENTE				Mom	Nor	σC	wkP			
	Af	Afc	Mom	Nor	σC	σf	Mom	Nor	wkF	Mom	Nor	σC	wkP
1201	20.52	20.52	10.93	0.00	0.25	11.	10.33	0.00	0.004	0.00	0.00	0.00	0.000
1202	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1203	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1204	20.52	20.52	10.95	0.00	0.25	11.	10.35	0.00	0.004	0.00	0.00	0.00	0.000
1205	20.52	20.52	10.39	0.00	0.24	11.	9.83	0.00	0.004	0.00	0.00	0.00	0.000
1206	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1207	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1208	20.52	20.52	10.41	0.00	0.24	11.	9.85	0.00	0.004	0.00	0.00	0.00	0.000
1209	20.52	20.52	10.82	0.00	0.13	7.	10.19	0.00	0.003	0.00	0.00	0.00	0.000
1210	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1211	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1212	20.52	20.52	10.86	0.00	0.13	7.	10.22	0.00	0.003	0.00	0.00	0.00	0.000
1213	20.52	20.52	11.27	0.00	0.14	7.	10.65	0.00	0.003	0.00	0.00	0.00	0.000
1214	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1215	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1216	20.52	20.52	11.30	0.00	0.14	7.	10.68	0.00	0.003	0.00	0.00	0.00	0.000
1217	20.52	20.52	16.35	0.00	0.38	17.	15.45	0.00	0.006	0.00	0.00	0.00	0.000
1218	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1219	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1220	20.52	20.52	16.37	0.00	0.38	17.	15.46	0.00	0.006	0.00	0.00	0.00	0.000
1221	20.52	20.52	18.02	0.00	0.42	18.	17.02	0.00	0.007	0.00	0.00	0.00	0.000
1222	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1223	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1224	20.52	20.52	18.03	0.00	0.42	18.	17.02	0.00	0.007	0.00	0.00	0.00	0.000

GUSCI	ARMATURA INFERIORE VERTICALE						COMB. QUASI PERMANENTE						
	COMBINAZIONE RARA		COMB. FREQUENTE				Mom	Nor	σC	wkP			
	Af	Afc	Mom	Nor	σC	σf	Mom	Nor	wkF	Mom	Nor	σC	wkP
1201	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1202	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1203	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1204	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1205	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1206	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1207	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1208	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1209	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1210	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1211	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1212	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1213	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1214	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1215	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1216	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1217	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1218	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1219	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1220	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1221	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1222	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1223	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1224	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000

GUSCI	ARMATURA SUPERIORE ORIZZONTALE						COMB. QUASI PERMANENTE						
	COMBINAZIONE RARA		COMB. FREQUENTE				Mom	Nor	σC	wkP			
	Af	Afc	Mom	Nor	σC	σf	Mom	Nor	wkF	Mom	Nor	σC	wkP
1201	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	8.80	0.00	0.20	0.003
1202	20.52	20.52	151.47	0.00	3.51	154.	143.50	0.00	0.069	116.73	0.00	2.70	0.052
1203	20.52	20.52	140.57	0.00	3.26	143.	132.92	0.00	0.062	116.57	0.00	2.70	0.052
1204	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	8.81	0.00	0.20	0.003
1205	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.84	0.00	0.16	0.003
1206	20.52	20.52	157.61	0.00	3.65	160.	149.27	0.00	0.073	125.78	0.00	2.91	0.058
1207	20.52	20.52	148.53	0.00	3.44	151.	140.47	0.00	0.067	125.62	0.00	2.91	0.058
1208	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.84	0.00	0.16	0.003
1209	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.91	0.00	0.10	0.002
1210	20.52	20.52	159.78	0.00	1.95	105.	151.39	0.00	0.040	125.99	0.00	1.53	0.032
1211	20.52	20.52	154.92	0.00	1.89	102.	146.68	0.00	0.038	125.88	0.00	1.53	0.032
1212	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.90	0.00	0.10	0.002
1213	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.22	0.00	0.06	0.001
1214	20.52	20.52	158.85	0.00	1.93	105.	150.52	0.00	0.039	124.24	0.00	1.51	0.031
1215	20.52	20.52	154.40	0.00	1.88	102.	146.20	0.00	0.038	124.16	0.00	1.51	0.031
1216	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.22	0.00	0.06	0.001
1217	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	3.63	0.00	0.08	0.001
1218	20.52	20.52	140.87	0.00	3.26	143.	133.52	0.00	0.063	114.55	0.00	2.65	0.050
1219	20.52	20.52	141.91	0.00	3.29	144.	134.54	0.00	0.063	114.38	0.00	2.65	0.050
1220	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	3.62	0.00	0.08	0.001
1221	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.91	0.00	0.16	0.003
1222	20.52	20.52	131.36	0.00	3.04	133.	124.53	0.00	0.057	110.14	0.00	2.55	0.048
1223	20.52	20.52	132.66	0.00	3.07	135.	125.80	0.00	0.058	109.97	0.00	2.55	0.047
1224	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.91	0.00	0.16	0.003

GUSCI	ARMATURA SUPERIORE VERTICALE						COMB. QUASI PERMANENTE			
	COMBINAZIONE RARA		COMB. FREQUENTE				Mom	Nor	σC	wkP

GUSCI	Af	Afc	Mom	Nor	σ_c	σ_f	Mom	Nor	wkF	Mom	Nor	σ_c	wkP
1201	34.27	19.99	8.16	0.00	0.16	5.	7.75	0.00	0.001	6.27	0.00	0.12	0.001
1202	34.27	19.99	4.81	0.00	0.09	3.	4.75	0.00	0.001	2.65	0.00	0.05	0.000
1203	34.27	19.99	5.79	0.00	0.11	4.	5.69	0.00	0.001	2.25	0.00	0.04	0.000
1204	34.27	19.99	9.25	0.00	0.18	6.	8.80	0.00	0.001	5.77	0.00	0.11	0.001
1205	34.27	19.99	95.51	0.00	1.88	59.	89.32	0.00	0.013	75.55	0.00	1.48	0.011
1206	34.27	19.99	89.25	0.00	1.75	55.	83.05	0.00	0.012	67.42	0.00	1.32	0.010
1207	34.27	19.99	93.01	0.00	1.83	58.	86.64	0.00	0.013	65.52	0.00	1.29	0.010
1208	34.27	19.99	92.47	0.00	1.82	57.	85.83	0.00	0.013	69.15	0.00	1.36	0.010
1209	34.27	19.99	490.83	0.00	5.02	197.	466.02	0.00	0.066	373.44	0.00	3.82	0.051
1210	34.27	19.99	491.00	0.00	5.02	197.	466.18	0.00	0.066	373.51	0.00	3.82	0.051
1211	34.27	19.99	491.00	0.00	5.02	197.	466.18	0.00	0.066	373.51	0.00	3.82	0.051
1212	34.27	19.99	491.39	0.00	5.02	198.	466.56	0.00	0.067	373.62	0.00	3.82	0.051
1213	34.27	19.99	494.63	0.00	5.06	199.	466.76	0.00	0.067	373.44	0.00	3.82	0.051
1214	34.27	19.99	494.84	0.00	5.06	199.	466.96	0.00	0.067	373.51	0.00	3.82	0.051
1215	34.27	19.99	494.84	0.00	5.06	199.	466.96	0.00	0.067	373.51	0.00	3.82	0.051
1216	34.27	19.99	495.24	0.00	5.06	199.	467.33	0.00	0.067	373.62	0.00	3.82	0.051
1217	34.27	19.99	84.07	0.00	1.65	52.	88.80	0.00	0.013	75.55	0.00	1.48	0.011
1218	34.27	19.99	79.40	0.00	1.56	49.	82.38	0.00	0.012	67.42	0.00	1.32	0.010
1219	34.27	19.99	84.88	0.00	1.67	53.	85.99	0.00	0.013	65.52	0.00	1.29	0.010
1220	34.27	19.99	86.14	0.00	1.69	53.	85.04	0.00	0.013	69.15	0.00	1.36	0.010
1221	34.27	19.99	8.17	0.00	0.16	5.	7.75	0.00	0.001	6.27	0.00	0.12	0.001
1222	34.27	19.99	4.84	0.00	0.10	3.	4.75	0.00	0.001	2.65	0.00	0.05	0.000
1223	34.27	19.99	5.82	0.00	0.11	4.	5.69	0.00	0.001	2.25	0.00	0.04	0.000
1224	34.27	19.99	9.27	0.00	0.18	6.	8.80	0.00	0.001	5.77	0.00	0.11	0.001

MACROGUSCIO: Pulvino13

ARMATURA INFERIORE ORIZZONTALE													
GUSCI	COMBINAZIONE RARA						COMB. FREQUENTE			COMB. QUASI PERMANENTE			
	Af	Afc	Mom	Nor	σ_c	σ_f	Mom	Nor	wkF	Mom	Nor	σ_c	wkP
1301	20.52	20.52	10.94	0.00	0.25	11.	10.34	0.00	0.004	0.00	0.00	0.00	0.000
1302	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1303	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1304	20.52	20.52	10.96	0.00	0.25	11.	10.36	0.00	0.004	0.00	0.00	0.00	0.000
1305	20.52	20.52	10.40	0.00	0.24	11.	9.84	0.00	0.004	0.00	0.00	0.00	0.000
1306	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1307	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1308	20.52	20.52	10.42	0.00	0.24	11.	9.86	0.00	0.004	0.00	0.00	0.00	0.000
1309	20.52	20.52	10.84	0.00	0.13	7.	10.21	0.00	0.003	0.00	0.00	0.00	0.000
1310	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1311	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1312	20.52	20.52	10.87	0.00	0.13	7.	10.24	0.00	0.003	0.00	0.00	0.00	0.000
1313	20.52	20.52	11.29	0.00	0.14	7.	10.66	0.00	0.003	0.00	0.00	0.00	0.000
1314	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1315	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1316	20.52	20.52	11.32	0.00	0.14	7.	10.69	0.00	0.003	0.00	0.00	0.00	0.000
1317	20.52	20.52	16.36	0.00	0.38	17.	15.46	0.00	0.006	0.00	0.00	0.00	0.000
1318	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1319	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1320	20.52	20.52	16.37	0.00	0.38	17.	15.47	0.00	0.006	0.00	0.00	0.00	0.000
1321	20.52	20.52	18.02	0.00	0.42	18.	17.02	0.00	0.007	0.00	0.00	0.00	0.000
1322	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1323	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1324	20.52	20.52	18.02	0.00	0.42	18.	17.02	0.00	0.007	0.00	0.00	0.00	0.000

ARMATURA INFERIORE VERTICALE													
GUSCI	COMBINAZIONE RARA						COMB. FREQUENTE			COMB. QUASI PERMANENTE			
	Af	Afc	Mom	Nor	σ_c	σ_f	Mom	Nor	wkF	Mom	Nor	σ_c	wkP
1301	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1302	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1303	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1304	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1305	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1306	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1307	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1308	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1309	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1310	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1311	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1312	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1313	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1314	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1315	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1316	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1317	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1318	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1319	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1320	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1321	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1322	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1323	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1324	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000

ARMATURA SUPERIORE ORIZZONTALE													
GUSCI	COMBINAZIONE RARA						COMB. FREQUENTE			COMB. QUASI PERMANENTE			
	Af	Afc	Mom	Nor	σ_c	σ_f	Mom	Nor	wkF	Mom	Nor	σ_c	wkP
1301	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	8.80	0.00	0.20	0.003
1302	20.52	20.52	151.72	0.00	3.51	154.	143.49	0.00	0.069	116.60	0.00	2.70	0.052
1303	20.52	20.52	140.15	0.00	3.25	142.	132.76	0.00	0.062	116.44	0.00	2.70	0.052
1304	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	8.81	0.00	0.20	0.003
1305	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.84	0.00	0.16	0.003
1306	20.52	20.52	157.81	0.00	3.65	160.	149.25	0.00	0.073	125.67	0.00	2.91	0.058
1307	20.52	20.52	148.17	0.00	3.43	151.	140.31	0.00	0.067	125.50	0.00	2.91	0.058
1308	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.84	0.00	0.16	0.003
1309	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.91	0.00	0.10	0.002
1310	20.52	20.52	159.85	0.00	1.95	105.	151.35	0.00	0.040	125.89	0.00	1.53	0.032

1311	20.52	20.52	154.69	0.00	1.88	102.	146.56	0.00	0.038	125.76	0.00	1.53	0.032
1312	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.90	0.00	0.10	0.002
1313	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.22	0.00	0.06	0.001
1314	20.52	20.52	158.92	0.00	1.94	105.	150.49	0.00	0.039	124.15	0.00	1.51	0.031
1315	20.52	20.52	154.18	0.00	1.88	102.	146.08	0.00	0.038	124.04	0.00	1.51	0.031
1316	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.22	0.00	0.06	0.001
1317	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	3.62	0.00	0.08	0.001
1318	20.52	20.52	140.77	0.00	3.26	143.	133.47	0.00	0.063	114.43	0.00	2.65	0.050
1319	20.52	20.52	141.86	0.00	3.28	144.	134.47	0.00	0.063	114.26	0.00	2.65	0.050
1320	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	3.60	0.00	0.08	0.001
1321	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.91	0.00	0.16	0.003
1322	20.52	20.52	131.25	0.00	3.04	133.	124.48	0.00	0.057	110.01	0.00	2.55	0.048
1323	20.52	20.52	132.62	0.00	3.07	135.	125.73	0.00	0.058	109.84	0.00	2.54	0.047
1324	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.91	0.00	0.16	0.003

ARMATURA SUPERIORE VERTICALE

GUSCI	COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE					
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	wkF	Mom	Nor	σc	wkP
1301	34.27	19.99	8.11	0.00	0.16	5.	7.70	0.00	0.001	6.25	0.00	0.12	0.001
1302	34.27	19.99	4.82	0.00	0.09	3.	4.75	0.00	0.001	2.63	0.00	0.05	0.000
1303	34.27	19.99	5.79	0.00	0.11	4.	5.69	0.00	0.001	2.26	0.00	0.04	0.000
1304	34.27	19.99	9.24	0.00	0.18	6.	8.78	0.00	0.001	5.77	0.00	0.11	0.001
1305	34.27	19.99	95.76	0.00	1.88	59.	89.33	0.00	0.013	75.45	0.00	1.48	0.011
1306	34.27	19.99	89.47	0.00	1.76	56.	83.07	0.00	0.012	67.36	0.00	1.32	0.010
1307	34.27	19.99	93.23	0.00	1.83	58.	86.67	0.00	0.013	65.47	0.00	1.29	0.010
1308	34.27	19.99	92.68	0.00	1.82	58.	85.88	0.00	0.013	69.10	0.00	1.36	0.010
1309	34.27	19.99	490.54	0.00	5.01	197.	465.93	0.00	0.066	373.39	0.00	3.82	0.051
1310	34.27	19.99	490.71	0.00	5.01	197.	466.09	0.00	0.066	373.46	0.00	3.82	0.051
1311	34.27	19.99	490.71	0.00	5.01	197.	466.09	0.00	0.066	373.46	0.00	3.82	0.051
1312	34.27	19.99	491.10	0.00	5.02	198.	466.46	0.00	0.066	373.57	0.00	3.82	0.051
1313	34.27	19.99	494.99	0.00	5.06	199.	466.80	0.00	0.067	373.39	0.00	3.82	0.051
1314	34.27	19.99	495.20	0.00	5.06	199.	466.99	0.00	0.067	373.46	0.00	3.82	0.051
1315	34.27	19.99	495.20	0.00	5.06	199.	466.99	0.00	0.067	373.46	0.00	3.82	0.051
1316	34.27	19.99	495.60	0.00	5.07	199.	467.37	0.00	0.067	373.57	0.00	3.82	0.051
1317	34.27	19.99	83.86	0.00	1.65	52.	88.70	0.00	0.013	75.45	0.00	1.48	0.011
1318	34.27	19.99	79.24	0.00	1.56	49.	82.32	0.00	0.012	67.36	0.00	1.32	0.010
1319	34.27	19.99	84.91	0.00	1.67	53.	85.94	0.00	0.013	65.47	0.00	1.29	0.010
1320	34.27	19.99	86.09	0.00	1.69	53.	85.04	0.00	0.013	69.10	0.00	1.36	0.010
1321	34.27	19.99	8.12	0.00	0.16	5.	7.71	0.00	0.001	6.25	0.00	0.12	0.001
1322	34.27	19.99	4.85	0.00	0.10	3.	4.76	0.00	0.001	2.63	0.00	0.05	0.000
1323	34.27	19.99	5.82	0.00	0.11	4.	5.70	0.00	0.001	2.26	0.00	0.04	0.000
1324	34.27	19.99	9.26	0.00	0.18	6.	8.78	0.00	0.001	5.77	0.00	0.11	0.001

MACROGUSCIO: Pulvino14

ARMATURA INFERIORE ORIZZONTALE

GUSCI	COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE					
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	wkF	Mom	Nor	σc	wkP
1401	20.52	20.52	10.95	0.00	0.25	11.	10.35	0.00	0.004	0.00	0.00	0.00	0.000
1402	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1403	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1404	20.52	20.52	10.97	0.00	0.25	11.	10.37	0.00	0.004	0.00	0.00	0.00	0.000
1405	20.52	20.52	10.41	0.00	0.24	11.	9.86	0.00	0.004	0.00	0.00	0.00	0.000
1406	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1407	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1408	20.52	20.52	10.45	0.00	0.24	11.	9.89	0.00	0.004	0.00	0.00	0.00	0.000
1409	20.52	20.52	10.85	0.00	0.13	7.	10.22	0.00	0.003	0.00	0.00	0.00	0.000
1410	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1411	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1412	20.52	20.52	10.90	0.00	0.13	7.	10.26	0.00	0.003	0.00	0.00	0.00	0.000
1413	20.52	20.52	11.30	0.00	0.14	7.	10.67	0.00	0.003	0.00	0.00	0.00	0.000
1414	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1415	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1416	20.52	20.52	11.34	0.00	0.14	7.	10.72	0.00	0.003	0.00	0.00	0.00	0.000
1417	20.52	20.52	16.36	0.00	0.38	17.	15.46	0.00	0.006	0.00	0.00	0.00	0.000
1418	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1419	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1420	20.52	20.52	16.37	0.00	0.38	17.	15.47	0.00	0.006	0.00	0.00	0.00	0.000
1421	20.52	20.52	18.02	0.00	0.42	18.	17.01	0.00	0.007	0.00	0.00	0.00	0.000
1422	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1423	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1424	20.52	20.52	18.01	0.00	0.42	18.	17.01	0.00	0.007	0.00	0.00	0.00	0.000

ARMATURA INFERIORE VERTICALE

GUSCI	COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE					
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	wkF	Mom	Nor	σc	wkP
1401	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1402	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1403	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1404	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1405	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1406	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1407	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1408	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1409	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1410	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1411	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1412	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1413	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1414	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1415	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1416	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1417	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1418	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1419	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1420	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1421	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000

1422	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1423	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1424	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000

ARMATURA SUPERIORE ORIZZONTALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE						
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	wkF	Mom	Nor	σc	wkP
1401	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	8.80	0.00	0.20	0.003
1402	20.52	20.52	151.61	0.00	3.51	154.	143.40	0.00	0.069	116.50	0.00	2.70	0.052
1403	20.52	20.52	139.98	0.00	3.24	142.	132.61	0.00	0.062	116.25	0.00	2.69	0.052
1404	20.52	20.52	9.00	0.00	0.00	0.	0.00	0.00	0.000	8.81	0.00	0.20	0.003
1405	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.83	0.00	0.16	0.003
1406	20.52	20.52	157.71	0.00	3.65	160.	149.17	0.00	0.073	125.58	0.00	2.91	0.058
1407	20.52	20.52	148.01	0.00	3.43	150.	140.17	0.00	0.067	125.31	0.00	2.90	0.057
1408	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.83	0.00	0.16	0.003
1409	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.90	0.00	0.10	0.002
1410	20.52	20.52	159.77	0.00	1.95	105.	151.29	0.00	0.040	125.80	0.00	1.53	0.032
1411	20.52	20.52	154.54	0.00	1.88	102.	146.42	0.00	0.038	125.60	0.00	1.53	0.032
1412	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.89	0.00	0.10	0.002
1413	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.23	0.00	0.06	0.001
1414	20.52	20.52	158.84	0.00	1.93	105.	150.42	0.00	0.039	124.05	0.00	1.51	0.031
1415	20.52	20.52	154.03	0.00	1.88	102.	145.94	0.00	0.038	123.89	0.00	1.51	0.031
1416	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.23	0.00	0.06	0.001
1417	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	3.61	0.00	0.08	0.001
1418	20.52	20.52	140.70	0.00	3.26	143.	133.40	0.00	0.063	114.34	0.00	2.65	0.050
1419	20.52	20.52	141.74	0.00	3.28	144.	134.35	0.00	0.063	114.06	0.00	2.64	0.050
1420	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	3.58	0.00	0.08	0.001
1421	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.90	0.00	0.16	0.003
1422	20.52	20.52	131.18	0.00	3.04	133.	124.41	0.00	0.057	109.91	0.00	2.54	0.047
1423	20.52	20.52	132.51	0.00	3.07	135.	125.61	0.00	0.058	109.64	0.00	2.54	0.047
1424	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.90	0.00	0.16	0.003

ARMATURA SUPERIORE VERTICALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE						
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	wkF	Mom	Nor	σc	wkP
1401	34.27	19.99	8.11	0.00	0.16	5.	7.71	0.00	0.001	6.24	0.00	0.12	0.001
1402	34.27	19.99	4.80	0.00	0.09	3.	4.73	0.00	0.001	2.63	0.00	0.05	0.000
1403	34.27	19.99	5.78	0.00	0.11	4.	5.67	0.00	0.001	2.24	0.00	0.04	0.000
1404	34.27	19.99	9.23	0.00	0.18	6.	8.76	0.00	0.001	5.77	0.00	0.11	0.001
1405	34.27	19.99	95.82	0.00	1.88	59.	89.40	0.00	0.013	75.51	0.00	1.48	0.011
1406	34.27	19.99	89.54	0.00	1.76	56.	83.15	0.00	0.012	67.43	0.00	1.32	0.010
1407	34.27	19.99	93.29	0.00	1.83	58.	86.74	0.00	0.013	65.54	0.00	1.29	0.010
1408	34.27	19.99	92.74	0.00	1.82	58.	85.95	0.00	0.013	69.06	0.00	1.36	0.010
1409	34.27	19.99	490.65	0.00	5.01	197.	466.00	0.00	0.066	373.43	0.00	3.82	0.051
1410	34.27	19.99	490.82	0.00	5.02	197.	466.16	0.00	0.066	373.51	0.00	3.82	0.051
1411	34.27	19.99	490.82	0.00	5.02	197.	466.16	0.00	0.066	373.51	0.00	3.82	0.051
1412	34.27	19.99	491.21	0.00	5.02	198.	466.53	0.00	0.067	373.62	0.00	3.82	0.051
1413	34.27	19.99	495.00	0.00	5.06	199.	466.85	0.00	0.067	373.43	0.00	3.82	0.051
1414	34.27	19.99	495.21	0.00	5.06	199.	467.05	0.00	0.067	373.51	0.00	3.82	0.051
1415	34.27	19.99	495.21	0.00	5.06	199.	467.05	0.00	0.067	373.51	0.00	3.82	0.051
1416	34.27	19.99	495.61	0.00	5.07	199.	467.42	0.00	0.067	373.62	0.00	3.82	0.051
1417	34.27	19.99	83.93	0.00	1.65	52.	88.78	0.00	0.013	75.51	0.00	1.48	0.011
1418	34.27	19.99	79.34	0.00	1.56	49.	82.41	0.00	0.012	67.43	0.00	1.32	0.010
1419	34.27	19.99	84.92	0.00	1.67	53.	86.02	0.00	0.013	65.54	0.00	1.29	0.010
1420	34.27	19.99	86.10	0.00	1.69	53.	85.12	0.00	0.013	69.06	0.00	1.36	0.010
1421	34.27	19.99	8.10	0.00	0.16	5.	7.70	0.00	0.001	6.24	0.00	0.12	0.001
1422	34.27	19.99	4.78	0.00	0.09	3.	4.73	0.00	0.001	2.63	0.00	0.05	0.000
1423	34.27	19.99	5.77	0.00	0.11	4.	5.67	0.00	0.001	2.24	0.00	0.04	0.000
1424	34.27	19.99	9.19	0.00	0.18	6.	8.76	0.00	0.001	5.77	0.00	0.11	0.001

MACROGUSCIO: Pulvino15

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE						
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	wkF	Mom	Nor	σc	wkP
1501	20.52	20.52	10.96	0.00	0.25	11.	10.37	0.00	0.004	0.00	0.00	0.00	0.000
1502	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1503	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1504	20.52	20.52	10.99	0.00	0.25	11.	10.40	0.00	0.004	0.00	0.00	0.00	0.000
1505	20.52	20.52	10.43	0.00	0.24	11.	9.88	0.00	0.004	0.00	0.00	0.00	0.000
1506	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1507	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1508	20.52	20.52	10.48	0.00	0.24	11.	9.92	0.00	0.004	0.00	0.00	0.00	0.000
1509	20.52	20.52	10.88	0.00	0.13	7.	10.25	0.00	0.003	0.00	0.00	0.00	0.000
1510	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1511	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1512	20.52	20.52	10.95	0.00	0.13	7.	10.32	0.00	0.003	0.00	0.00	0.00	0.000
1513	20.52	20.52	11.32	0.00	0.14	7.	10.70	0.00	0.003	0.00	0.00	0.00	0.000
1514	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1515	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1516	20.52	20.52	11.38	0.00	0.14	8.	10.76	0.00	0.003	0.00	0.00	0.00	0.000
1517	20.52	20.52	16.35	0.00	0.38	17.	15.46	0.00	0.006	0.00	0.00	0.00	0.000
1518	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1519	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1520	20.52	20.52	16.36	0.00	0.38	17.	15.48	0.00	0.006	0.00	0.00	0.00	0.000
1521	20.52	20.52	17.99	0.00	0.42	18.	17.01	0.00	0.007	0.00	0.00	0.00	0.000
1522	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1523	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1524	20.52	20.52	17.97	0.00	0.42	18.	17.00	0.00	0.007	0.00	0.00	0.00	0.000

ARMATURA INFERIORE VERTICALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE						
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	wkF	Mom	Nor	σc	wkP
1501	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1502	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1503	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1504	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1505	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000

1506	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1507	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1508	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1509	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1510	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1511	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1512	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1513	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1514	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1515	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1516	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1517	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1518	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1519	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1520	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1521	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1522	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1523	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1524	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000

ARMATURA SUPERIORE ORIZZONTALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE						
	Af	AfC	Mom	Nor	σ_c	σ_f	Mom	Nor	wkF	Mom	Nor	σ_c	wkP
1501	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	8.80	0.00	0.20	0.003
1502	20.52	20.52	151.41	0.00	3.51	154.	143.24	0.00	0.069	116.28	0.00	2.69	0.052
1503	20.52	20.52	139.59	0.00	3.23	142.	132.29	0.00	0.062	115.87	0.00	2.68	0.051
1504	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	8.80	0.00	0.20	0.003
1505	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.83	0.00	0.16	0.003
1506	20.52	20.52	157.54	0.00	3.65	160.	149.03	0.00	0.073	125.39	0.00	2.90	0.058
1507	20.52	20.52	147.65	0.00	3.42	150.	139.85	0.00	0.067	124.95	0.00	2.89	0.057
1508	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.82	0.00	0.16	0.003
1509	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.89	0.00	0.10	0.002
1510	20.52	20.52	159.66	0.00	1.94	105.	151.19	0.00	0.040	125.63	0.00	1.53	0.032
1511	20.52	20.52	154.23	0.00	1.88	102.	146.12	0.00	0.038	125.28	0.00	1.53	0.032
1512	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.87	0.00	0.10	0.002
1513	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.23	0.00	0.06	0.001
1514	20.52	20.52	158.72	0.00	1.93	105.	150.32	0.00	0.039	123.89	0.00	1.51	0.031
1515	20.52	20.52	153.73	0.00	1.87	101.	145.65	0.00	0.037	123.58	0.00	1.51	0.031
1516	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.23	0.00	0.06	0.001
1517	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	3.59	0.00	0.08	0.001
1518	20.52	20.52	140.62	0.00	3.26	143.	133.34	0.00	0.063	114.15	0.00	2.64	0.050
1519	20.52	20.52	141.50	0.00	3.28	144.	134.10	0.00	0.063	113.69	0.00	2.63	0.050
1520	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	3.54	0.00	0.08	0.001
1521	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.90	0.00	0.16	0.003
1522	20.52	20.52	131.09	0.00	3.04	133.	124.33	0.00	0.057	109.69	0.00	2.54	0.047
1523	20.52	20.52	132.28	0.00	3.06	134.	125.38	0.00	0.058	109.26	0.00	2.53	0.047
1524	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.88	0.00	0.16	0.003

ARMATURA SUPERIORE VERTICALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE						
	Af	AfC	Mom	Nor	σ_c	σ_f	Mom	Nor	wkF	Mom	Nor	σ_c	wkP
1501	34.27	19.99	8.03	0.00	0.16	5.	7.63	0.00	0.001	6.20	0.00	0.12	0.001
1502	34.27	19.99	4.80	0.00	0.09	3.	4.71	0.00	0.001	2.60	0.00	0.05	0.000
1503	34.27	19.99	5.78	0.00	0.11	4.	5.66	0.00	0.001	2.24	0.00	0.04	0.000
1504	34.27	19.99	9.20	0.00	0.18	6.	8.72	0.00	0.001	5.76	0.00	0.11	0.001
1505	34.27	19.99	95.79	0.00	1.88	59.	89.36	0.00	0.013	75.41	0.00	1.48	0.011
1506	34.27	19.99	89.60	0.00	1.76	56.	83.18	0.00	0.012	67.40	0.00	1.32	0.010
1507	34.27	19.99	93.34	0.00	1.83	58.	86.76	0.00	0.013	65.52	0.00	1.29	0.010
1508	34.27	19.99	92.85	0.00	1.82	58.	86.01	0.00	0.013	68.92	0.00	1.35	0.010
1509	34.27	19.99	490.61	0.00	5.01	197.	465.96	0.00	0.066	373.37	0.00	3.82	0.051
1510	34.27	19.99	490.78	0.00	5.02	197.	466.12	0.00	0.066	373.45	0.00	3.82	0.051
1511	34.27	19.99	490.78	0.00	5.02	197.	466.12	0.00	0.066	373.45	0.00	3.82	0.051
1512	34.27	19.99	491.17	0.00	5.02	198.	466.49	0.00	0.066	373.56	0.00	3.82	0.051
1513	34.27	19.99	494.97	0.00	5.06	199.	466.82	0.00	0.067	373.37	0.00	3.82	0.051
1514	34.27	19.99	495.18	0.00	5.06	199.	467.02	0.00	0.067	373.45	0.00	3.82	0.051
1515	34.27	19.99	495.18	0.00	5.06	199.	467.02	0.00	0.067	373.45	0.00	3.82	0.051
1516	34.27	19.99	495.58	0.00	5.06	199.	467.39	0.00	0.067	373.56	0.00	3.82	0.051
1517	34.27	19.99	83.88	0.00	1.65	52.	88.74	0.00	0.013	75.41	0.00	1.48	0.011
1518	34.27	19.99	79.03	0.00	1.55	49.	82.36	0.00	0.012	67.40	0.00	1.32	0.010
1519	34.27	19.99	84.74	0.00	1.66	53.	85.96	0.00	0.013	65.52	0.00	1.29	0.010
1520	34.27	19.99	85.87	0.00	1.69	53.	85.07	0.00	0.013	68.92	0.00	1.35	0.010
1521	34.27	19.99	7.97	0.00	0.16	5.	7.62	0.00	0.001	6.20	0.00	0.12	0.001
1522	34.27	19.99	4.85	0.00	0.10	3.	4.72	0.00	0.001	2.60	0.00	0.05	0.000
1523	34.27	19.99	5.83	0.00	0.11	4.	5.67	0.00	0.001	2.24	0.00	0.04	0.000
1524	34.27	19.99	9.23	0.00	0.18	6.	8.73	0.00	0.001	5.76	0.00	0.11	0.001

VERIFICA SEZIONI PULVINI (sezione x-z):

PARAMETRI GENERALI

Tipo verifica : stati limite - pressoflessione retta.
 Unità di misura generiche: kN; cm; kNm; N/mm²; d in mm; deformazioni*1000.
 ferri : diametri in mm; aree in cm².

Simboli :

vert. = contorno_vertice del CLS; d = diametro;
 S = Sigma (tensioni sui materiali);
 D = Deformazioni x 1000 (epsilon);
 Ve = colonna che indica se la verifica e' soddisfatta;

CARATTERISTICHE MATERIALI

Calcestruzzo: Rck = 30. ; fck = 24.9 ; fcd = 14.11 (.35%)
 Acciaio : Tipo= B450C ; ftk = 540. ; fyk = 450. ; ftd = 469.565 (6.75%)

CARATTERISTICHE SEZIONE

L'asse Z e' rivolto verso destra, l'asse Y e' rivolto verso l'alto.

Tipo sezione: RETTANGOLARE

ClS: Acciaio lento:

vert.	Z	Y	ferro	Z	Y	d[mm]	Af[cm ²]
1- 1	-2673.	70.6	1	-2456.	40.6	20.	3.1416
1- 2	-2453.	70.6	2	-2466.	40.6	20.	3.1416
1- 3	-2453.	-11.4	3	-2476.	40.6	20.	3.1416
1- 4	-2673.	-11.4	4	-2487.	40.6	20.	3.1416
			5	-2497.	40.6	20.	3.1416
			6	-2507.	40.6	20.	3.1416
			7	-2517.	40.6	20.	3.1416
			8	-2527.	40.6	20.	3.1416
			9	-2538.	40.6	20.	3.1416
			10	-2548.	40.6	20.	3.1416
			11	-2558.	40.6	20.	3.1416
			12	-2568.	40.6	20.	3.1416
			13	-2578.	40.6	20.	3.1416
			14	-2589.	40.6	20.	3.1416
			15	-2599.	40.6	20.	3.1416
			16	-2609.	40.6	20.	3.1416
			17	-2619.	40.6	20.	3.1416
			18	-2629.	40.6	20.	3.1416
			19	-2639.	40.6	20.	3.1416
			20	-2650.	40.6	20.	3.1416
			21	-2660.	40.6	20.	3.1416
			22	-2670.	40.6	20.	3.1416
			23	-2456.	67.6	20.	3.1416
			24	-2466.	67.6	20.	3.1416
			25	-2476.	67.6	20.	3.1416
			26	-2487.	67.6	20.	3.1416
			27	-2497.	67.6	20.	3.1416
			28	-2507.	67.6	20.	3.1416
			29	-2517.	67.6	20.	3.1416
			30	-2527.	67.6	20.	3.1416
			31	-2538.	67.6	20.	3.1416
			32	-2548.	67.6	20.	3.1416
			33	-2558.	67.6	20.	3.1416
			34	-2568.	67.6	20.	3.1416
			35	-2578.	67.6	20.	3.1416
			36	-2589.	67.6	20.	3.1416
			37	-2599.	67.6	20.	3.1416
			38	-2609.	67.6	20.	3.1416
			39	-2619.	67.6	20.	3.1416
			40	-2629.	67.6	20.	3.1416
			41	-2639.	67.6	20.	3.1416
			42	-2650.	67.6	20.	3.1416
			43	-2660.	67.6	20.	3.1416
			44	-2670.	67.6	20.	3.1416
			45	-2456.	-8.4	20.	3.1416
			46	-2473.	-8.4	20.	3.1416
			47	-2489.	-8.4	20.	3.1416
			48	-2505.	-8.4	20.	3.1416
			49	-2522.	-8.4	20.	3.1416
			50	-2538.	-8.4	20.	3.1416
			51	-2555.	-8.4	20.	3.1416
			52	-2571.	-8.4	20.	3.1416
			53	-2588.	-8.4	20.	3.1416
			54	-2604.	-8.4	20.	3.1416
			55	-2621.	-8.4	20.	3.1416
			56	-2637.	-8.4	20.	3.1416
			57	-2654.	-8.4	20.	3.1416
			58	-2670.	-8.4	20.	3.1416

Descrizione : Pulvino 1

SOLLECITAZIONI AGENTI

Sforzi normali applicati in y= 29.55 (baricentro CLS)
 Convenzioni: N + trazione; Mz + fib.inferiori tese; My + fib.sinistra tese.

N.	N	Mz	My	Descrizione
1	-31.5	-1771.9308	-6.3116	Caso 2.1
2	-20.79	-1138.0727	-9.7479	Caso 7.28
3	-106.22	-1153.5307	11.6842	Caso 7.5
4	-175.61	-1757.2781	-19.3171	Caso 2.2
5	33.36	-972.8584	-3.5947	Caso 13.1

RISULTATI

Piani di equilibrio (eps= muz * y + muy * z + lam):

Sol.	muz	muy	lambda
1.	.00002570277	0.	-.00036641484
2.	.00001631688	0.	-.00022641939
3.	.00001635398	0.	-.00023489916
4.	.00002517197	0.	-.00037221725

5. | .00001402343 | 0. | - .00018857371 |
 Deformazioni sui materiali:

C1s					Acciaio lento			
sol	vert.	D c1s	S c1s	Ve	ferro	D ferri	S ferri	Ve
1	1- 1	1.4469	0.	si	1	.6758	135.17	si
1	1- 2	1.4469	0.	si	2	.6758	135.17	si
1	1- 3	-.6607	-7.78	si	3	.6758	135.17	si
1	1- 4	-.6607	-7.78	si	4	.6758	135.17	si
1					5	.6758	135.17	si
1					6	.6758	135.17	si
1					7	.6758	135.17	si
1					8	.6758	135.17	si
1					9	.6758	135.17	si
1					10	.6758	135.17	si
1					11	.6758	135.17	si
1					12	.6758	135.17	si
1					13	.6758	135.17	si
1					14	.6758	135.17	si
1					15	.6758	135.17	si
1					16	.6758	135.17	si
1					17	.6758	135.17	si
1					18	.6758	135.17	si
1					19	.6758	135.17	si
1					20	.6758	135.17	si
1					21	.6758	135.17	si
1					22	.6758	135.17	si
1					23	1.3698	273.96	si
1					24	1.3698	273.96	si
1					25	1.3698	273.96	si
1					26	1.3698	273.96	si
1					27	1.3698	273.96	si
1					28	1.3698	273.96	si
1					29	1.3698	273.96	si
1					30	1.3698	273.96	si
1					31	1.3698	273.96	si
1					32	1.3698	273.96	si
1					33	1.3698	273.96	si
1					34	1.3698	273.96	si
1					35	1.3698	273.96	si
1					36	1.3698	273.96	si
1					37	1.3698	273.96	si
1					38	1.3698	273.96	si
1					39	1.3698	273.96	si
1					40	1.3698	273.96	si
1					41	1.3698	273.96	si
1					42	1.3698	273.96	si
1					43	1.3698	273.96	si
1					44	1.3698	273.96	si
1					45	-.5836	-116.72	si
1					46	-.5836	-116.72	si
1					47	-.5836	-116.72	si
1					48	-.5836	-116.72	si
1					49	-.5836	-116.72	si
1					50	-.5836	-116.72	si
1					51	-.5836	-116.72	si
1					52	-.5836	-116.72	si
1					53	-.5836	-116.72	si
1					54	-.5836	-116.72	si
1					55	-.5836	-116.72	si
1					56	-.5836	-116.72	si
1					57	-.5836	-116.72	si
1					58	-.5836	-116.72	si
2	1- 1	.9247	0.	si	1	.4352	87.05	si
2	1- 2	.9247	0.	si	2	.4352	87.05	si
2	1- 3	-.4132	-5.23	si	3	.4352	87.05	si
2	1- 4	-.4132	-5.23	si	4	.4352	87.05	si
2					5	.4352	87.05	si
2					6	.4352	87.05	si
2					7	.4352	87.05	si
2					8	.4352	87.05	si
2					9	.4352	87.05	si
2					10	.4352	87.05	si
2					11	.4352	87.05	si
2					12	.4352	87.05	si
2					13	.4352	87.05	si
2					14	.4352	87.05	si
2					15	.4352	87.05	si
2					16	.4352	87.05	si
2					17	.4352	87.05	si
2					18	.4352	87.05	si
2					19	.4352	87.05	si
2					20	.4352	87.05	si
2					21	.4352	87.05	si
2					22	.4352	87.05	si
2					23	.8758	175.16	si
2					24	.8758	175.16	si
2					25	.8758	175.16	si
2					26	.8758	175.16	si
2					27	.8758	175.16	si
2					28	.8758	175.16	si
2					29	.8758	175.16	si
2					30	.8758	175.16	si
2					31	.8758	175.16	si
2					32	.8758	175.16	si
2					33	.8758	175.16	si
2					34	.8758	175.16	si
2					35	.8758	175.16	si

2				36	.8758	175.16	si
2				37	.8758	175.16	si
2				38	.8758	175.16	si
2				39	.8758	175.16	si
2				40	.8758	175.16	si
2				41	.8758	175.16	si
2				42	.8758	175.16	si
2				43	.8758	175.16	si
2				44	.8758	175.16	si
2				45	-.3643	-72.86	si
2				46	-.3643	-72.86	si
2				47	-.3643	-72.86	si
2				48	-.3643	-72.86	si
2				49	-.3643	-72.86	si
2				50	-.3643	-72.86	si
2				51	-.3643	-72.86	si
2				52	-.3643	-72.86	si
2				53	-.3643	-72.86	si
2				54	-.3643	-72.86	si
2				55	-.3643	-72.86	si
2				56	-.3643	-72.86	si
2				57	-.3643	-72.86	si
2				58	-.3643	-72.86	si
3	1- 1	.9189	0.	1	.4283	85.65	si
3	1- 2	.9189	0.	2	.4283	85.65	si
3	1- 3	-.4222	-5.33	3	.4283	85.65	si
3	1- 4	-.4222	-5.33	4	.4283	85.65	si
3				5	.4283	85.65	si
3				6	.4283	85.65	si
3				7	.4283	85.65	si
3				8	.4283	85.65	si
3				9	.4283	85.65	si
3				10	.4283	85.65	si
3				11	.4283	85.65	si
3				12	.4283	85.65	si
3				13	.4283	85.65	si
3				14	.4283	85.65	si
3				15	.4283	85.65	si
3				16	.4283	85.65	si
3				17	.4283	85.65	si
3				18	.4283	85.65	si
3				19	.4283	85.65	si
3				20	.4283	85.65	si
3				21	.4283	85.65	si
3				22	.4283	85.65	si
3				23	.8698	173.96	si
3				24	.8698	173.96	si
3				25	.8698	173.96	si
3				26	.8698	173.96	si
3				27	.8698	173.96	si
3				28	.8698	173.96	si
3				29	.8698	173.96	si
3				30	.8698	173.96	si
3				31	.8698	173.96	si
3				32	.8698	173.96	si
3				33	.8698	173.96	si
3				34	.8698	173.96	si
3				35	.8698	173.96	si
3				36	.8698	173.96	si
3				37	.8698	173.96	si
3				38	.8698	173.96	si
3				39	.8698	173.96	si
3				40	.8698	173.96	si
3				41	.8698	173.96	si
3				42	.8698	173.96	si
3				43	.8698	173.96	si
3				44	.8698	173.96	si
3				45	-.3731	-74.62	si
3				46	-.3731	-74.62	si
3				47	-.3731	-74.62	si
3				48	-.3731	-74.62	si
3				49	-.3731	-74.62	si
3				50	-.3731	-74.62	si
3				51	-.3731	-74.62	si
3				52	-.3731	-74.62	si
3				53	-.3731	-74.62	si
3				54	-.3731	-74.62	si
3				55	-.3731	-74.62	si
3				56	-.3731	-74.62	si
3				57	-.3731	-74.62	si
3				58	-.3731	-74.62	si
4	1- 1	1.4037	0.	1	.6485	129.7	si
4	1- 2	1.4037	0.	2	.6485	129.7	si
4	1- 3	-.6604	-7.78	3	.6485	129.7	si
4	1- 4	-.6604	-7.78	4	.6485	129.7	si
4				5	.6485	129.7	si
4				6	.6485	129.7	si
4				7	.6485	129.7	si
4				8	.6485	129.7	si
4				9	.6485	129.7	si
4				10	.6485	129.7	si
4				11	.6485	129.7	si
4				12	.6485	129.7	si
4				13	.6485	129.7	si
4				14	.6485	129.7	si
4				15	.6485	129.7	si
4				16	.6485	129.7	si

4				17	.6485	129.7	si
4				18	.6485	129.7	si
4				19	.6485	129.7	si
4				20	.6485	129.7	si
4				21	.6485	129.7	si
4				22	.6485	129.7	si
4				23	1.3281	265.63	si
4				24	1.3281	265.63	si
4				25	1.3281	265.63	si
4				26	1.3281	265.63	si
4				27	1.3281	265.63	si
4				28	1.3281	265.63	si
4				29	1.3281	265.63	si
4				30	1.3281	265.63	si
4				31	1.3281	265.63	si
4				32	1.3281	265.63	si
4				33	1.3281	265.63	si
4				34	1.3281	265.63	si
4				35	1.3281	265.63	si
4				36	1.3281	265.63	si
4				37	1.3281	265.63	si
4				38	1.3281	265.63	si
4				39	1.3281	265.63	si
4				40	1.3281	265.63	si
4				41	1.3281	265.63	si
4				42	1.3281	265.63	si
4				43	1.3281	265.63	si
4				44	1.3281	265.63	si
4				45	-.5849	-116.98	si
4				46	-.5849	-116.98	si
4				47	-.5849	-116.98	si
4				48	-.5849	-116.98	si
4				49	-.5849	-116.98	si
4				50	-.5849	-116.98	si
4				51	-.5849	-116.98	si
4				52	-.5849	-116.98	si
4				53	-.5849	-116.98	si
4				54	-.5849	-116.98	si
4				55	-.5849	-116.98	si
4				56	-.5849	-116.98	si
4				57	-.5849	-116.98	si
4				58	-.5849	-116.98	si
5	1- 1	.8008	0.	1	.3801	76.02	si
5	1- 2	.8008	0.	2	.3801	76.02	si
5	1- 3	-.3491	-4.5	3	.3801	76.02	si
5	1- 4	-.3491	-4.5	4	.3801	76.02	si
5				5	.3801	76.02	si
5				6	.3801	76.02	si
5				7	.3801	76.02	si
5				8	.3801	76.02	si
5				9	.3801	76.02	si
5				10	.3801	76.02	si
5				11	.3801	76.02	si
5				12	.3801	76.02	si
5				13	.3801	76.02	si
5				14	.3801	76.02	si
5				15	.3801	76.02	si
5				16	.3801	76.02	si
5				17	.3801	76.02	si
5				18	.3801	76.02	si
5				19	.3801	76.02	si
5				20	.3801	76.02	si
5				21	.3801	76.02	si
5				22	.3801	76.02	si
5				23	.7587	151.74	si
5				24	.7587	151.74	si
5				25	.7587	151.74	si
5				26	.7587	151.74	si
5				27	.7587	151.74	si
5				28	.7587	151.74	si
5				29	.7587	151.74	si
5				30	.7587	151.74	si
5				31	.7587	151.74	si
5				32	.7587	151.74	si
5				33	.7587	151.74	si
5				34	.7587	151.74	si
5				35	.7587	151.74	si
5				36	.7587	151.74	si
5				37	.7587	151.74	si
5				38	.7587	151.74	si
5				39	.7587	151.74	si
5				40	.7587	151.74	si
5				41	.7587	151.74	si
5				42	.7587	151.74	si
5				43	.7587	151.74	si
5				44	.7587	151.74	si
5				45	-.3071	-61.41	si
5				46	-.3071	-61.41	si
5				47	-.3071	-61.41	si
5				48	-.3071	-61.41	si
5				49	-.3071	-61.41	si
5				50	-.3071	-61.41	si
5				51	-.3071	-61.41	si
5				52	-.3071	-61.41	si
5				53	-.3071	-61.41	si
5				54	-.3071	-61.41	si
5				55	-.3071	-61.41	si

5	56	-.3071	-61.41	si
5	57	-.3071	-61.41	si
5	58	-.3071	-61.41	si

Descrizione : Pulvino 2

SOLLECITAZIONI AGENTI

Sforzi normali applicati in y= 29.55 (baricentro CLS)
 Convenzioni: N + trazione; Mz + fib.inferiori tese; My + fib.sinistra tese.

N.	N	Mz	My	Descrizione
1	-20.63	-1771.5199	-529.1301	Caso 2.1
2	-409.11	-664.8837	-10610.6269	Caso 8.23
3	-1478.02	-1139.1912	-38220.3253	Caso 7.22
4	1350.7	-1148.9898	34952.5624	Caso 7.11

RISULTATI

Piani di equilibrio (eps= muz * y + muy * z + lam):	Sol.	muz	muy	lambda
1.	.00002572	0.		-.00036562208
2.	.00000856448	0.		-.0001507861
3.	.00001317761	0.		-.00030315631
4.	.00001948565	0.		-.00013087267

Deformazioni sui materiali:

Cls					Acciaio lento							
sol	vert.	D	cls	S	cls	Ve	ferro	D	ferri	S	ferri	Ve
1	1- 1		1.4489		0.	si	1		.6773		135.46	si
1	1- 2		1.4489		0.	si	2		.6773		135.46	si
1	1- 3		-.6601		-7.78	si	3		.6773		135.46	si
1	1- 4		-.6601		-7.78	si	4		.6773		135.46	si
1							5		.6773		135.46	si
1							6		.6773		135.46	si
1							7		.6773		135.46	si
1							8		.6773		135.46	si
1							9		.6773		135.46	si
1							10		.6773		135.46	si
1							11		.6773		135.46	si
1							12		.6773		135.46	si
1							13		.6773		135.46	si
1							14		.6773		135.46	si
1							15		.6773		135.46	si
1							16		.6773		135.46	si
1							17		.6773		135.46	si
1							18		.6773		135.46	si
1							19		.6773		135.46	si
1							20		.6773		135.46	si
1							21		.6773		135.46	si
1							22		.6773		135.46	si
1							23		1.3718		274.35	si
1							24		1.3718		274.35	si
1							25		1.3718		274.35	si
1							26		1.3718		274.35	si
1							27		1.3718		274.35	si
1							28		1.3718		274.35	si
1							29		1.3718		274.35	si
1							30		1.3718		274.35	si
1							31		1.3718		274.35	si
1							32		1.3718		274.35	si
1							33		1.3718		274.35	si
1							34		1.3718		274.35	si
1							35		1.3718		274.35	si
1							36		1.3718		274.35	si
1							37		1.3718		274.35	si
1							38		1.3718		274.35	si
1							39		1.3718		274.35	si
1							40		1.3718		274.35	si
1							41		1.3718		274.35	si
1							42		1.3718		274.35	si
1							43		1.3718		274.35	si
1							44		1.3718		274.35	si
1							45		-.583		-116.59	si
1							46		-.583		-116.59	si
1							47		-.583		-116.59	si
1							48		-.583		-116.59	si
1							49		-.583		-116.59	si
1							50		-.583		-116.59	si
1							51		-.583		-116.59	si
1							52		-.583		-116.59	si
1							53		-.583		-116.59	si
1							54		-.583		-116.59	si
1							55		-.583		-116.59	si
1							56		-.583		-116.59	si
1							57		-.583		-116.59	si
1							58		-.583		-116.59	si
2	1- 1		.4534		0.	si	1		.1965		39.3	si
2	1- 2		.4534		0.	si	2		.1965		39.3	si
2	1- 3		-.2488		-3.29	si	3		.1965		39.3	si
2	1- 4		-.2488		-3.29	si	4		.1965		39.3	si
2							5		.1965		39.3	si
2							6		.1965		39.3	si
2							7		.1965		39.3	si
2							8		.1965		39.3	si
2							9		.1965		39.3	si
2							10		.1965		39.3	si
2							11		.1965		39.3	si
2							12		.1965		39.3	si
2							13		.1965		39.3	si

2				14	.1965	39.3	si
2				15	.1965	39.3	si
2				16	.1965	39.3	si
2				17	.1965	39.3	si
2				18	.1965	39.3	si
2				19	.1965	39.3	si
2				20	.1965	39.3	si
2				21	.1965	39.3	si
2				22	.1965	39.3	si
2				23	.4277	85.55	si
2				24	.4277	85.55	si
2				25	.4277	85.55	si
2				26	.4277	85.55	si
2				27	.4277	85.55	si
2				28	.4277	85.55	si
2				29	.4277	85.55	si
2				30	.4277	85.55	si
2				31	.4277	85.55	si
2				32	.4277	85.55	si
2				33	.4277	85.55	si
2				34	.4277	85.55	si
2				35	.4277	85.55	si
2				36	.4277	85.55	si
2				37	.4277	85.55	si
2				38	.4277	85.55	si
2				39	.4277	85.55	si
2				40	.4277	85.55	si
2				41	.4277	85.55	si
2				42	.4277	85.55	si
2				43	.4277	85.55	si
2				44	.4277	85.55	si
2				45	-.2232	-44.63	si
2				46	-.2232	-44.63	si
2				47	-.2232	-44.63	si
2				48	-.2232	-44.63	si
2				49	-.2232	-44.63	si
2				50	-.2232	-44.63	si
2				51	-.2232	-44.63	si
2				52	-.2232	-44.63	si
2				53	-.2232	-44.63	si
2				54	-.2232	-44.63	si
2				55	-.2232	-44.63	si
2				56	-.2232	-44.63	si
2				57	-.2232	-44.63	si
2				58	-.2232	-44.63	si
3	1- 1	.6265	0.	1	.2312	46.24	si
3	1- 2	.6265	0.	2	.2312	46.24	si
3	1- 3	-.454	-5.68	3	.2312	46.24	si
3	1- 4	-.454	-5.68	4	.2312	46.24	si
3				5	.2312	46.24	si
3				6	.2312	46.24	si
3				7	.2312	46.24	si
3				8	.2312	46.24	si
3				9	.2312	46.24	si
3				10	.2312	46.24	si
3				11	.2312	46.24	si
3				12	.2312	46.24	si
3				13	.2312	46.24	si
3				14	.2312	46.24	si
3				15	.2312	46.24	si
3				16	.2312	46.24	si
3				17	.2312	46.24	si
3				18	.2312	46.24	si
3				19	.2312	46.24	si
3				20	.2312	46.24	si
3				21	.2312	46.24	si
3				22	.2312	46.24	si
3				23	.587	117.4	si
3				24	.587	117.4	si
3				25	.587	117.4	si
3				26	.587	117.4	si
3				27	.587	117.4	si
3				28	.587	117.4	si
3				29	.587	117.4	si
3				30	.587	117.4	si
3				31	.587	117.4	si
3				32	.587	117.4	si
3				33	.587	117.4	si
3				34	.587	117.4	si
3				35	.587	117.4	si
3				36	.587	117.4	si
3				37	.587	117.4	si
3				38	.587	117.4	si
3				39	.587	117.4	si
3				40	.587	117.4	si
3				41	.587	117.4	si
3				42	.587	117.4	si
3				43	.587	117.4	si
3				44	.587	117.4	si
3				45	-.4145	-82.9	si
3				46	-.4145	-82.9	si
3				47	-.4145	-82.9	si
3				48	-.4145	-82.9	si
3				49	-.4145	-82.9	si
3				50	-.4145	-82.9	si
3				51	-.4145	-82.9	si
3				52	-.4145	-82.9	si

3				53	-.4145	-82.9	si
3				54	-.4145	-82.9	si
3				55	-.4145	-82.9	si
3				56	-.4145	-82.9	si
3				57	-.4145	-82.9	si
3				58	-.4145	-82.9	si
4	1- 1	1.2438	0.	1	.6593	131.85	si
4	1- 2	1.2438	0.	2	.6593	131.85	si
4	1- 3	-.354	-4.55	3	.6593	131.85	si
4	1- 4	-.354	-4.55	4	.6593	131.85	si
4				5	.6593	131.85	si
4				6	.6593	131.85	si
4				7	.6593	131.85	si
4				8	.6593	131.85	si
4				9	.6593	131.85	si
4				10	.6593	131.85	si
4				11	.6593	131.85	si
4				12	.6593	131.85	si
4				13	.6593	131.85	si
4				14	.6593	131.85	si
4				15	.6593	131.85	si
4				16	.6593	131.85	si
4				17	.6593	131.85	si
4				18	.6593	131.85	si
4				19	.6593	131.85	si
4				20	.6593	131.85	si
4				21	.6593	131.85	si
4				22	.6593	131.85	si
4				23	1.1854	237.08	si
4				24	1.1854	237.08	si
4				25	1.1854	237.08	si
4				26	1.1854	237.08	si
4				27	1.1854	237.08	si
4				28	1.1854	237.08	si
4				29	1.1854	237.08	si
4				30	1.1854	237.08	si
4				31	1.1854	237.08	si
4				32	1.1854	237.08	si
4				33	1.1854	237.08	si
4				34	1.1854	237.08	si
4				35	1.1854	237.08	si
4				36	1.1854	237.08	si
4				37	1.1854	237.08	si
4				38	1.1854	237.08	si
4				39	1.1854	237.08	si
4				40	1.1854	237.08	si
4				41	1.1854	237.08	si
4				42	1.1854	237.08	si
4				43	1.1854	237.08	si
4				44	1.1854	237.08	si
4				45	-.2955	-59.11	si
4				46	-.2955	-59.11	si
4				47	-.2955	-59.11	si
4				48	-.2955	-59.11	si
4				49	-.2955	-59.11	si
4				50	-.2955	-59.11	si
4				51	-.2955	-59.11	si
4				52	-.2955	-59.11	si
4				53	-.2955	-59.11	si
4				54	-.2955	-59.11	si
4				55	-.2955	-59.11	si
4				56	-.2955	-59.11	si
4				57	-.2955	-59.11	si
4				58	-.2955	-59.11	si

Descrizione : Pulvino 3

SOLLECITAZIONI AGENTI

Sforzi normali applicati in $y = 29.55$ (baricentro CLS)

Convenzioni: N + trazione; Mz + fib.inferiori tese; My + fib.sinistra tese.

N.	N	Mz	My	Descrizione
1	-29.82	-1769.3066	-1526.0302	Caso 2.1
2	40.79	-974.8072	2090.455	Caso 13.1
3	-159.07	-1152.774	-8139.703	Caso 7.20
4	50.14	-1132.9552	2554.7423	Caso 7.13

RISULTATI

Piani di equilibrio ($\epsilon = \mu z + \lambda$):

Sol.	μz	μy	λ
1.	.00002566692	0.	-.00036570574
2.	.00001406844	0.	-.00018851755
3.	.00001622568	0.	-.00023791648
4.	.00001639947	0.	-.00022094267

Deformazioni sui materiali:

Cls					Acciaio lento					
sol	vert.	D	cls	S cls	Ve	ferro	D	ferri	S ferri	Ve
1	1- 1		1.4451	0.	si	1	.6751	135.02	si	
1	1- 2		1.4451	0.	si	2	.6751	135.02	si	
1	1- 3		-.6596	-7.77	si	3	.6751	135.02	si	
1	1- 4		-.6596	-7.77	si	4	.6751	135.02	si	
1						5	.6751	135.02	si	
1						6	.6751	135.02	si	
1						7	.6751	135.02	si	
1						8	.6751	135.02	si	
1						9	.6751	135.02	si	
1						10	.6751	135.02	si	

4	31	.8868	177.37	si
4	32	.8868	177.37	si
4	33	.8868	177.37	si
4	34	.8868	177.37	si
4	35	.8868	177.37	si
4	36	.8868	177.37	si
4	37	.8868	177.37	si
4	38	.8868	177.37	si
4	39	.8868	177.37	si
4	40	.8868	177.37	si
4	41	.8868	177.37	si
4	42	.8868	177.37	si
4	43	.8868	177.37	si
4	44	.8868	177.37	si
4	45	-.3595	-71.9	si
4	46	-.3595	-71.9	si
4	47	-.3595	-71.9	si
4	48	-.3595	-71.9	si
4	49	-.3595	-71.9	si
4	50	-.3595	-71.9	si
4	51	-.3595	-71.9	si
4	52	-.3595	-71.9	si
4	53	-.3595	-71.9	si
4	54	-.3595	-71.9	si
4	55	-.3595	-71.9	si
4	56	-.3595	-71.9	si
4	57	-.3595	-71.9	si
4	58	-.3595	-71.9	si

Descrizione : Pulvino 4

SOLLECITAZIONI AGENTI

Sforzi normali applicati in y= 29.55 (baricentro CLS)
 Convenzioni: N + trazione; Mz + fib.inferiori tese; My + fib.sinistra tese.

N.	N	Mz	My	Descrizione
1	-15.86	-1770.3612	-1221.2203	Caso 2.1
2	-159.93	-1745.3216	-12298.8966	Caso 2.2
3	41.74	-975.9903	3208.6309	Caso 13.1

RISULTATI

Piani di equilibrio (eps= muz * y + muy * z + lam):

Sol.	muz	muy	lambda
1.	.00002571285	0.	-.00036504981
2.	.00002502586	0.	-.0003684895
3.	.0000140878	0.	-.00018870342

Deformazioni sui materiali:

sol	vert.	CLS		Ve	Acciaio lento			
		D cls	S cls		ferro	D ferri	S ferri	Ve
1	1- 1	1.449	0.	si	1	.6776	135.52	si
1	1- 2	1.449	0.	si	2	.6776	135.52	si
1	1- 3	-.6595	-7.77	si	3	.6776	135.52	si
1	1- 4	-.6595	-7.77	si	4	.6776	135.52	si
1					5	.6776	135.52	si
1					6	.6776	135.52	si
1					7	.6776	135.52	si
1					8	.6776	135.52	si
1					9	.6776	135.52	si
1					10	.6776	135.52	si
1					11	.6776	135.52	si
1					12	.6776	135.52	si
1					13	.6776	135.52	si
1					14	.6776	135.52	si
1					15	.6776	135.52	si
1					16	.6776	135.52	si
1					17	.6776	135.52	si
1					18	.6776	135.52	si
1					19	.6776	135.52	si
1					20	.6776	135.52	si
1					21	.6776	135.52	si
1					22	.6776	135.52	si
1					23	1.3719	274.37	si
1					24	1.3719	274.37	si
1					25	1.3719	274.37	si
1					26	1.3719	274.37	si
1					27	1.3719	274.37	si
1					28	1.3719	274.37	si
1					29	1.3719	274.37	si
1					30	1.3719	274.37	si
1					31	1.3719	274.37	si
1					32	1.3719	274.37	si
1					33	1.3719	274.37	si
1					34	1.3719	274.37	si
1					35	1.3719	274.37	si
1					36	1.3719	274.37	si
1					37	1.3719	274.37	si
1					38	1.3719	274.37	si
1					39	1.3719	274.37	si
1					40	1.3719	274.37	si
1					41	1.3719	274.37	si
1					42	1.3719	274.37	si
1					43	1.3719	274.37	si
1					44	1.3719	274.37	si
1					45	-.5823	-116.46	si
1					46	-.5823	-116.46	si
1					47	-.5823	-116.46	si
1					48	-.5823	-116.46	si

1				49	-.5823	-116.46	si
1				50	-.5823	-116.46	si
1				51	-.5823	-116.46	si
1				52	-.5823	-116.46	si
1				53	-.5823	-116.46	si
1				54	-.5823	-116.46	si
1				55	-.5823	-116.46	si
1				56	-.5823	-116.46	si
1				57	-.5823	-116.46	si
1				58	-.5823	-116.46	si
2	1- 1	1.3971	0.	1	.6463	129.26	si
2	1- 2	1.3971	0.	2	.6463	129.26	si
2	1- 3	-.655	-7.73	3	.6463	129.26	si
2	1- 4	-.655	-7.73	4	.6463	129.26	si
2				5	.6463	129.26	si
2				6	.6463	129.26	si
2				7	.6463	129.26	si
2				8	.6463	129.26	si
2				9	.6463	129.26	si
2				10	.6463	129.26	si
2				11	.6463	129.26	si
2				12	.6463	129.26	si
2				13	.6463	129.26	si
2				14	.6463	129.26	si
2				15	.6463	129.26	si
2				16	.6463	129.26	si
2				17	.6463	129.26	si
2				18	.6463	129.26	si
2				19	.6463	129.26	si
2				20	.6463	129.26	si
2				21	.6463	129.26	si
2				22	.6463	129.26	si
2				23	1.322	264.4	si
2				24	1.322	264.4	si
2				25	1.322	264.4	si
2				26	1.322	264.4	si
2				27	1.322	264.4	si
2				28	1.322	264.4	si
2				29	1.322	264.4	si
2				30	1.322	264.4	si
2				31	1.322	264.4	si
2				32	1.322	264.4	si
2				33	1.322	264.4	si
2				34	1.322	264.4	si
2				35	1.322	264.4	si
2				36	1.322	264.4	si
2				37	1.322	264.4	si
2				38	1.322	264.4	si
2				39	1.322	264.4	si
2				40	1.322	264.4	si
2				41	1.322	264.4	si
2				42	1.322	264.4	si
2				43	1.322	264.4	si
2				44	1.322	264.4	si
2				45	-.58	-115.99	si
2				46	-.58	-115.99	si
2				47	-.58	-115.99	si
2				48	-.58	-115.99	si
2				49	-.58	-115.99	si
2				50	-.58	-115.99	si
2				51	-.58	-115.99	si
2				52	-.58	-115.99	si
2				53	-.58	-115.99	si
2				54	-.58	-115.99	si
2				55	-.58	-115.99	si
2				56	-.58	-115.99	si
2				57	-.58	-115.99	si
2				58	-.58	-115.99	si
3	1- 1	.8052	0.	1	.3826	76.51	si
3	1- 2	.8052	0.	2	.3826	76.51	si
3	1- 3	-.35	-4.51	3	.3826	76.51	si
3	1- 4	-.35	-4.51	4	.3826	76.51	si
3				5	.3826	76.51	si
3				6	.3826	76.51	si
3				7	.3826	76.51	si
3				8	.3826	76.51	si
3				9	.3826	76.51	si
3				10	.3826	76.51	si
3				11	.3826	76.51	si
3				12	.3826	76.51	si
3				13	.3826	76.51	si
3				14	.3826	76.51	si
3				15	.3826	76.51	si
3				16	.3826	76.51	si
3				17	.3826	76.51	si
3				18	.3826	76.51	si
3				19	.3826	76.51	si
3				20	.3826	76.51	si
3				21	.3826	76.51	si
3				22	.3826	76.51	si
3				23	.7629	152.59	si
3				24	.7629	152.59	si
3				25	.7629	152.59	si
3				26	.7629	152.59	si
3				27	.7629	152.59	si
3				28	.7629	152.59	si
3				29	.7629	152.59	si

30	.7629	152.59	si
31	.7629	152.59	si
32	.7629	152.59	si
33	.7629	152.59	si
34	.7629	152.59	si
35	.7629	152.59	si
36	.7629	152.59	si
37	.7629	152.59	si
38	.7629	152.59	si
39	.7629	152.59	si
40	.7629	152.59	si
41	.7629	152.59	si
42	.7629	152.59	si
43	.7629	152.59	si
44	.7629	152.59	si
45	-.3077	-61.55	si
46	-.3077	-61.55	si
47	-.3077	-61.55	si
48	-.3077	-61.55	si
49	-.3077	-61.55	si
50	-.3077	-61.55	si
51	-.3077	-61.55	si
52	-.3077	-61.55	si
53	-.3077	-61.55	si
54	-.3077	-61.55	si
55	-.3077	-61.55	si
56	-.3077	-61.55	si
57	-.3077	-61.55	si
58	-.3077	-61.55	si

Descrizione : Pulvino 5

SOLLECITAZIONI AGENTI

Sforzi normali applicati in y= 29.55 (baricentro CLS)
 Convenzioni: N + trazione; Mz + fib.inferiori tese; My + fib.sinistra tese.

N.	N	Mz	My	Descrizione
1	-18.39	-1769.3525	-1885.8519	Caso 2.1
2	-160.98	-1741.1537	-16503.8001	Caso 2.2
3	40.7	-976.9008	4171.7311	Caso 13.1

RISULTATI

Piani di equilibrio (eps= muz * y + muy * z + lam):

Sol.	muz	muy	lambda
1.	.00002569223	0.	-.00036498158
2.	.00002496091	0.	-.00036760154
3.	.00001409874	0.	-.00018895604

Deformazioni sui materiali:

Cls					Acciaio lento						
sol	vert.	D	cls	S	cls	Ve	ferro	D	S	ferri	Ve
1	1- 1		1.4476		0.	si	1		.6768	135.37	si
1	1- 2		1.4476		0.	si	2		.6768	135.37	si
1	1- 3		-.6592		-7.77	si	3		.6768	135.37	si
1	1- 4		-.6592		-7.77	si	4		.6768	135.37	si
1							5		.6768	135.37	si
1							6		.6768	135.37	si
1							7		.6768	135.37	si
1							8		.6768	135.37	si
1							9		.6768	135.37	si
1							10		.6768	135.37	si
1							11		.6768	135.37	si
1							12		.6768	135.37	si
1							13		.6768	135.37	si
1							14		.6768	135.37	si
1							15		.6768	135.37	si
1							16		.6768	135.37	si
1							17		.6768	135.37	si
1							18		.6768	135.37	si
1							19		.6768	135.37	si
1							20		.6768	135.37	si
1							21		.6768	135.37	si
1							22		.6768	135.37	si
1							23		1.3705	274.11	si
1							24		1.3705	274.11	si
1							25		1.3705	274.11	si
1							26		1.3705	274.11	si
1							27		1.3705	274.11	si
1							28		1.3705	274.11	si
1							29		1.3705	274.11	si
1							30		1.3705	274.11	si
1							31		1.3705	274.11	si
1							32		1.3705	274.11	si
1							33		1.3705	274.11	si
1							34		1.3705	274.11	si
1							35		1.3705	274.11	si
1							36		1.3705	274.11	si
1							37		1.3705	274.11	si
1							38		1.3705	274.11	si
1							39		1.3705	274.11	si
1							40		1.3705	274.11	si
1							41		1.3705	274.11	si
1							42		1.3705	274.11	si
1							43		1.3705	274.11	si
1							44		1.3705	274.11	si
1							45		-.5821	-116.42	si
1							46		-.5821	-116.42	si
1							47		-.5821	-116.42	si

1				48	-.5821	-116.42	si
1				49	-.5821	-116.42	si
1				50	-.5821	-116.42	si
1				51	-.5821	-116.42	si
1				52	-.5821	-116.42	si
1				53	-.5821	-116.42	si
1				54	-.5821	-116.42	si
1				55	-.5821	-116.42	si
1				56	-.5821	-116.42	si
1				57	-.5821	-116.42	si
1				58	-.5821	-116.42	si
2	1- 1	1.3934	0.	1	.6446	128.91	si
2	1- 2	1.3934	0.	2	.6446	128.91	si
2	1- 3	-.6534	-7.71	3	.6446	128.91	si
2	1- 4	-.6534	-7.71	4	.6446	128.91	si
2				5	.6446	128.91	si
2				6	.6446	128.91	si
2				7	.6446	128.91	si
2				8	.6446	128.91	si
2				9	.6446	128.91	si
2				10	.6446	128.91	si
2				11	.6446	128.91	si
2				12	.6446	128.91	si
2				13	.6446	128.91	si
2				14	.6446	128.91	si
2				15	.6446	128.91	si
2				16	.6446	128.91	si
2				17	.6446	128.91	si
2				18	.6446	128.91	si
2				19	.6446	128.91	si
2				20	.6446	128.91	si
2				21	.6446	128.91	si
2				22	.6446	128.91	si
2				23	1.3185	263.7	si
2				24	1.3185	263.7	si
2				25	1.3185	263.7	si
2				26	1.3185	263.7	si
2				27	1.3185	263.7	si
2				28	1.3185	263.7	si
2				29	1.3185	263.7	si
2				30	1.3185	263.7	si
2				31	1.3185	263.7	si
2				32	1.3185	263.7	si
2				33	1.3185	263.7	si
2				34	1.3185	263.7	si
2				35	1.3185	263.7	si
2				36	1.3185	263.7	si
2				37	1.3185	263.7	si
2				38	1.3185	263.7	si
2				39	1.3185	263.7	si
2				40	1.3185	263.7	si
2				41	1.3185	263.7	si
2				42	1.3185	263.7	si
2				43	1.3185	263.7	si
2				44	1.3185	263.7	si
2				45	-.5785	-115.7	si
2				46	-.5785	-115.7	si
2				47	-.5785	-115.7	si
2				48	-.5785	-115.7	si
2				49	-.5785	-115.7	si
2				50	-.5785	-115.7	si
2				51	-.5785	-115.7	si
2				52	-.5785	-115.7	si
2				53	-.5785	-115.7	si
2				54	-.5785	-115.7	si
2				55	-.5785	-115.7	si
2				56	-.5785	-115.7	si
2				57	-.5785	-115.7	si
2				58	-.5785	-115.7	si
3	1- 1	.8057	0.	1	.3827	76.55	si
3	1- 2	.8057	0.	2	.3827	76.55	si
3	1- 3	-.3504	-4.51	3	.3827	76.55	si
3	1- 4	-.3504	-4.51	4	.3827	76.55	si
3				5	.3827	76.55	si
3				6	.3827	76.55	si
3				7	.3827	76.55	si
3				8	.3827	76.55	si
3				9	.3827	76.55	si
3				10	.3827	76.55	si
3				11	.3827	76.55	si
3				12	.3827	76.55	si
3				13	.3827	76.55	si
3				14	.3827	76.55	si
3				15	.3827	76.55	si
3				16	.3827	76.55	si
3				17	.3827	76.55	si
3				18	.3827	76.55	si
3				19	.3827	76.55	si
3				20	.3827	76.55	si
3				21	.3827	76.55	si
3				22	.3827	76.55	si
3				23	.7634	152.68	si
3				24	.7634	152.68	si
3				25	.7634	152.68	si
3				26	.7634	152.68	si
3				27	.7634	152.68	si
3				28	.7634	152.68	si

3	29	.7634	152.68	si
3	30	.7634	152.68	si
3	31	.7634	152.68	si
3	32	.7634	152.68	si
3	33	.7634	152.68	si
3	34	.7634	152.68	si
3	35	.7634	152.68	si
3	36	.7634	152.68	si
3	37	.7634	152.68	si
3	38	.7634	152.68	si
3	39	.7634	152.68	si
3	40	.7634	152.68	si
3	41	.7634	152.68	si
3	42	.7634	152.68	si
3	43	.7634	152.68	si
3	44	.7634	152.68	si
3	45	-.3081	-61.62	si
3	46	-.3081	-61.62	si
3	47	-.3081	-61.62	si
3	48	-.3081	-61.62	si
3	49	-.3081	-61.62	si
3	50	-.3081	-61.62	si
3	51	-.3081	-61.62	si
3	52	-.3081	-61.62	si
3	53	-.3081	-61.62	si
3	54	-.3081	-61.62	si
3	55	-.3081	-61.62	si
3	56	-.3081	-61.62	si
3	57	-.3081	-61.62	si
3	58	-.3081	-61.62	si

Descrizione : Pulvino 6

SOLLECITAZIONI AGENTI

Sforzi normali applicati in y= 29.55 (baricentro CLS)
 Convenzioni: N + trazione; Mz + fib.inferiori tese; My + fib.sinistra tese.

N.	N	Mz	My	Descrizione
1	-16.06	-1769.9667	-2059.8551	Caso 2.1
2	-160.18	-1736.7025	-20528.5025	Caso 2.2
3	41.62	-978.1058	5333.0012	Caso 13.1

RISULTATI

Piani di equilibrio (eps= muz * y + muy * z + lam):

Sol.	muz	muy	lambda
1.	.00002570649	0.	-.00036497233
2.	.00002489571	0.	-.00036653284
3.	.00001411835	0.	-.00018914835

Deformazioni sui materiali:

sol	Cls			Ve	Acciaio lento			Ve
	vert.	D cls	S cls		ferro	D ferri	S ferri	
1	1- 1	1.4486	0.	si	1	.6774	135.49	si
1	1- 2	1.4486	0.	si	2	.6774	135.49	si
1	1- 3	-.6593	-7.77	si	3	.6774	135.49	si
1	1- 4	-.6593	-7.77	si	4	.6774	135.49	si
1					5	.6774	135.49	si
1					6	.6774	135.49	si
1					7	.6774	135.49	si
1					8	.6774	135.49	si
1					9	.6774	135.49	si
1					10	.6774	135.49	si
1					11	.6774	135.49	si
1					12	.6774	135.49	si
1					13	.6774	135.49	si
1					14	.6774	135.49	si
1					15	.6774	135.49	si
1					16	.6774	135.49	si
1					17	.6774	135.49	si
1					18	.6774	135.49	si
1					19	.6774	135.49	si
1					20	.6774	135.49	si
1					21	.6774	135.49	si
1					22	.6774	135.49	si
1					23	1.3715	274.3	si
1					24	1.3715	274.3	si
1					25	1.3715	274.3	si
1					26	1.3715	274.3	si
1					27	1.3715	274.3	si
1					28	1.3715	274.3	si
1					29	1.3715	274.3	si
1					30	1.3715	274.3	si
1					31	1.3715	274.3	si
1					32	1.3715	274.3	si
1					33	1.3715	274.3	si
1					34	1.3715	274.3	si
1					35	1.3715	274.3	si
1					36	1.3715	274.3	si
1					37	1.3715	274.3	si
1					38	1.3715	274.3	si
1					39	1.3715	274.3	si
1					40	1.3715	274.3	si
1					41	1.3715	274.3	si
1					42	1.3715	274.3	si
1					43	1.3715	274.3	si
1					44	1.3715	274.3	si
1					45	-.5822	-116.44	si
1					46	-.5822	-116.44	si

1					47	-.5822	-116.44	si
1					48	-.5822	-116.44	si
1					49	-.5822	-116.44	si
1					50	-.5822	-116.44	si
1					51	-.5822	-116.44	si
1					52	-.5822	-116.44	si
1					53	-.5822	-116.44	si
1					54	-.5822	-116.44	si
1					55	-.5822	-116.44	si
1					56	-.5822	-116.44	si
1					57	-.5822	-116.44	si
1					58	-.5822	-116.44	si
2	1- 1	1.3899	0.	si	1	.643	128.6	si
2	1- 2	1.3899	0.	si	2	.643	128.6	si
2	1- 3	-.6516	-7.7	si	3	.643	128.6	si
2	1- 4	-.6516	-7.7	si	4	.643	128.6	si
2					5	.643	128.6	si
2					6	.643	128.6	si
2					7	.643	128.6	si
2					8	.643	128.6	si
2					9	.643	128.6	si
2					10	.643	128.6	si
2					11	.643	128.6	si
2					12	.643	128.6	si
2					13	.643	128.6	si
2					14	.643	128.6	si
2					15	.643	128.6	si
2					16	.643	128.6	si
2					17	.643	128.6	si
2					18	.643	128.6	si
2					19	.643	128.6	si
2					20	.643	128.6	si
2					21	.643	128.6	si
2					22	.643	128.6	si
2					23	1.3152	263.03	si
2					24	1.3152	263.03	si
2					25	1.3152	263.03	si
2					26	1.3152	263.03	si
2					27	1.3152	263.03	si
2					28	1.3152	263.03	si
2					29	1.3152	263.03	si
2					30	1.3152	263.03	si
2					31	1.3152	263.03	si
2					32	1.3152	263.03	si
2					33	1.3152	263.03	si
2					34	1.3152	263.03	si
2					35	1.3152	263.03	si
2					36	1.3152	263.03	si
2					37	1.3152	263.03	si
2					38	1.3152	263.03	si
2					39	1.3152	263.03	si
2					40	1.3152	263.03	si
2					41	1.3152	263.03	si
2					42	1.3152	263.03	si
2					43	1.3152	263.03	si
2					44	1.3152	263.03	si
2					45	-.5769	-115.38	si
2					46	-.5769	-115.38	si
2					47	-.5769	-115.38	si
2					48	-.5769	-115.38	si
2					49	-.5769	-115.38	si
2					50	-.5769	-115.38	si
2					51	-.5769	-115.38	si
2					52	-.5769	-115.38	si
2					53	-.5769	-115.38	si
2					54	-.5769	-115.38	si
2					55	-.5769	-115.38	si
2					56	-.5769	-115.38	si
2					57	-.5769	-115.38	si
2					58	-.5769	-115.38	si
3	1- 1	.8069	0.	si	1	.3834	76.67	si
3	1- 2	.8069	0.	si	2	.3834	76.67	si
3	1- 3	-.3508	-4.52	si	3	.3834	76.67	si
3	1- 4	-.3508	-4.52	si	4	.3834	76.67	si
3					5	.3834	76.67	si
3					6	.3834	76.67	si
3					7	.3834	76.67	si
3					8	.3834	76.67	si
3					9	.3834	76.67	si
3					10	.3834	76.67	si
3					11	.3834	76.67	si
3					12	.3834	76.67	si
3					13	.3834	76.67	si
3					14	.3834	76.67	si
3					15	.3834	76.67	si
3					16	.3834	76.67	si
3					17	.3834	76.67	si
3					18	.3834	76.67	si
3					19	.3834	76.67	si
3					20	.3834	76.67	si
3					21	.3834	76.67	si
3					22	.3834	76.67	si
3					23	.7645	152.91	si
3					24	.7645	152.91	si
3					25	.7645	152.91	si
3					26	.7645	152.91	si
3					27	.7645	152.91	si

3	28	.7645	152.91	si
3	29	.7645	152.91	si
3	30	.7645	152.91	si
3	31	.7645	152.91	si
3	32	.7645	152.91	si
3	33	.7645	152.91	si
3	34	.7645	152.91	si
3	35	.7645	152.91	si
3	36	.7645	152.91	si
3	37	.7645	152.91	si
3	38	.7645	152.91	si
3	39	.7645	152.91	si
3	40	.7645	152.91	si
3	41	.7645	152.91	si
3	42	.7645	152.91	si
3	43	.7645	152.91	si
3	44	.7645	152.91	si
3	45	-.3084	-61.69	si
3	46	-.3084	-61.69	si
3	47	-.3084	-61.69	si
3	48	-.3084	-61.69	si
3	49	-.3084	-61.69	si
3	50	-.3084	-61.69	si
3	51	-.3084	-61.69	si
3	52	-.3084	-61.69	si
3	53	-.3084	-61.69	si
3	54	-.3084	-61.69	si
3	55	-.3084	-61.69	si
3	56	-.3084	-61.69	si
3	57	-.3084	-61.69	si
3	58	-.3084	-61.69	si

Descrizione : Pulvino 7

SOLLECITAZIONI AGENTI

Sforzi normali applicati in y= 29.55

Convenzioni: N + trazione; Mz + fib.inferiori tese; My + fib.sinistra tese.

N.	N	Mz	My	Descrizione
1	-20.83	-1779.9301	-3202.5579	Caso 2.1
2	-163.18	-1743.9341	-25093.564	Caso 2.2
3	40.53	-978.9531	6232.3143	Caso 13.1

RISULTATI

Piani di equilibrio (eps= muz * y +muy * z + lam):

Sol.	muz	muy	lambda
1.	.0000258461	0.	-.00036756269
2.	.00002499799	0.	-.00036837649
3.	.00001412825	0.	-.00018939104

Deformazioni sui materiali:

sol	cls				Acciaio lento					
	vert.	D	cls	S	cls	Ve	ferro	D	S	ferri
1	1- 1		1.4559	0.	si	1	.6805		136.1	si
1	1- 2		1.4559	0.	si	2	.6805		136.1	si
1	1- 3		-.6635	-7.81	si	3	.6805		136.1	si
1	1- 4		-.6635	-7.81	si	4	.6805		136.1	si
1						5	.6805		136.1	si
1						6	.6805		136.1	si
1						7	.6805		136.1	si
1						8	.6805		136.1	si
1						9	.6805		136.1	si
1						10	.6805		136.1	si
1						11	.6805		136.1	si
1						12	.6805		136.1	si
1						13	.6805		136.1	si
1						14	.6805		136.1	si
1						15	.6805		136.1	si
1						16	.6805		136.1	si
1						17	.6805		136.1	si
1						18	.6805		136.1	si
1						19	.6805		136.1	si
1						20	.6805		136.1	si
1						21	.6805		136.1	si
1						22	.6805		136.1	si
1						23	1.3783		275.67	si
1						24	1.3783		275.67	si
1						25	1.3783		275.67	si
1						26	1.3783		275.67	si
1						27	1.3783		275.67	si
1						28	1.3783		275.67	si
1						29	1.3783		275.67	si
1						30	1.3783		275.67	si
1						31	1.3783		275.67	si
1						32	1.3783		275.67	si
1						33	1.3783		275.67	si
1						34	1.3783		275.67	si
1						35	1.3783		275.67	si
1						36	1.3783		275.67	si
1						37	1.3783		275.67	si
1						38	1.3783		275.67	si
1						39	1.3783		275.67	si
1						40	1.3783		275.67	si
1						41	1.3783		275.67	si
1						42	1.3783		275.67	si
1						43	1.3783		275.67	si
1						44	1.3783		275.67	si
1						45	-.586		-117.19	si

3	27	.765	152.99	si
3	28	.765	152.99	si
3	29	.765	152.99	si
3	30	.765	152.99	si
3	31	.765	152.99	si
3	32	.765	152.99	si
3	33	.765	152.99	si
3	34	.765	152.99	si
3	35	.765	152.99	si
3	36	.765	152.99	si
3	37	.765	152.99	si
3	38	.765	152.99	si
3	39	.765	152.99	si
3	40	.765	152.99	si
3	41	.765	152.99	si
3	42	.765	152.99	si
3	43	.765	152.99	si
3	44	.765	152.99	si
3	45	-.3088	-61.75	si
3	46	-.3088	-61.75	si
3	47	-.3088	-61.75	si
3	48	-.3088	-61.75	si
3	49	-.3088	-61.75	si
3	50	-.3088	-61.75	si
3	51	-.3088	-61.75	si
3	52	-.3088	-61.75	si
3	53	-.3088	-61.75	si
3	54	-.3088	-61.75	si
3	55	-.3088	-61.75	si
3	56	-.3088	-61.75	si
3	57	-.3088	-61.75	si
3	58	-.3088	-61.75	si

Descrizione : Pulvino 8

SOLLECITAZIONI AGENTI

Sforzi normali applicati in y= 29.55 (baricentro CLS)
 Convenzioni: N + trazione; Mz + fib.inferiori tese; My + fib.sinistra tese.

N.	N	Mz	My	Descrizione
1	-20.99	-1791.1745	-3766.5241	Caso 2.1
2	-163.98	-1751.3749	-29421.0883	Caso 2.2
3	41.43	-980.1965	7431.3618	Caso 13.1

RISULTATI

Piani di equilibrio (eps= muz * y + muy * z + lam):

Sol.	muz	muy	lambda
1.	.00002601499	0.	-.00037015387
2.	.00002510819	0.	-.00037013133
3.	.00001414838	0.	-.00018959259

Deformazioni sui materiali:

sol	CLS				Acciaio lento			
	vert.	D cls	S cls	Ve	ferro	D ferri	S ferri	Ve
1	1- 1	1.4652	0.	si	1	.6848	136.95	si
1	1- 2	1.4652	0.	si	2	.6848	136.95	si
1	1- 3	-.668	-7.85	si	3	.6848	136.95	si
1	1- 4	-.668	-7.85	si	4	.6848	136.95	si
1					5	.6848	136.95	si
1					6	.6848	136.95	si
1					7	.6848	136.95	si
1					8	.6848	136.95	si
1					9	.6848	136.95	si
1					10	.6848	136.95	si
1					11	.6848	136.95	si
1					12	.6848	136.95	si
1					13	.6848	136.95	si
1					14	.6848	136.95	si
1					15	.6848	136.95	si
1					16	.6848	136.95	si
1					17	.6848	136.95	si
1					18	.6848	136.95	si
1					19	.6848	136.95	si
1					20	.6848	136.95	si
1					21	.6848	136.95	si
1					22	.6848	136.95	si
1					23	1.3872	277.43	si
1					24	1.3872	277.43	si
1					25	1.3872	277.43	si
1					26	1.3872	277.43	si
1					27	1.3872	277.43	si
1					28	1.3872	277.43	si
1					29	1.3872	277.43	si
1					30	1.3872	277.43	si
1					31	1.3872	277.43	si
1					32	1.3872	277.43	si
1					33	1.3872	277.43	si
1					34	1.3872	277.43	si
1					35	1.3872	277.43	si
1					36	1.3872	277.43	si
1					37	1.3872	277.43	si
1					38	1.3872	277.43	si
1					39	1.3872	277.43	si
1					40	1.3872	277.43	si
1					41	1.3872	277.43	si
1					42	1.3872	277.43	si
1					43	1.3872	277.43	si
1					44	1.3872	277.43	si

1				45	-.59	-118.	si
1				46	-.59	-118.	si
1				47	-.59	-118.	si
1				48	-.59	-118.	si
1				49	-.59	-118.	si
1				50	-.59	-118.	si
1				51	-.59	-118.	si
1				52	-.59	-118.	si
1				53	-.59	-118.	si
1				54	-.59	-118.	si
1				55	-.59	-118.	si
1				56	-.59	-118.	si
1				57	-.59	-118.	si
1				58	-.59	-118.	si
2	1- 1	1.4013	0.	1	.648	129.6	si
2	1- 2	1.4013	0.	2	.648	129.6	si
2	1- 3	-.6576	-7.75	3	.648	129.6	si
2	1- 4	-.6576	-7.75	4	.648	129.6	si
2				5	.648	129.6	si
2				6	.648	129.6	si
2				7	.648	129.6	si
2				8	.648	129.6	si
2				9	.648	129.6	si
2				10	.648	129.6	si
2				11	.648	129.6	si
2				12	.648	129.6	si
2				13	.648	129.6	si
2				14	.648	129.6	si
2				15	.648	129.6	si
2				16	.648	129.6	si
2				17	.648	129.6	si
2				18	.648	129.6	si
2				19	.648	129.6	si
2				20	.648	129.6	si
2				21	.648	129.6	si
2				22	.648	129.6	si
2				23	1.3259	265.19	si
2				24	1.3259	265.19	si
2				25	1.3259	265.19	si
2				26	1.3259	265.19	si
2				27	1.3259	265.19	si
2				28	1.3259	265.19	si
2				29	1.3259	265.19	si
2				30	1.3259	265.19	si
2				31	1.3259	265.19	si
2				32	1.3259	265.19	si
2				33	1.3259	265.19	si
2				34	1.3259	265.19	si
2				35	1.3259	265.19	si
2				36	1.3259	265.19	si
2				37	1.3259	265.19	si
2				38	1.3259	265.19	si
2				39	1.3259	265.19	si
2				40	1.3259	265.19	si
2				41	1.3259	265.19	si
2				42	1.3259	265.19	si
2				43	1.3259	265.19	si
2				44	1.3259	265.19	si
2				45	-.5823	-116.46	si
2				46	-.5823	-116.46	si
2				47	-.5823	-116.46	si
2				48	-.5823	-116.46	si
2				49	-.5823	-116.46	si
2				50	-.5823	-116.46	si
2				51	-.5823	-116.46	si
2				52	-.5823	-116.46	si
2				53	-.5823	-116.46	si
2				54	-.5823	-116.46	si
2				55	-.5823	-116.46	si
2				56	-.5823	-116.46	si
2				57	-.5823	-116.46	si
2				58	-.5823	-116.46	si
3	1- 1	.8086	0.	1	.3841	76.82	si
3	1- 2	.8086	0.	2	.3841	76.82	si
3	1- 3	-.3516	-4.52	3	.3841	76.82	si
3	1- 4	-.3516	-4.52	4	.3841	76.82	si
3				5	.3841	76.82	si
3				6	.3841	76.82	si
3				7	.3841	76.82	si
3				8	.3841	76.82	si
3				9	.3841	76.82	si
3				10	.3841	76.82	si
3				11	.3841	76.82	si
3				12	.3841	76.82	si
3				13	.3841	76.82	si
3				14	.3841	76.82	si
3				15	.3841	76.82	si
3				16	.3841	76.82	si
3				17	.3841	76.82	si
3				18	.3841	76.82	si
3				19	.3841	76.82	si
3				20	.3841	76.82	si
3				21	.3841	76.82	si
3				22	.3841	76.82	si
3				23	.7661	153.23	si
3				24	.7661	153.23	si
3				25	.7661	153.23	si

1				44	1.3775	275.5	si
1				45	-.5856	-117.12	si
1				46	-.5856	-117.12	si
1				47	-.5856	-117.12	si
1				48	-.5856	-117.12	si
1				49	-.5856	-117.12	si
1				50	-.5856	-117.12	si
1				51	-.5856	-117.12	si
1				52	-.5856	-117.12	si
1				53	-.5856	-117.12	si
1				54	-.5856	-117.12	si
1				55	-.5856	-117.12	si
1				56	-.5856	-117.12	si
1				57	-.5856	-117.12	si
1				58	-.5856	-117.12	si
2	1- 1	1.388	0.	1	.642	128.39	si
2	1- 2	1.388	0.	2	.642	128.39	si
2	1- 3	-.6512	-7.69	3	.642	128.39	si
2	1- 4	-.6512	-7.69	4	.642	128.39	si
2				5	.642	128.39	si
2				6	.642	128.39	si
2				7	.642	128.39	si
2				8	.642	128.39	si
2				9	.642	128.39	si
2				10	.642	128.39	si
2				11	.642	128.39	si
2				12	.642	128.39	si
2				13	.642	128.39	si
2				14	.642	128.39	si
2				15	.642	128.39	si
2				16	.642	128.39	si
2				17	.642	128.39	si
2				18	.642	128.39	si
2				19	.642	128.39	si
2				20	.642	128.39	si
2				21	.642	128.39	si
2				22	.642	128.39	si
2				23	1.3134	262.68	si
2				24	1.3134	262.68	si
2				25	1.3134	262.68	si
2				26	1.3134	262.68	si
2				27	1.3134	262.68	si
2				28	1.3134	262.68	si
2				29	1.3134	262.68	si
2				30	1.3134	262.68	si
2				31	1.3134	262.68	si
2				32	1.3134	262.68	si
2				33	1.3134	262.68	si
2				34	1.3134	262.68	si
2				35	1.3134	262.68	si
2				36	1.3134	262.68	si
2				37	1.3134	262.68	si
2				38	1.3134	262.68	si
2				39	1.3134	262.68	si
2				40	1.3134	262.68	si
2				41	1.3134	262.68	si
2				42	1.3134	262.68	si
2				43	1.3134	262.68	si
2				44	1.3134	262.68	si
2				45	-.5766	-115.33	si
2				46	-.5766	-115.33	si
2				47	-.5766	-115.33	si
2				48	-.5766	-115.33	si
2				49	-.5766	-115.33	si
2				50	-.5766	-115.33	si
2				51	-.5766	-115.33	si
2				52	-.5766	-115.33	si
2				53	-.5766	-115.33	si
2				54	-.5766	-115.33	si
2				55	-.5766	-115.33	si
2				56	-.5766	-115.33	si
2				57	-.5766	-115.33	si
2				58	-.5766	-115.33	si
3	1- 1	.809	0.	1	.3843	76.85	si
3	1- 2	.809	0.	2	.3843	76.85	si
3	1- 3	-.3519	-4.53	3	.3843	76.85	si
3	1- 4	-.3519	-4.53	4	.3843	76.85	si
3				5	.3843	76.85	si
3				6	.3843	76.85	si
3				7	.3843	76.85	si
3				8	.3843	76.85	si
3				9	.3843	76.85	si
3				10	.3843	76.85	si
3				11	.3843	76.85	si
3				12	.3843	76.85	si
3				13	.3843	76.85	si
3				14	.3843	76.85	si
3				15	.3843	76.85	si
3				16	.3843	76.85	si
3				17	.3843	76.85	si
3				18	.3843	76.85	si
3				19	.3843	76.85	si
3				20	.3843	76.85	si
3				21	.3843	76.85	si
3				22	.3843	76.85	si
3				23	.7665	153.3	si
3				24	.7665	153.3	si

3	25	.7665	153.3	si
3	26	.7665	153.3	si
3	27	.7665	153.3	si
3	28	.7665	153.3	si
3	29	.7665	153.3	si
3	30	.7665	153.3	si
3	31	.7665	153.3	si
3	32	.7665	153.3	si
3	33	.7665	153.3	si
3	34	.7665	153.3	si
3	35	.7665	153.3	si
3	36	.7665	153.3	si
3	37	.7665	153.3	si
3	38	.7665	153.3	si
3	39	.7665	153.3	si
3	40	.7665	153.3	si
3	41	.7665	153.3	si
3	42	.7665	153.3	si
3	43	.7665	153.3	si
3	44	.7665	153.3	si
3	45	-.3095	-61.89	si
3	46	-.3095	-61.89	si
3	47	-.3095	-61.89	si
3	48	-.3095	-61.89	si
3	49	-.3095	-61.89	si
3	50	-.3095	-61.89	si
3	51	-.3095	-61.89	si
3	52	-.3095	-61.89	si
3	53	-.3095	-61.89	si
3	54	-.3095	-61.89	si
3	55	-.3095	-61.89	si
3	56	-.3095	-61.89	si
3	57	-.3095	-61.89	si
3	58	-.3095	-61.89	si

Descrizione : Pulvino 10

SOLLECITAZIONI AGENTI

Sforzi normali applicati in y= 29.55 (baricentro CLS)

Convenzioni: N + trazione; Mz + fib.inferiori tese; My + fib.sinistra tese.

N.	N	Mz	My	Descrizione
1	-17.89	-1767.4454	-4586.3427	Caso 2.1
2	-160.07	-1720.8836	-41026.4677	Caso 2.2
3	41.17	-982.2551	10551.7361	Caso 13.1

RISULTATI

Piani di equilibrio (eps= muz * y + muy * z + lam):

Sol.	muz	muy	lambda
1.	.00002566463	0.	-.00036451275
2.	.0000246582	0.	-.00036291193
3.	.00001417779	0.	-.00019003464

Deformazioni sui materiali:

sol	Cls				Acciaio lento				
	vert.	D	cls	S cls	ferro	D	ferri	S	ferri
1	1- 1		1.4461	0.	1	.6762	135.24	si	
1	1- 2		1.4461	0.	2	.6762	135.24	si	
1	1- 3		-.6584	-7.76	3	.6762	135.24	si	
1	1- 4		-.6584	-7.76	4	.6762	135.24	si	
1					5	.6762	135.24	si	
1					6	.6762	135.24	si	
1					7	.6762	135.24	si	
1					8	.6762	135.24	si	
1					9	.6762	135.24	si	
1					10	.6762	135.24	si	
1					11	.6762	135.24	si	
1					12	.6762	135.24	si	
1					13	.6762	135.24	si	
1					14	.6762	135.24	si	
1					15	.6762	135.24	si	
1					16	.6762	135.24	si	
1					17	.6762	135.24	si	
1					18	.6762	135.24	si	
1					19	.6762	135.24	si	
1					20	.6762	135.24	si	
1					21	.6762	135.24	si	
1					22	.6762	135.24	si	
1					23	1.3691	273.83	si	
1					24	1.3691	273.83	si	
1					25	1.3691	273.83	si	
1					26	1.3691	273.83	si	
1					27	1.3691	273.83	si	
1					28	1.3691	273.83	si	
1					29	1.3691	273.83	si	
1					30	1.3691	273.83	si	
1					31	1.3691	273.83	si	
1					32	1.3691	273.83	si	
1					33	1.3691	273.83	si	
1					34	1.3691	273.83	si	
1					35	1.3691	273.83	si	
1					36	1.3691	273.83	si	
1					37	1.3691	273.83	si	
1					38	1.3691	273.83	si	
1					39	1.3691	273.83	si	
1					40	1.3691	273.83	si	
1					41	1.3691	273.83	si	
1					42	1.3691	273.83	si	

1				43	1.3691	273.83	si
1				44	1.3691	273.83	si
1				45	-.5814	-116.28	si
1				46	-.5814	-116.28	si
1				47	-.5814	-116.28	si
1				48	-.5814	-116.28	si
1				49	-.5814	-116.28	si
1				50	-.5814	-116.28	si
1				51	-.5814	-116.28	si
1				52	-.5814	-116.28	si
1				53	-.5814	-116.28	si
1				54	-.5814	-116.28	si
1				55	-.5814	-116.28	si
1				56	-.5814	-116.28	si
1				57	-.5814	-116.28	si
1				58	-.5814	-116.28	si
2	1- 1	1.3767	0.	1	.637	127.4	si
2	1- 2	1.3767	0.	2	.637	127.4	si
2	1- 3	-.6452	-7.64	3	.637	127.4	si
2	1- 4	-.6452	-7.64	4	.637	127.4	si
2				5	.637	127.4	si
2				6	.637	127.4	si
2				7	.637	127.4	si
2				8	.637	127.4	si
2				9	.637	127.4	si
2				10	.637	127.4	si
2				11	.637	127.4	si
2				12	.637	127.4	si
2				13	.637	127.4	si
2				14	.637	127.4	si
2				15	.637	127.4	si
2				16	.637	127.4	si
2				17	.637	127.4	si
2				18	.637	127.4	si
2				19	.637	127.4	si
2				20	.637	127.4	si
2				21	.637	127.4	si
2				22	.637	127.4	si
2				23	1.3027	260.55	si
2				24	1.3027	260.55	si
2				25	1.3027	260.55	si
2				26	1.3027	260.55	si
2				27	1.3027	260.55	si
2				28	1.3027	260.55	si
2				29	1.3027	260.55	si
2				30	1.3027	260.55	si
2				31	1.3027	260.55	si
2				32	1.3027	260.55	si
2				33	1.3027	260.55	si
2				34	1.3027	260.55	si
2				35	1.3027	260.55	si
2				36	1.3027	260.55	si
2				37	1.3027	260.55	si
2				38	1.3027	260.55	si
2				39	1.3027	260.55	si
2				40	1.3027	260.55	si
2				41	1.3027	260.55	si
2				42	1.3027	260.55	si
2				43	1.3027	260.55	si
2				44	1.3027	260.55	si
2				45	-.5713	-114.25	si
2				46	-.5713	-114.25	si
2				47	-.5713	-114.25	si
2				48	-.5713	-114.25	si
2				49	-.5713	-114.25	si
2				50	-.5713	-114.25	si
2				51	-.5713	-114.25	si
2				52	-.5713	-114.25	si
2				53	-.5713	-114.25	si
2				54	-.5713	-114.25	si
2				55	-.5713	-114.25	si
2				56	-.5713	-114.25	si
2				57	-.5713	-114.25	si
2				58	-.5713	-114.25	si
3	1- 1	.8102	0.	1	.3849	76.97	si
3	1- 2	.8102	0.	2	.3849	76.97	si
3	1- 3	-.3524	-4.53	3	.3849	76.97	si
3	1- 4	-.3524	-4.53	4	.3849	76.97	si
3				5	.3849	76.97	si
3				6	.3849	76.97	si
3				7	.3849	76.97	si
3				8	.3849	76.97	si
3				9	.3849	76.97	si
3				10	.3849	76.97	si
3				11	.3849	76.97	si
3				12	.3849	76.97	si
3				13	.3849	76.97	si
3				14	.3849	76.97	si
3				15	.3849	76.97	si
3				16	.3849	76.97	si
3				17	.3849	76.97	si
3				18	.3849	76.97	si
3				19	.3849	76.97	si
3				20	.3849	76.97	si
3				21	.3849	76.97	si
3				22	.3849	76.97	si
3				23	.7677	153.54	si

3	24	.7677	153.54	si
3	25	.7677	153.54	si
3	26	.7677	153.54	si
3	27	.7677	153.54	si
3	28	.7677	153.54	si
3	29	.7677	153.54	si
3	30	.7677	153.54	si
3	31	.7677	153.54	si
3	32	.7677	153.54	si
3	33	.7677	153.54	si
3	34	.7677	153.54	si
3	35	.7677	153.54	si
3	36	.7677	153.54	si
3	37	.7677	153.54	si
3	38	.7677	153.54	si
3	39	.7677	153.54	si
3	40	.7677	153.54	si
3	41	.7677	153.54	si
3	42	.7677	153.54	si
3	43	.7677	153.54	si
3	44	.7677	153.54	si
3	45	-.3098	-61.97	si
3	46	-.3098	-61.97	si
3	47	-.3098	-61.97	si
3	48	-.3098	-61.97	si
3	49	-.3098	-61.97	si
3	50	-.3098	-61.97	si
3	51	-.3098	-61.97	si
3	52	-.3098	-61.97	si
3	53	-.3098	-61.97	si
3	54	-.3098	-61.97	si
3	55	-.3098	-61.97	si
3	56	-.3098	-61.97	si
3	57	-.3098	-61.97	si
3	58	-.3098	-61.97	si

Descrizione : Pulvino 11

SOLLECITAZIONI AGENTI

Sforzi normali applicati in y= 29.55

Convenzioni: N + trazione; Mz + fib.inferiori tese; My + fib.sinistra tese.

N.	N	Mz	My	Descrizione
1	-18.96	-1767.1348	-5343.9319	Caso 2.1
2	-163.14	-1715.2507	-45993.1162	Caso 2.2
3	39.98	-982.9469	11270.6413	Caso 13.1

RISULTATI

Piani di equilibrio (eps= muz * y +muy * z + lam):

Sol.	muz	muy	lambda
1.	.00002565765	0.	-.00036451045
2.	.00002456696	0.	-.00036181977
3.	.00001418521	0.	-.00019025143

Deformazioni sui materiali:

sol	ClS				Acciaio lento					
	vert.	D	clS	S	clS	Ve	ferro	D	S	ferri
1	1- 1		1.4456	0.	si	1	.6759		135.18	si
1	1- 2		1.4456	0.	si	2	.6759		135.18	si
1	1- 3		-.6583	-7.76	si	3	.6759		135.18	si
1	1- 4		-.6583	-7.76	si	4	.6759		135.18	si
1						5	.6759		135.18	si
1						6	.6759		135.18	si
1						7	.6759		135.18	si
1						8	.6759		135.18	si
1						9	.6759		135.18	si
1						10	.6759		135.18	si
1						11	.6759		135.18	si
1						12	.6759		135.18	si
1						13	.6759		135.18	si
1						14	.6759		135.18	si
1						15	.6759		135.18	si
1						16	.6759		135.18	si
1						17	.6759		135.18	si
1						18	.6759		135.18	si
1						19	.6759		135.18	si
1						20	.6759		135.18	si
1						21	.6759		135.18	si
1						22	.6759		135.18	si
1						23	1.3687		273.73	si
1						24	1.3687		273.73	si
1						25	1.3687		273.73	si
1						26	1.3687		273.73	si
1						27	1.3687		273.73	si
1						28	1.3687		273.73	si
1						29	1.3687		273.73	si
1						30	1.3687		273.73	si
1						31	1.3687		273.73	si
1						32	1.3687		273.73	si
1						33	1.3687		273.73	si
1						34	1.3687		273.73	si
1						35	1.3687		273.73	si
1						36	1.3687		273.73	si
1						37	1.3687		273.73	si
1						38	1.3687		273.73	si
1						39	1.3687		273.73	si
1						40	1.3687		273.73	si
1						41	1.3687		273.73	si

1				42	1.3687	273.73	si
1				43	1.3687	273.73	si
1				44	1.3687	273.73	si
1				45	-.5813	-116.26	si
1				46	-.5813	-116.26	si
1				47	-.5813	-116.26	si
1				48	-.5813	-116.26	si
1				49	-.5813	-116.26	si
1				50	-.5813	-116.26	si
1				51	-.5813	-116.26	si
1				52	-.5813	-116.26	si
1				53	-.5813	-116.26	si
1				54	-.5813	-116.26	si
1				55	-.5813	-116.26	si
1				56	-.5813	-116.26	si
1				57	-.5813	-116.26	si
1				58	-.5813	-116.26	si
2	1- 1	1.3714	0.	1	.6344	126.87	si
2	1- 2	1.3714	0.	2	.6344	126.87	si
2	1- 3	-.6431	-7.62	3	.6344	126.87	si
2	1- 4	-.6431	-7.62	4	.6344	126.87	si
2				5	.6344	126.87	si
2				6	.6344	126.87	si
2				7	.6344	126.87	si
2				8	.6344	126.87	si
2				9	.6344	126.87	si
2				10	.6344	126.87	si
2				11	.6344	126.87	si
2				12	.6344	126.87	si
2				13	.6344	126.87	si
2				14	.6344	126.87	si
2				15	.6344	126.87	si
2				16	.6344	126.87	si
2				17	.6344	126.87	si
2				18	.6344	126.87	si
2				19	.6344	126.87	si
2				20	.6344	126.87	si
2				21	.6344	126.87	si
2				22	.6344	126.87	si
2				23	1.2977	259.54	si
2				24	1.2977	259.54	si
2				25	1.2977	259.54	si
2				26	1.2977	259.54	si
2				27	1.2977	259.54	si
2				28	1.2977	259.54	si
2				29	1.2977	259.54	si
2				30	1.2977	259.54	si
2				31	1.2977	259.54	si
2				32	1.2977	259.54	si
2				33	1.2977	259.54	si
2				34	1.2977	259.54	si
2				35	1.2977	259.54	si
2				36	1.2977	259.54	si
2				37	1.2977	259.54	si
2				38	1.2977	259.54	si
2				39	1.2977	259.54	si
2				40	1.2977	259.54	si
2				41	1.2977	259.54	si
2				42	1.2977	259.54	si
2				43	1.2977	259.54	si
2				44	1.2977	259.54	si
2				45	-.5694	-113.88	si
2				46	-.5694	-113.88	si
2				47	-.5694	-113.88	si
2				48	-.5694	-113.88	si
2				49	-.5694	-113.88	si
2				50	-.5694	-113.88	si
2				51	-.5694	-113.88	si
2				52	-.5694	-113.88	si
2				53	-.5694	-113.88	si
2				54	-.5694	-113.88	si
2				55	-.5694	-113.88	si
2				56	-.5694	-113.88	si
2				57	-.5694	-113.88	si
2				58	-.5694	-113.88	si
3	1- 1	.8105	0.	1	.385	76.99	si
3	1- 2	.8105	0.	2	.385	76.99	si
3	1- 3	-.3527	-4.54	3	.385	76.99	si
3	1- 4	-.3527	-4.54	4	.385	76.99	si
3				5	.385	76.99	si
3				6	.385	76.99	si
3				7	.385	76.99	si
3				8	.385	76.99	si
3				9	.385	76.99	si
3				10	.385	76.99	si
3				11	.385	76.99	si
3				12	.385	76.99	si
3				13	.385	76.99	si
3				14	.385	76.99	si
3				15	.385	76.99	si
3				16	.385	76.99	si
3				17	.385	76.99	si
3				18	.385	76.99	si
3				19	.385	76.99	si
3				20	.385	76.99	si
3				21	.385	76.99	si
3				22	.385	76.99	si

3	23	.768	153.59	si
3	24	.768	153.59	si
3	25	.768	153.59	si
3	26	.768	153.59	si
3	27	.768	153.59	si
3	28	.768	153.59	si
3	29	.768	153.59	si
3	30	.768	153.59	si
3	31	.768	153.59	si
3	32	.768	153.59	si
3	33	.768	153.59	si
3	34	.768	153.59	si
3	35	.768	153.59	si
3	36	.768	153.59	si
3	37	.768	153.59	si
3	38	.768	153.59	si
3	39	.768	153.59	si
3	40	.768	153.59	si
3	41	.768	153.59	si
3	42	.768	153.59	si
3	43	.768	153.59	si
3	44	.768	153.59	si
3	45	-.3101	-62.02	si
3	46	-.3101	-62.02	si
3	47	-.3101	-62.02	si
3	48	-.3101	-62.02	si
3	49	-.3101	-62.02	si
3	50	-.3101	-62.02	si
3	51	-.3101	-62.02	si
3	52	-.3101	-62.02	si
3	53	-.3101	-62.02	si
3	54	-.3101	-62.02	si
3	55	-.3101	-62.02	si
3	56	-.3101	-62.02	si
3	57	-.3101	-62.02	si
3	58	-.3101	-62.02	si

Descrizione : Pulvino 12

SOLLECITAZIONI AGENTI

Sforzi normali applicati in y= 29.55

Convenzioni: N + trazione; Mz + fib.inferiori tese; My + fib.sinistra tese.

N.	N	Mz	My	Descrizione
1	-18.75	-1766.1454	-5768.1536	Caso 2.1
2	-160.8	-1712.6877	-49456.7506	Caso 2.2
3	40.75	-984.2439	12533.2292	Caso 13.1

RISULTATI

Piani di equilibrio (eps= muz * y + muy * z + lam):

Sol.	muz	muy	lambda
1.	.00002564322	0.	-.00036427046
2.	.00002453351	0.	-.00036108842
3.	.00001420583	0.	-.00019047224

Deformazioni sui materiali:

sol	vert.	cls		Ve	Acciaio lento			
		D	S		ferro	D	S	ferri
1	1- 1	1.4449	0.	si	1	.6756	135.11	si
1	1- 2	1.4449	0.	si	2	.6756	135.11	si
1	1- 3	-.6579	-7.76	si	3	.6756	135.11	si
1	1- 4	-.6579	-7.76	si	4	.6756	135.11	si
1					5	.6756	135.11	si
1					6	.6756	135.11	si
1					7	.6756	135.11	si
1					8	.6756	135.11	si
1					9	.6756	135.11	si
1					10	.6756	135.11	si
1					11	.6756	135.11	si
1					12	.6756	135.11	si
1					13	.6756	135.11	si
1					14	.6756	135.11	si
1					15	.6756	135.11	si
1					16	.6756	135.11	si
1					17	.6756	135.11	si
1					18	.6756	135.11	si
1					19	.6756	135.11	si
1					20	.6756	135.11	si
1					21	.6756	135.11	si
1					22	.6756	135.11	si
1					23	1.3679	273.59	si
1					24	1.3679	273.59	si
1					25	1.3679	273.59	si
1					26	1.3679	273.59	si
1					27	1.3679	273.59	si
1					28	1.3679	273.59	si
1					29	1.3679	273.59	si
1					30	1.3679	273.59	si
1					31	1.3679	273.59	si
1					32	1.3679	273.59	si
1					33	1.3679	273.59	si
1					34	1.3679	273.59	si
1					35	1.3679	273.59	si
1					36	1.3679	273.59	si
1					37	1.3679	273.59	si
1					38	1.3679	273.59	si
1					39	1.3679	273.59	si
1					40	1.3679	273.59	si

1					41	1.3679	273.59	si
1					42	1.3679	273.59	si
1					43	1.3679	273.59	si
1					44	1.3679	273.59	si
1					45	-.581	-116.19	si
1					46	-.581	-116.19	si
1					47	-.581	-116.19	si
1					48	-.581	-116.19	si
1					49	-.581	-116.19	si
1					50	-.581	-116.19	si
1					51	-.581	-116.19	si
1					52	-.581	-116.19	si
1					53	-.581	-116.19	si
1					54	-.581	-116.19	si
1					55	-.581	-116.19	si
1					56	-.581	-116.19	si
1					57	-.581	-116.19	si
1					58	-.581	-116.19	si
2	1- 1	1.3698	0.	si	1	.6337	126.75	si
2	1- 2	1.3698	0.	si	2	.6337	126.75	si
2	1- 3	-.642	-7.6	si	3	.6337	126.75	si
2	1- 4	-.642	-7.6	si	4	.6337	126.75	si
2					5	.6337	126.75	si
2					6	.6337	126.75	si
2					7	.6337	126.75	si
2					8	.6337	126.75	si
2					9	.6337	126.75	si
2					10	.6337	126.75	si
2					11	.6337	126.75	si
2					12	.6337	126.75	si
2					13	.6337	126.75	si
2					14	.6337	126.75	si
2					15	.6337	126.75	si
2					16	.6337	126.75	si
2					17	.6337	126.75	si
2					18	.6337	126.75	si
2					19	.6337	126.75	si
2					20	.6337	126.75	si
2					21	.6337	126.75	si
2					22	.6337	126.75	si
2					23	1.2962	259.23	si
2					24	1.2962	259.23	si
2					25	1.2962	259.23	si
2					26	1.2962	259.23	si
2					27	1.2962	259.23	si
2					28	1.2962	259.23	si
2					29	1.2962	259.23	si
2					30	1.2962	259.23	si
2					31	1.2962	259.23	si
2					32	1.2962	259.23	si
2					33	1.2962	259.23	si
2					34	1.2962	259.23	si
2					35	1.2962	259.23	si
2					36	1.2962	259.23	si
2					37	1.2962	259.23	si
2					38	1.2962	259.23	si
2					39	1.2962	259.23	si
2					40	1.2962	259.23	si
2					41	1.2962	259.23	si
2					42	1.2962	259.23	si
2					43	1.2962	259.23	si
2					44	1.2962	259.23	si
2					45	-.5684	-113.68	si
2					46	-.5684	-113.68	si
2					47	-.5684	-113.68	si
2					48	-.5684	-113.68	si
2					49	-.5684	-113.68	si
2					50	-.5684	-113.68	si
2					51	-.5684	-113.68	si
2					52	-.5684	-113.68	si
2					53	-.5684	-113.68	si
2					54	-.5684	-113.68	si
2					55	-.5684	-113.68	si
2					56	-.5684	-113.68	si
2					57	-.5684	-113.68	si
2					58	-.5684	-113.68	si
3	1- 1	.8117	0.	si	1	.3856	77.11	si
3	1- 2	.8117	0.	si	2	.3856	77.11	si
3	1- 3	-.3531	-4.54	si	3	.3856	77.11	si
3	1- 4	-.3531	-4.54	si	4	.3856	77.11	si
3					5	.3856	77.11	si
3					6	.3856	77.11	si
3					7	.3856	77.11	si
3					8	.3856	77.11	si
3					9	.3856	77.11	si
3					10	.3856	77.11	si
3					11	.3856	77.11	si
3					12	.3856	77.11	si
3					13	.3856	77.11	si
3					14	.3856	77.11	si
3					15	.3856	77.11	si
3					16	.3856	77.11	si
3					17	.3856	77.11	si
3					18	.3856	77.11	si
3					19	.3856	77.11	si
3					20	.3856	77.11	si
3					21	.3856	77.11	si

3	22	.3856	77.11	si
3	23	.7691	153.83	si
3	24	.7691	153.83	si
3	25	.7691	153.83	si
3	26	.7691	153.83	si
3	27	.7691	153.83	si
3	28	.7691	153.83	si
3	29	.7691	153.83	si
3	30	.7691	153.83	si
3	31	.7691	153.83	si
3	32	.7691	153.83	si
3	33	.7691	153.83	si
3	34	.7691	153.83	si
3	35	.7691	153.83	si
3	36	.7691	153.83	si
3	37	.7691	153.83	si
3	38	.7691	153.83	si
3	39	.7691	153.83	si
3	40	.7691	153.83	si
3	41	.7691	153.83	si
3	42	.7691	153.83	si
3	43	.7691	153.83	si
3	44	.7691	153.83	si
3	45	-.3105	-62.1	si
3	46	-.3105	-62.1	si
3	47	-.3105	-62.1	si
3	48	-.3105	-62.1	si
3	49	-.3105	-62.1	si
3	50	-.3105	-62.1	si
3	51	-.3105	-62.1	si
3	52	-.3105	-62.1	si
3	53	-.3105	-62.1	si
3	54	-.3105	-62.1	si
3	55	-.3105	-62.1	si
3	56	-.3105	-62.1	si
3	57	-.3105	-62.1	si
3	58	-.3105	-62.1	si

Descrizione : Pulvino 13

SOLLECITAZIONI AGENTI

Sforzi normali applicati in y= 29.55
 Convenzioni: N + trazione; Mz + fib.inferiori tese; My + fib.sinistra tese.

N.	N	Mz	My	Descrizione
1	-20.1	-1765.4582	-6695.1881	Caso 2.1
2	-163.76	-1707.1663	-54560.4891	Caso 2.2
3	39.51	-984.8607	13165.735	Caso 13.1

RISULTATI

Piani di equilibrio (eps= muz * y + muy * z + lam):

Sol.	muz	muy	lambda
1.	.00002562998	0.	-.00036419996
2.	.00002444421	0.	-.000360016
3.	.00001421205	0.	-.00019067663

Deformazioni sui materiali:

C/s					Acciaio lento				
sol	vert.	D	c/s	S c/s	Ve	ferro	D	s ferri	Ve
1	1- 1		1.444	0.	si	1	.6751	135.02	si
1	1- 2		1.444	0.	si	2	.6751	135.02	si
1	1- 3		-.6577	-7.75	si	3	.6751	135.02	si
1	1- 4		-.6577	-7.75	si	4	.6751	135.02	si
1						5	.6751	135.02	si
1						6	.6751	135.02	si
1						7	.6751	135.02	si
1						8	.6751	135.02	si
1						9	.6751	135.02	si
1						10	.6751	135.02	si
1						11	.6751	135.02	si
1						12	.6751	135.02	si
1						13	.6751	135.02	si
1						14	.6751	135.02	si
1						15	.6751	135.02	si
1						16	.6751	135.02	si
1						17	.6751	135.02	si
1						18	.6751	135.02	si
1						19	.6751	135.02	si
1						20	.6751	135.02	si
1						21	.6751	135.02	si
1						22	.6751	135.02	si
1						23	1.3671	273.42	si
1						24	1.3671	273.42	si
1						25	1.3671	273.42	si
1						26	1.3671	273.42	si
1						27	1.3671	273.42	si
1						28	1.3671	273.42	si
1						29	1.3671	273.42	si
1						30	1.3671	273.42	si
1						31	1.3671	273.42	si
1						32	1.3671	273.42	si
1						33	1.3671	273.42	si
1						34	1.3671	273.42	si
1						35	1.3671	273.42	si
1						36	1.3671	273.42	si
1						37	1.3671	273.42	si
1						38	1.3671	273.42	si
1						39	1.3671	273.42	si

1				40	1.3671	273.42	si
1				41	1.3671	273.42	si
1				42	1.3671	273.42	si
1				43	1.3671	273.42	si
1				44	1.3671	273.42	si
1				45	-.5808	-116.15	si
1				46	-.5808	-116.15	si
1				47	-.5808	-116.15	si
1				48	-.5808	-116.15	si
1				49	-.5808	-116.15	si
1				50	-.5808	-116.15	si
1				51	-.5808	-116.15	si
1				52	-.5808	-116.15	si
1				53	-.5808	-116.15	si
1				54	-.5808	-116.15	si
1				55	-.5808	-116.15	si
1				56	-.5808	-116.15	si
1				57	-.5808	-116.15	si
2				58	-.5808	-116.15	si
2	1- 1	1.3645	0.	1	.6312	126.24	si
2	1- 2	1.3645	0.	2	.6312	126.24	si
2	1- 3	-.6399	-7.58	3	.6312	126.24	si
2	1- 4	-.6399	-7.58	4	.6312	126.24	si
2				5	.6312	126.24	si
2				6	.6312	126.24	si
2				7	.6312	126.24	si
2				8	.6312	126.24	si
2				9	.6312	126.24	si
2				10	.6312	126.24	si
2				11	.6312	126.24	si
2				12	.6312	126.24	si
2				13	.6312	126.24	si
2				14	.6312	126.24	si
2				15	.6312	126.24	si
2				16	.6312	126.24	si
2				17	.6312	126.24	si
2				18	.6312	126.24	si
2				19	.6312	126.24	si
2				20	.6312	126.24	si
2				21	.6312	126.24	si
2				22	.6312	126.24	si
2				23	1.2912	258.24	si
2				24	1.2912	258.24	si
2				25	1.2912	258.24	si
2				26	1.2912	258.24	si
2				27	1.2912	258.24	si
2				28	1.2912	258.24	si
2				29	1.2912	258.24	si
2				30	1.2912	258.24	si
2				31	1.2912	258.24	si
2				32	1.2912	258.24	si
2				33	1.2912	258.24	si
2				34	1.2912	258.24	si
2				35	1.2912	258.24	si
2				36	1.2912	258.24	si
2				37	1.2912	258.24	si
2				38	1.2912	258.24	si
2				39	1.2912	258.24	si
2				40	1.2912	258.24	si
2				41	1.2912	258.24	si
2				42	1.2912	258.24	si
2				43	1.2912	258.24	si
2				44	1.2912	258.24	si
2				45	-.5666	-113.31	si
2				46	-.5666	-113.31	si
2				47	-.5666	-113.31	si
2				48	-.5666	-113.31	si
2				49	-.5666	-113.31	si
2				50	-.5666	-113.31	si
2				51	-.5666	-113.31	si
2				52	-.5666	-113.31	si
2				53	-.5666	-113.31	si
2				54	-.5666	-113.31	si
2				55	-.5666	-113.31	si
2				56	-.5666	-113.31	si
2				57	-.5666	-113.31	si
2				58	-.5666	-113.31	si
3	1- 1	.812	0.	1	.3856	77.12	si
3	1- 2	.812	0.	2	.3856	77.12	si
3	1- 3	-.3534	-4.55	3	.3856	77.12	si
3	1- 4	-.3534	-4.55	4	.3856	77.12	si
3				5	.3856	77.12	si
3				6	.3856	77.12	si
3				7	.3856	77.12	si
3				8	.3856	77.12	si
3				9	.3856	77.12	si
3				10	.3856	77.12	si
3				11	.3856	77.12	si
3				12	.3856	77.12	si
3				13	.3856	77.12	si
3				14	.3856	77.12	si
3				15	.3856	77.12	si
3				16	.3856	77.12	si
3				17	.3856	77.12	si
3				18	.3856	77.12	si
3				19	.3856	77.12	si
3				20	.3856	77.12	si

3	21	.3856	77.12	si
3	22	.3856	77.12	si
3	23	.7693	153.87	si
3	24	.7693	153.87	si
3	25	.7693	153.87	si
3	26	.7693	153.87	si
3	27	.7693	153.87	si
3	28	.7693	153.87	si
3	29	.7693	153.87	si
3	30	.7693	153.87	si
3	31	.7693	153.87	si
3	32	.7693	153.87	si
3	33	.7693	153.87	si
3	34	.7693	153.87	si
3	35	.7693	153.87	si
3	36	.7693	153.87	si
3	37	.7693	153.87	si
3	38	.7693	153.87	si
3	39	.7693	153.87	si
3	40	.7693	153.87	si
3	41	.7693	153.87	si
3	42	.7693	153.87	si
3	43	.7693	153.87	si
3	44	.7693	153.87	si
3	45	-.3108	-62.15	si
3	46	-.3108	-62.15	si
3	47	-.3108	-62.15	si
3	48	-.3108	-62.15	si
3	49	-.3108	-62.15	si
3	50	-.3108	-62.15	si
3	51	-.3108	-62.15	si
3	52	-.3108	-62.15	si
3	53	-.3108	-62.15	si
3	54	-.3108	-62.15	si
3	55	-.3108	-62.15	si
3	56	-.3108	-62.15	si
3	57	-.3108	-62.15	si
3	58	-.3108	-62.15	si

Descrizione : Pulvino 14

SOLLECITAZIONI AGENTI

Sforzi normali applicati in y= 29.55

Convenzioni: N + trazione; Mz + fib.inferiori tese; My + fib.sinistra tese.

N.	N	Mz	My	Descrizione
1	-19.58	-1765.1075	-7025.9303	Caso 2.1
2	-162.14	-1703.8895	-58178.9347	Caso 2.2
3	40.18	-986.1421	14416.7298	Caso 13.1

RISULTATI

Piani di equilibrio (eps= muz * y + muy * z + lam):

Sol.	muz	muy	lambda
1.	.00002562583	0.	-.00036408626
2.	.00002439851	0.	-.00035916805
3.	.00001423222	0.	-.00019090046

Deformazioni sui materiali:

sol	Cls			Ve	D	ferro	Acciaio lento		
	vert.	D	cls				S	ferri	Ve
1	1- 1	1.4438	0.	si	1	.675	135.01	si	
1	1- 2	1.4438	0.	si	2	.675	135.01	si	
1	1- 3	-.6575	-7.75	si	3	.675	135.01	si	
1	1- 4	-.6575	-7.75	si	4	.675	135.01	si	
1					5	.675	135.01	si	
1					6	.675	135.01	si	
1					7	.675	135.01	si	
1					8	.675	135.01	si	
1					9	.675	135.01	si	
1					10	.675	135.01	si	
1					11	.675	135.01	si	
1					12	.675	135.01	si	
1					13	.675	135.01	si	
1					14	.675	135.01	si	
1					15	.675	135.01	si	
1					16	.675	135.01	si	
1					17	.675	135.01	si	
1					18	.675	135.01	si	
1					19	.675	135.01	si	
1					20	.675	135.01	si	
1					21	.675	135.01	si	
1					22	.675	135.01	si	
1					23	1.3669	273.39	si	
1					24	1.3669	273.39	si	
1					25	1.3669	273.39	si	
1					26	1.3669	273.39	si	
1					27	1.3669	273.39	si	
1					28	1.3669	273.39	si	
1					29	1.3669	273.39	si	
1					30	1.3669	273.39	si	
1					31	1.3669	273.39	si	
1					32	1.3669	273.39	si	
1					33	1.3669	273.39	si	
1					34	1.3669	273.39	si	
1					35	1.3669	273.39	si	
1					36	1.3669	273.39	si	
1					37	1.3669	273.39	si	
1					38	1.3669	273.39	si	

1				39	1.3669	273.39	si
1				40	1.3669	273.39	si
1				41	1.3669	273.39	si
1				42	1.3669	273.39	si
1				43	1.3669	273.39	si
1				44	1.3669	273.39	si
1				45	-.5806	-116.12	si
1				46	-.5806	-116.12	si
1				47	-.5806	-116.12	si
1				48	-.5806	-116.12	si
1				49	-.5806	-116.12	si
1				50	-.5806	-116.12	si
1				51	-.5806	-116.12	si
1				52	-.5806	-116.12	si
1				53	-.5806	-116.12	si
1				54	-.5806	-116.12	si
1				55	-.5806	-116.12	si
1				56	-.5806	-116.12	si
1				57	-.5806	-116.12	si
1				58	-.5806	-116.12	si
2	1- 1	1.3621	0.	1	.6302	126.04	si
2	1- 2	1.3621	0.	2	.6302	126.04	si
2	1- 3	-.6385	-7.57	3	.6302	126.04	si
2	1- 4	-.6385	-7.57	4	.6302	126.04	si
2				5	.6302	126.04	si
2				6	.6302	126.04	si
2				7	.6302	126.04	si
2				8	.6302	126.04	si
2				9	.6302	126.04	si
2				10	.6302	126.04	si
2				11	.6302	126.04	si
2				12	.6302	126.04	si
2				13	.6302	126.04	si
2				14	.6302	126.04	si
2				15	.6302	126.04	si
2				16	.6302	126.04	si
2				17	.6302	126.04	si
2				18	.6302	126.04	si
2				19	.6302	126.04	si
2				20	.6302	126.04	si
2				21	.6302	126.04	si
2				22	.6302	126.04	si
2				23	1.289	257.79	si
2				24	1.289	257.79	si
2				25	1.289	257.79	si
2				26	1.289	257.79	si
2				27	1.289	257.79	si
2				28	1.289	257.79	si
2				29	1.289	257.79	si
2				30	1.289	257.79	si
2				31	1.289	257.79	si
2				32	1.289	257.79	si
2				33	1.289	257.79	si
2				34	1.289	257.79	si
2				35	1.289	257.79	si
2				36	1.289	257.79	si
2				37	1.289	257.79	si
2				38	1.289	257.79	si
2				39	1.289	257.79	si
2				40	1.289	257.79	si
2				41	1.289	257.79	si
2				42	1.289	257.79	si
2				43	1.289	257.79	si
2				44	1.289	257.79	si
2				45	-.5653	-113.07	si
2				46	-.5653	-113.07	si
2				47	-.5653	-113.07	si
2				48	-.5653	-113.07	si
2				49	-.5653	-113.07	si
2				50	-.5653	-113.07	si
2				51	-.5653	-113.07	si
2				52	-.5653	-113.07	si
2				53	-.5653	-113.07	si
2				54	-.5653	-113.07	si
2				55	-.5653	-113.07	si
2				56	-.5653	-113.07	si
2				57	-.5653	-113.07	si
2				58	-.5653	-113.07	si
3	1- 1	.8132	0.	1	.3862	77.24	si
3	1- 2	.8132	0.	2	.3862	77.24	si
3	1- 3	-.3539	-4.55	3	.3862	77.24	si
3	1- 4	-.3539	-4.55	4	.3862	77.24	si
3				5	.3862	77.24	si
3				6	.3862	77.24	si
3				7	.3862	77.24	si
3				8	.3862	77.24	si
3				9	.3862	77.24	si
3				10	.3862	77.24	si
3				11	.3862	77.24	si
3				12	.3862	77.24	si
3				13	.3862	77.24	si
3				14	.3862	77.24	si
3				15	.3862	77.24	si
3				16	.3862	77.24	si
3				17	.3862	77.24	si
3				18	.3862	77.24	si
3				19	.3862	77.24	si

20	.3862	77.24	si
21	.3862	77.24	si
22	.3862	77.24	si
23	.7705	154.1	si
24	.7705	154.1	si
25	.7705	154.1	si
26	.7705	154.1	si
27	.7705	154.1	si
28	.7705	154.1	si
29	.7705	154.1	si
30	.7705	154.1	si
31	.7705	154.1	si
32	.7705	154.1	si
33	.7705	154.1	si
34	.7705	154.1	si
35	.7705	154.1	si
36	.7705	154.1	si
37	.7705	154.1	si
38	.7705	154.1	si
39	.7705	154.1	si
40	.7705	154.1	si
41	.7705	154.1	si
42	.7705	154.1	si
43	.7705	154.1	si
44	.7705	154.1	si
45	-.3112	-62.23	si
46	-.3112	-62.23	si
47	-.3112	-62.23	si
48	-.3112	-62.23	si
49	-.3112	-62.23	si
50	-.3112	-62.23	si
51	-.3112	-62.23	si
52	-.3112	-62.23	si
53	-.3112	-62.23	si
54	-.3112	-62.23	si
55	-.3112	-62.23	si
56	-.3112	-62.23	si
57	-.3112	-62.23	si
58	-.3112	-62.23	si

Descrizione : Pulvino 15

SOLLECITAZIONI AGENTI

Sforzi normali applicati in y= 29.55
 Convenzioni: N + trazione; Mz + fib.inferiori tese; My + fib.sinistra tese.

N.	N	Mz	My	Descrizione
1	-22.81	-1763.3182	-8765.1599	Caso 2.1
2	-164.52	-1698.7608	-63244.0809	Caso 2.2
3	38.59	-986.5655	14838.6441	Caso 13.1

RISULTATI

Piani di equilibrio (eps= muz * y + muy * z + lam):

Sol.	muz	muy	lambda
1.	.00002559196	0.	-.00036388438
2.	.00002431638	0.	-.00035814991
3.	.00001423484	0.	-.00019108648

Deformazioni sui materiali:

sol	cls				Acciaio lento					
	vert.	D	cls	S	cls	Ve	ferro	D	S	ferri
1	1- 1		1.4416	0.	si	1	.6739		134.77	si
1	1- 2		1.4416	0.	si	2	.6739		134.77	si
1	1- 3		-.6569	-7.75	si	3	.6739		134.77	si
1	1- 4		-.6569	-7.75	si	4	.6739		134.77	si
1						5	.6739		134.77	si
1						6	.6739		134.77	si
1						7	.6739		134.77	si
1						8	.6739		134.77	si
1						9	.6739		134.77	si
1						10	.6739		134.77	si
1						11	.6739		134.77	si
1						12	.6739		134.77	si
1						13	.6739		134.77	si
1						14	.6739		134.77	si
1						15	.6739		134.77	si
1						16	.6739		134.77	si
1						17	.6739		134.77	si
1						18	.6739		134.77	si
1						19	.6739		134.77	si
1						20	.6739		134.77	si
1						21	.6739		134.77	si
1						22	.6739		134.77	si
1						23	1.3649		272.97	si
1						24	1.3649		272.97	si
1						25	1.3649		272.97	si
1						26	1.3649		272.97	si
1						27	1.3649		272.97	si
1						28	1.3649		272.97	si
1						29	1.3649		272.97	si
1						30	1.3649		272.97	si
1						31	1.3649		272.97	si
1						32	1.3649		272.97	si
1						33	1.3649		272.97	si
1						34	1.3649		272.97	si
1						35	1.3649		272.97	si
1						36	1.3649		272.97	si
1						37	1.3649		272.97	si

1				38	1.3649	272.97	si
1				39	1.3649	272.97	si
1				40	1.3649	272.97	si
1				41	1.3649	272.97	si
1				42	1.3649	272.97	si
1				43	1.3649	272.97	si
1				44	1.3649	272.97	si
1				45	-.5801	-116.03	si
1				46	-.5801	-116.03	si
1				47	-.5801	-116.03	si
1				48	-.5801	-116.03	si
1				49	-.5801	-116.03	si
1				50	-.5801	-116.03	si
1				51	-.5801	-116.03	si
1				52	-.5801	-116.03	si
1				53	-.5801	-116.03	si
1				54	-.5801	-116.03	si
1				55	-.5801	-116.03	si
1				56	-.5801	-116.03	si
1				57	-.5801	-116.03	si
1				58	-.5801	-116.03	si
2	1- 1	1.3574	0.	1	.6279	125.58	si
2	1- 2	1.3574	0.	2	.6279	125.58	si
2	1- 3	-.6366	-7.55	3	.6279	125.58	si
2	1- 4	-.6366	-7.55	4	.6279	125.58	si
2				5	.6279	125.58	si
2				6	.6279	125.58	si
2				7	.6279	125.58	si
2				8	.6279	125.58	si
2				9	.6279	125.58	si
2				10	.6279	125.58	si
2				11	.6279	125.58	si
2				12	.6279	125.58	si
2				13	.6279	125.58	si
2				14	.6279	125.58	si
2				15	.6279	125.58	si
2				16	.6279	125.58	si
2				17	.6279	125.58	si
2				18	.6279	125.58	si
2				19	.6279	125.58	si
2				20	.6279	125.58	si
2				21	.6279	125.58	si
2				22	.6279	125.58	si
2				23	1.2844	256.88	si
2				24	1.2844	256.88	si
2				25	1.2844	256.88	si
2				26	1.2844	256.88	si
2				27	1.2844	256.88	si
2				28	1.2844	256.88	si
2				29	1.2844	256.88	si
2				30	1.2844	256.88	si
2				31	1.2844	256.88	si
2				32	1.2844	256.88	si
2				33	1.2844	256.88	si
2				34	1.2844	256.88	si
2				35	1.2844	256.88	si
2				36	1.2844	256.88	si
2				37	1.2844	256.88	si
2				38	1.2844	256.88	si
2				39	1.2844	256.88	si
2				40	1.2844	256.88	si
2				41	1.2844	256.88	si
2				42	1.2844	256.88	si
2				43	1.2844	256.88	si
2				44	1.2844	256.88	si
2				45	-.5636	-112.72	si
2				46	-.5636	-112.72	si
2				47	-.5636	-112.72	si
2				48	-.5636	-112.72	si
2				49	-.5636	-112.72	si
2				50	-.5636	-112.72	si
2				51	-.5636	-112.72	si
2				52	-.5636	-112.72	si
2				53	-.5636	-112.72	si
2				54	-.5636	-112.72	si
2				55	-.5636	-112.72	si
2				56	-.5636	-112.72	si
2				57	-.5636	-112.72	si
2				58	-.5636	-112.72	si
3	1- 1	.8132	0.	1	.3861	77.23	si
3	1- 2	.8132	0.	2	.3861	77.23	si
3	1- 3	-.3541	-4.55	3	.3861	77.23	si
3	1- 4	-.3541	-4.55	4	.3861	77.23	si
3				5	.3861	77.23	si
3				6	.3861	77.23	si
3				7	.3861	77.23	si
3				8	.3861	77.23	si
3				9	.3861	77.23	si
3				10	.3861	77.23	si
3				11	.3861	77.23	si
3				12	.3861	77.23	si
3				13	.3861	77.23	si
3				14	.3861	77.23	si
3				15	.3861	77.23	si
3				16	.3861	77.23	si
3				17	.3861	77.23	si
3				18	.3861	77.23	si

VERIFICA SEZIONI PULVINI (sezione y-z):

PARAMETRI GENERALI

Tipo verifica : stati limite - pressoflessione deviata.
 Unità di misura generiche: kN; cm; kNm; N/mm²; d in mm; deformazioni*1000.
 ferri : diametri in mm; aree in cm².

Simboli :

Vert. = contorno_vertice del CLS; d = diametro;
 S = Sigma (tensioni sui materiali);
 D = Deformazioni x 1000 (epsilon);
 Ve = colonna che indica se la verifica e' soddisfatta;

CARATTERISTICHE MATERIALI

Calcestruzzo: Rck = 30. ; fck = 24.9 ; fcd = 14.11 (.35%)
 Acciaio : Tipo= B450C ; ftk = 540. ; fyk = 450. ; ftd = 469.565 (6.75%)

CARATTERISTICHE SEZIONE

L'asse Z e' rivolto verso destra, l'asse Y e' rivolto verso l'alto.

Tipo sezione: U_Pul

CLS:

vert.		Z	Y	Acciaio lento:		d[mm]	Af[cm ²]
ferro		Z	Y	ferro			
1- 1	0.	55.	1	301.4	79.	20.	3.1416
1- 2	63.	55.	2	285.7	79.	20.	3.1416
1- 3	63.	82.	3	270.	79.	20.	3.1416
1- 4	304.4	82.	4	254.3	79.	20.	3.1416
1- 5	304.4	55.	5	238.6	79.	20.	3.1416
1- 6	367.4	55.	6	222.9	79.	20.	3.1416
1- 7	367.4	0.	7	207.2	79.	20.	3.1416
1- 8	0.	0.	8	191.5	79.	20.	3.1416
			9	175.9	79.	20.	3.1416
			10	160.2	79.	20.	3.1416
			11	144.5	79.	20.	3.1416
			12	128.8	79.	20.	3.1416
			13	113.1	79.	20.	3.1416
			14	97.4	79.	20.	3.1416
			15	81.7	79.	20.	3.1416
			16	66.	79.	20.	3.1416
			17	66.	52.	20.	3.1416
			18	45.	52.	20.	3.1416
			19	24.	52.	20.	3.1416
			20	3.	52.	20.	3.1416
			21	364.4	52.	20.	3.1416
			22	343.4	52.	20.	3.1416
			23	322.4	52.	20.	3.1416
			24	301.4	52.	20.	3.1416
			25	364.4	3.	20.	3.1416
			26	348.7	3.	20.	3.1416
			27	333.	3.	20.	3.1416
			28	317.3	3.	20.	3.1416
			29	301.5	3.	20.	3.1416
			30	285.8	3.	20.	3.1416
			31	270.1	3.	20.	3.1416
			32	254.4	3.	20.	3.1416
			33	238.7	3.	20.	3.1416
			34	223.	3.	20.	3.1416
			35	207.3	3.	20.	3.1416
			36	191.6	3.	20.	3.1416
			37	175.8	3.	20.	3.1416
			38	160.1	3.	20.	3.1416
			39	144.4	3.	20.	3.1416
			40	128.7	3.	20.	3.1416
			41	113.	3.	20.	3.1416
			42	97.3	3.	20.	3.1416
			43	81.6	3.	20.	3.1416
			44	65.9	3.	20.	3.1416
			45	50.1	3.	20.	3.1416
			46	34.4	3.	20.	3.1416
			47	18.7	3.	20.	3.1416
			48	3.	3.	20.	3.1416

Descrizione : Pulvino 1

SOLLECITAZIONI AGENTI

Sforzi normali applicati in z= 183.7 ; y= 37.5 (baricentro CLS)
 convenzioni: N + trazione; Mz + fib.inferiori tese; My + fib.sinistra tese.

N.	N	Mz	My	Descrizione
1	-224.16	-853.9879	-195.1938	Caso 2.1
2	-110.63	-470.8122	-203.2253	Caso 13.1
3	-174.98	-555.6568	-1045.1818	Caso 7.21
4	-112.95	-555.3194	516.2582	Caso 7.12
5	-234.7	-555.7454	-651.839	Caso 6.29
6	-53.23	-555.2308	122.9154	Caso 6.4

RISULTATI

Piani di equilibrio (eps= muz * y + muy * z + lam):

Sol.	muz	muy	lambda
1.	.00001446262	.00000015181	-.00027654609
2.	.0000080013	.00000015689	-.00016371608
3.	.00000926902	.00000087385	-.00030191859
4.	.0000095182	-.00000040937	-.0000805666
5.	.00000907183	.00000049642	-.00024827869
6.	.00000973926	-.00000009803	-.000139927

Deformazioni sui materiali:

CLS		Acciaio lento					
sol	vert.	D cls	S cls	ferro	D ferri	S ferri	Ve
1	1- 1	.5189	0.	1	.9118	182.35	si
1	1- 2	.5285	0.	2	.9094	181.87	si
1	1- 3	.919	0.	3	.907	181.4	si
1	1- 4	.9556	0.	4	.9046	180.92	si

1				5	.9022	180.45	si
1	1- 5	.5651	0.	6	.8998	179.97	si
1	1- 6	.5747	0.	7	.8975	179.49	si
1	1- 7	-.2208	-2.94	8	.8951	179.02	si
1	1- 8	-.2765	-3.63	9	.8927	178.54	si
1				10	.8903	178.06	si
1				11	.8879	177.59	si
1				12	.8855	177.11	si
1				13	.8832	176.63	si
1				14	.8808	176.16	si
1				15	.8784	175.68	si
1				16	.876	175.2	si
1				17	.4855	97.11	si
1				18	.4823	96.47	si
1				19	.4792	95.83	si
1				20	.476	95.19	si
1				21	.5308	106.17	si
1				22	.5276	105.53	si
1				23	.5245	104.89	si
1				24	.5213	104.25	si
1				25	-.1778	-35.57	si
1				26	-.1802	-36.04	si
1				27	-.1826	-36.52	si
1				28	-.185	-37.	si
1				29	-.1874	-37.48	si
1				30	-.1898	-37.95	si
1				31	-.1922	-38.43	si
1				32	-.1945	-38.91	si
1				33	-.1969	-39.38	si
1				34	-.1993	-39.86	si
1				35	-.2017	-40.34	si
1				36	-.2041	-40.82	si
1				37	-.2065	-41.29	si
1				38	-.2088	-41.77	si
1				39	-.2112	-42.25	si
1				40	-.2136	-42.72	si
1				41	-.216	-43.2	si
1				42	-.2184	-43.68	si
1				43	-.2208	-44.16	si
1				44	-.2232	-44.63	si
1				45	-.2255	-45.11	si
1				46	-.2279	-45.59	si
1				47	-.2303	-46.06	si
1				48	-.2327	-46.54	si
2	1- 1	.2764	0.	1	.5157	103.13	si
2	1- 2	.2862	0.	2	.5132	102.64	si
2	1- 3	.5023	0.	3	.5107	102.15	si
2	1- 4	.5401	0.	4	.5083	101.66	si
2	1- 5	.3241	0.	5	.5058	101.17	si
2	1- 6	.334	0.	6	.5034	100.67	si
2	1- 7	-.1061	-1.46	7	.5009	100.18	si
2	1- 8	-.1637	-2.22	8	.4984	99.69	si
2				9	.496	99.2	si
2				10	.4935	98.7	si
2				11	.4911	98.21	si
2				12	.4886	97.72	si
2				13	.4861	97.23	si
2				14	.4837	96.73	si
2				15	.4812	96.24	si
2				16	.4787	95.75	si
2				17	.2627	52.54	si
2				18	.2594	51.88	si
2				19	.2561	51.22	si
2				20	.2528	50.56	si
2				21	.3095	61.9	si
2				22	.3062	61.25	si
2				23	.3029	60.59	si
2				24	.2996	59.93	si
2				25	-.0825	-16.51	si
2				26	-.085	-17.	si
2				27	-.0875	-17.49	si
2				28	-.0899	-17.99	si
2				29	-.0924	-18.48	si
2				30	-.0949	-18.97	si
2				31	-.0973	-19.47	si
2				32	-.0998	-19.96	si
2				33	-.1023	-20.45	si
2				34	-.1047	-20.95	si
2				35	-.1072	-21.44	si
2				36	-.1097	-21.93	si
2				37	-.1121	-22.42	si
2				38	-.1146	-22.92	si
2				39	-.1171	-23.41	si
2				40	-.1195	-23.9	si
2				41	-.122	-24.4	si
2				42	-.1245	-24.89	si
2				43	-.1269	-25.38	si
2				44	-.1294	-25.88	si
2				45	-.1318	-26.37	si
2				46	-.1343	-26.86	si
2				47	-.1368	-27.36	si
2				48	-.1392	-27.85	si
3	1- 1	.2079	0.	1	.6937	138.74	si
3	1- 2	.2629	0.	2	.68	136.	si
3	1- 3	.5132	0.	3	.6663	133.26	si
3	1- 4	.7241	0.	4	.6526	130.51	si
3	1- 5	.4739	0.	5	.6389	127.77	si

3	1- 6	.5289	0.	si	6	.6251	125.03	si
3	1- 7	.0191	0.	si	7	.6114	122.29	si
3	1- 8	-.3019	-3.94	si	8	.5977	119.54	si
3					9	.584	116.8	si
3					10	.5703	114.06	si
3					11	.5566	111.32	si
3					12	.5429	108.57	si
3					13	.5291	105.83	si
3					14	.5154	103.09	si
3					15	.5017	100.34	si
3					16	.488	97.6	si
3					17	.2377	47.55	si
3					18	.2194	43.88	si
3					19	.201	40.21	si
3					20	.1827	36.54	si
3					21	.4985	99.7	si
3					22	.4801	96.03	si
3					23	.4618	92.36	si
3					24	.4434	88.69	si
3					25	.0443	8.86	si
3					26	.0306	6.12	si
3					27	.0169	3.37	si
3					28	.0031	.63	si
3					29	-.0106	-2.12	si
3					30	-.0243	-4.87	si
3					31	-.0381	-7.61	si
3					32	-.0518	-10.36	si
3					33	-.0655	-13.11	si
3					34	-.0793	-15.85	si
3					35	-.093	-18.6	si
3					36	-.1067	-21.34	si
3					37	-.1205	-24.09	si
3					38	-.1342	-26.84	si
3					39	-.1479	-29.58	si
3					40	-.1616	-32.33	si
3					41	-.1754	-35.07	si
3					42	-.1891	-37.82	si
3					43	-.2028	-40.57	si
3					44	-.2166	-43.31	si
3					45	-.2303	-46.06	si
3					46	-.244	-48.81	si
3					47	-.2578	-51.55	si
3					48	-.2715	-54.3	si
4	1- 1	.4429	0.	si	1	.548	109.6	si
4	1- 2	.4171	0.	si	2	.5544	110.88	si
4	1- 3	.6741	0.	si	3	.5608	112.17	si
4	1- 4	.5753	0.	si	4	.5673	113.45	si
4	1- 5	.3183	0.	si	5	.5737	114.74	si
4	1- 6	.2925	0.	si	6	.5801	116.02	si
4	1- 7	-.231	-3.07	si	7	.5865	117.31	si
4	1- 8	-.0806	-1.11	si	8	.593	118.59	si
4					9	.5994	119.88	si
4					10	.6058	121.16	si
4					11	.6122	122.45	si
4					12	.6187	123.73	si
4					13	.6251	125.02	si
4					14	.6315	126.3	si
4					15	.6379	127.59	si
4					16	.6444	128.87	si
4					17	.3874	77.47	si
4					18	.396	79.19	si
4					19	.4046	80.91	si
4					20	.4132	82.63	si
4					21	.2652	53.04	si
4					22	.2738	54.76	si
4					23	.2824	56.48	si
4					24	.291	58.2	si
4					25	-.2012	-40.24	si
4					26	-.1948	-38.95	si
4					27	-.1883	-37.66	si
4					28	-.1819	-36.38	si
4					29	-.1755	-35.09	si
4					30	-.169	-33.81	si
4					31	-.1626	-32.52	si
4					32	-.1562	-31.23	si
4					33	-.1497	-29.95	si
4					34	-.1433	-28.66	si
4					35	-.1369	-27.37	si
4					36	-.1304	-26.09	si
4					37	-.124	-24.8	si
4					38	-.1176	-23.51	si
4					39	-.1111	-22.23	si
4					40	-.1047	-20.94	si
4					41	-.0983	-19.65	si
4					42	-.0918	-18.37	si
4					43	-.0854	-17.08	si
4					44	-.079	-15.79	si
4					45	-.0725	-14.51	si
4					46	-.0661	-13.22	si
4					47	-.0597	-11.93	si
4					48	-.0532	-10.65	si
5	1- 1	.2507	0.	si	1	.618	123.6	si
5	1- 2	.2819	0.	si	2	.6102	122.04	si
5	1- 3	.5269	0.	si	3	.6024	120.49	si
5	1- 4	.6467	0.	si	4	.5946	118.93	si
5	1- 5	.4018	0.	si	5	.5869	117.37	si
5	1- 6	.4331	0.	si	6	.5791	115.81	si

5	1- 7	-.0659	-.91	si	7	.5713	114.25	si
5	1- 8	-.2483	-3.29	si	8	.5635	112.7	si
5					9	.5557	111.14	si
5					10	.5479	109.58	si
5					11	.5401	108.02	si
5					12	.5323	106.46	si
5					13	.5245	104.91	si
5					14	.5167	103.35	si
5					15	.5089	101.79	si
5					16	.5012	100.23	si
5					17	.2562	51.24	si
5					18	.2458	49.16	si
5					19	.2354	47.07	si
5					20	.2249	44.99	si
5					21	.4044	80.87	si
5					22	.3939	78.79	si
5					23	.3835	76.7	si
5					24	.3731	74.62	si
5					25	-.0402	-8.03	si
5					26	-.048	-9.59	si
5					27	-.0558	-11.15	si
5					28	-.0636	-12.71	si
5					29	-.0714	-14.27	si
5					30	-.0792	-15.83	si
5					31	-.087	-17.39	si
5					32	-.0948	-18.95	si
5					33	-.1026	-20.51	si
5					34	-.1104	-22.07	si
5					35	-.1182	-23.63	si
5					36	-.126	-25.19	si
5					37	-.1338	-26.75	si
5					38	-.1416	-28.31	si
5					39	-.1494	-29.87	si
5					40	-.1572	-31.43	si
5					41	-.165	-32.99	si
5					42	-.1728	-34.55	si
5					43	-.1806	-36.11	si
5					44	-.1884	-37.67	si
5					45	-.1962	-39.23	si
5					46	-.204	-40.79	si
5					47	-.2118	-42.35	si
5					48	-.2196	-43.91	si
6	1- 1	.3957	0.	si	1	.5999	119.99	si
6	1- 2	.3896	0.	si	2	.6015	120.29	si
6	1- 3	.6525	0.	si	3	.603	120.6	si
6	1- 4	.6289	0.	si	4	.6045	120.91	si
6	1- 5	.3659	0.	si	5	.6061	121.22	si
6	1- 6	.3597	0.	si	6	.6076	121.52	si
6	1- 7	-.1759	-2.37	si	7	.6092	121.83	si
6	1- 8	-.1399	-1.91	si	8	.6107	122.14	si
6					9	.6122	122.45	si
6					10	.6138	122.75	si
6					11	.6153	123.06	si
6					12	.6169	123.37	si
6					13	.6184	123.68	si
6					14	.6199	123.99	si
6					15	.6215	124.29	si
6					16	.623	124.6	si
6					17	.36	72.01	si
6					18	.3621	72.42	si
6					19	.3642	72.83	si
6					20	.3662	73.24	si
6					21	.3308	66.16	si
6					22	.3329	66.57	si
6					23	.3349	66.98	si
6					24	.337	67.39	si
6					25	-.1464	-29.29	si
6					26	-.1449	-28.98	si
6					27	-.1434	-28.67	si
6					28	-.1418	-28.36	si
6					29	-.1403	-28.05	si
6					30	-.1387	-27.75	si
6					31	-.1372	-27.44	si
6					32	-.1356	-27.13	si
6					33	-.1341	-26.82	si
6					34	-.1326	-26.51	si
6					35	-.131	-26.21	si
6					36	-.1295	-25.9	si
6					37	-.1279	-25.59	si
6					38	-.1264	-25.28	si
6					39	-.1249	-24.97	si
6					40	-.1233	-24.67	si
6					41	-.1218	-24.36	si
6					42	-.1202	-24.05	si
6					43	-.1187	-23.74	si
6					44	-.1172	-23.43	si
6					45	-.1156	-23.12	si
6					46	-.1141	-22.82	si
6					47	-.1125	-22.51	si
6					48	-.111	-22.2	si

Descrizione : Pulvino 2

SOLLECITAZIONI AGENTI

Sforzi normali applicati in z= 183.7 ; y= 37.5 (baricentro CLS)

Convenzioni: N + trazione; Mz + fib.inferiori tese; My + fib.sinistra tese.

N.	N	Mz	My	Descrizione
1	-237.39	-954.1015	-765.574	Caso 8.10
2	-50.27	-149.5459	237.1411	Caso 8.23
3	-206.69	-671.6013	-1714.424	Caso 7.8
4	-80.97	-432.046	1185.9911	Caso 7.25
5	-294.89	-952.6072	-210.7182	Caso 8.24
6	7.23	-151.0401	-317.7147	Caso 8.9

RISULTATI

Piani di equilibrio (eps= muz * y +muy * z + lam):			
Sol.	muz	muy	lambda
1.	.00001624014	.00000060793	-.0003854937
2.	.00000247899	-.00000018708	-.00000527813
3.	.00001104893	.00000159426	-.00043050369
4.	.00000717584	-.00000116073	.00013894547
5.	.000015973	.00000016286	-.00030919523
6.	.00000267163	.00000030254	-.0000872711

Deformazioni sui materiali:

C/s				Acciaio lento				
sol	vert.	D c/s	S c/s	Ve	ferro	D ferri	S ferri	Ve
1	1- 1	.5077	0.	si	1	1.0807	216.14	si
1	1- 2	.546	0.	si	2	1.0712	214.23	si
1	1- 3	.9845	0.	si	3	1.0616	212.33	si
1	1- 4	1.1313	0.	si	4	1.0521	210.42	si
1	1- 5	.6928	0.	si	5	1.0425	208.51	si
1	1- 6	.7311	0.	si	6	1.033	206.6	si
1	1- 7	-.1621	-2.2	si	7	1.0235	204.69	si
1	1- 8	-.3855	-4.92	si	8	1.0139	202.78	si
1					9	1.0044	200.88	si
1					10	.9948	198.97	si
1					11	.9853	197.06	si
1					12	.9758	195.15	si
1					13	.9662	193.24	si
1					14	.9567	191.34	si
1					15	.9471	189.43	si
1					16	.9376	187.52	si
1					17	.4991	99.82	si
1					18	.4864	97.27	si
1					19	.4736	94.72	si
1					20	.4608	92.16	si
1					21	.6805	136.1	si
1					22	.6678	133.55	si
1					23	.655	131.	si
1					24	.6422	128.44	si
1					25	-.1152	-23.05	si
1					26	-.1248	-24.96	si
1					27	-.1343	-26.87	si
1					28	-.1439	-28.78	si
1					29	-.1535	-30.69	si
1					30	-.163	-32.6	si
1					31	-.1726	-34.51	si
1					32	-.1821	-36.42	si
1					33	-.1917	-38.33	si
1					34	-.2012	-40.24	si
1					35	-.2108	-42.15	si
1					36	-.2203	-44.06	si
1					37	-.2299	-45.97	si
1					38	-.2394	-47.89	si
1					39	-.249	-49.8	si
1					40	-.2585	-51.71	si
1					41	-.2681	-53.62	si
1					42	-.2776	-55.53	si
1					43	-.2872	-57.44	si
1					44	-.2967	-59.35	si
1					45	-.3063	-61.26	si
1					46	-.3158	-63.17	si
1					47	-.3254	-65.08	si
1					48	-.3349	-66.99	si
2	1- 1	.1311	0.	si	1	.1342	26.84	si
2	1- 2	.1193	0.	si	2	.1371	27.42	si
2	1- 3	.1862	0.	si	3	.14	28.01	si
2	1- 4	.1411	0.	si	4	.143	28.6	si
2	1- 5	.0741	0.	si	5	.1459	29.18	si
2	1- 6	-.0623	0.	si	6	.1489	29.77	si
2	1- 7	-.074	-1.02	si	7	.1518	30.36	si
2	1- 8	-.0053	-.07	si	8	.1547	30.95	si
2					9	.1577	31.53	si
2					10	.1606	32.12	si
2					11	.1635	32.71	si
2					12	.1665	33.29	si
2					13	.1694	33.88	si
2					14	.1723	34.47	si
2					15	.1753	35.06	si
2					16	.1782	35.64	si
2					17	.1113	22.26	si
2					18	.1152	23.04	si
2					19	.1191	23.83	si
2					20	.1231	24.61	si
2					21	.0555	11.09	si
2					22	.0594	11.88	si
2					23	.0633	12.66	si
2					24	.0672	13.45	si
2					25	-.066	-13.2	si
2					26	-.0631	-12.61	si
2					27	-.0601	-12.03	si
2					28	-.0572	-11.44	si
2					29	-.0543	-10.85	si

4				31	-.1531	-30.61	si
4				32	-.1348	-26.97	si
4				33	-.1166	-23.32	si
4				34	-.0983	-19.67	si
4				35	-.0801	-16.02	si
4				36	-.0619	-12.37	si
4				37	-.0436	-8.73	si
4				38	-.0254	-5.08	si
4				39	-.0072	-1.43	si
4				40	.0111	2.22	si
4				41	.0293	5.86	si
4				42	.0476	9.51	si
4				43	.0658	13.16	si
4				44	.084	16.81	si
4				45	.1023	20.46	si
4				46	.1205	24.1	si
4				47	.1388	27.75	si
4				48	.157	31.4	si
5	1- 1	.5693	0.	1	1.0018	200.35	si
5	1- 2	.5796	0.	2	.9992	199.84	si
5	1- 3	1.0109	0.	3	.9966	199.33	si
5	1- 4	1.0502	0.	4	.9941	198.82	si
5	1- 5	.6189	0.	5	.9915	198.31	si
5	1- 6	.6292	0.	6	.989	197.8	si
5	1- 7	-.2494	-3.3	7	.9864	197.28	si
5	1- 8	-.3092	-4.03	8	.9839	196.77	si
5				9	.9813	196.26	si
5				10	.9788	195.75	si
5				11	.9762	195.24	si
5				12	.9736	194.73	si
5				13	.9711	194.22	si
5				14	.9685	193.71	si
5				15	.966	193.2	si
5				16	.9634	192.68	si
5				17	.9608	192.17	si
5				18	.9582	191.65	si
5				19	.9556	191.14	si
5				20	.953	190.62	si
5				21	.9504	190.11	si
5				22	.9478	189.59	si
5				23	.9452	189.08	si
5				24	.9426	188.56	si
5				25	.94	188.05	si
5				26	.9374	187.53	si
5				27	.9348	187.02	si
5				28	.9322	186.5	si
5				29	.9296	185.98	si
5				30	.927	185.47	si
5				31	.9244	184.95	si
5				32	.9218	184.43	si
5				33	.9192	183.92	si
5				34	.9166	183.4	si
5				35	.914	182.88	si
5				36	.9114	182.37	si
5				37	.9088	181.85	si
5				38	.9062	181.33	si
5				39	.9036	180.82	si
5				40	.901	180.3	si
5				41	.8984	179.78	si
5				42	.8958	179.27	si
5				43	.8932	178.75	si
5				44	.8906	178.23	si
5				45	.888	177.72	si
5				46	.8854	177.2	si
5				47	.8828	176.68	si
5				48	.8802	176.17	si
6	1- 1	.0597	0.	1	.215	42.99	si
6	1- 2	.0787	0.	2	.2102	42.04	si
6	1- 3	.1509	0.	3	.2055	41.1	si
6	1- 4	.2239	0.	4	.2007	40.15	si
6	1- 5	.1518	0.	5	.196	39.2	si
6	1- 6	.1708	0.	6	.1912	38.25	si
6	1- 7	.0239	0.	7	.1865	37.3	si
6	1- 8	-.0873	-1.2	8	.1817	36.35	si
6				9	.177	35.4	si
6				10	.1722	34.45	si
6				11	.1675	33.5	si
6				12	.1627	32.55	si
6				13	.158	31.6	si
6				14	.1533	30.65	si
6				15	.1485	29.7	si
6				16	.1438	28.75	si
6				17	.139	27.8	si
6				18	.1343	26.85	si
6				19	.1295	25.9	si
6				20	.1248	24.95	si
6				21	.12	24	si
6				22	.1153	23.05	si
6				23	.1105	22.1	si
6				24	.1058	21.15	si
6				25	.101	20.2	si
6				26	.0963	19.25	si
6				27	.0915	18.3	si
6				28	.0868	17.35	si
6				29	.082	16.4	si
6				30	.0773	15.45	si
6				31	.0725	14.5	si

6	32	-0.0023	-0.46	si
6	33	-0.007	-1.41	si
6	34	-0.0118	-2.36	si
6	35	-0.0165	-3.31	si
6	36	-0.0213	-4.26	si
6	37	-0.0261	-5.21	si
6	38	-0.0308	-6.16	si
6	39	-0.0356	-7.11	si
6	40	-0.0403	-8.06	si
6	41	-0.0451	-9.01	si
6	42	-0.0498	-9.97	si
6	43	-0.0546	-10.92	si
6	44	-0.0593	-11.87	si
6	45	-0.0641	-12.82	si
6	46	-0.0688	-13.77	si
6	47	-0.0736	-14.72	si
6	48	-0.0783	-15.67	si

Descrizione : Pulvino 3

SOLLECITAZIONI AGENTI

Sforzi normali applicati in z= 183.7 ; y= 37.5 (baricentro CLS)
 Convenzioni: N + trazione; Mz + fib.inferiori tese; My + fib.sinistra tese.

N.	N	Mz	My	Descrizione
1	-14.31	-469.8714	-26.295	Caso 13.1
2	-40.91	-851.3607	-270.5802	Caso 2.2
3	-42.1	-851.4424	118.0844	Caso 2.1
4	-62.17	-544.9594	-47.204	Caso 6.14
5	8.49	-562.7666	-51.4072	Caso 6.19

RISULTATI

Piani di equilibrio (eps= muz * y +muy * z + lam):

sol.	muz	muy	lambda
1.	.00000835621	.00000002119	-.00013656312
2.	.00001512305	.00000022118	-.00028302445
3.	.00001511867	-.00000009631	-.00022536196
4.	.0000095195	.00000003744	-.00016232272
5.	.00001011391	.00000004203	-.00016617878

Deformazioni sui materiali:

Cls						Acciaio lento						
sol	vert.	D	cls	S	cls	Ve	ferro	D	ferri	S	ferri	Ve
1	1- 1		.323	0.	0.	si	1		.53		105.99	si
1	1- 2		.3244	0.	0.	si	2		.5296		105.93	si
1	1- 3		.55	0.	0.	si	3		.5293		105.86	si
1	1- 4		.5551	0.	0.	si	4		.529		105.79	si
1	1- 5		.3295	0.	0.	si	5		.5286		105.73	si
1	1- 6		.3308	0.	0.	si	6		.5283		105.66	si
1	1- 7		-.1288	-1.76	0.	si	7		.528		105.59	si
1	1- 8		-.1366	-1.86	0.	si	8		.5276		105.53	si
1							9		.5273		105.46	si
1							10		.527		105.39	si
1							11		.5266		105.33	si
1							12		.5263		105.26	si
1							13		.526		105.19	si
1							14		.5256		105.13	si
1							15		.5253		105.06	si
1							16		.525		105.	si
1							17		.2994		59.87	si
1							18		.2989		59.78	si
1							19		.2985		59.69	si
1							20		.298		59.6	si
1							21		.3057		61.14	si
1							22		.3052		61.05	si
1							23		.3048		60.96	si
1							24		.3043		60.87	si
1							25		-.1038		-20.75	si
1							26		-.1041		-20.82	si
1							27		-.1044		-20.89	si
1							28		-.1048		-20.95	si
1							29		-.1051		-21.02	si
1							30		-.1054		-21.09	si
1							31		-.1058		-21.15	si
1							32		-.1061		-21.22	si
1							33		-.1064		-21.29	si
1							34		-.1068		-21.35	si
1							35		-.1071		-21.42	si
1							36		-.1074		-21.49	si
1							37		-.1078		-21.55	si
1							38		-.1081		-21.62	si
1							39		-.1084		-21.69	si
1							40		-.1088		-21.75	si
1							41		-.1091		-21.82	si
1							42		-.1094		-21.89	si
1							43		-.1098		-21.95	si
1							44		-.1101		-22.02	si
1							45		-.1104		-22.09	si
1							46		-.1108		-22.15	si
1							47		-.1111		-22.22	si
1							48		-.1114		-22.29	si
2	1- 1		.5487	0.	0.	si	1		.9784		195.67	si
2	1- 2		.5627	0.	0.	si	2		.9749		194.98	si
2	1- 3		.971	0.	0.	si	3		.9714		194.28	si
2	1- 4		1.0244	0.	0.	si	4		.9679		193.59	si
2	1- 5		.6161	0.	0.	si	5		.9645		192.9	si
2	1- 6		.63	0.	0.	si	6		.961		192.2	si
2	1- 7		-.2018	-2.7	0.	si	7		.9575		191.51	si

2	1- 8	-.283		-3.71		si	8	.9541	190.81		si
2							9	.9506	190.12		si
2							10	.9471	189.42		si
2							11	.9436	188.73		si
2							12	.9402	188.04		si
2							13	.9367	187.34		si
2							14	.9332	186.65		si
2							15	.9298	185.95		si
2							16	.9263	185.26		si
2							17	.518	103.59		si
2							18	.5133	102.67		si
2							19	.5087	101.74		si
2							20	.504	100.81		si
2							21	.584	116.79		si
2							22	.5793	115.87		si
2							23	.5747	114.94		si
2							24	.57	114.01		si
2							25	-.1571	-31.41		si
2							26	-.1605	-32.11		si
2							27	-.164	-32.8		si
2							28	-.1675	-33.5		si
2							29	-.171	-34.19		si
2							30	-.1744	-34.89		si
2							31	-.1779	-35.58		si
2							32	-.1814	-36.28		si
2							33	-.1849	-36.97		si
2							34	-.1883	-37.67		si
2							35	-.1918	-38.36		si
2							36	-.1953	-39.06		si
2							37	-.1988	-39.75		si
2							38	-.2022	-40.45		si
2							39	-.2057	-41.14		si
2							40	-.2092	-41.84		si
2							41	-.2127	-42.53		si
2							42	-.2161	-43.23		si
2							43	-.2196	-43.92		si
2							44	-.2231	-44.62		si
2							45	-.2266	-45.31		si
2							46	-.23	-46.01		si
2							47	-.2335	-46.7		si
2							48	-.237	-47.4		si
3	1- 1	.6062		0.		si	1	.94	188.		si
3	1- 2	.6001		0.		si	2	.9415	188.3		si
3	1- 3	1.0083		0.		si	3	.943	188.6		si
3	1- 4	.9851		0.		si	4	.9445	188.9		si
3	1- 5	.5768		0.		si	5	.946	189.21		si
3	1- 6	.5708		0.		si	6	.9475	189.51		si
3	1- 7	-.2607		-3.44		si	7	.9491	189.81		si
3	1- 8	-.2254		-3.		si	8	.9506	190.11		si
3							9	.9521	190.42		si
3							10	.9536	190.72		si
3							11	.9551	191.02		si
3							12	.9566	191.32		si
3							13	.9581	191.62		si
3							14	.9596	191.93		si
3							15	.9611	192.23		si
3							16	.9627	192.53		si
3							17	.5545	110.89		si
3							18	.5565	111.29		si
3							19	.5585	111.7		si
3							20	.5605	112.1		si
3							21	.5257	105.14		si
3							22	.5277	105.55		si
3							23	.5298	105.95		si
3							24	.5318	106.36		si
3							25	-.2151	-43.02		si
3							26	-.2136	-42.72		si
3							27	-.2121	-42.41		si
3							28	-.2106	-42.11		si
3							29	-.209	-41.81		si
3							30	-.2075	-41.51		si
3							31	-.206	-41.2		si
3							32	-.2045	-40.9		si
3							33	-.203	-40.6		si
3							34	-.2015	-40.3		si
3							35	-.2	-39.99		si
3							36	-.1985	-39.69		si
3							37	-.1969	-39.39		si
3							38	-.1954	-39.09		si
3							39	-.1939	-38.78		si
3							40	-.1924	-38.48		si
3							41	-.1909	-38.18		si
3							42	-.1894	-37.87		si
3							43	-.1879	-37.57		si
3							44	-.1863	-37.27		si
3							45	-.1848	-36.97		si
3							46	-.1833	-36.66		si
3							47	-.1818	-36.36		si
3							48	-.1803	-36.06		si
4	1- 1	.3612		0.		si	1	.601	120.2		si
4	1- 2	.3636		0.		si	2	.6004	120.08		si
4	1- 3	.6206		0.		si	3	.5998	119.97		si
4	1- 4	.6297		0.		si	4	.5992	119.85		si
4	1- 5	.3726		0.		si	5	.5987	119.73		si
4	1- 6	.375		0.		si	6	.5981	119.61		si
4	1- 7	-.1486		-2.02		si	7	.5975	119.5		si
4	1- 8	-.1623		-2.2		si	8	.5969	119.38		si

4				9	.5963	119.26	si
4				10	.5957	119.14	si
4				11	.5951	119.03	si
4				12	.5945	118.91	si
4				13	.594	118.79	si
4				14	.5934	118.67	si
4				15	.5928	118.56	si
4				16	.5922	118.44	si
4				17	.3352	67.03	si
4				18	.3344	66.88	si
4				19	.3336	66.72	si
4				20	.3328	66.56	si
4				21	.3463	69.27	si
4				22	.3455	69.11	si
4				23	.3448	68.95	si
4				24	.344	68.79	si
4				25	-.1201	-24.02	si
4				26	-.1207	-24.14	si
4				27	-.1213	-24.26	si
4				28	-.1219	-24.38	si
4				29	-.1225	-24.49	si
4				30	-.1231	-24.61	si
4				31	-.1237	-24.73	si
4				32	-.1242	-24.85	si
4				33	-.1248	-24.97	si
4				34	-.1254	-25.08	si
4				35	-.126	-25.2	si
4				36	-.1266	-25.32	si
4				37	-.1272	-25.44	si
4				38	-.1278	-25.55	si
4				39	-.1284	-25.67	si
4				40	-.1289	-25.79	si
4				41	-.1295	-25.91	si
4				42	-.1301	-26.02	si
4				43	-.1307	-26.14	si
4				44	-.1313	-26.26	si
4				45	-.1319	-26.38	si
4				46	-.1325	-26.5	si
4				47	-.1331	-26.61	si
4				48	-.1337	-26.73	si
5	1- 1	.3901	0.	1	.6455	129.1	si
5	1- 2	.3927	0.	2	.6448	128.97	si
5	1- 3	.6658	0.	3	.6442	128.83	si
5	1- 4	.676	0.	4	.6435	128.7	si
5	1- 5	.4029	0.	5	.6429	128.57	si
5	1- 6	.4055	0.	6	.6422	128.44	si
5	1- 7	-.1507	-2.05	7	.6415	128.31	si
5	1- 8	-.1662	-2.25	8	.6409	128.17	si
5				9	.6402	128.04	si
5				10	.6396	127.91	si
5				11	.6389	127.78	si
5				12	.6382	127.65	si
5				13	.6376	127.51	si
5				14	.6369	127.38	si
5				15	.6363	127.25	si
5				16	.6356	127.12	si
5				17	.3625	72.5	si
5				18	.3616	72.33	si
5				19	.3608	72.15	si
5				20	.3599	71.97	si
5				21	.3751	75.01	si
5				22	.3742	74.84	si
5				23	.3733	74.66	si
5				24	.3724	74.48	si
5				25	-.1205	-24.1	si
5				26	-.1212	-24.24	si
5				27	-.1218	-24.37	si
5				28	-.1225	-24.5	si
5				29	-.1232	-24.63	si
5				30	-.1238	-24.76	si
5				31	-.1245	-24.9	si
5				32	-.1251	-25.03	si
5				33	-.1258	-25.16	si
5				34	-.1265	-25.29	si
5				35	-.1271	-25.43	si
5				36	-.1278	-25.56	si
5				37	-.1284	-25.69	si
5				38	-.1291	-25.82	si
5				39	-.1298	-25.95	si
5				40	-.1304	-26.09	si
5				41	-.1311	-26.22	si
5				42	-.1317	-26.35	si
5				43	-.1324	-26.48	si
5				44	-.1331	-26.61	si
5				45	-.1337	-26.75	si
5				46	-.1344	-26.88	si
5				47	-.1351	-27.01	si
5				48	-.1357	-27.14	si

Descrizione : Pulvino 4

SOLLECITAZIONI AGENTI

Sforzi normali applicati in $z=183.7$; $y=37.5$ (baricentro CLS)
 Convenzioni: N + trazione; MZ + fib.inferiori tese; My + fib.sinistra tese.
 N. | N | MZ | My | Descrizione |

1	-15.11	-469.4644	-27.7627	Caso 13.1
2	-42.38	-850.2439	-271.5108	Caso 2.2
3	-43.57	-850.2955	113.6124	Caso 2.1
4	-58.66	-550.8491	-78.3319	Caso 6.14
5	3.06	-555.4113	-23.8118	Caso 6.19

RISULTATI

Piani di equilibrio (eps= muz * y +muy * z + lam):

Sol.	muz	muy	lambda
1.	.00000834579	.00000002237	-.00013668496
2.	.00001509723	.00000022184	-.00028286116
3.	.00001509226	-.00000009262	-.00022576182
4.	.00000963914	.00000006227	-.00016841063
5.	.00000996057	.00000001942	-.00016012133

Deformazioni sui materiali:

sol	vert.	cls			Acciaio lento			
		D cls	S cls	Ve	ferro	D ferri	S ferri	Ve
1	1- 1	.3223	0.	si	1	.5294	105.87	si
1	1- 2	.3237	0.	si	2	.529	105.8	si
1	1- 3	.5491	0.	si	3	.5287	105.73	si
1	1- 4	.5545	0.	si	4	.5283	105.66	si
1	1- 5	.3291	0.	si	5	.528	105.59	si
1	1- 6	.3306	0.	si	6	.5276	105.52	si
1	1- 7	-.1285	-1.75	si	7	.5273	105.45	si
1	1- 8	-.1367	-1.86	si	8	.5269	105.38	si
1					9	.5266	105.31	si
1					10	.5262	105.24	si
1					11	.5259	105.17	si
1					12	.5255	105.1	si
1					13	.5252	105.03	si
1					14	.5248	104.96	si
1					15	.5245	104.89	si
1					16	.5241	104.82	si
1					17	.2988	59.75	si
1					18	.2983	59.66	si
1					19	.2978	59.57	si
1					20	.2974	59.47	si
1					21	.3054	61.09	si
1					22	.305	61.	si
1					23	.3045	60.9	si
1					24	.304	60.81	si
1					25	-.1035	-20.7	si
1					26	-.1038	-20.77	si
1					27	-.1042	-20.84	si
1					28	-.1046	-20.91	si
1					29	-.1049	-20.98	si
1					30	-.1053	-21.05	si
1					31	-.1056	-21.12	si
1					32	-.106	-21.19	si
1					33	-.1063	-21.26	si
1					34	-.1067	-21.33	si
1					35	-.107	-21.4	si
1					36	-.1074	-21.47	si
1					37	-.1077	-21.54	si
1					38	-.1081	-21.61	si
1					39	-.1084	-21.68	si
1					40	-.1088	-21.75	si
1					41	-.1091	-21.82	si
1					42	-.1095	-21.89	si
1					43	-.1098	-21.96	si
1					44	-.1102	-22.03	si
1					45	-.1105	-22.11	si
1					46	-.1109	-22.18	si
1					47	-.1112	-22.25	si
1					48	-.1116	-22.32	si
2	1- 1	.5475	0.	si	1	.9767	195.34	si
2	1- 2	.5615	0.	si	2	.9732	194.64	si
2	1- 3	.9691	0.	si	3	.9697	193.94	si
2	1- 4	1.0226	0.	si	4	.9662	193.25	si
2	1- 5	.615	0.	si	5	.9628	192.55	si
2	1- 6	.629	0.	si	6	.9593	191.86	si
2	1- 7	-.2014	-2.7	si	7	.9558	191.16	si
2	1- 8	-.2829	-3.71	si	8	.9523	190.46	si
2					9	.9488	189.77	si
2					10	.9454	189.07	si
2					11	.9419	188.37	si
2					12	.9384	187.68	si
2					13	.9349	186.98	si
2					14	.9314	186.28	si
2					15	.9279	185.59	si
2					16	.9245	184.89	si
2					17	.5168	103.37	si
2					18	.5122	102.44	si
2					19	.5075	101.5	si
2					20	.5029	100.57	si
2					21	.583	116.61	si
2					22	.5784	115.68	si
2					23	.5737	114.74	si
2					24	.5691	113.81	si
2					25	-.1567	-31.35	si
2					26	-.1602	-32.04	si
2					27	-.1637	-32.74	si
2					28	-.1672	-33.44	si
2					29	-.1707	-34.13	si
2					30	-.1742	-34.83	si
2					31	-.1776	-35.53	si
2					32	-.1811	-36.23	si
2					33	-.1846	-36.92	si

2						34	-.1881	-37.62	si
2						35	-.1916	-38.32	si
2						36	-.1951	-39.01	si
2						37	-.1986	-39.71	si
2						38	-.202	-40.41	si
2						39	-.2055	-41.11	si
2						40	-.209	-41.8	si
2						41	-.2125	-42.5	si
2						42	-.216	-43.2	si
2						43	-.2195	-43.89	si
2						44	-.223	-44.59	si
2						45	-.2264	-45.29	si
2						46	-.2299	-45.99	si
2						47	-.2334	-46.68	si
2						48	-.2369	-47.38	si
3	1- 1	.6043	0.	si		1	.9386	187.72	si
3	1- 2	.5985	0.	si		2	.9401	188.01	si
3	1- 3	1.006	0.	si		3	.9415	188.3	si
3	1- 4	.9836	0.	si		4	.943	188.59	si
3	1- 5	.5761	0.	si		5	.9444	188.89	si
3	1- 6	.5703	0.	si		6	.9459	189.18	si
3	1- 7	-.2598	-3.43	si		7	.9473	189.47	si
3	1- 8	-.2258	-3.01	si		8	.9488	189.76	si
3						9	.9502	190.05	si
3						10	.9517	190.34	si
3						11	.9531	190.63	si
3						12	.9546	190.92	si
3						13	.9561	191.21	si
3						14	.9575	191.5	si
3						15	.959	191.79	si
3						16	.9604	192.08	si
3						17	.9529	110.58	si
3						18	.9549	110.97	si
3						19	.9568	111.36	si
3						20	.9588	111.75	si
3						21	.9553	105.06	si
3						22	.9572	105.45	si
3						23	.9592	105.84	si
3						24	.9531	106.22	si
3						25	-.2142	-42.85	si
3						26	-.2128	-42.56	si
3						27	-.2113	-42.26	si
3						28	-.2099	-41.97	si
3						29	-.2084	-41.68	si
3						30	-.207	-41.39	si
3						31	-.2055	-41.1	si
3						32	-.204	-40.81	si
3						33	-.2026	-40.52	si
3						34	-.2011	-40.23	si
3						35	-.1997	-39.94	si
3						36	-.1982	-39.65	si
3						37	-.1968	-39.35	si
3						38	-.1953	-39.06	si
3						39	-.1939	-38.77	si
3						40	-.1924	-38.48	si
3						41	-.1909	-38.19	si
3						42	-.1895	-37.9	si
3						43	-.188	-37.61	si
3						44	-.1866	-37.32	si
3						45	-.1851	-37.03	si
3						46	-.1837	-36.73	si
3						47	-.1822	-36.44	si
3						48	-.1808	-36.15	si
4	1- 1	.3617	0.	si		1	.6118	122.37	si
4	1- 2	.3657	0.	si		2	.6109	122.17	si
4	1- 3	.6259	0.	si		3	.6099	121.98	si
4	1- 4	.641	0.	si		4	.6089	121.78	si
4	1- 5	.3807	0.	si		5	.6079	121.59	si
4	1- 6	.3846	0.	si		6	.607	121.39	si
4	1- 7	-.1455	-1.98	si		7	.606	121.2	si
4	1- 8	-.1684	-2.28	si		8	.605	121.	si
4						9	.604	120.81	si
4						10	.6031	120.61	si
4						11	.6021	120.42	si
4						12	.6011	120.22	si
4						13	.6001	120.02	si
4						14	.5991	119.83	si
4						15	.5982	119.63	si
4						16	.5972	119.44	si
4						17	.3369	67.39	si
4						18	.3356	67.13	si
4						19	.3343	66.86	si
4						20	.333	66.6	si
4						21	.3555	71.1	si
4						22	.3542	70.84	si
4						23	.3529	70.58	si
4						24	.3516	70.32	si
4						25	-.1168	-23.36	si
4						26	-.1178	-23.56	si
4						27	-.1188	-23.75	si
4						28	-.1197	-23.95	si
4						29	-.1207	-24.14	si
4						30	-.1217	-24.34	si
4						31	-.1227	-24.53	si
4						32	-.1237	-24.73	si
4						33	-.1246	-24.93	si
4						34	-.1256	-25.12	si

4					35	-.1266	-25.32	si
4					36	-.1276	-25.51	si
4					37	-.1285	-25.71	si
4					38	-.1295	-25.9	si
4					39	-.1305	-26.1	si
4					40	-.1315	-26.3	si
4					41	-.1325	-26.49	si
4					42	-.1334	-26.69	si
4					43	-.1344	-26.88	si
4					44	-.1354	-27.08	si
4					45	-.1364	-27.27	si
4					46	-.1373	-27.47	si
4					47	-.1383	-27.67	si
4					48	-.1393	-27.86	si
5	1- 1	.3877	0.	si	1	.6326	126.52	si
5	1- 2	.3889	0.	si	2	.6323	126.46	si
5	1- 3	.6579	0.	si	3	.632	126.4	si
5	1- 4	.6626	0.	si	4	.6317	126.34	si
5	1- 5	.3936	0.	si	5	.6314	126.28	si
5	1- 6	.3948	0.	si	6	.6311	126.22	si
5	1- 7	-.153	-2.08	si	7	.6308	126.16	si
5	1- 8	-.1601	-2.17	si	8	.6305	126.1	si
5					9	.6302	126.04	si
5					10	.6299	125.97	si
5					11	.6296	125.91	si
5					12	.6293	125.85	si
5					13	.629	125.79	si
5					14	.6287	125.73	si
5					15	.6284	125.67	si
5					16	.628	125.61	si
5					17	.3591	71.82	si
5					18	.3587	71.74	si
5					19	.3583	71.66	si
5					20	.3579	71.58	si
5					21	.3649	72.98	si
5					22	.3645	72.9	si
5					23	.3641	72.82	si
5					24	.3637	72.74	si
5					25	-.1232	-24.63	si
5					26	-.1235	-24.69	si
5					27	-.1238	-24.75	si
5					28	-.1241	-24.82	si
5					29	-.1244	-24.88	si
5					30	-.1247	-24.94	si
5					31	-.125	-25.	si
5					32	-.1253	-25.06	si
5					33	-.1256	-25.12	si
5					34	-.1259	-25.18	si
5					35	-.1262	-25.24	si
5					36	-.1265	-25.3	si
5					37	-.1268	-25.37	si
5					38	-.1271	-25.43	si
5					39	-.1274	-25.49	si
5					40	-.1277	-25.55	si
5					41	-.128	-25.61	si
5					42	-.1284	-25.67	si
5					43	-.1287	-25.73	si
5					44	-.129	-25.79	si
5					45	-.1293	-25.85	si
5					46	-.1296	-25.91	si
5					47	-.1299	-25.98	si
5					48	-.1302	-26.04	si

Descrizione : Pulvino 5

SOLLECITAZIONI AGENTI

Sforzi normali applicati in z= 183.7 ; y= 37.5 (baricentro CLS)
 convenzioni: N + trazione; Mz + fib.inferiori tese; My + fib.sinistra tese.

N.	N	Mz	My	Descrizione
1	-15.62	-469.0105	-28.7024	Caso 13.1
2	-43.35	-849.0304	-269.0794	Caso 2.2
3	-44.55	-849.0511	107.5982	Caso 2.1
4	-58.81	-549.2973	-112.9117	Caso 8.20
5	1.92	-555.3705	8.4007	Caso 8.13

RISULTATI

Piani di equilibrio (eps= muz * y + muy * z + lam):

Sol.	muz	muy	lambda
1.	.00000833566	.00000002312	-.00013670766
2.	.00001507156	.00000021977	-.00028217119
3.	.00001506598	-.00000008768	-.0002263499
4.	.00000961088	.00000008978	-.00017292372
5.	.00000995541	-.00000000685	-.00015532779

Deformazioni sui materiali:

sol	Cls				Acciaio lento			
	vert.	D cls	S cls	Ve	ferro	D ferri	S ferri	Ve
1	1- 1	.3218	0.	si	1	.5288	105.76	si
1	1- 2	.3232	0.	si	2	.5284	105.68	si
1	1- 3	.5483	0.	si	3	.5281	105.61	si
1	1- 4	.5539	0.	si	4	.5277	105.54	si
1	1- 5	.3288	0.	si	5	.5273	105.47	si
1	1- 6	.3302	0.	si	6	.527	105.39	si
1	1- 7	-.1282	-1.75	si	7	.5266	105.32	si
1	1- 8	-.1367	-1.86	si	8	.5262	105.25	si
1					9	.5259	105.17	si
1					10	.5255	105.1	si

1				11	.5251	105.03	si
1				12	.5248	104.96	si
1				13	.5244	104.88	si
1				14	.5241	104.81	si
1				15	.5237	104.74	si
1				16	.5233	104.67	si
1				17	.2983	59.65	si
1				18	.2978	59.56	si
1				19	.2973	59.46	si
1				20	.2968	59.36	si
1				21	.3052	61.03	si
1				22	.3047	60.94	si
1				23	.3042	60.84	si
1				24	.3037	60.74	si
1				25	-.1033	-20.66	si
1				26	-.1036	-20.73	si
1				27	-.104	-20.8	si
1				28	-.1044	-20.87	si
1				29	-.1047	-20.95	si
1				30	-.1051	-21.02	si
1				31	-.1055	-21.09	si
1				32	-.1058	-21.16	si
1				33	-.1062	-21.24	si
1				34	-.1065	-21.31	si
1				35	-.1069	-21.38	si
1				36	-.1073	-21.45	si
1				37	-.1076	-21.53	si
1				38	-.108	-21.6	si
1				39	-.1084	-21.67	si
1				40	-.1087	-21.75	si
1				41	-.1091	-21.82	si
1				42	-.1095	-21.89	si
1				43	-.1098	-21.96	si
1				44	-.1102	-22.04	si
1				45	-.1105	-22.11	si
1				46	-.1109	-22.18	si
1				47	-.1113	-22.25	si
1				48	-.1116	-22.33	si
2	1- 1	.5468	0.	1	.9747	194.94	si
2	1- 2	.5606	0.	2	.9713	194.25	si
2	1- 3	.9675	0.	3	.9678	193.56	si
2	1- 4	1.0206	0.	4	.9644	192.87	si
2	1- 5	.6137	0.	5	.9609	192.19	si
2	1- 6	.6275	0.	6	.9575	191.5	si
2	1- 7	-.2014	-2.7	7	.954	190.81	si
2	1- 8	-.2822	-3.7	8	.9506	190.12	si
2				9	.9471	189.43	si
2				10	.9437	188.74	si
2				11	.9402	188.05	si
2				12	.9368	187.36	si
2				13	.9333	186.67	si
2				14	.9299	185.98	si
2				15	.9264	185.29	si
2				16	.923	184.6	si
2				17	.5161	103.21	si
2				18	.5114	102.29	si
2				19	.5068	101.36	si
2				20	.5022	100.44	si
2				21	.5816	116.33	si
2				22	.577	115.4	si
2				23	.5724	114.48	si
2				24	.5678	113.56	si
2				25	-.1569	-31.37	si
2				26	-.1603	-32.06	si
2				27	-.1638	-32.76	si
2				28	-.1672	-33.45	si
2				29	-.1707	-34.14	si
2				30	-.1741	-34.83	si
2				31	-.1776	-35.52	si
2				32	-.181	-36.21	si
2				33	-.1845	-36.9	si
2				34	-.188	-37.59	si
2				35	-.1914	-38.28	si
2				36	-.1949	-38.97	si
2				37	-.1983	-39.66	si
2				38	-.2018	-40.35	si
2				39	-.2052	-41.04	si
2				40	-.2087	-41.73	si
2				41	-.2121	-42.42	si
2				42	-.2156	-43.12	si
2				43	-.219	-43.81	si
2				44	-.2225	-44.5	si
2				45	-.2259	-45.19	si
2				46	-.2294	-45.88	si
2				47	-.2328	-46.57	si
2				48	-.2363	-47.26	si
3	1- 1	.6023	0.	1	.9374	187.49	si
3	1- 2	.5968	0.	2	.9388	187.76	si
3	1- 3	1.0035	0.	3	.9402	188.04	si
3	1- 4	.9824	0.	4	.9416	188.31	si
3	1- 5	.5756	0.	5	.9429	188.59	si
3	1- 6	.5701	0.	6	.9443	188.86	si
3	1- 7	-.2586	-3.41	7	.9457	189.14	si
3	1- 8	-.2263	-3.01	8	.9471	189.41	si
3				9	.9484	189.69	si
3				10	.9498	189.96	si
3				11	.9512	190.24	si

3				12	.9526	190.51	si
3				13	.9539	190.79	si
3				14	.9553	191.06	si
3				15	.9567	191.34	si
3				16	.9581	191.62	si
3				17	.5513	110.26	si
3				18	.5531	110.63	si
3				19	.555	111.	si
3				20	.5568	111.36	si
3				21	.5251	105.03	si
3				22	.527	105.39	si
3				23	.5288	105.76	si
3				24	.5307	106.13	si
3				25	-.2131	-42.62	si
3				26	-.2117	-42.34	si
3				27	-.2103	-42.07	si
3				28	-.209	-41.79	si
3				29	-.2076	-41.52	si
3				30	-.2062	-41.24	si
3				31	-.2048	-40.97	si
3				32	-.2035	-40.69	si
3				33	-.2021	-40.42	si
3				34	-.2007	-40.14	si
3				35	-.1993	-39.87	si
3				36	-.1979	-39.59	si
3				37	-.1966	-39.31	si
3				38	-.1952	-39.04	si
3				39	-.1938	-38.76	si
3				40	-.1924	-38.49	si
3				41	-.1911	-38.21	si
3				42	-.1897	-37.94	si
3				43	-.1883	-37.66	si
3				44	-.1869	-37.39	si
3				45	-.1855	-37.11	si
3				46	-.1842	-36.83	si
3				47	-.1828	-36.56	si
3				48	-.1814	-36.28	si
4	1- 1	.3557	0.	1	.6134	122.68	si
4	1- 2	.3613	0.	2	.612	122.4	si
4	1- 3	.6208	0.	3	.6106	122.12	si
4	1- 4	.6425	0.	4	.6092	121.83	si
4	1- 5	.383	0.	5	.6078	121.55	si
4	1- 6	.3887	0.	6	.6064	121.27	si
4	1- 7	-.1399	-1.91	7	.6049	120.99	si
4	1- 8	-.1729	-2.33	8	.6035	120.71	si
4				9	.6021	120.42	si
4				10	.6007	120.14	si
4				11	.5993	119.86	si
4				12	.5979	119.58	si
4				13	.5965	119.3	si
4				14	.5951	119.02	si
4				15	.5937	118.73	si
4				16	.5923	118.45	si
4				17	.3328	66.55	si
4				18	.3309	66.18	si
4				19	.329	65.8	si
4				20	.3271	65.42	si
4				21	.3596	71.91	si
4				22	.3577	71.53	si
4				23	.3558	71.16	si
4				24	.3539	70.78	si
4				25	-.1114	-22.27	si
4				26	-.1128	-22.56	si
4				27	-.1142	-22.84	si
4				28	-.1156	-23.12	si
4				29	-.117	-23.4	si
4				30	-.1184	-23.69	si
4				31	-.1198	-23.97	si
4				32	-.1212	-24.25	si
4				33	-.1227	-24.53	si
4				34	-.1241	-24.81	si
4				35	-.1255	-25.1	si
4				36	-.1269	-25.38	si
4				37	-.1283	-25.66	si
4				38	-.1297	-25.94	si
4				39	-.1311	-26.22	si
4				40	-.1325	-26.51	si
4				41	-.1339	-26.79	si
4				42	-.1354	-27.07	si
4				43	-.1368	-27.35	si
4				44	-.1382	-27.64	si
4				45	-.1396	-27.92	si
4				46	-.141	-28.2	si
4				47	-.1424	-28.48	si
4				48	-.1438	-28.76	si
5	1- 1	.3922	0.	1	.6291	125.82	si
5	1- 2	.3918	0.	2	.6292	125.84	si
5	1- 3	.6606	0.	3	.6293	125.86	si
5	1- 4	.6589	0.	4	.6294	125.88	si
5	1- 5	.3901	0.	5	.6295	125.9	si
5	1- 6	.3897	0.	6	.6296	125.92	si
5	1- 7	-.1578	-2.14	7	.6297	125.95	si
5	1- 8	-.1553	-2.11	8	.6298	125.97	si
5				9	.6299	125.99	si
5				10	.6301	126.01	si
5				11	.6302	126.03	si
5				12	.6303	126.05	si

5	13	.6304	126.08	si
5	14	.6305	126.1	si
5	15	.6306	126.12	si
5	16	.6307	126.14	si
5	17	.3619	72.38	si
5	18	.362	72.41	si
5	19	.3622	72.44	si
5	20	.3623	72.47	si
5	21	.3599	71.97	si
5	22	.36	72.	si
5	23	.3601	72.03	si
5	24	.3603	72.06	si
5	25	-.128	-25.59	si
5	26	-.1278	-25.57	si
5	27	-.1277	-25.55	si
5	28	-.1276	-25.53	si
5	29	-.1275	-25.51	si
5	30	-.1274	-25.48	si
5	31	-.1273	-25.46	si
5	32	-.1272	-25.44	si
5	33	-.1271	-25.42	si
5	34	-.127	-25.4	si
5	35	-.1269	-25.38	si
5	36	-.1268	-25.35	si
5	37	-.1267	-25.33	si
5	38	-.1266	-25.31	si
5	39	-.1265	-25.29	si
5	40	-.1263	-25.27	si
5	41	-.1262	-25.25	si
5	42	-.1261	-25.23	si
5	43	-.126	-25.2	si
5	44	-.1259	-25.18	si
5	45	-.1258	-25.16	si
5	46	-.1257	-25.14	si
5	47	-.1256	-25.12	si
5	48	-.1255	-25.1	si

Descrizione : Pulvino 6

SOLLECITAZIONI AGENTI

Sforzi normali applicati in z= 183.7 ; y= 37.5

Convenzioni: N + trazione; Mz + fib.inferiori tese; My + fib.sinistra tese.

N.	N	Mz	My	Descrizione
1	-17.03	-468.4511	-31.2777	Caso 13.1
2	-45.92	-847.6341	-308.5721	Caso 2.2
3	-47.11	-847.6247	137.6681	Caso 2.1
4	-62.12	-547.3944	-119.6235	Caso 8.20
5	1.84	-555.4383	8.8986	Caso 8.13

RISULTATI

Piani di equilibrio (eps= muz * y +muy * z + lam):

Sol.	muz	muy	lambda
1.	.00000832014	.00000002517	-.00013696471
2.	.00001503691	.00000025203	-.00028753502
3.	.00001503051	-.00000011212	-.00022144792
4.	.00000956389	.00000009498	-.00017340371
5.	.00000995631	-.00000000725	-.00015527495

Deformazioni sui materiali:

sol	C1s			Ve	Acciaio lento			
	vert.	D c1s	S c1s		ferro	D ferri	S ferri	
1	1- 1	.3206	0.	si	1	.5279	105.58	si
1	1- 2	.3222	0.	si	2	.5275	105.5	si
1	1- 3	.5469	0.	si	3	.5271	105.42	si
1	1- 4	.5529	0.	si	4	.5267	105.35	si
1	1- 5	.3283	0.	si	5	.5263	105.27	si
1	1- 6	.3299	0.	si	6	.5259	105.19	si
1	1- 7	-.1277	-1.74	si	7	.5255	105.11	si
1	1- 8	-.137	-1.87	si	8	.5251	105.03	si
1					9	.5248	104.95	si
1					10	.5244	104.87	si
1					11	.524	104.79	si
1					12	.5236	104.71	si
1					13	.5232	104.63	si
1					14	.5228	104.56	si
1					15	.5224	104.48	si
1					16	.522	104.4	si
1					17	.2973	59.47	si
1					18	.2968	59.36	si
1					19	.2963	59.26	si
1					20	.2958	59.15	si
1					21	.3049	60.97	si
1					22	.3043	60.87	si
1					23	.3038	60.76	si
1					24	.3033	60.65	si
1					25	-.1028	-20.57	si
1					26	-.1032	-20.65	si
1					27	-.1036	-20.72	si
1					28	-.104	-20.8	si
1					29	-.1044	-20.88	si
1					30	-.1048	-20.96	si
1					31	-.1052	-21.04	si
1					32	-.1056	-21.12	si
1					33	-.106	-21.2	si
1					34	-.1064	-21.28	si
1					35	-.1068	-21.36	si
1					36	-.1072	-21.44	si

1				37	-.1076	-21.52	si
1				38	-.108	-21.59	si
1				39	-.1084	-21.67	si
1				40	-.1088	-21.75	si
1				41	-.1092	-21.83	si
1				42	-.1096	-21.91	si
1				43	-.11	-21.99	si
1				44	-.1103	-22.07	si
1				45	-.1107	-22.15	si
1				46	-.1111	-22.23	si
1				47	-.1115	-22.31	si
1				48	-.1119	-22.39	si
2	1- 1	.5395	0.	1	.9763	195.27	si
2	1- 2	.5554	0.	2	.9724	194.48	si
2	1- 3	.9614	0.	3	.9684	193.69	si
2	1- 4	1.0222	0.	4	.9645	192.9	si
2	1- 5	.6162	0.	5	.9605	192.1	si
2	1- 6	.6321	0.	6	.9566	191.31	si
2	1- 7	-.1949	-2.62	7	.9526	190.52	si
2	1- 8	-.2875	-3.77	8	.9487	189.73	si
2				9	.9447	188.94	si
2				10	.9407	188.15	si
2				11	.9368	187.36	si
2				12	.9328	186.57	si
2				13	.9289	185.78	si
2				14	.9249	184.99	si
2				15	.921	184.19	si
2				16	.917	183.4	si
2				17	.511	102.2	si
2				18	.5057	101.15	si
2				19	.5004	100.09	si
2				20	.4951	99.03	si
2				21	.5862	117.24	si
2				22	.5809	116.19	si
2				23	.5756	115.13	si
2				24	.5703	114.07	si
2				25	-.1506	-30.12	si
2				26	-.1545	-30.91	si
2				27	-.1585	-31.7	si
2				28	-.1625	-32.49	si
2				29	-.1664	-33.29	si
2				30	-.1704	-34.08	si
2				31	-.1743	-34.87	si
2				32	-.1783	-35.66	si
2				33	-.1823	-36.45	si
2				34	-.1862	-37.25	si
2				35	-.1902	-38.04	si
2				36	-.1941	-38.83	si
2				37	-.1981	-39.62	si
2				38	-.2021	-40.41	si
2				39	-.206	-41.21	si
2				40	-.21	-42.	si
2				41	-.2139	-42.79	si
2				42	-.2179	-43.58	si
2				43	-.2219	-44.37	si
2				44	-.2258	-45.17	si
2				45	-.2298	-45.96	si
2				46	-.2337	-46.75	si
2				47	-.2377	-47.54	si
2				48	-.2417	-48.33	si
3	1- 1	.6052	0.	1	.9322	186.43	si
3	1- 2	.5982	0.	2	.9339	186.79	si
3	1- 3	1.004	0.	3	.9357	187.14	si
3	1- 4	.9769	0.	4	.9374	187.49	si
3	1- 5	.5711	0.	5	.9392	187.84	si
3	1- 6	.564	0.	6	.941	188.19	si
3	1- 7	-.2626	-3.46	7	.9427	188.55	si
3	1- 8	-.2214	-2.95	8	.9445	188.9	si
3				9	.9462	189.25	si
3				10	.948	189.6	si
3				11	.9498	189.95	si
3				12	.9515	190.3	si
3				13	.9533	190.66	si
3				14	.955	191.01	si
3				15	.9568	191.36	si
3				16	.9586	191.71	si
3				17	.5527	110.55	si
3				18	.5551	111.02	si
3				19	.5574	111.49	si
3				20	.5598	111.96	si
3				21	.5193	103.86	si
3				22	.5216	104.33	si
3				23	.524	104.8	si
3				24	.5263	105.27	si
3				25	-.2172	-43.44	si
3				26	-.2155	-43.09	si
3				27	-.2137	-42.74	si
3				28	-.2119	-42.39	si
3				29	-.2102	-42.03	si
3				30	-.2084	-41.68	si
3				31	-.2066	-41.33	si
3				32	-.2049	-40.98	si
3				33	-.2031	-40.62	si
3				34	-.2014	-40.27	si
3				35	-.1996	-39.92	si
3				36	-.1978	-39.57	si
3				37	-.1961	-39.21	si

5	39	-.1265	-25.29	si
5	40	-.1263	-25.27	si
5	41	-.1262	-25.25	si
5	42	-.1261	-25.22	si
5	43	-.126	-25.2	si
5	44	-.1259	-25.18	si
5	45	-.1258	-25.15	si
5	46	-.1257	-25.13	si
5	47	-.1255	-25.11	si
5	48	-.1254	-25.09	si

Descrizione : Pulvino 7

SOLLECITAZIONI AGENTI

Sforzi normali applicati in z= 183.7 ; y= 37.5 (baricentro CLS)
 Convenzioni: N + trazione; Mz + fib.inferiori tese; My + fib.sinistra tese.

N.	N	Mz	My	Descrizione
1	-18.13	-469.1654	-3.3305	Caso 13.1
2	-51.23	-860.0767	-213.2864	Caso 2.2
3	-52.42	-860.1243	213.2854	Caso 2.1
4	-65.81	-550.0619	-12.0893	Caso 8.20
5	2.81	-555.4066	2.377	Caso 8.13

RISULTATI

Piani di equilibrio (eps= muz * y +muy * z + lam):

Sol.	muz	muy	lambda
1.	.00000832867	.00000000268	-.00013308645
2.	.00001523999	.00000017379	-.0002774491
3.	.00001523625	-.00000017373	-.00021365864
4.	.00000959703	.00000000958	-.00015879746
5.	.00000995951	-.00000000194	-.00015621381

Deformazioni sui materiali:

sol	cls				Acciaio lento			
	vert.	D cls	S cls	Ve	ferro	D	S	ferriferri
1	1- 1	.325	0.	si	1	.5257	105.14	si
1	1- 2	.3252	0.	si	2	.5256	105.13	si
1	1- 3	.55	0.	si	3	.5256	105.12	si
1	1- 4	.5507	0.	si	4	.5256	105.11	si
1	1- 5	.3258	0.	si	5	.5255	105.1	si
1	1- 6	.326	0.	si	6	.5255	105.1	si
1	1- 7	-.1321	-1.8	si	7	.5254	105.09	si
1	1- 8	-.1331	-1.82	si	8	.5254	105.08	si
1					9	.5253	105.07	si
1					10	.5253	105.06	si
1					11	.5253	105.05	si
1					12	.5252	105.04	si
1					13	.5252	105.04	si
1					14	.5251	105.03	si
1					15	.5251	105.02	si
1					16	.5251	105.01	si
1					17	.3002	60.04	si
1					18	.3001	60.02	si
1					19	.3001	60.01	si
1					20	.3	60.	si
1					21	.301	60.2	si
1					22	.3009	60.18	si
1					23	.3009	60.17	si
1					24	.3008	60.16	si
1					25	-.1071	-21.42	si
1					26	-.1072	-21.43	si
1					27	-.1072	-21.44	si
1					28	-.1073	-21.45	si
1					29	-.1073	-21.46	si
1					30	-.1073	-21.47	si
1					31	-.1074	-21.48	si
1					32	-.1074	-21.48	si
1					33	-.1075	-21.49	si
1					34	-.1075	-21.5	si
1					35	-.1075	-21.51	si
1					36	-.1076	-21.52	si
1					37	-.1076	-21.53	si
1					38	-.1077	-21.53	si
1					39	-.1077	-21.54	si
1					40	-.1078	-21.55	si
1					41	-.1078	-21.56	si
1					42	-.1078	-21.57	si
1					43	-.1079	-21.58	si
1					44	-.1079	-21.58	si
1					45	-.108	-21.59	si
1					46	-.108	-21.6	si
1					47	-.1081	-21.61	si
1					48	-.1081	-21.62	si
2	1- 1	.5608	0.	si	1	.9789	195.78	si
2	1- 2	.5717	0.	si	2	.9762	195.23	si
2	1- 3	.9832	0.	si	3	.9734	194.69	si
2	1- 4	1.0251	0.	si	4	.9707	194.14	si
2	1- 5	.6137	0.	si	5	.968	193.6	si
2	1- 6	.6246	0.	si	6	.9653	193.05	si
2	1- 7	-.2136	-2.85	si	7	.9625	192.51	si
2	1- 8	-.2774	-3.64	si	8	.9598	191.96	si
2					9	.9571	191.41	si
2					10	.9543	190.87	si
2					11	.9516	190.32	si
2					12	.9489	189.78	si
2					13	.9462	189.23	si
2					14	.9434	188.69	si

2				15	.9407	188.14	si
2				16	.938	187.6	si
2				17	.5265	105.3	si
2				18	.5229	104.57	si
2				19	.5192	103.84	si
2				20	.5156	103.11	si
2				21	.5784	115.67	si
2				22	.5747	114.94	si
2				23	.5711	114.21	si
2				24	.5674	113.48	si
2				25	-.1684	-33.68	si
2				26	-.1711	-34.23	si
2				27	-.1739	-34.77	si
2				28	-.1766	-35.32	si
2				29	-.1793	-35.86	si
2				30	-.1821	-36.41	si
2				31	-.1848	-36.96	si
2				32	-.1875	-37.5	si
2				33	-.1902	-38.05	si
2				34	-.193	-38.6	si
2				35	-.1957	-39.14	si
2				36	-.1984	-39.69	si
2				37	-.2012	-40.23	si
2				38	-.2039	-40.78	si
2				39	-.2066	-41.33	si
2				40	-.2094	-41.87	si
2				41	-.2121	-42.42	si
2				42	-.2148	-42.96	si
2				43	-.2176	-43.51	si
2				44	-.2203	-44.06	si
2				45	-.223	-44.6	si
2				46	-.2257	-45.15	si
2				47	-.2285	-45.7	si
2				48	-.2312	-46.24	si
3	1- 1	.6243	0.	1	.9376	187.53	si
3	1- 2	.6134	0.	2	.9404	188.07	si
3	1- 3	1.0248	0.	3	.9431	188.62	si
3	1- 4	.9828	0.	4	.9458	189.16	si
3	1- 5	.5715	0.	5	.9485	189.71	si
3	1- 6	.5605	0.	6	.9513	190.25	si
3	1- 7	-.2775	-3.64	7	.954	190.8	si
3	1- 8	-.2137	-2.85	8	.9567	191.35	si
3				9	.9595	191.89	si
3				10	.9622	192.44	si
3				11	.9649	192.98	si
3				12	.9676	193.53	si
3				13	.9704	194.07	si
3				14	.9731	194.62	si
3				15	.9758	195.16	si
3				16	.9785	195.71	si
3				17	.5672	113.43	si
3				18	.5708	114.16	si
3				19	.5745	114.89	si
3				20	.5781	115.62	si
3				21	.5153	103.06	si
3				22	.519	103.79	si
3				23	.5226	104.52	si
3				24	.5263	105.25	si
3				25	-.2313	-46.25	si
3				26	-.2285	-45.71	si
3				27	-.2258	-45.16	si
3				28	-.2231	-44.61	si
3				29	-.2203	-44.07	si
3				30	-.2176	-43.52	si
3				31	-.2149	-42.98	si
3				32	-.2121	-42.43	si
3				33	-.2094	-41.88	si
3				34	-.2067	-41.34	si
3				35	-.204	-40.79	si
3				36	-.2012	-40.25	si
3				37	-.1985	-39.7	si
3				38	-.1958	-39.15	si
3				39	-.193	-38.61	si
3				40	-.1903	-38.06	si
3				41	-.1876	-37.52	si
3				42	-.1849	-36.97	si
3				43	-.1821	-36.42	si
3				44	-.1794	-35.88	si
3				45	-.1767	-35.33	si
3				46	-.1739	-34.79	si
3				47	-.1712	-34.24	si
3				48	-.1685	-33.69	si
4	1- 1	.369	0.	1	.6023	120.45	si
4	1- 2	.3696	0.	2	.6021	120.42	si
4	1- 3	.6288	0.	3	.602	120.39	si
4	1- 4	.6311	0.	4	.6018	120.36	si
4	1- 5	.372	0.	5	.6017	120.33	si
4	1- 6	.3726	0.	6	.6015	120.3	si
4	1- 7	-.1553	-2.11	7	.6014	120.27	si
4	1- 8	-.1588	-2.15	8	.6012	120.24	si
4				9	.6011	120.21	si
4				10	.6009	120.18	si
4				11	.6008	120.15	si
4				12	.6006	120.12	si
4				13	.6005	120.09	si
4				14	.6003	120.06	si
4				15	.6002	120.03	si

4				16	.6	120.	si
4				17	.3409	68.18	si
4				18	.3407	68.14	si
4				19	.3405	68.1	si
4				20	.3403	68.06	si
4				21	.3437	68.75	si
4				22	.3435	68.71	si
4				23	.3433	68.67	si
4				24	.3431	68.63	si
4				25	-.1265	-25.3	si
4				26	-.1267	-25.33	si
4				27	-.1268	-25.36	si
4				28	-.127	-25.39	si
4				29	-.1271	-25.42	si
4				30	-.1273	-25.45	si
4				31	-.1274	-25.48	si
4				32	-.1276	-25.51	si
4				33	-.1277	-25.54	si
4				34	-.1279	-25.57	si
4				35	-.128	-25.6	si
4				36	-.1282	-25.63	si
4				37	-.1283	-25.66	si
4				38	-.1285	-25.69	si
4				39	-.1286	-25.72	si
4				40	-.1288	-25.75	si
4				41	-.1289	-25.78	si
4				42	-.1291	-25.81	si
4				43	-.1292	-25.85	si
4				44	-.1294	-25.88	si
4				45	-.1295	-25.91	si
4				46	-.1297	-25.94	si
4				47	-.1298	-25.97	si
4				48	-.13	-26.	si
5	1- 1	.3916	0.	1	.63	126.	si
5	1- 2	.3914	0.	2	.63	126.01	si
5	1- 3	.6603	0.	3	.6301	126.01	si
5	1- 4	.6599	0.	4	.6301	126.02	si
5	1- 5	.391	0.	5	.6301	126.02	si
5	1- 6	.3908	0.	6	.6302	126.03	si
5	1- 7	-.1569	-2.13	7	.6302	126.04	si
5	1- 8	-.1562	-2.12	8	.6302	126.04	si
5				9	.6302	126.05	si
5				10	.6303	126.06	si
5				11	.6303	126.06	si
5				12	.6303	126.07	si
5				13	.6304	126.07	si
5				14	.6304	126.08	si
5				15	.6304	126.09	si
5				16	.6305	126.09	si
5				17	.3616	72.31	si
5				18	.3616	72.32	si
5				19	.3616	72.33	si
5				20	.3617	72.33	si
5				21	.361	72.19	si
5				22	.361	72.2	si
5				23	.3611	72.21	si
5				24	.3611	72.22	si
5				25	-.127	-25.41	si
5				26	-.127	-25.4	si
5				27	-.127	-25.4	si
5				28	-.127	-25.39	si
5				29	-.1269	-25.38	si
5				30	-.1269	-25.38	si
5				31	-.1269	-25.37	si
5				32	-.1268	-25.37	si
5				33	-.1268	-25.36	si
5				34	-.1268	-25.35	si
5				35	-.1267	-25.35	si
5				36	-.1267	-25.34	si
5				37	-.1267	-25.34	si
5				38	-.1266	-25.33	si
5				39	-.1266	-25.32	si
5				40	-.1266	-25.32	si
5				41	-.1266	-25.31	si
5				42	-.1265	-25.3	si
5				43	-.1265	-25.3	si
5				44	-.1265	-25.29	si
5				45	-.1264	-25.29	si
5				46	-.1264	-25.28	si
5				47	-.1264	-25.27	si
5				48	-.1263	-25.27	si

Descrizione : Pulvino 8

SOLLECITAZIONI AGENTI

Sforzi normali applicati in z= 183.7 ; y= 37.5 (baricentro CLS)
 Convenzioni: N + trazione; Mz + fib.inferiori tese; My + fib.sinistra tese.

N.	N	Mz	My	Descrizione
1	-19.77	-469.0543	-3.6317	Caso 13.1
2	-54.54	-860.3879	-212.3401	Caso 2.2
3	-55.74	-860.4358	212.3395	Caso 2.1
4	-70.97	-549.681	13.0372	Caso 8.20
5	4.01	-555.5239	-.574	Caso 8.13

RISULTATI

Piani di equilibrio (eps= muz * y +muy * z + lam):

Sol.	muz	muy	lambda
1.	.0000083203	.00000000292	-.00013314689
2.	.00001523282	.00000017287	-.00027747405
3.	.00001522905	-.00000017281	-.00021402246
4.	.00000957016	-.0000000103	-.00015517892
5.	.00000996628	.00000000047	-.00015665288

Deformazioni sui materiali:

Cls					Acciaio lento			
sol	vert.	D cls	S cls	Ve	ferro	D ferri	S ferri	Ve
1	1- 1	.3245	0.	si	1	.525	105.01	si
1	1- 2	.3247	0.	si	2	.525	105.	si
1	1- 3	.5493	0.	si	3	.5249	104.99	si
1	1- 4	.55	0.	si	4	.5249	104.98	si
1	1- 5	.3254	0.	si	5	.5249	104.97	si
1	1- 6	.3255	0.	si	6	.5248	104.96	si
1	1- 7	-.1321	-1.8	si	7	.5248	104.95	si
1	1- 8	-.1331	-1.82	si	8	.5247	104.94	si
1					9	.5247	104.93	si
1					10	.5246	104.92	si
1					11	.5246	104.92	si
1					12	.5245	104.91	si
1					13	.5245	104.9	si
1					14	.5244	104.89	si
1					15	.5244	104.88	si
1					16	.5243	104.87	si
1					17	.2997	59.94	si
1					18	.2996	59.93	si
1					19	.2996	59.92	si
1					20	.2995	59.9	si
1					21	.3006	60.11	si
1					22	.3005	60.1	si
1					23	.3004	60.09	si
1					24	.3004	60.08	si
1					25	-.1071	-21.42	si
1					26	-.1072	-21.43	si
1					27	-.1072	-21.44	si
1					28	-.1073	-21.45	si
1					29	-.1073	-21.46	si
1					30	-.1074	-21.47	si
1					31	-.1074	-21.48	si
1					32	-.1074	-21.49	si
1					33	-.1075	-21.5	si
1					34	-.1075	-21.51	si
1					35	-.1076	-21.52	si
1					36	-.1076	-21.53	si
1					37	-.1077	-21.53	si
1					38	-.1077	-21.54	si
1					39	-.1078	-21.55	si
1					40	-.1078	-21.56	si
1					41	-.1079	-21.57	si
1					42	-.1079	-21.58	si
1					43	-.1079	-21.59	si
1					44	-.108	-21.6	si
1					45	-.108	-21.61	si
1					46	-.1081	-21.62	si
1					47	-.1081	-21.63	si
1					48	-.1082	-21.64	si
2	1- 1	.5603	0.	si	1	.978	195.6	si
2	1- 2	.5712	0.	si	2	.9753	195.06	si
2	1- 3	.9825	0.	si	3	.9726	194.52	si
2	1- 4	1.0242	0.	si	4	.9699	193.98	si
2	1- 5	.613	0.	si	5	.9672	193.43	si
2	1- 6	.6238	0.	si	6	.9645	192.89	si
2	1- 7	-.214	-2.86	si	7	.9617	192.35	si
2	1- 8	-.2775	-3.64	si	8	.959	191.81	si
2					9	.9563	191.26	si
2					10	.9536	190.72	si
2					11	.9509	190.18	si
2					12	.9482	189.64	si
2					13	.9455	189.09	si
2					14	.9428	188.55	si
2					15	.94	188.01	si
2					16	.9373	187.47	si
2					17	.526	105.21	si
2					18	.5224	104.48	si
2					19	.5188	103.76	si
2					20	.5152	103.03	si
2					21	.5776	115.53	si
2					22	.574	114.8	si
2					23	.5704	114.07	si
2					24	.5667	113.35	si
2					25	-.1688	-33.76	si
2					26	-.1715	-34.3	si
2					27	-.1742	-34.84	si
2					28	-.1769	-35.39	si
2					29	-.1796	-35.93	si
2					30	-.1824	-36.47	si
2					31	-.1851	-37.02	si
2					32	-.1878	-37.56	si
2					33	-.1905	-38.1	si
2					34	-.1932	-38.65	si
2					35	-.1959	-39.19	si
2					36	-.1987	-39.73	si
2					37	-.2014	-40.28	si
2					38	-.2041	-40.82	si
2					39	-.2068	-41.36	si

2					40	-.2095	-41.91	si
2					41	-.2122	-42.45	si
2					42	-.215	-42.99	si
2					43	-.2177	-43.54	si
2					44	-.2204	-44.08	si
2					45	-.2231	-44.62	si
2					46	-.2258	-45.16	si
2					47	-.2285	-45.71	si
2					48	-.2313	-46.25	si
3	1- 1	.6236	0.	si	1	.937	187.4	si
3	1- 2	.6127	0.	si	2	.9397	187.94	si
3	1- 3	1.0239	0.	si	3	.9424	188.48	si
3	1- 4	.9822	0.	si	4	.9451	189.02	si
3	1- 5	.571	0.	si	5	.9478	189.57	si
3	1- 6	.5601	0.	si	6	.9505	190.11	si
3	1- 7	-.2775	-3.64	si	7	.9533	190.65	si
3	1- 8	-.214	-2.86	si	8	.956	191.19	si
3					9	.9587	191.74	si
3					10	.9614	192.28	si
3					11	.9641	192.82	si
3					12	.9668	193.36	si
3					13	.9695	193.91	si
3					14	.9722	194.45	si
3					15	.975	194.99	si
3					16	.9777	195.53	si
3					17	.5665	113.3	si
3					18	.5701	114.02	si
3					19	.5737	114.75	si
3					20	.5774	115.47	si
3					21	.5149	102.98	si
3					22	.5185	103.71	si
3					23	.5222	104.43	si
3					24	.5258	105.16	si
3					25	-.2313	-46.26	si
3					26	-.2286	-45.72	si
3					27	-.2259	-45.18	si
3					28	-.2232	-44.63	si
3					29	-.2204	-44.09	si
3					30	-.2177	-43.55	si
3					31	-.215	-43.	si
3					32	-.2123	-42.46	si
3					33	-.2096	-41.92	si
3					34	-.2069	-41.37	si
3					35	-.2042	-40.83	si
3					36	-.2014	-40.29	si
3					37	-.1987	-39.74	si
3					38	-.196	-39.2	si
3					39	-.1933	-38.66	si
3					40	-.1906	-38.12	si
3					41	-.1879	-37.57	si
3					42	-.1851	-37.03	si
3					43	-.1824	-36.49	si
3					44	-.1797	-35.94	si
3					45	-.177	-35.4	si
3					46	-.1743	-34.86	si
3					47	-.1716	-34.31	si
3					48	-.1689	-33.77	si
4	1- 1	.3712	0.	si	1	.5978	119.55	si
4	1- 2	.3705	0.	si	2	.5979	119.58	si
4	1- 3	.6289	0.	si	3	.5981	119.62	si
4	1- 4	.6264	0.	si	4	.5982	119.65	si
4	1- 5	.368	0.	si	5	.5984	119.68	si
4	1- 6	.3674	0.	si	6	.5986	119.71	si
4	1- 7	-.159	-2.15	si	7	.5987	119.75	si
4	1- 8	-.1552	-2.1	si	8	.5989	119.78	si
4					9	.5991	119.81	si
4					10	.5992	119.84	si
4					11	.5994	119.87	si
4					12	.5995	119.91	si
4					13	.5997	119.94	si
4					14	.5999	119.97	si
4					15	.6	120.	si
4					16	.6002	120.04	si
4					17	.3418	68.36	si
4					18	.342	68.4	si
4					19	.3422	68.44	si
4					20	.3424	68.49	si
4					21	.3387	67.74	si
4					22	.3389	67.79	si
4					23	.3391	67.83	si
4					24	.3394	67.87	si
4					25	-.1302	-26.04	si
4					26	-.1301	-26.01	si
4					27	-.1299	-25.98	si
4					28	-.1297	-25.95	si
4					29	-.1296	-25.92	si
4					30	-.1294	-25.88	si
4					31	-.1293	-25.85	si
4					32	-.1291	-25.82	si
4					33	-.1289	-25.79	si
4					34	-.1288	-25.75	si
4					35	-.1286	-25.72	si
4					36	-.1284	-25.69	si
4					37	-.1283	-25.66	si
4					38	-.1281	-25.62	si
4					39	-.128	-25.59	si
4					40	-.1278	-25.56	si

4					41	-.1276	-25.53	si
4					42	-.1275	-25.49	si
4					43	-.1273	-25.46	si
4					44	-.1271	-25.43	si
4					45	-.127	-25.4	si
4					46	-.1268	-25.36	si
4					47	-.1267	-25.33	si
4					48	-.1265	-25.3	si
5	1- 1	.3915	0.	si	1	.6308	126.16	si
5	1- 2	.3915	0.	si	2	.6308	126.16	si
5	1- 3	.6606	0.	si	3	.6308	126.16	si
5	1- 4	.6607	0.	si	4	.6308	126.16	si
5	1- 5	.3916	0.	si	5	.6308	126.16	si
5	1- 6	.3917	0.	si	6	.6308	126.16	si
5	1- 7	-.1565	-2.12	si	7	.6308	126.16	si
5	1- 8	-.1567	-2.12	si	8	.6308	126.15	si
5					9	.6308	126.15	si
5					10	.6308	126.15	si
5					11	.6308	126.15	si
5					12	.6307	126.15	si
5					13	.6307	126.15	si
5					14	.6307	126.15	si
5					15	.6307	126.14	si
5					16	.6307	126.14	si
5					17	.3616	72.32	si
5					18	.3616	72.32	si
5					19	.3616	72.32	si
5					20	.3616	72.32	si
5					21	.3618	72.35	si
5					22	.3618	72.35	si
5					23	.3617	72.35	si
5					24	.3617	72.35	si
5					25	-.1266	-25.32	si
5					26	-.1266	-25.32	si
5					27	-.1266	-25.32	si
5					28	-.1266	-25.32	si
5					29	-.1266	-25.32	si
5					30	-.1266	-25.32	si
5					31	-.1266	-25.33	si
5					32	-.1266	-25.33	si
5					33	-.1266	-25.33	si
5					34	-.1266	-25.33	si
5					35	-.1267	-25.33	si
5					36	-.1267	-25.33	si
5					37	-.1267	-25.33	si
5					38	-.1267	-25.34	si
5					39	-.1267	-25.34	si
5					40	-.1267	-25.34	si
5					41	-.1267	-25.34	si
5					42	-.1267	-25.34	si
5					43	-.1267	-25.34	si
5					44	-.1267	-25.34	si
5					45	-.1267	-25.35	si
5					46	-.1267	-25.35	si
5					47	-.1267	-25.35	si
5					48	-.1268	-25.35	si

Descrizione : Pulvino 9

SOLLECITAZIONI AGENTI

Sforzi normali applicati in z= 183.7 ; y= 37.5 (baricentro CLS)
 Convenzioni: N + trazione; MZ + fib.inferiori tese; My + fib.sinistra tese.

N.	N	MZ	My	Descrizione
1	-21.27	-468.9204	-3.9073	Caso 13.1
2	-54.3	-849.6826	-207.9791	Caso 2.2
3	-55.5	-849.7302	207.9787	Caso 2.1
4	-76.77	-549.2032	14.1026	Caso 8.20
5	6.15	-555.67	-3.4086	Caso 8.13

RISULTATI

Piani di equilibrio (eps= muz * y +muy * z + lam):

Sol.	muz	muy	lambda
1.	.00000831206	.00000000314	-.0001331928
2.	.00001504044	.00000016922	-.00027369996
3.	.00001503666	-.00000016916	-.00021158973
4.	.00000953906	-.00000001112	-.00015505158
5.	.00000997721	.00000000278	-.00015705431

Deformazioni sui materiali:

sol	cls			Ve	Acciaio lento			
	vert.	D cls	S cls		ferro	D ferri	S ferri	Vel
1	1- 1	.324	0.	si	1	.5244	104.88	si
1	1- 2	.3242	0.	si	2	.5244	104.87	si
1	1- 3	.5486	0.	si	3	.5243	104.86	si
1	1- 4	.5494	0.	si	4	.5243	104.85	si
1	1- 5	.3249	0.	si	5	.5242	104.84	si
1	1- 6	.3251	0.	si	6	.5242	104.83	si
1	1- 7	-.132	-1.8	si	7	.5241	104.82	si
1	1- 8	-.1332	-1.82	si	8	.5241	104.81	si
1					9	.524	104.8	si
1					10	.524	104.79	si
1					11	.5239	104.78	si
1					12	.5239	104.77	si
1					13	.5238	104.76	si
1					14	.5238	104.75	si
1					15	.5237	104.74	si
1					16	.5237	104.73	si

1				17	.2992	59.85	si
1				18	.2992	59.84	si
1				19	.2991	59.82	si
1				20	.299	59.81	si
1				21	.3002	60.04	si
1				22	.3001	60.02	si
1				23	.3	60.01	si
1				24	.3	60.	si
1				25	-.1071	-21.42	si
1				26	-.1072	-21.43	si
1				27	-.1072	-21.44	si
1				28	-.1073	-21.45	si
1				29	-.1073	-21.46	si
1				30	-.1074	-21.47	si
1				31	-.1074	-21.48	si
1				32	-.1075	-21.49	si
1				33	-.1075	-21.5	si
1				34	-.1076	-21.51	si
1				35	-.1076	-21.52	si
1				36	-.1077	-21.53	si
1				37	-.1077	-21.54	si
1				38	-.1078	-21.55	si
1				39	-.1078	-21.56	si
1				40	-.1079	-21.57	si
1				41	-.1079	-21.58	si
1				42	-.108	-21.59	si
1				43	-.108	-21.6	si
1				44	-.108	-21.61	si
1				45	-.1081	-21.62	si
1				46	-.1081	-21.63	si
1				47	-.1082	-21.64	si
1				48	-.1082	-21.65	si
2	1- 1	.5535	0.	1	.9655	193.1	si
2	1- 2	.5642	0.	2	.9628	192.57	si
2	1- 3	.9703	0.	3	.9602	192.04	si
2	1- 4	1.0111	0.	4	.9575	191.51	si
2	1- 5	.605	0.	5	.9549	190.97	si
2	1- 6	.6157	0.	6	.9522	190.44	si
2	1- 7	-.2115	-2.83	7	.9496	189.91	si
2	1- 8	-.2737	-3.6	8	.9469	189.38	si
2				9	.9443	188.85	si
2				10	.9416	188.32	si
2				11	.9389	187.79	si
2				12	.9363	187.26	si
2				13	.9336	186.73	si
2				14	.931	186.19	si
2				15	.9283	185.66	si
2				16	.9257	185.13	si
2				17	.5196	103.91	si
2				18	.516	103.2	si
2				19	.5125	102.49	si
2				20	.5089	101.78	si
2				21	.5701	114.01	si
2				22	.5665	113.3	si
2				23	.563	112.59	si
2				24	.5594	111.88	si
2				25	-.1669	-33.38	si
2				26	-.1696	-33.92	si
2				27	-.1722	-34.45	si
2				28	-.1749	-34.98	si
2				29	-.1776	-35.51	si
2				30	-.1802	-36.04	si
2				31	-.1829	-36.57	si
2				32	-.1855	-37.11	si
2				33	-.1882	-37.64	si
2				34	-.1908	-38.17	si
2				35	-.1935	-38.7	si
2				36	-.1962	-39.23	si
2				37	-.1988	-39.76	si
2				38	-.2015	-40.3	si
2				39	-.2041	-40.83	si
2				40	-.2068	-41.36	si
2				41	-.2095	-41.89	si
2				42	-.2121	-42.42	si
2				43	-.2148	-42.96	si
2				44	-.2174	-43.49	si
2				45	-.2201	-44.02	si
2				46	-.2228	-44.55	si
2				47	-.2254	-45.08	si
2				48	-.2281	-45.61	si
3	1- 1	.6154	0.	1	.9253	185.06	si
3	1- 2	.6048	0.	2	.928	185.6	si
3	1- 3	1.0108	0.	3	.9306	186.13	si
3	1- 4	.9699	0.	4	.9333	186.66	si
3	1- 5	.5639	0.	5	.9359	187.19	si
3	1- 6	.5533	0.	6	.9386	187.72	si
3	1- 7	-.2737	-3.6	7	.9412	188.25	si
3	1- 8	-.2116	-2.83	8	.9439	188.78	si
3				9	.9466	189.31	si
3				10	.9492	189.84	si
3				11	.9519	190.37	si
3				12	.9545	190.9	si
3				13	.9572	191.44	si
3				14	.9598	191.97	si
3				15	.9625	192.5	si
3				16	.9651	193.03	si
3				17	.5592	111.83	si

3				18	.5627	112.54	si
3				19	.5663	113.25	si
3				20	.5698	113.96	si
3				21	.5087	101.73	si
3				22	.5122	102.45	si
3				23	.5158	103.16	si
3				24	.5193	103.87	si
3				25	-.2281	-45.62	si
3				26	-.2255	-45.09	si
3				27	-.2228	-44.56	si
3				28	-.2201	-44.03	si
3				29	-.2175	-43.5	si
3				30	-.2148	-42.97	si
3				31	-.2122	-42.43	si
3				32	-.2095	-41.9	si
3				33	-.2069	-41.37	si
3				34	-.2042	-40.84	si
3				35	-.2015	-40.31	si
3				36	-.1989	-39.78	si
3				37	-.1962	-39.25	si
3				38	-.1936	-38.71	si
3				39	-.1909	-38.18	si
3				40	-.1883	-37.65	si
3				41	-.1856	-37.12	si
3				42	-.1829	-36.59	si
3				43	-.1803	-36.06	si
3				44	-.1776	-35.52	si
3				45	-.175	-34.99	si
3				46	-.1723	-34.46	si
3				47	-.1696	-33.93	si
3				48	-.167	-33.4	si
4	1- 1	.3696	0.	1	.5952	119.04	si
4	1- 2	.3689	0.	2	.5954	119.07	si
4	1- 3	.6265	0.	3	.5955	119.11	si
4	1- 4	.6238	0.	4	.5957	119.14	si
4	1- 5	.3662	0.	5	.5959	119.18	si
4	1- 6	.3655	0.	6	.5961	119.21	si
4	1- 7	-.1591	-2.16	7	.5962	119.25	si
4	1- 8	-.1551	-2.1	8	.5964	119.28	si
4				9	.5966	119.32	si
4				10	.5968	119.35	si
4				11	.5969	119.39	si
4				12	.5971	119.42	si
4				13	.5973	119.46	si
4				14	.5975	119.49	si
4				15	.5976	119.53	si
4				16	.5978	119.56	si
4				17	.3402	68.05	si
4				18	.3405	68.1	si
4				19	.3407	68.14	si
4				20	.3409	68.19	si
4				21	.3369	67.39	si
4				22	.3372	67.43	si
4				23	.3374	67.48	si
4				24	.3376	67.53	si
4				25	-.1305	-26.1	si
4				26	-.1303	-26.06	si
4				27	-.1301	-26.03	si
4				28	-.13	-25.99	si
4				29	-.1298	-25.96	si
4				30	-.1296	-25.92	si
4				31	-.1294	-25.89	si
4				32	-.1293	-25.85	si
4				33	-.1291	-25.82	si
4				34	-.1289	-25.78	si
4				35	-.1287	-25.75	si
4				36	-.1286	-25.71	si
4				37	-.1284	-25.68	si
4				38	-.1282	-25.64	si
4				39	-.128	-25.61	si
4				40	-.1279	-25.57	si
4				41	-.1277	-25.54	si
4				42	-.1275	-25.5	si
4				43	-.1273	-25.47	si
4				44	-.1272	-25.43	si
4				45	-.127	-25.4	si
4				46	-.1268	-25.36	si
4				47	-.1266	-25.33	si
4				48	-.1265	-25.29	si
5	1- 1	.3917	0.	1	.632	126.4	si
5	1- 2	.3919	0.	2	.6319	126.39	si
5	1- 3	.6613	0.	3	.6319	126.38	si
5	1- 4	.6619	0.	4	.6319	126.37	si
5	1- 5	.3925	0.	5	.6318	126.36	si
5	1- 6	.3927	0.	6	.6318	126.35	si
5	1- 7	-.156	-2.12	7	.6317	126.34	si
5	1- 8	-.1571	-2.13	8	.6317	126.34	si
5				9	.6316	126.33	si
5				10	.6316	126.32	si
5				11	.6315	126.31	si
5				12	.6315	126.3	si
5				13	.6315	126.29	si
5				14	.6314	126.28	si
5				15	.6314	126.27	si
5				16	.6313	126.27	si
5				17	.3619	72.39	si
5				18	.3619	72.38	si

5	19	.3618	72.37	si
5	20	.3618	72.35	si
5	21	.3628	72.55	si
5	22	.3627	72.54	si
5	23	.3627	72.53	si
5	24	.3626	72.52	si
5	25	-.1261	-25.22	si
5	26	-.1262	-25.23	si
5	27	-.1262	-25.24	si
5	28	-.1262	-25.25	si
5	29	-.1263	-25.26	si
5	30	-.1263	-25.27	si
5	31	-.1264	-25.27	si
5	32	-.1264	-25.28	si
5	33	-.1265	-25.29	si
5	34	-.1265	-25.3	si
5	35	-.1265	-25.31	si
5	36	-.1266	-25.32	si
5	37	-.1266	-25.33	si
5	38	-.1267	-25.34	si
5	39	-.1267	-25.34	si
5	40	-.1268	-25.35	si
5	41	-.1268	-25.36	si
5	42	-.1269	-25.37	si
5	43	-.1269	-25.38	si
5	44	-.1269	-25.39	si
5	45	-.127	-25.4	si
5	46	-.127	-25.41	si
5	47	-.1271	-25.41	si
5	48	-.1271	-25.42	si

Descrizione : Pulvino 10

SOLLECITAZIONI AGENTI

Sforzi normali applicati in z= 183.7 ; y= 37.5 (baricentro CLS)
 Convenzioni: N + trazione; Mz + fib.inferiori tese; My + fib.sinistra tese.

N.	N	Mz	My	Descrizione
1	-23.43	-468.7688	-4.3041	Caso 13.1
2	-58.16	-848.8829	-207.8429	Caso 2.2
3	-59.35	-848.931	207.8427	Caso 2.1
4	-84.41	-548.6296	15.5061	Caso 8.20
5	8.57	-555.8819	-5.9792	Caso 8.13

RISULTATI

Piani di equilibrio (eps= muz * y +muy * z + lam):

sol.	muz	muy	lambda
1.	.00000830094	.00000000345	-.00013327036
2.	.00001501109	.00000016892	-.00027352975
3.	.00001500737	-.00000016887	-.00021152701
4.	.0000094991	-.00000001219	-.0001548989
5.	.00000999042	.00000000489	-.0001574268

Deformazioni sui materiali:

sol	Cls			Acciaio lento		
	vert.	D cls	S cls Ve	ferro	D ferri	S ferri Ve
1	1- 1	.3233	0. si	1	.5235	104.71 si
1	1- 2	.3235	0. si	2	.5235	104.7 si
1	1- 3	.5476	0. si	3	.5234	104.69 si
1	1- 4	.5485	0. si	4	.5234	104.68 si
1	1- 5	.3243	0. si	5	.5233	104.67 si
1	1- 6	.3246	0. si	6	.5233	104.65 si
1	1- 7	-.132	-1.8 si	7	.5232	104.64 si
1	1- 8	-.1333	-1.82 si	8	.5232	104.63 si
1				9	.5231	104.62 si
1				10	.5231	104.61 si
1				11	.523	104.6 si
1				12	.5229	104.59 si
1				13	.5229	104.58 si
1				14	.5228	104.57 si
1				15	.5228	104.56 si
1				16	.5227	104.55 si
1				17	.2986	59.72 si
1				18	.2985	59.71 si
1				19	.2985	59.69 si
1				20	.2984	59.68 si
1				21	.2996	59.93 si
1				22	.2996	59.91 si
1				23	.2995	59.9 si
1				24	.2994	59.88 si
1				25	-.1071	-21.42 si
1				26	-.1072	-21.43 si
1				27	-.1072	-21.44 si
1				28	-.1073	-21.45 si
1				29	-.1073	-21.47 si
1				30	-.1074	-21.48 si
1				31	-.1074	-21.49 si
1				32	-.1075	-21.5 si
1				33	-.1075	-21.51 si
1				34	-.1076	-21.52 si
1				35	-.1077	-21.53 si
1				36	-.1077	-21.54 si
1				37	-.1078	-21.55 si
1				38	-.1078	-21.56 si
1				39	-.1079	-21.57 si
1				40	-.1079	-21.58 si
1				41	-.108	-21.6 si

5	44	-.1271	-25.43	si
5	45	-.1272	-25.44	si
5	46	-.1273	-25.46	si
5	47	-.1274	-25.47	si
5	48	-.1274	-25.49	si

Descrizione : Pulvino 11

SOLLECITAZIONI AGENTI

Sforzi normali applicati in z= 183.7 ; y= 37.5 (baricentro CLS)
 Convenzioni: N + trazione; Mz + fib.inferiori tese; My + fib.sinistra tese.

N.	N	Mz	My	Descrizione
1	-26.48	-468.5098	-4.8644	Caso 13.1
2	-63.99	-848.3858	-228.7311	Caso 2.2
3	-65.19	-848.4335	228.731	Caso 2.1
4	-96.63	-547.6382	17.7509	Caso 8.20
5	13.34	-556.2376	-9.4531	Caso 8.13

RISULTATI

Piani di equilibrio (eps= muz * y + muy * z + lam):

Sol.	muz	muy	lambda
1.	.00000828444	.00000000039	-.00013336649
2.	.00001497983	.00000018566	-.00027654258
3.	.00001497606	-.0000001856	-.00020839229
4.	.00000943387	-.00000001388	-.00015463143
5.	.00001001533	.000000000774	-.00015790518

Deformazioni sui materiali:

sol	Cls			Acciaio lento				
	vert.	D cls	S cls	Ve	ferro	D ferri	S ferri	Ve
1	1- 1	.3223	0.	si	1	.5223	104.46	si
1	1- 2	.3225	0.	si	2	.5222	104.44	si
1	1- 3	.5462	0.	si	3	.5222	104.43	si
1	1- 4	.5471	0.	si	4	.5221	104.42	si
1	1- 5	.3235	0.	si	5	.522	104.41	si
1	1- 6	.3237	0.	si	6	.522	104.39	si
1	1- 7	-.1319	-1.8	si	7	.5219	104.38	si
1	1- 8	-.1334	-1.82	si	8	.5219	104.37	si
1					9	.5218	104.36	si
1					10	.5217	104.35	si
1					11	.5217	104.33	si
1					12	.5216	104.32	si
1					13	.5215	104.31	si
1					14	.5215	104.3	si
1					15	.5214	104.28	si
1					16	.5214	104.27	si
1					17	.2977	59.54	si
1					18	.2976	59.52	si
1					19	.2975	59.5	si
1					20	.2974	59.49	si
1					21	.2988	59.77	si
1					22	.2988	59.75	si
1					23	.2987	59.74	si
1					24	.2986	59.72	si
1					25	-.1071	-21.42	si
1					26	-.1072	-21.43	si
1					27	-.1072	-21.44	si
1					28	-.1073	-21.46	si
1					29	-.1073	-21.47	si
1					30	-.1074	-21.48	si
1					31	-.1075	-21.49	si
1					32	-.1075	-21.5	si
1					33	-.1076	-21.52	si
1					34	-.1076	-21.53	si
1					35	-.1077	-21.54	si
1					36	-.1078	-21.55	si
1					37	-.1078	-21.57	si
1					38	-.1079	-21.58	si
1					39	-.108	-21.59	si
1					40	-.108	-21.6	si
1					41	-.1081	-21.61	si
1					42	-.1081	-21.63	si
1					43	-.1082	-21.64	si
1					44	-.1083	-21.65	si
1					45	-.1083	-21.66	si
1					46	-.1084	-21.68	si
1					47	-.1084	-21.69	si
1					48	-.1085	-21.7	si
2	1- 1	.5473	0.	si	1	.9628	192.56	si
2	1- 2	.559	0.	si	2	.9599	191.98	si
2	1- 3	.9635	0.	si	3	.957	191.4	si
2	1- 4	1.0083	0.	si	4	.9541	190.82	si
2	1- 5	.6039	0.	si	5	.9512	190.23	si
2	1- 6	.6156	0.	si	6	.9483	189.65	si
2	1- 7	-.2083	-2.79	si	7	.9453	189.07	si
2	1- 8	-.2765	-3.63	si	8	.9424	188.49	si
2					9	.9395	187.9	si
2					10	.9366	187.32	si
2					11	.9337	186.74	si
2					12	.9308	186.15	si
2					13	.9279	185.57	si
2					14	.9249	184.99	si
2					15	.922	184.41	si
2					16	.9191	183.82	si
2					17	.5147	102.93	si
2					18	.5108	102.15	si
2					19	.5069	101.37	si

2				20	.503	100.59	si
2				21	.5701	114.01	si
2				22	.5662	113.23	si
2				23	.5623	112.45	si
2				24	.5584	111.67	si
2				25	-.1639	-32.79	si
2				26	-.1669	-33.37	si
2				27	-.1698	-33.96	si
2				28	-.1727	-34.54	si
2				29	-.1756	-35.12	si
2				30	-.1785	-35.71	si
2				31	-.1815	-36.29	si
2				32	-.1844	-36.87	si
2				33	-.1873	-37.46	si
2				34	-.1902	-38.04	si
2				35	-.1931	-38.62	si
2				36	-.196	-39.21	si
2				37	-.199	-39.79	si
2				38	-.2019	-40.37	si
2				39	-.2048	-40.96	si
2				40	-.2077	-41.54	si
2				41	-.2106	-42.13	si
2				42	-.2135	-42.71	si
2				43	-.2165	-43.29	si
2				44	-.2194	-43.88	si
2				45	-.2223	-44.46	si
2				46	-.2252	-45.04	si
2				47	-.2281	-45.63	si
2				48	-.231	-46.21	si
3	1- 1	.6153	0.	1	.9188	183.76	si
3	1- 2	.6036	0.	2	.9217	184.34	si
3	1- 3	1.008	0.	3	.9246	184.92	si
3	1- 4	.9631	0.	4	.9275	185.5	si
3	1- 5	.5588	0.	5	.9304	186.09	si
3	1- 6	.5471	0.	6	.9333	186.67	si
3	1- 7	-.2766	-3.63	7	.9363	187.25	si
3	1- 8	-.2084	-2.79	8	.9392	187.83	si
3				9	.9421	188.42	si
3				10	.945	189.	si
3				11	.9479	189.58	si
3				12	.9508	190.16	si
3				13	.9537	190.75	si
3				14	.9566	191.33	si
3				15	.9596	191.91	si
3				16	.9625	192.49	si
3				17	.5581	111.62	si
3				18	.562	112.4	si
3				19	.5659	113.18	si
3				20	.5698	113.96	si
3				21	.5027	100.55	si
3				22	.5066	101.33	si
3				23	.5105	102.11	si
3				24	.5144	102.88	si
3				25	-.2311	-46.22	si
3				26	-.2282	-45.64	si
3				27	-.2253	-45.05	si
3				28	-.2223	-44.47	si
3				29	-.2194	-43.89	si
3				30	-.2165	-43.3	si
3				31	-.2136	-42.72	si
3				32	-.2107	-42.14	si
3				33	-.2078	-41.55	si
3				34	-.2048	-40.97	si
3				35	-.2019	-40.39	si
3				36	-.199	-39.8	si
3				37	-.1961	-39.22	si
3				38	-.1932	-38.64	si
3				39	-.1903	-38.05	si
3				40	-.1874	-37.47	si
3				41	-.1844	-36.89	si
3				42	-.1815	-36.3	si
3				43	-.1786	-35.72	si
3				44	-.1757	-35.14	si
3				45	-.1728	-34.55	si
3				46	-.1699	-33.97	si
3				47	-.1669	-33.39	si
3				48	-.164	-32.8	si
4	1- 1	.3642	0.	1	.5865	117.29	si
4	1- 2	.3634	0.	2	.5867	117.34	si
4	1- 3	.6181	0.	3	.5869	117.38	si
4	1- 4	.6147	0.	4	.5871	117.42	si
4	1- 5	.36	0.	5	.5873	117.47	si
4	1- 6	.3591	0.	6	.5876	117.51	si
4	1- 7	-.1597	-2.16	7	.5878	117.55	si
4	1- 8	-.1546	-2.1	8	.588	117.6	si
4				9	.5882	117.64	si
4				10	.5884	117.68	si
4				11	.5886	117.73	si
4				12	.5889	117.77	si
4				13	.5891	117.82	si
4				14	.5893	117.86	si
4				15	.5895	117.9	si
4				16	.5897	117.95	si
4				17	.335	67.	si
4				18	.3353	67.06	si
4				19	.3356	67.12	si
4				20	.3359	67.18	si

4				21	.3309	66.17	si
4				22	.3312	66.23	si
4				23	.3315	66.29	si
4				24	.3317	66.35	si
4				25	-.1314	-26.28	si
4				26	-.1312	-26.23	si
4				27	-.131	-26.19	si
4				28	-.1307	-26.15	si
4				29	-.1305	-26.1	si
4				30	-.1303	-26.06	si
4				31	-.1301	-26.02	si
4				32	-.1299	-25.97	si
4				33	-.1296	-25.93	si
4				34	-.1294	-25.88	si
4				35	-.1292	-25.84	si
4				36	-.129	-25.8	si
4				37	-.1288	-25.75	si
4				38	-.1286	-25.71	si
4				39	-.1283	-25.67	si
4				40	-.1281	-25.62	si
4				41	-.1279	-25.58	si
4				42	-.1277	-25.54	si
4				43	-.1275	-25.49	si
4				44	-.1272	-25.45	si
4				45	-.127	-25.41	si
4				46	-.1268	-25.36	si
4				47	-.1266	-25.32	si
4				48	-.1264	-25.27	si
5	1- 1	.3929	0.	1	.6356	127.13	si
5	1- 2	.3934	0.	2	.6355	127.1	si
5	1- 3	.6638	0.	3	.6354	127.08	si
5	1- 4	.6657	0.	4	.6353	127.05	si
5	1- 5	.3953	0.	5	.6352	127.03	si
5	1- 6	.3958	0.	6	.635	127.01	si
5	1- 7	-.1551	-2.1	7	.6349	126.98	si
5	1- 8	-.1579	-2.14	8	.6348	126.96	si
5				9	.6347	126.93	si
5				10	.6345	126.91	si
5				11	.6344	126.88	si
5				12	.6343	126.86	si
5				13	.6342	126.84	si
5				14	.6341	126.81	si
5				15	.6339	126.79	si
5				16	.6338	126.76	si
5				17	.3634	72.68	si
5				18	.3632	72.65	si
5				19	.3631	72.62	si
5				20	.3629	72.58	si
5				21	.3657	73.14	si
5				22	.3656	73.11	si
5				23	.3654	73.08	si
5				24	.3652	73.05	si
5				25	-.125	-25.01	si
5				26	-.1252	-25.03	si
5				27	-.1253	-25.06	si
5				28	-.1254	-25.08	si
5				29	-.1255	-25.1	si
5				30	-.1256	-25.13	si
5				31	-.1258	-25.15	si
5				32	-.1259	-25.18	si
5				33	-.126	-25.2	si
5				34	-.1261	-25.23	si
5				35	-.1263	-25.25	si
5				36	-.1264	-25.28	si
5				37	-.1265	-25.3	si
5				38	-.1266	-25.32	si
5				39	-.1267	-25.35	si
5				40	-.1269	-25.37	si
5				41	-.127	-25.4	si
5				42	-.1271	-25.42	si
5				43	-.1272	-25.45	si
5				44	-.1273	-25.47	si
5				45	-.1275	-25.49	si
5				46	-.1276	-25.52	si
5				47	-.1277	-25.54	si
5				48	-.1278	-25.57	si

Descrizione : Pulvino 12

SOLLECITAZIONI AGENTI

Sforzi normali applicati in z= 183.7 ; y= 37.5 (baricentro CLS)
 Convenzioni: N + trazione; Mz + fib.inferiori tese; My + fib.sinistra tese.

N.	N	Mz	My	Descrizione
1	-29.4	-468.3026	-5.4008	Caso 13.1
2	-69.49	-847.9986	-196.2183	Caso 2.2
3	-70.68	-848.0467	196.2182	Caso 2.1
4	-107.59	-546.8203	19.7643	Caso 8.20
5	17.25	-556.559	-7.4106	Caso 8.13

RISULTATI

Piani di equilibrio (eps= muz * y +muy * z + lam):

Sol.	muz	muy	lambda
1.	.00000826937	.00000000432	-.0001334695
2.	.00001495127	.00000015896	-.0002718263
3.	.00001494754	-.00000015891	-.00021348341
4.	.00000937666	-.00000001538	-.00015440969

5. | .00001003629 | .00000000608 | -.00015757118 |
 Deformazioni sui materiali:

C1s					Acciaio lento				
sol	vert.	D c1s	S c1s	Ve	ferro	D ferri	S ferri	Ve	
1	1- 1	.3213	0.	si	1	.5211	104.22	si	
1	1- 2	.3216	0.	si	2	.521	104.21	si	
1	1- 3	.5449	0.	si	3	.521	104.2	si	
1	1- 4	.5459	0.	si	4	.5209	104.18	si	
1	1- 5	.3227	0.	si	5	.5208	104.17	si	
1	1- 6	.3229	0.	si	6	.5208	104.15	si	
1	1- 7	-.1319	-1.8	si	7	.5207	104.14	si	
1	1- 8	-.1335	-1.82	si	8	.5206	104.13	si	
1					9	.5206	104.11	si	
1					10	.5205	104.1	si	
1					11	.5204	104.09	si	
1					12	.5204	104.07	si	
1					13	.5203	104.06	si	
1					14	.5202	104.05	si	
1					15	.5202	104.03	si	
1					16	.5201	104.02	si	
1					17	.2968	59.36	si	
1					18	.2967	59.35	si	
1					19	.2966	59.33	si	
1					20	.2966	59.31	si	
1					21	.2981	59.62	si	
1					22	.298	59.6	si	
1					23	.2979	59.59	si	
1					24	.2978	59.57	si	
1					25	-.1071	-21.42	si	
1					26	-.1072	-21.43	si	
1					27	-.1072	-21.44	si	
1					28	-.1073	-21.46	si	
1					29	-.1074	-21.47	si	
1					30	-.1074	-21.49	si	
1					31	-.1075	-21.5	si	
1					32	-.1076	-21.51	si	
1					33	-.1076	-21.53	si	
1					34	-.1077	-21.54	si	
1					35	-.1078	-21.55	si	
1					36	-.1078	-21.57	si	
1					37	-.1079	-21.58	si	
1					38	-.108	-21.59	si	
1					39	-.108	-21.61	si	
1					40	-.1081	-21.62	si	
1					41	-.1082	-21.63	si	
1					42	-.1082	-21.65	si	
1					43	-.1083	-21.66	si	
1					44	-.1084	-21.68	si	
1					45	-.1084	-21.69	si	
1					46	-.1085	-21.7	si	
1					47	-.1086	-21.72	si	
1					48	-.1086	-21.73	si	
2	1- 1	.5505	0.	si	1	.9572	191.45	si	
2	1- 2	.5605	0.	si	2	.9547	190.95	si	
2	1- 3	.9642	0.	si	3	.9522	190.45	si	
2	1- 4	1.0026	0.	si	4	.9498	189.95	si	
2	1- 5	.5989	0.	si	5	.9473	189.45	si	
2	1- 6	.6089	0.	si	6	.9448	188.95	si	
2	1- 7	-.2134	-2.85	si	7	.9423	188.45	si	
2	1- 8	-.2718	-3.57	si	8	.9398	187.95	si	
2					9	.9373	187.46	si	
2					10	.9348	186.96	si	
2					11	.9323	186.46	si	
2					12	.9298	185.96	si	
2					13	.9273	185.46	si	
2					14	.9248	184.96	si	
2					15	.9223	184.46	si	
2					16	.9198	183.96	si	
2					17	.5161	103.23	si	
2					18	.5128	102.56	si	
2					19	.5095	101.89	si	
2					20	.5061	101.22	si	
2					21	.5636	112.71	si	
2					22	.5602	112.05	si	
2					23	.5569	111.38	si	
2					24	.5535	110.71	si	
2					25	-.169	-33.81	si	
2					26	-.1715	-34.31	si	
2					27	-.174	-34.81	si	
2					28	-.1765	-35.31	si	
2					29	-.179	-35.81	si	
2					30	-.1815	-36.31	si	
2					31	-.184	-36.81	si	
2					32	-.1865	-37.31	si	
2					33	-.189	-37.81	si	
2					34	-.1915	-38.31	si	
2					35	-.194	-38.81	si	
2					36	-.1965	-39.3	si	
2					37	-.199	-39.8	si	
2					38	-.2015	-40.3	si	
2					39	-.204	-40.8	si	
2					40	-.2065	-41.3	si	
2					41	-.209	-41.8	si	
2					42	-.2115	-42.3	si	
2					43	-.214	-42.8	si	
2					44	-.2165	-43.3	si	
2					45	-.219	-43.8	si	

2				
2				
3				
3	1- 1	.6086	0.	si
3	1- 2	.5986	0.	si
3	1- 3	1.0022	0.	si
3	1- 4	.9638	0.	si
3	1- 5	.5603	0.	si
3	1- 6	.5502	0.	si
3	1- 7	-.2719	-3.58	si
3	1- 8	-.2135	-2.85	si

46	-.2215	-44.3	si
47	-.224	-44.8	si
48	-.2265	-45.3	si
1	.9195	183.9	si
2	.922	184.39	si
3	.9245	184.89	si
4	.927	185.39	si
5	.9295	185.89	si
6	.9319	186.39	si
7	.9344	186.89	si
8	.9369	187.39	si
9	.9394	187.89	si
10	.9419	188.38	si
11	.9444	188.88	si
12	.9469	189.38	si
13	.9494	189.88	si
14	.9519	190.38	si
15	.9544	190.88	si
16	.9569	191.38	si
17	.5533	110.66	si
18	.5566	111.33	si
19	.56	111.99	si
20	.5633	112.66	si
21	.5059	101.18	si
22	.5092	101.84	si
23	.5126	102.51	si
24	.5159	103.18	si
25	-.2265	-45.31	si
26	-.224	-44.81	si
27	-.2216	-44.31	si
28	-.2191	-43.81	si
29	-.2166	-43.31	si
30	-.2141	-42.81	si
31	-.2116	-42.31	si
32	-.2091	-41.81	si
33	-.2066	-41.31	si
34	-.2041	-40.81	si
35	-.2016	-40.32	si
36	-.1991	-39.82	si
37	-.1966	-39.32	si
38	-.1941	-38.82	si
39	-.1916	-38.32	si
40	-.1891	-37.82	si
41	-.1866	-37.32	si
42	-.1841	-36.82	si
43	-.1816	-36.32	si
44	-.1791	-35.82	si
45	-.1766	-35.32	si
46	-.1741	-34.82	si
47	-.1716	-34.32	si
48	-.1691	-33.82	si
1	.5817	116.34	si
2	.582	116.39	si
3	.5822	116.44	si
4	.5824	116.49	si
5	.5827	116.54	si
6	.5829	116.58	si
7	.5832	116.63	si
8	.5834	116.68	si
9	.5836	116.73	si
10	.5839	116.78	si
11	.5841	116.82	si
12	.5844	116.87	si
13	.5846	116.92	si
14	.5848	116.97	si
15	.5851	117.02	si
16	.5853	117.07	si
17	.3322	66.43	si
18	.3325	66.5	si
19	.3328	66.56	si
20	.3331	66.63	si
21	.3276	65.51	si
22	.3279	65.58	si
23	.3282	65.64	si
24	.3285	65.71	si
25	-.1319	-26.38	si
26	-.1316	-26.33	si
27	-.1314	-26.28	si
28	-.1312	-26.23	si
29	-.1309	-26.18	si
30	-.1307	-26.14	si
31	-.1304	-26.09	si
32	-.1302	-26.04	si
33	-.13	-25.99	si
34	-.1297	-25.94	si
35	-.1295	-25.89	si
36	-.1292	-25.85	si
37	-.129	-25.8	si
38	-.1287	-25.75	si
39	-.1285	-25.7	si
40	-.1283	-25.65	si
41	-.128	-25.6	si
42	-.1278	-25.56	si
43	-.1275	-25.51	si
44	-.1273	-25.46	si
45	-.1271	-25.41	si
46	-.1268	-25.36	si

4	1- 1	.3613	0.	si
4	1- 2	.3603	0.	si
4	1- 3	.6135	0.	si
4	1- 4	.6098	0.	si
4	1- 5	.3566	0.	si
4	1- 6	.3557	0.	si
4	1- 7	-.1601	-2.17	si
4	1- 8	-.1544	-2.09	si

4				47	-.1266	-25.31	si
4				48	-.1263	-25.27	si
5	1- 1	.3944	0.	1	.6371	127.43	si
5	1- 2	.3948	0.	2	.637	127.41	si
5	1- 3	.6658	0.	3	.6369	127.39	si
5	1- 4	.6673	0.	4	.6368	127.37	si
5	1- 5	.3963	0.	5	.6367	127.35	si
5	1- 6	.3967	0.	6	.6367	127.33	si
5	1- 7	-.1553	-2.11	7	.6366	127.31	si
5	1- 8	-.1576	-2.14	8	.6365	127.29	si
5				9	.6364	127.27	si
5				10	.6363	127.25	si
5				11	.6362	127.23	si
5				12	.6361	127.22	si
5				13	.636	127.2	si
5				14	.6359	127.18	si
5				15	.6358	127.16	si
5				16	.6357	127.14	si
5				17	.3647	72.94	si
5				18	.3646	72.92	si
5				19	.3645	72.89	si
5				20	.3643	72.87	si
5				21	.3665	73.31	si
5				22	.3664	73.28	si
5				23	.3663	73.26	si
5				24	.3661	73.23	si
5				25	-.1252	-25.05	si
5				26	-.1253	-25.07	si
5				27	-.1254	-25.09	si
5				28	-.1255	-25.11	si
5				29	-.1256	-25.13	si
5				30	-.1257	-25.14	si
5				31	-.1258	-25.16	si
5				32	-.1259	-25.18	si
5				33	-.126	-25.2	si
5				34	-.1261	-25.22	si
5				35	-.1262	-25.24	si
5				36	-.1263	-25.26	si
5				37	-.1264	-25.28	si
5				38	-.1265	-25.3	si
5				39	-.1266	-25.32	si
5				40	-.1267	-25.34	si
5				41	-.1268	-25.36	si
5				42	-.1269	-25.37	si
5				43	-.127	-25.39	si
5				44	-.1271	-25.41	si
5				45	-.1272	-25.43	si
5				46	-.1273	-25.45	si
5				47	-.1273	-25.47	si
5				48	-.1274	-25.49	si

Descrizione : Pulvino 13

SOLLECITAZIONI AGENTI

Sforzi normali applicati in z= 183.7 ; y= 37.5 (baricentro CLS)
 convenzioni: N + trazione; Mz + fib.inferiori tese; My + fib.sinistra tese.

N.	N	Mz	My	Descrizione
1	-32.96	-468.0051	6.0548	Caso 13.1
2	-76.25	-847.4315	-204.9077	Caso 2.2
3	-77.44	-847.4793	204.9076	Caso 2.1
4	-122.23	-545.6456	22.4537	Caso 8.20
5	23.21	-557.005	-6.8503	Caso 8.13

RISULTATI

Piani di equilibrio (eps= muz * y +muy * z + lam):

Sol.	muz	muy	lambda
1.	.00000825019	-.00000000483	-.0001318053
2.	.00001491502	.00000016571	-.00027306672
3.	.00001491129	-.00000016566	-.00021224357
4.	.00000929877	-.00000001736	-.0001540867
5.	.00001006745	.00000000563	-.00015743137

Deformazioni sui materiali:

sol	Cls				Acciaio lento			
	vert.	D	cls	S	ferro	D	S	ferri
1	1- 1	.322	0.	si	1	.5185	103.7	si
1	1- 2	.3217	0.	si	2	.5186	103.72	si
1	1- 3	.5444	0.	si	3	.5187	103.73	si
1	1- 4	.5432	0.	si	4	.5187	103.75	si
1	1- 5	.3205	0.	si	5	.5188	103.76	si
1	1- 6	.3202	0.	si	6	.5189	103.78	si
1	1- 7	-.1336	-1.82	si	7	.519	103.79	si
1	1- 8	-.1318	-1.8	si	8	.519	103.81	si
1					9	.5191	103.82	si
1					10	.5192	103.84	si
1					11	.5193	103.85	si
1					12	.5193	103.87	si
1					13	.5194	103.88	si
1					14	.5195	103.9	si
1					15	.5196	103.91	si
1					16	.5196	103.93	si
1					17	.2969	59.38	si
1					18	.297	59.4	si
1					19	.2971	59.42	si
1					20	.2972	59.44	si
1					21	.2954	59.09	si
1					22	.2955	59.11	si

1				23	.2956	59.13	si
1				24	.2957	59.15	si
1				25	-.1088	-21.76	si
1				26	-.1087	-21.75	si
1				27	-.1087	-21.73	si
1				28	-.1086	-21.72	si
1				29	-.1085	-21.7	si
1				30	-.1084	-21.69	si
1				31	-.1084	-21.67	si
1				32	-.1083	-21.66	si
1				33	-.1082	-21.64	si
1				34	-.1081	-21.63	si
1				35	-.1081	-21.61	si
1				36	-.108	-21.6	si
1				37	-.1079	-21.58	si
1				38	-.1078	-21.57	si
1				39	-.1078	-21.55	si
1				40	-.1077	-21.54	si
1				41	-.1076	-21.52	si
1				42	-.1075	-21.51	si
1				43	-.1074	-21.49	si
1				44	-.1074	-21.47	si
1				45	-.1073	-21.46	si
1				46	-.1072	-21.44	si
1				47	-.1071	-21.43	si
1				48	-.1071	-21.41	si
2	1- 1	.5473	0.	1	.9552	191.03	si
2	1- 2	.5577	0.	2	.9526	190.51	si
2	1- 3	.9604	0.	3	.95	189.99	si
2	1- 4	1.0004	0.	4	.9474	189.47	si
2	1- 5	.5977	0.	5	.9448	188.95	si
2	1- 6	.6081	0.	6	.9422	188.43	si
2	1- 7	-.2122	-2.84	7	.9396	187.91	si
2	1- 8	-.2731	-3.59	8	.937	187.39	si
2				9	.9344	186.87	si
2				10	.9318	186.35	si
2				11	.9292	185.83	si
2				12	.9266	185.31	si
2				13	.924	184.79	si
2				14	.9214	184.27	si
2				15	.9188	183.75	si
2				16	.9162	183.23	si
2				17	.9135	182.71	si
2				18	.9108	182.19	si
2				19	.9081	181.67	si
2				20	.9054	181.15	si
2				21	.9027	180.63	si
2				22	.9001	180.11	si
2				23	.8974	179.59	si
2				24	.8948	179.07	si
2				25	.8921	178.55	si
2				26	.8895	178.03	si
2				27	.8868	177.51	si
2				28	.8842	176.99	si
2				29	.8815	176.47	si
2				30	.8789	175.95	si
2				31	.8762	175.43	si
2				32	.8736	174.91	si
2				33	.8709	174.39	si
2				34	.8683	173.87	si
2				35	.8656	173.35	si
2				36	.863	172.83	si
2				37	.8603	172.31	si
2				38	.8577	171.79	si
2				39	.855	171.27	si
2				40	.8524	170.75	si
2				41	.8497	170.23	si
2				42	.8471	169.71	si
2				43	.8444	169.19	si
2				44	.8418	168.67	si
2				45	.8391	168.15	si
2				46	.8365	167.63	si
2				47	.8338	167.11	si
2				48	.8312	166.59	si
3	1- 1	.6079	0.	1	.9158	183.16	si
3	1- 2	.5974	0.	2	.9184	183.68	si
3	1- 3	1.	0.	3	.921	184.2	si
3	1- 4	.9601	0.	4	.9236	184.72	si
3	1- 5	.5575	0.	5	.9262	185.24	si
3	1- 6	.547	0.	6	.9288	185.76	si
3	1- 7	-.2731	-3.59	7	.9314	186.28	si
3	1- 8	-.2122	-2.84	8	.934	186.8	si
3				9	.9366	187.32	si
3				10	.9392	187.84	si
3				11	.9418	188.36	si
3				12	.9444	188.88	si
3				13	.947	189.4	si
3				14	.9496	189.92	si
3				15	.9522	190.44	si
3				16	.9548	190.96	si
3				17	.9574	191.48	si
3				18	.96	192	si
3				19	.9626	192.52	si
3				20	.9652	193.04	si
3				21	.9678	193.56	si
3				22	.9704	194.08	si
3				23	.973	194.6	si

3					24	.5132	102.64	si
3					25	-.2279	-45.58	si
3					26	-.2253	-45.05	si
3					27	-.2227	-44.53	si
3					28	-.2201	-44.01	si
3					29	-.2175	-43.49	si
3					30	-.2149	-42.97	si
3					31	-.2123	-42.45	si
3					32	-.2097	-41.93	si
3					33	-.2071	-41.41	si
3					34	-.2044	-40.89	si
3					35	-.2018	-40.37	si
3					36	-.1992	-39.85	si
3					37	-.1966	-39.33	si
3					38	-.194	-38.81	si
3					39	-.1914	-38.29	si
3					40	-.1888	-37.77	si
3					41	-.1862	-37.25	si
3					42	-.1836	-36.72	si
3					43	-.181	-36.2	si
3					44	-.1784	-35.68	si
3					45	-.1758	-35.16	si
3					46	-.1732	-34.64	si
3					47	-.1706	-34.12	si
3					48	-.168	-33.6	si
4	1- 1	.3573	0.	si	1	.5753	115.06	si
4	1- 2	.3563	0.	si	2	.5756	115.11	si
4	1- 3	.6073	0.	si	3	.5758	115.17	si
4	1- 4	.6031	0.	si	4	.5761	115.22	si
4	1- 5	.3521	0.	si	5	.5764	115.27	si
4	1- 6	.351	0.	si	6	.5766	115.33	si
4	1- 7	-.1605	-2.17	si	7	.5769	115.38	si
4	1- 8	-.1541	-2.09	si	8	.5772	115.44	si
4					9	.5775	115.49	si
4					10	.5777	115.55	si
4					11	.578	115.6	si
4					12	.5783	115.66	si
4					13	.5786	115.71	si
4					14	.5788	115.77	si
4					15	.5791	115.82	si
4					16	.5794	115.87	si
4					17	.3283	65.66	si
4					18	.3287	65.73	si
4					19	.329	65.81	si
4					20	.3294	65.88	si
4					21	.3231	64.62	si
4					22	.3235	64.7	si
4					23	.3239	64.77	si
4					24	.3242	64.84	si
4					25	-.1325	-26.5	si
4					26	-.1322	-26.45	si
4					27	-.132	-26.39	si
4					28	-.1317	-26.34	si
4					29	-.1314	-26.29	si
4					30	-.1312	-26.23	si
4					31	-.1309	-26.18	si
4					32	-.1306	-26.12	si
4					33	-.1303	-26.07	si
4					34	-.1301	-26.01	si
4					35	-.1298	-25.96	si
4					36	-.1295	-25.9	si
4					37	-.1292	-25.85	si
4					38	-.129	-25.79	si
4					39	-.1287	-25.74	si
4					40	-.1284	-25.69	si
4					41	-.1282	-25.63	si
4					42	-.1279	-25.58	si
4					43	-.1276	-25.52	si
4					44	-.1273	-25.47	si
4					45	-.1271	-25.41	si
4					46	-.1268	-25.36	si
4					47	-.1265	-25.3	si
4					48	-.1262	-25.25	si
5	1- 1	.3963	0.	si	1	.6396	127.92	si
5	1- 2	.3966	0.	si	2	.6395	127.9	si
5	1- 3	.6685	0.	si	3	.6394	127.88	si
5	1- 4	.6698	0.	si	4	.6393	127.87	si
5	1- 5	.398	0.	si	5	.6392	127.85	si
5	1- 6	.3983	0.	si	6	.6392	127.83	si
5	1- 7	-.1554	-2.11	si	7	.6391	127.81	si
5	1- 8	-.1574	-2.13	si	8	.639	127.8	si
5					9	.6389	127.78	si
5					10	.6388	127.76	si
5					11	.6387	127.74	si
5					12	.6386	127.72	si
5					13	.6385	127.71	si
5					14	.6384	127.69	si
5					15	.6384	127.67	si
5					16	.6383	127.65	si
5					17	.3664	73.29	si
5					18	.3663	73.27	si
5					19	.3662	73.24	si
5					20	.3661	73.22	si
5					21	.3681	73.63	si
5					22	.368	73.6	si
5					23	.3679	73.58	si
5					24	.3678	73.55	si

5	25	-.1252	-25.04	si
5	26	-.1253	-25.05	si
5	27	-.1254	-25.07	si
5	28	-.1254	-25.09	si
5	29	-.1255	-25.11	si
5	30	-.1256	-25.12	si
5	31	-.1257	-25.14	si
5	32	-.1258	-25.16	si
5	33	-.1259	-25.18	si
5	34	-.126	-25.19	si
5	35	-.1261	-25.21	si
5	36	-.1262	-25.23	si
5	37	-.1262	-25.25	si
5	38	-.1263	-25.27	si
5	39	-.1264	-25.28	si
5	40	-.1265	-25.3	si
5	41	-.1266	-25.32	si
5	42	-.1267	-25.34	si
5	43	-.1268	-25.35	si
5	44	-.1269	-25.37	si
5	45	-.1269	-25.39	si
5	46	-.127	-25.41	si
5	47	-.1271	-25.42	si
5	48	-.1272	-25.44	si

Descrizione : Pulvino 14

SOLLECITAZIONI AGENTI

Sforzi normali applicati in z= 183.7 ; y= 37.5 (baricentro CLS)
 Convenzioni: N + trazione; Mz + fib.inferiori tese; My + fib.sinistra tese.

N.	N	Mz	My	Descrizione
1	-38.25	-467.6075	7.0265	Caso 13.1
2	-86.19	-846.6866	-206.4791	Caso 2.2
3	-87.38	-846.7349	206.4791	Caso 2.1
4	-142.95	-544.0472	26.2599	Caso 8.20
5	31.13	-557.6448	-2.3419	Caso 8.13

RISULTATI

Piani di equilibrio (eps= muz * y +muy * z + lam):

Sol.	muz	muy	lambda
1.	.00000822249	-.0000000056	-.00013170294
2.	.00001486321	.00000016653	-.00027328614
3.	.00001485949	-.00000016648	-.00021216123
4.	.00000918973	-.00000002013	-.00015364146
5.	.0000101097	.00000000193	-.00015668639

Deformazioni sui materiali:

sol	CLS			Acciaio lento				
	vert.	D cls	S cls	Ve	ferro	D ferri	S ferri	Ve
1	1- 1	.3205	0.	si	1	.5162	103.24	si
1	1- 2	.3202	0.	si	2	.5163	103.26	si
1	1- 3	.5422	0.	si	3	.5164	103.27	si
1	1- 4	.5408	0.	si	4	.5165	103.29	si
1	1- 5	.3188	0.	si	5	.5165	103.31	si
1	1- 6	.3185	0.	si	6	.5166	103.33	si
1	1- 7	-.1338	-1.82	si	7	.5167	103.34	si
1	1- 8	-.1317	-1.8	si	8	.5168	103.36	si
1					9	.5169	103.38	si
1					10	.517	103.4	si
1					11	.5171	103.41	si
1					12	.5172	103.43	si
1					13	.5172	103.45	si
1					14	.5173	103.47	si
1					15	.5174	103.48	si
1					16	.5175	103.5	si
1					17	.2955	59.1	si
1					18	.2956	59.12	si
1					19	.2957	59.15	si
1					20	.2958	59.17	si
1					21	.2938	58.77	si
1					22	.2939	58.79	si
1					23	.2941	58.81	si
1					24	.2942	58.84	si
1					25	-.1091	-21.81	si
1					26	-.109	-21.8	si
1					27	-.1089	-21.78	si
1					28	-.1088	-21.76	si
1					29	-.1087	-21.74	si
1					30	-.1086	-21.73	si
1					31	-.1085	-21.71	si
1					32	-.1085	-21.69	si
1					33	-.1084	-21.67	si
1					34	-.1083	-21.66	si
1					35	-.1082	-21.64	si
1					36	-.1081	-21.62	si
1					37	-.108	-21.6	si
1					38	-.1079	-21.59	si
1					39	-.1078	-21.57	si
1					40	-.1078	-21.55	si
1					41	-.1077	-21.53	si
1					42	-.1076	-21.52	si
1					43	-.1075	-21.5	si
1					44	-.1074	-21.48	si
1					45	-.1073	-21.46	si
1					46	-.1072	-21.45	si
1					47	-.1071	-21.43	si
1					48	-.1071	-21.41	si

2	1- 1	.5442	0.	si	1	.9511	190.22	si
2	1- 2	.5547	0.	si	2	.9485	189.7	si
2	1- 3	.956	0.	si	3	.9459	189.17	si
2	1- 4	.9962	0.	si	4	.9433	188.65	si
2	1- 5	.5949	0.	si	5	.9406	188.13	si
2	1- 6	.6054	0.	si	6	.938	187.61	si
2	1- 7	-.2121	-2.83	si	7	.9354	187.08	si
2	1- 8	-.2733	-3.59	si	8	.9328	186.56	si
2					9	.9302	186.04	si
2					10	.9276	185.52	si
2					11	.925	184.99	si
2					12	.9224	184.47	si
2					13	.9197	183.95	si
2					14	.9171	183.43	si
2					15	.9145	182.9	si
2					16	.9119	182.38	si
2					17	.5106	102.12	si
2					18	.5071	101.42	si
2					19	.5036	100.72	si
2					20	.5001	100.02	si
2					21	.5603	112.06	si
2					22	.5568	111.36	si
2					23	.5533	110.66	si
2					24	.5498	109.96	si
2					25	-.168	-33.6	si
2					26	-.1706	-34.13	si
2					27	-.1732	-34.65	si
2					28	-.1759	-35.17	si
2					29	-.1785	-35.7	si
2					30	-.1811	-36.22	si
2					31	-.1837	-36.74	si
2					32	-.1863	-37.27	si
2					33	-.1889	-37.79	si
2					34	-.1916	-38.31	si
2					35	-.1942	-38.84	si
2					36	-.1968	-39.36	si
2					37	-.1994	-39.88	si
2					38	-.202	-40.41	si
2					39	-.2046	-40.93	si
2					40	-.2073	-41.45	si
2					41	-.2099	-41.98	si
2					42	-.2125	-42.5	si
2					43	-.2151	-43.02	si
2					44	-.2177	-43.55	si
2					45	-.2203	-44.07	si
2					46	-.223	-44.59	si
2					47	-.2256	-45.12	si
2					48	-.2282	-45.64	si
3	1- 1	.6051	0.	si	1	.9116	182.31	si
3	1- 2	.5946	0.	si	2	.9142	182.83	si
3	1- 3	.9958	0.	si	3	.9168	183.36	si
3	1- 4	.9556	0.	si	4	.9194	183.88	si
3	1- 5	.5544	0.	si	5	.922	184.4	si
3	1- 6	.5439	0.	si	6	.9246	184.92	si
3	1- 7	-.2733	-3.59	si	7	.9272	185.45	si
3	1- 8	-.2122	-2.83	si	8	.9298	185.97	si
3					9	.9325	186.49	si
3					10	.9351	187.02	si
3					11	.9377	187.54	si
3					12	.9403	188.06	si
3					13	.9429	188.58	si
3					14	.9455	189.11	si
3					15	.9481	189.63	si
3					16	.9508	190.15	si
3					17	.5495	109.91	si
3					18	.553	110.61	si
3					19	.5565	111.31	si
3					20	.56	112.01	si
3					21	.4999	99.97	si
3					22	.5034	100.67	si
3					23	.5069	101.37	si
3					24	.5104	102.07	si
3					25	-.2282	-45.65	si
3					26	-.2256	-45.13	si
3					27	-.223	-44.6	si
3					28	-.2204	-44.08	si
3					29	-.2178	-43.56	si
3					30	-.2152	-43.03	si
3					31	-.2126	-42.51	si
3					32	-.2099	-41.99	si
3					33	-.2073	-41.46	si
3					34	-.2047	-40.94	si
3					35	-.2021	-40.42	si
3					36	-.1995	-39.89	si
3					37	-.1969	-39.37	si
3					38	-.1942	-38.85	si
3					39	-.1916	-38.33	si
3					40	-.189	-37.8	si
3					41	-.1864	-37.28	si
3					42	-.1838	-36.76	si
3					43	-.1812	-36.23	si
3					44	-.1785	-35.71	si
3					45	-.1759	-35.19	si
3					46	-.1733	-34.66	si
3					47	-.1707	-34.14	si
3					48	-.1681	-33.62	si
4	1- 1	.3518	0.	si	1	.5663	113.26	si

4	1- 2	.3505	0.	si	2	.5666	113.32	si
4	1- 3	.5986	0.	si	3	.5669	113.38	si
4	1- 4	.5938	0.	si	4	.5672	113.45	si
4	1- 5	.3457	0.	si	5	.5675	113.51	si
4	1- 6	.3444	0.	si	6	.5679	113.57	si
4	1- 7	-.161	-2.18	si	7	.5682	113.64	si
4	1- 8	-.1536	-2.08	si	8	.5685	113.7	si
4					9	.5688	113.76	si
4					10	.5691	113.82	si
4					11	.5694	113.89	si
4					12	.5698	113.95	si
4					13	.5701	114.01	si
4					14	.5704	114.08	si
4					15	.5707	114.14	si
4					16	.571	114.2	si
4					17	.3229	64.58	si
4					18	.3233	64.66	si
4					19	.3237	64.75	si
4					20	.3242	64.83	si
4					21	.3169	63.38	si
4					22	.3173	63.46	si
4					23	.3177	63.55	si
4					24	.3182	63.63	si
4					25	-.1334	-26.68	si
4					26	-.1331	-26.62	si
4					27	-.1328	-26.55	si
4					28	-.1325	-26.49	si
4					29	-.1321	-26.43	si
4					30	-.1318	-26.36	si
4					31	-.1315	-26.3	si
4					32	-.1312	-26.24	si
4					33	-.1309	-26.18	si
4					34	-.1306	-26.11	si
4					35	-.1302	-26.05	si
4					36	-.1299	-25.99	si
4					37	-.1296	-25.92	si
4					38	-.1293	-25.86	si
4					39	-.129	-25.8	si
4					40	-.1287	-25.73	si
4					41	-.1283	-25.67	si
4					42	-.128	-25.61	si
4					43	-.1277	-25.54	si
4					44	-.1274	-25.48	si
4					45	-.1271	-25.42	si
4					46	-.1268	-25.35	si
4					47	-.1264	-25.29	si
4					48	-.1261	-25.23	si
5	1- 1	.3993	0.	si	1	.6426	128.51	si
5	1- 2	.3995	0.	si	2	.6425	128.51	si
5	1- 3	.6724	0.	si	3	.6425	128.5	si
5	1- 4	.6729	0.	si	4	.6425	128.49	si
5	1- 5	.3999	0.	si	5	.6424	128.49	si
5	1- 6	.4001	0.	si	6	.6424	128.48	si
5	1- 7	-.156	-2.12	si	7	.6424	128.48	si
5	1- 8	-.1567	-2.12	si	8	.6423	128.47	si
5					9	.6423	128.46	si
5					10	.6423	128.46	si
5					11	.6423	128.45	si
5					12	.6422	128.45	si
5					13	.6422	128.44	si
5					14	.6422	128.43	si
5					15	.6421	128.43	si
5					16	.6421	128.42	si
5					17	.3691	73.83	si
5					18	.3691	73.82	si
5					19	.3691	73.81	si
5					20	.369	73.8	si
5					21	.3697	73.94	si
5					22	.3697	73.94	si
5					23	.3696	73.93	si
5					24	.3696	73.92	si
5					25	-.1257	-25.13	si
5					26	-.1257	-25.14	si
5					27	-.1257	-25.14	si
5					28	-.1257	-25.15	si
5					29	-.1258	-25.15	si
5					30	-.1258	-25.16	si
5					31	-.1258	-25.17	si
5					32	-.1259	-25.17	si
5					33	-.1259	-25.18	si
5					34	-.1259	-25.19	si
5					35	-.126	-25.19	si
5					36	-.126	-25.2	si
5					37	-.126	-25.2	si
5					38	-.126	-25.21	si
5					39	-.1261	-25.22	si
5					40	-.1261	-25.22	si
5					41	-.1261	-25.23	si
5					42	-.1262	-25.23	si
5					43	-.1262	-25.24	si
5					44	-.1262	-25.25	si
5					45	-.1263	-25.25	si
5					46	-.1263	-25.26	si
5					47	-.1263	-25.26	si
5					48	-.1264	-25.27	si

Descrizione : Pulvino 15

SOLLECITAZIONI AGENTI

Sforzi normali applicati in z= 183.7 ; y= 37.5 (baricentro CLS)
 Convenzioni: N + trazione; Mz + fib.inferiori tese; My + fib.sinistra tese.

N.	N	Mz	My	Descrizione
1	-48.32	-466.79	8.8764	Caso 13.1
2	-105.19	-845.1414	-223.5068	Caso 2.2
3	-106.37	-845.1895	223.5068	Caso 2.1
4	-184.09	-540.7622	-33.8173	Caso 8.20
5	47.81	-558.9393	4.7521	Caso 8.13

RISULTATI

Piani di equilibrio (eps= muz * y + muy * z + lam):

Sol.	muz	muy	lambda
1.	.00000816868	-.00000000703	-.00013148925
2.	.00001476218	.00000017937	-.00027567431
3.	.0000147585	-.00000017931	-.00020983283
4.	.00000897139	.00000002546	-.00016205613
5.	.00001019772	-.00000000395	-.00015544428

Deformazioni sui materiali:

CLS					Acciaio lento				
sol	vert.	D cls	S cls	Ve	ferro	D	S	ferri	Ve
1	1- 1	.3178	0.	si	1	.5117	102.34	si	
1	1- 2	.3173	0.	si	2	.5118	102.37	si	
1	1- 3	.5379	0.	si	3	.5119	102.39	si	
1	1- 4	.5362	0.	si	4	.512	102.41	si	
1	1- 5	.3156	0.	si	5	.5122	102.43	si	
1	1- 6	.3152	0.	si	6	.5123	102.45	si	
1	1- 7	-.1341	-1.83	si	7	.5124	102.48	si	
1	1- 8	-.1315	-1.79	si	8	.5125	102.5	si	
1					9	.5126	102.52	si	
1					10	.5127	102.54	si	
1					11	.5128	102.56	si	
1					12	.5129	102.59	si	
1					13	.513	102.61	si	
1					14	.5132	102.63	si	
1					15	.5133	102.65	si	
1					16	.5134	102.67	si	
1					17	.2928	58.56	si	
1					18	.293	58.59	si	
1					19	.2931	58.62	si	
1					20	.2933	58.65	si	
1					21	.2907	58.14	si	
1					22	.2909	58.17	si	
1					23	.291	58.2	si	
1					24	.2912	58.23	si	
1					25	-.1095	-21.91	si	
1					26	-.1094	-21.89	si	
1					27	-.1093	-21.87	si	
1					28	-.1092	-21.84	si	
1					29	-.1091	-21.82	si	
1					30	-.109	-21.8	si	
1					31	-.1089	-21.78	si	
1					32	-.1088	-21.75	si	
1					33	-.1087	-21.73	si	
1					34	-.1086	-21.71	si	
1					35	-.1084	-21.69	si	
1					36	-.1083	-21.67	si	
1					37	-.1082	-21.64	si	
1					38	-.1081	-21.62	si	
1					39	-.108	-21.6	si	
1					40	-.1079	-21.58	si	
1					41	-.1078	-21.56	si	
1					42	-.1077	-21.53	si	
1					43	-.1076	-21.51	si	
1					44	-.1074	-21.49	si	
1					45	-.1073	-21.47	si	
1					46	-.1072	-21.45	si	
1					47	-.1071	-21.42	si	
1					48	-.107	-21.4	si	
2	1- 1	.5362	0.	si	1	.9446	188.92	si	
2	1- 2	.5475	0.	si	2	.9418	188.36	si	
2	1- 3	.9461	0.	si	3	.939	187.79	si	
2	1- 4	.9894	0.	si	4	.9362	187.23	si	
2	1- 5	.5908	0.	si	5	.9333	186.67	si	
2	1- 6	.6021	0.	si	6	.9305	186.11	si	
2	1- 7	-.2098	-2.8	si	7	.9277	185.54	si	
2	1- 8	-.2757	-3.62	si	8	.9249	184.98	si	
2					9	.9221	184.42	si	
2					10	.9193	183.85	si	
2					11	.9165	183.29	si	
2					12	.9136	182.73	si	
2					13	.9108	182.16	si	
2					14	.908	181.6	si	
2					15	.9052	181.04	si	
2					16	.9024	180.48	si	
2					17	.5038	100.76	si	
2					18	.5	100.01	si	
2					19	.4963	99.25	si	
2					20	.4925	98.5	si	
2					21	.5573	111.46	si	
2					22	.5536	110.71	si	
2					23	.5498	109.96	si	
2					24	.546	109.2	si	
2					25	-.166	-33.21	si	

2				26	-.1688	-33.77	si
2				27	-.1717	-34.33	si
2				28	-.1745	-34.9	si
2				29	-.1773	-35.46	si
2				30	-.1801	-36.02	si
2				31	-.1829	-36.59	si
2				32	-.1858	-37.15	si
2				33	-.1886	-37.71	si
2				34	-.1914	-38.28	si
2				35	-.1942	-38.84	si
2				36	-.197	-39.41	si
2				37	-.1998	-39.97	si
2				38	-.2027	-40.53	si
2				39	-.2055	-41.1	si
2				40	-.2083	-41.66	si
2				41	-.2111	-42.22	si
2				42	-.2139	-42.79	si
2				43	-.2168	-43.35	si
2				44	-.2196	-43.92	si
2				45	-.2224	-44.48	si
2				46	-.2252	-45.04	si
2				47	-.228	-45.61	si
2				48	-.2308	-46.17	si
3	1- 1	.6019	0.	1	.902	180.41	si
3	1- 2	.5906	0.	2	.9049	180.97	si
3	1- 3	.9891	0.	3	.9077	181.53	si
3	1- 4	.9458	0.	4	.9105	182.1	si
3	1- 5	.5473	0.	5	.9133	182.66	si
3	1- 6	.536	0.	6	.9161	183.22	si
3	1- 7	-.2757	-3.62	7	.9189	183.79	si
3	1- 8	-.2098	-2.81	8	.9217	184.35	si
3				9	.9246	184.91	si
3				10	.9274	185.47	si
3				11	.9302	186.04	si
3				12	.933	186.6	si
3				13	.9358	187.16	si
3				14	.9386	187.73	si
3				15	.9414	188.29	si
3				16	.9443	188.85	si
3				17	.5458	109.15	si
3				18	.5495	109.91	si
3				19	.5533	110.66	si
3				20	.5571	111.41	si
3				21	.4923	98.45	si
3				22	.496	99.21	si
3				23	.4998	99.96	si
3				24	.5036	100.71	si
3				25	-.2309	-46.18	si
3				26	-.2281	-45.62	si
3				27	-.2253	-45.05	si
3				28	-.2224	-44.49	si
3				29	-.2196	-43.93	si
3				30	-.2168	-43.36	si
3				31	-.214	-42.8	si
3				32	-.2112	-42.24	si
3				33	-.2084	-41.67	si
3				34	-.2055	-41.11	si
3				35	-.2027	-40.54	si
3				36	-.1999	-39.98	si
3				37	-.1971	-39.42	si
3				38	-.1943	-38.85	si
3				39	-.1915	-38.29	si
3				40	-.1886	-37.73	si
3				41	-.1858	-37.16	si
3				42	-.183	-36.6	si
3				43	-.1802	-36.04	si
3				44	-.1774	-35.47	si
3				45	-.1745	-34.91	si
3				46	-.1717	-34.35	si
3				47	-.1689	-33.78	si
3				48	-.1661	-33.22	si
4	1- 1	.3314	0.	1	.5544	110.87	si
4	1- 2	.333	0.	2	.554	110.79	si
4	1- 3	.5752	0.	3	.5536	110.71	si
4	1- 4	.5813	0.	4	.5532	110.63	si
4	1- 5	.3391	0.	5	.5528	110.55	si
4	1- 6	.3407	0.	6	.5524	110.47	si
4	1- 7	-.1527	-2.07	7	.552	110.39	si
4	1- 8	-.1621	-2.19	8	.5516	110.31	si
4				9	.5512	110.23	si
4				10	.5508	110.15	si
4				11	.5504	110.07	si
4				12	.55	109.99	si
4				13	.5496	109.91	si
4				14	.5492	109.83	si
4				15	.5488	109.75	si
4				16	.5484	109.67	si
4				17	.3061	61.23	si
4				18	.3056	61.12	si
4				19	.3051	61.01	si
4				20	.3045	60.91	si
4				21	.3137	62.75	si
4				22	.3132	62.64	si
4				23	.3127	62.53	si
4				24	.3121	62.43	si
4				25	-.1259	-25.17	si
4				26	-.1263	-25.25	si

4				27	-.1267	-25.33	si
4				28	-.1271	-25.41	si
4				29	-.1275	-25.49	si
4				30	-.1279	-25.57	si
4				31	-.1283	-25.65	si
4				32	-.1287	-25.73	si
4				33	-.1291	-25.81	si
4				34	-.1295	-25.89	si
4				35	-.1299	-25.97	si
4				36	-.1303	-26.05	si
4				37	-.1307	-26.13	si
4				38	-.1311	-26.21	si
4				39	-.1315	-26.29	si
4				40	-.1319	-26.37	si
4				41	-.1323	-26.45	si
4				42	-.1327	-26.53	si
4				43	-.1331	-26.61	si
4				44	-.1335	-26.69	si
4				45	-.1339	-26.77	si
4				46	-.1343	-26.85	si
4				47	-.1347	-26.93	si
4				48	-.1351	-27.01	si
5	1- 1	.4054	0.	1	.649	129.8	si
5	1- 2	.4052	0.	2	.649	129.81	si
5	1- 3	.6805	0.	3	.6491	129.82	si
5	1- 4	.6796	0.	4	.6492	129.83	si
5	1- 5	.4042	0.	5	.6492	129.85	si
5	1- 6	.404	0.	6	.6493	129.86	si
5	1- 7	-.1569	-2.13	7	.6494	129.87	si
5	1- 8	-.1554	-2.11	8	.6494	129.88	si
5				9	.6495	129.9	si
5				10	.6495	129.91	si
5				11	.6496	129.92	si
5				12	.6497	129.93	si
5				13	.6497	129.95	si
5				14	.6498	129.96	si
5				15	.6499	129.97	si
5				16	.6499	129.98	si
5				17	.3746	74.92	si
5				18	.3747	74.93	si
5				19	.3747	74.95	si
5				20	.3748	74.97	si
5				21	.3734	74.68	si
5				22	.3735	74.7	si
5				23	.3736	74.71	si
5				24	.3736	74.73	si
5				25	-.1263	-25.26	si
5				26	-.1262	-25.25	si
5				27	-.1262	-25.23	si
5				28	-.1261	-25.22	si
5				29	-.126	-25.21	si
5				30	-.126	-25.2	si
5				31	-.1259	-25.18	si
5				32	-.1259	-25.17	si
5				33	-.1258	-25.16	si
5				34	-.1257	-25.15	si
5				35	-.1257	-25.13	si
5				36	-.1256	-25.12	si
5				37	-.1255	-25.11	si
5				38	-.1255	-25.1	si
5				39	-.1254	-25.08	si
5				40	-.1254	-25.07	si
5				41	-.1253	-25.06	si
5				42	-.1252	-25.05	si
5				43	-.1252	-25.03	si
5				44	-.1251	-25.02	si
5				45	-.125	-25.01	si
5				46	-.125	-25.	si
5				47	-.1249	-24.98	si
5				48	-.1249	-24.97	si

DIAGRAMMI SFORZI-DEFORMAZIONI DELLE SEZIONI:

N.B. Per ogni pulvino (in sezione XZ e in sezione YZ) è rappresentata la sezione soggetta al sestetto del caso di carico che induce la massima combinazione sforzi-deformazioni.

Ripristino Ponte-Tubo

VERIFICA PULVINO XZ 1

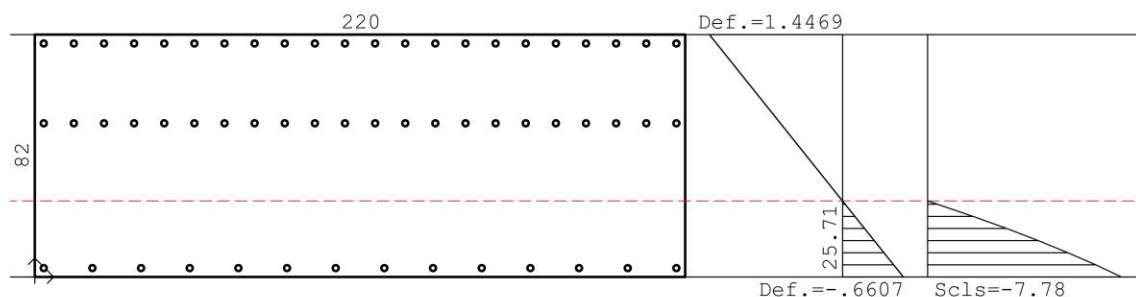
DESCRIZIONI
 Tipo sezione : RETTANGOLARE
 Tipo verifica: stato limite ultimo

CARATTERISTICHE DEI MATERIALI
 Calcestruzzo: Rck= 30.
 fck= 24.9
 fcd= 14.11 (.35%)
 Acciaio lento: Tipo= B450C
 fyk= 450.
 ftk= 540.
 ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
 eps= muz * y +muy * z + lam
 muz= 2.57027724705152E-05
 muy= 0
 lam=-3.66414843802945E-04

SOLLECITAZIONI AGENTI:
 Nd in y= 29.6 (baricentro CLS)
 Nd = -31.5
 Mdz=-1771.9308
 verifica in pressoflessione retta

UNITA' DI MISURA:
 kN; cm; kNm; N/mm2.
 Ø in mm; deformazioni*1000.
 SIMBOLI:
 S=sigma (tensioni sui materiali);
 D=deformazioni (epsilon):



TENSIONI NEL CLS:					
ver	Z	Y	Dcls	Scls	Vel
1	-2673.	70.6	1.44692	0.	si
2	-2453.	70.6	1.44692	0.	si
3	-2453.	-11.4	-0.66071	-7.78	si
4	-2673.	-11.4	-0.66071	-7.78	si

TENSIONI NEI FERRI:											
Fer	Z	Y	Ø (mm)	Af (cm2)	D	ferri	S	ferri	Vel		
1	-2456.	40.6	20	3.14		.67583		135.17	si		
2	-2456.	40.6	20	3.14		.67583		135.17	si		
3	-2476.	40.6	20	3.14		.67583		135.17	si		
4	-2487.	40.6	20	3.14		.67583		135.17	si		
5	-2497.	40.6	20	3.14		.67583		135.17	si		
6	-2507.	40.6	20	3.14		.67583		135.17	si		
7	-2517.	40.6	20	3.14		.67583		135.17	si		
8	-2527.	40.6	20	3.14		.67583		135.17	si		
9	-2538.	40.6	20	3.14		.67583		135.17	si		
10	-2548.	40.6	20	3.14		.67583		135.17	si		
11	-2558.	40.6	20	3.14		.67583		135.17	si		
12	-2568.	40.6	20	3.14		.67583		135.17	si		
13	-2578.	40.6	20	3.14		.67583		135.17	si		
14	-2589.	40.6	20	3.14		.67583		135.17	si		
15	-2599.	40.6	20	3.14		.67583		135.17	si		
16	-2609.	40.6	20	3.14		.67583		135.17	si		
17	-2619.	40.6	20	3.14		.67583		135.17	si		
18	-2629.	40.6	20	3.14		.67583		135.17	si		
19	-2639.	40.6	20	3.14		.67583		135.17	si		
20	-2650.	40.6	20	3.14		.67583		135.17	si		
21	-2660.	40.6	20	3.14		.67583		135.17	si		
22	-2670.	40.6	20	3.14		.67583		135.17	si		
23	-2456.	67.6	20	3.14	1.36981			273.96	si		
24	-2466.	67.6	20	3.14	1.36981			273.96	si		
25	-2476.	67.6	20	3.14	1.36981			273.96	si		
26	-2487.	67.6	20	3.14	1.36981			273.96	si		
27	-2497.	67.6	20	3.14	1.36981			273.96	si		
28	-2507.	67.6	20	3.14	1.36981			273.96	si		
29	-2517.	67.6	20	3.14	1.36981			273.96	si		
30	-2527.	67.6	20	3.14	1.36981			273.96	si		
31	-2538.	67.6	20	3.14	1.36981			273.96	si		
32	-2548.	67.6	20	3.14	1.36981			273.96	si		
33	-2558.	67.6	20	3.14	1.36981			273.96	si		
34	-2568.	67.6	20	3.14	1.36981			273.96	si		
35	-2578.	67.6	20	3.14	1.36981			273.96	si		
36	-2589.	67.6	20	3.14	1.36981			273.96	si		
37	-2599.	67.6	20	3.14	1.36981			273.96	si		
38	-2609.	67.6	20	3.14	1.36981			273.96	si		
39	-2619.	67.6	20	3.14	1.36981			273.96	si		
40	-2629.	67.6	20	3.14	1.36981			273.96	si		
41	-2639.	67.6	20	3.14	1.36981			273.96	si		
42	-2650.	67.6	20	3.14	1.36981			273.96	si		
43	-2660.	67.6	20	3.14	1.36981			273.96	si		
44	-2670.	67.6	20	3.14	1.36981			273.96	si		
45	-2456.	-8.4	20	3.14		-.5836		-116.72	si		
46	-2473.	-8.4	20	3.14		-.5836		-116.72	si		
47	-2489.	-8.4	20	3.14		-.5836		-116.72	si		
48	-2505.	-8.4	20	3.14		-.5836		-116.72	si		
49	-2522.	-8.4	20	3.14		-.5836		-116.72	si		
50	-2538.	-8.4	20	3.14		-.5836		-116.72	si		
51	-2555.	-8.4	20	3.14		-.5836		-116.72	si		
52	-2571.	-8.4	20	3.14		-.5836		-116.72	si		
53	-2588.	-8.4	20	3.14		-.5836		-116.72	si		
54	-2604.	-8.4	20	3.14		-.5836		-116.72	si		
55	-2621.	-8.4	20	3.14		-.5836		-116.72	si		
56	-2637.	-8.4	20	3.14		-.5836		-116.72	si		
57	-2654.	-8.4	20	3.14		-.5836		-116.72	si		
58	-2670.	-8.4	20	3.14		-.5836		-116.72	si		

% ARMAT.: tesa = .77; comp. = .24; tot. = 1.01

Ripristino Ponte-Tubo

VERIFICA PULVINO YZ 1

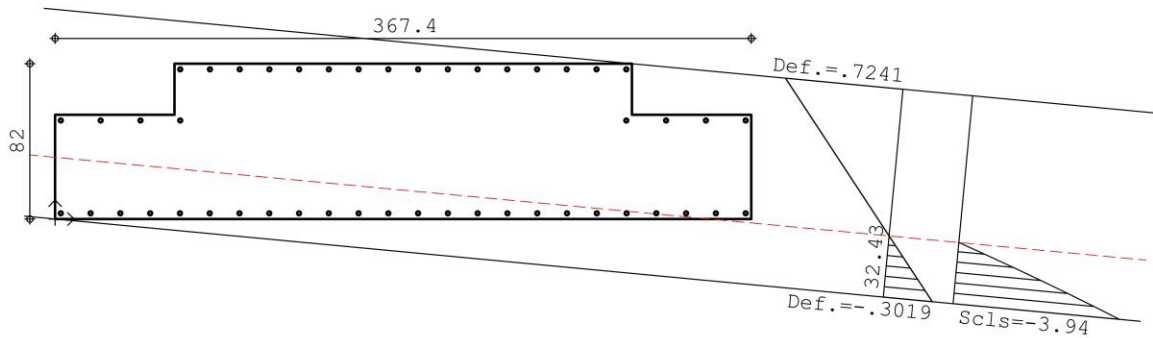
DESCRIZIONI
 Tipo sezione : U Pul
 Tipo verifica: stato limite ultimo

CARATTERISTICHE DEI MATERIALI
 Calcestruzzo: Rck= 30.
 fck= 24.9
 fcd= 14.11 (.35%)
 Acciaio lento: Tipo= B450C
 fyk= 450.
 ftk= 540.
 ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
 eps= muz * y +muy * z + lam
 muz= 9.26901994522476E-06
 muy= 8.73848386215035E-07
 lam=-3.0191859034969E-04

SOLLECITAZIONI AGENTI:
 Nd in z= 183.7; y= 37.5 (baricentro CLS)
 Nd = -174.98
 Mdz= -555.6568
 Mdy=-1045.1818

UNITA' DI MISURA:
 kN; cm; kNm; N/mm2.
 Ø in mm; deformazioni*1000.
 SIMBOLI:
 S=sigma (tensioni sui materiali);
 D=deformazioni (epsilon):



TENSIONI NEL CLS:			Dcls	Scls	Ve
ver	Z	Y			
1	0.	55.	.20788	0.	si
2	63.	55.	.26293	0.	si
3	63.	82.	.51319	0.	si
4	304.4	82.	.72414	0.	si
5	304.4	55.	.47388	0.	si
6	367.4	55.	.52893	0.	si
7	367.4	0.	.01913	0.	si
8	0.	0.	-.30192	-3.94	si

TENSIONI NEI FERRI:									
Fer	Z	Y	Ø (mm)	Af (cm2)	D	ferri	S	ferri	Ve
1	301.4	79.	20	3.14	3.14	.69371		138.74	si
2	285.7	79.	20	3.14	3.14	.68		136.	si
3	270.	79.	20	3.14	3.14	.66628		133.26	si
4	254.3	79.	20	3.14	3.14	.65257		130.51	si
5	238.6	79.	20	3.14	3.14	.63886		127.77	si
6	222.9	79.	20	3.14	3.14	.62514		125.03	si
7	207.2	79.	20	3.14	3.14	.61143		122.29	si
8	191.5	79.	20	3.14	3.14	.59772		119.54	si
9	175.9	79.	20	3.14	3.14	.584		116.8	si
10	160.2	79.	20	3.14	3.14	.57029		114.06	si
11	144.5	79.	20	3.14	3.14	.55658		111.32	si
12	128.8	79.	20	3.14	3.14	.54286		108.57	si
13	113.1	79.	20	3.14	3.14	.52915		105.83	si
14	97.4	79.	20	3.14	3.14	.51544		103.09	si
15	81.7	79.	20	3.14	3.14	.50172		100.34	si
16	66.	79.	20	3.14	3.14	.48801		97.6	si
17	66.	52.	20	3.14	3.14	.23774		47.55	si
18	45.	52.	20	3.14	3.14	.21939		43.88	si
19	24.	52.	20	3.14	3.14	.20104		40.21	si
20	3.	52.	20	3.14	3.14	.18269		36.54	si
21	364.4	52.	20	3.14	3.14	.4985		99.7	si
22	343.4	52.	20	3.14	3.14	.48015		96.03	si
23	322.4	52.	20	3.14	3.14	.4618		92.36	si
24	301.4	52.	20	3.14	3.14	.44345		88.69	si
25	364.4	3.	20	3.14	3.14	.04432		8.86	si
26	348.7	3.	20	3.14	3.14	.03059		6.12	si
27	333.	3.	20	3.14	3.14	.01686		3.37	si
28	317.3	3.	20	3.14	3.14	.00313		.63	si
29	301.5	3.	20	3.14	3.14	-.0106		-2.12	si
30	285.8	3.	20	3.14	3.14	-.02434		-4.87	si
31	270.1	3.	20	3.14	3.14	-.03807		-7.61	si
32	254.4	3.	20	3.14	3.14	-.0518		-10.36	si
33	238.7	3.	20	3.14	3.14	-.06553		-13.11	si
34	223.	3.	20	3.14	3.14	-.07926		-15.85	si
35	207.3	3.	20	3.14	3.14	-.09299		-18.6	si
36	191.6	3.	20	3.14	3.14	-.10672		-21.34	si
37	175.8	3.	20	3.14	3.14	-.12045		-24.09	si
38	160.1	3.	20	3.14	3.14	-.13418		-26.84	si
39	144.4	3.	20	3.14	3.14	-.14791		-29.58	si
40	128.7	3.	20	3.14	3.14	-.16164		-32.33	si
41	113.	3.	20	3.14	3.14	-.17537		-35.07	si
42	97.3	3.	20	3.14	3.14	-.18911		-37.82	si
43	81.6	3.	20	3.14	3.14	-.20284		-40.57	si
44	65.9	3.	20	3.14	3.14	-.21657		-43.31	si
45	50.1	3.	20	3.14	3.14	-.2303		-46.06	si
46	34.4	3.	20	3.14	3.14	-.24403		-48.81	si
47	18.7	3.	20	3.14	3.14	-.25776		-51.55	si
48	3.	3.	20	3.14	3.14	-.27149		-54.3	si

% ARMAT.: tesa = .33; comp. = .24; tot. = .56

Ripristino Ponte-Tubo

VERIFICA PULVINO XZ 2

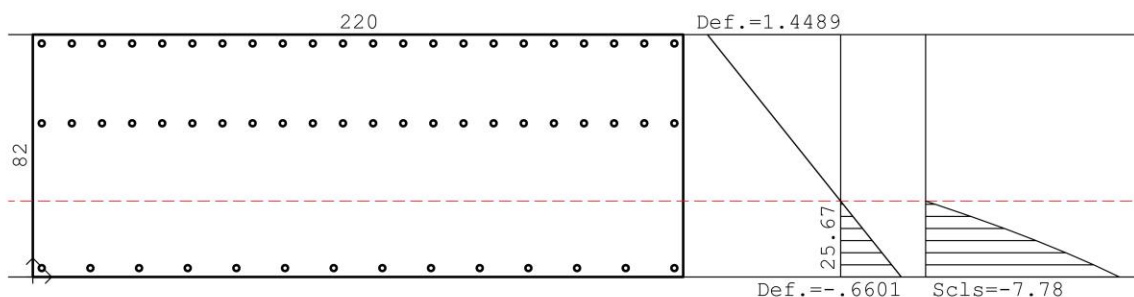
DESCRIZIONI
 Tipo sezione : RETTANGOLARE
 Tipo verifica: stato limite ultimo

CARATTERISTICHE DEI MATERIALI
 Calcestruzzo: Rck= 30.
 fck= 24.9
 fcd= 14.11 (.35%)
 Acciaio lento: Tipo= B450C
 fyk= 450.
 ftk= 540.
 ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
 eps= muz * y + muy * z + lam
 muz= 2.57200038071636E-05
 muy= 0
 lam=-3.65622080643258E-04

SOLLECITAZIONI AGENTI:
 Nd in y= 29.6 (baricentro CLS)
 Nd = -20.63
 Mdz=-1771.5199
 verifica in pressoflessione retta

UNITA' DI MISURA:
 kN; cm; kNm; N/mm2.
 Ø in mm; deformazioni*1000.
 SIMBOLI:
 S=sigma (tensioni sui materiali);
 D=deformazioni (epsilon):



TENSIONI NEL CLS:					
ver	Z	Y	Dcls	Scls	Ve
1	-2673.	70.6	1.44892	0.	si
2	-2453.	70.6	1.44892	0.	si
3	-2453.	-11.4	-.66012	-7.78	si
4	-2673.	-11.4	-.66012	-7.78	si

TENSIONI NEI FERRI:											
Fer	Z	Y	Ø (mm)	Af (cm2)	D	ferr	S	ferr	Ve		
1	-2456.	40.6	20	3.14		.67732		135.46	si		
2	-2456.	40.6	20	3.14		.67732		135.46	si		
3	-2476.	40.6	20	3.14		.67732		135.46	si		
4	-2487.	40.6	20	3.14		.67732		135.46	si		
5	-2497.	40.6	20	3.14		.67732		135.46	si		
6	-2507.	40.6	20	3.14		.67732		135.46	si		
7	-2517.	40.6	20	3.14		.67732		135.46	si		
8	-2527.	40.6	20	3.14		.67732		135.46	si		
9	-2538.	40.6	20	3.14		.67732		135.46	si		
10	-2548.	40.6	20	3.14		.67732		135.46	si		
11	-2558.	40.6	20	3.14		.67732		135.46	si		
12	-2568.	40.6	20	3.14		.67732		135.46	si		
13	-2578.	40.6	20	3.14		.67732		135.46	si		
14	-2589.	40.6	20	3.14		.67732		135.46	si		
15	-2599.	40.6	20	3.14		.67732		135.46	si		
16	-2609.	40.6	20	3.14		.67732		135.46	si		
17	-2619.	40.6	20	3.14		.67732		135.46	si		
18	-2629.	40.6	20	3.14		.67732		135.46	si		
19	-2639.	40.6	20	3.14		.67732		135.46	si		
20	-2650.	40.6	20	3.14		.67732		135.46	si		
21	-2660.	40.6	20	3.14		.67732		135.46	si		
22	-2670.	40.6	20	3.14		.67732		135.46	si		
23	-2456.	67.6	20	3.14	1.37176			274.35	si		
24	-2466.	67.6	20	3.14	1.37176			274.35	si		
25	-2476.	67.6	20	3.14	1.37176			274.35	si		
26	-2487.	67.6	20	3.14	1.37176			274.35	si		
27	-2497.	67.6	20	3.14	1.37176			274.35	si		
28	-2507.	67.6	20	3.14	1.37176			274.35	si		
29	-2517.	67.6	20	3.14	1.37176			274.35	si		
30	-2527.	67.6	20	3.14	1.37176			274.35	si		
31	-2538.	67.6	20	3.14	1.37176			274.35	si		
32	-2548.	67.6	20	3.14	1.37176			274.35	si		
33	-2558.	67.6	20	3.14	1.37176			274.35	si		
34	-2568.	67.6	20	3.14	1.37176			274.35	si		
35	-2578.	67.6	20	3.14	1.37176			274.35	si		
36	-2589.	67.6	20	3.14	1.37176			274.35	si		
37	-2599.	67.6	20	3.14	1.37176			274.35	si		
38	-2609.	67.6	20	3.14	1.37176			274.35	si		
39	-2619.	67.6	20	3.14	1.37176			274.35	si		
40	-2629.	67.6	20	3.14	1.37176			274.35	si		
41	-2639.	67.6	20	3.14	1.37176			274.35	si		
42	-2650.	67.6	20	3.14	1.37176			274.35	si		
43	-2660.	67.6	20	3.14	1.37176			274.35	si		
44	-2670.	67.6	20	3.14	1.37176			274.35	si		
45	-2456.	-8.4	20	3.14	-.58296			-116.59	si		
46	-2473.	-8.4	20	3.14	-.58296			-116.59	si		
47	-2489.	-8.4	20	3.14	-.58296			-116.59	si		
48	-2505.	-8.4	20	3.14	-.58296			-116.59	si		
49	-2522.	-8.4	20	3.14	-.58296			-116.59	si		
50	-2538.	-8.4	20	3.14	-.58296			-116.59	si		
51	-2555.	-8.4	20	3.14	-.58296			-116.59	si		
52	-2571.	-8.4	20	3.14	-.58296			-116.59	si		
53	-2588.	-8.4	20	3.14	-.58296			-116.59	si		
54	-2604.	-8.4	20	3.14	-.58296			-116.59	si		
55	-2621.	-8.4	20	3.14	-.58296			-116.59	si		
56	-2637.	-8.4	20	3.14	-.58296			-116.59	si		
57	-2654.	-8.4	20	3.14	-.58296			-116.59	si		
58	-2670.	-8.4	20	3.14	-.58296			-116.59	si		

% ARMAT.: tesa = .77; comp. = .24; tot. = 1.01

Ripristino Ponte-Tubo

VERIFICA PULVINO YZ 2

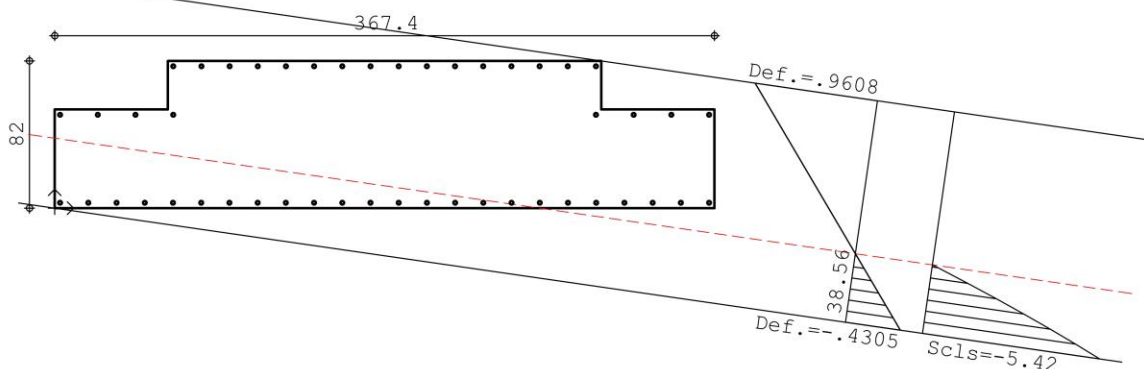
DESCRIZIONI
 Tipo sezione : U Pul
 Tipo verifica: stato limite ultimo

CARATTERISTICHE DEI MATERIALI
 Calcestruzzo: Rck= 30.
 fck= 24.9
 fcd= 14.11 (.35%)
 Acciaio lento: Tipo= B450C
 fyk= 450.
 ftk= 540.
 ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
 eps= muz * y + muy * z + lam
 muz= 1.10489328215218E-05
 muy= 1.59425866965021E-06
 lam=-4.30503694172218E-04

SOLLECITAZIONI AGENTI:
 Nd in z= 183.7; y= 37.5 (baricentro CLS)
 Nd = -206.69
 Mdz= -671.6013
 Mdy=-1714.424

UNITA' DI MISURA:
 kN; cm; kNm; N/mm2.
 Ø in mm; deformazioni*1000.
 SIMBOLI:
 S=sigma (tensioni sui materiali);
 D=deformazioni (epsilon):



TENSIONI NEL CLS:			Dcls	Scls	Ve
ver	Z	Y			
1	0.	55.	.17719	0.	si
2	63.	55.	.27763	0.	si
3	63.	82.	.57595	0.	si
4	304.4	82.	.9608	0.	si
5	304.4	55.	.66248	0.	si
6	367.4	55.	.76292	0.	si
7	367.4	0.	.15523	0.	si
8	0.	0.	-.4305	-5.42	si

TENSIONI NEI FERRI:									
Fer	Z	Y	Ø (mm)	Af (cm2)	D	ferri	S	ferri	Ve
1	301.4	79.	20	3.14	3.14	.92287		184.57	si
2	285.7	79.	20	3.14	3.14	.89785		179.57	si
3	270.	79.	20	3.14	3.14	.87283		174.57	si
4	254.3	79.	20	3.14	3.14	.84781		169.56	si
5	238.6	79.	20	3.14	3.14	.8228		164.56	si
6	222.9	79.	20	3.14	3.14	.79777		159.55	si
7	207.2	79.	20	3.14	3.14	.77276		154.55	si
8	191.5	79.	20	3.14	3.14	.74774		149.55	si
9	175.9	79.	20	3.14	3.14	.72272		144.54	si
10	160.2	79.	20	3.14	3.14	.6977		139.54	si
11	144.5	79.	20	3.14	3.14	.67268		134.54	si
12	128.8	79.	20	3.14	3.14	.64766		129.53	si
13	113.1	79.	20	3.14	3.14	.62264		124.53	si
14	97.4	79.	20	3.14	3.14	.59762		119.52	si
15	81.7	79.	20	3.14	3.14	.5726		114.52	si
16	66.	79.	20	3.14	3.14	.54758		109.52	si
17	66.	52.	20	3.14	3.14	.24926		49.85	si
18	45.	52.	20	3.14	3.14	.21578		43.16	si
19	24.	52.	20	3.14	3.14	.1823		36.46	si
20	3.	52.	20	3.14	3.14	.14882		29.76	si
21	364.4	52.	20	3.14	3.14	.72499		145.	si
22	343.4	52.	20	3.14	3.14	.69151		138.3	si
23	322.4	52.	20	3.14	3.14	.65803		131.61	si
24	301.4	52.	20	3.14	3.14	.62455		124.91	si
25	364.4	3.	20	3.14	3.14	.18359		36.72	si
26	348.7	3.	20	3.14	3.14	.15854		31.71	si
27	333.	3.	20	3.14	3.14	.13349		26.7	si
28	317.3	3.	20	3.14	3.14	.10844		21.69	si
29	301.5	3.	20	3.14	3.14	.08339		16.68	si
30	285.8	3.	20	3.14	3.14	.05834		11.67	si
31	270.1	3.	20	3.14	3.14	.03329		6.66	si
32	254.4	3.	20	3.14	3.14	.00824		1.65	si
33	238.7	3.	20	3.14	3.14	-.01681		-3.36	si
34	223.	3.	20	3.14	3.14	-.04186		-8.37	si
35	207.3	3.	20	3.14	3.14	-.06691		-13.38	si
36	191.6	3.	20	3.14	3.14	-.09197		-18.39	si
37	175.8	3.	20	3.14	3.14	-.11702		-23.4	si
38	160.1	3.	20	3.14	3.14	-.14207		-28.41	si
39	144.4	3.	20	3.14	3.14	-.16712		-33.42	si
40	128.7	3.	20	3.14	3.14	-.19217		-38.43	si
41	113.	3.	20	3.14	3.14	-.21722		-43.44	si
42	97.3	3.	20	3.14	3.14	-.24227		-48.45	si
43	81.6	3.	20	3.14	3.14	-.26732		-53.46	si
44	65.9	3.	20	3.14	3.14	-.29237		-58.47	si
45	50.1	3.	20	3.14	3.14	-.31742		-63.48	si
46	34.4	3.	20	3.14	3.14	-.34247		-68.49	si
47	18.7	3.	20	3.14	3.14	-.36752		-73.5	si
48	3.	3.	20	3.14	3.14	-.39257		-78.51	si

% ARMAT.: tesa= .38; comp.= .19; tot.= .56

Ripristino Ponte-Tubo

VERIFICA PULVINO XZ 3

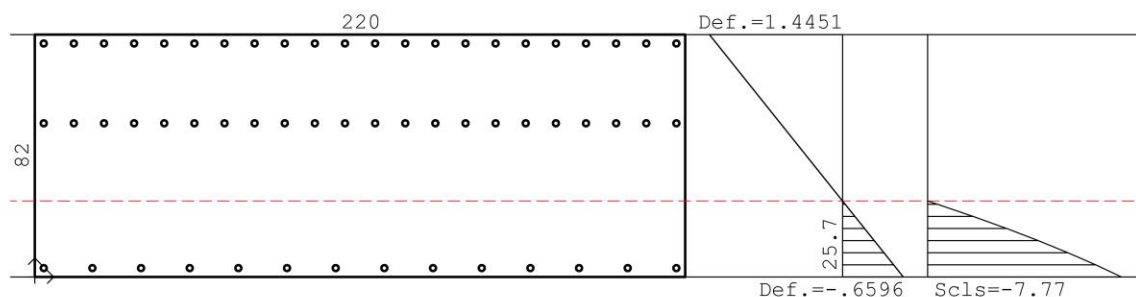
DESCRIZIONI
 Tipo sezione : RETTANGOLARE
 Tipo verifica: stato limite ultimo

CARATTERISTICHE DEI MATERIALI
 Calcestruzzo: Rck= 30.
 fck= 24.9
 fcd= 14.11 (.35%)
 Acciaio lento: Tipo= B450C
 fyk= 450.
 ftk= 540.
 ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
 eps= muz * y +muy * z + lam
 muz= 2.56669177387275E-05
 muy= 0
 lam=-3.65705735258854E-04

SOLLECITAZIONI AGENTI:
 Nd in y= 29.6 (baricentro CLS)
 Nd = -29.82
 Mdz=-1769.3066
 verifica in pressoflessione retta

UNITA' DI MISURA:
 kN; cm; kNm; N/mm2.
 Ø in mm; deformazioni*1000.
 SIMBOLI:
 S=sigma (tensioni sui materiali);
 D=deformazioni (epsilon):



TENSIONI NEL CLS:					
ver	Z	Y	Dcls	Scls	Ve
1	-2673.	70.6	1.4451	0.	si
2	-2453.	70.6	1.4451	0.	si
3	-2453.	-11.4	-.65959	-7.77	si
4	-2673.	-11.4	-.65959	-7.77	si

TENSIONI NEI FERRI:										
Fer	Z	Y	Ø (mm)	Af (cm2)	D	ferri	S	ferri	Ve	
1	-2456.	40.6	20	3.14		.67509		135.02	si	
3	-2466.	40.6	20	3.14		.67509		135.02	si	
3	-2476.	40.6	20	3.14		.67509		135.02	si	
4	-2487.	40.6	20	3.14		.67509		135.02	si	
5	-2497.	40.6	20	3.14		.67509		135.02	si	
6	-2507.	40.6	20	3.14		.67509		135.02	si	
7	-2517.	40.6	20	3.14		.67509		135.02	si	
8	-2527.	40.6	20	3.14		.67509		135.02	si	
9	-2538.	40.6	20	3.14		.67509		135.02	si	
10	-2548.	40.6	20	3.14		.67509		135.02	si	
11	-2558.	40.6	20	3.14		.67509		135.02	si	
12	-2568.	40.6	20	3.14		.67509		135.02	si	
13	-2578.	40.6	20	3.14		.67509		135.02	si	
14	-2589.	40.6	20	3.14		.67509		135.02	si	
15	-2599.	40.6	20	3.14		.67509		135.02	si	
16	-2609.	40.6	20	3.14		.67509		135.02	si	
17	-2619.	40.6	20	3.14		.67509		135.02	si	
18	-2629.	40.6	20	3.14		.67509		135.02	si	
19	-2639.	40.6	20	3.14		.67509		135.02	si	
20	-2650.	40.6	20	3.14		.67509		135.02	si	
21	-2660.	40.6	20	3.14		.67509		135.02	si	
22	-2670.	40.6	20	3.14		.67509		135.02	si	
23	-2456.	67.6	20	3.14	1.36809		273.62	si		
24	-2466.	67.6	20	3.14	1.36809		273.62	si		
25	-2476.	67.6	20	3.14	1.36809		273.62	si		
26	-2487.	67.6	20	3.14	1.36809		273.62	si		
27	-2497.	67.6	20	3.14	1.36809		273.62	si		
28	-2507.	67.6	20	3.14	1.36809		273.62	si		
29	-2517.	67.6	20	3.14	1.36809		273.62	si		
30	-2527.	67.6	20	3.14	1.36809		273.62	si		
31	-2538.	67.6	20	3.14	1.36809		273.62	si		
32	-2548.	67.6	20	3.14	1.36809		273.62	si		
33	-2558.	67.6	20	3.14	1.36809		273.62	si		
34	-2568.	67.6	20	3.14	1.36809		273.62	si		
35	-2578.	67.6	20	3.14	1.36809		273.62	si		
36	-2589.	67.6	20	3.14	1.36809		273.62	si		
37	-2599.	67.6	20	3.14	1.36809		273.62	si		
38	-2609.	67.6	20	3.14	1.36809		273.62	si		
39	-2619.	67.6	20	3.14	1.36809		273.62	si		
40	-2629.	67.6	20	3.14	1.36809		273.62	si		
41	-2639.	67.6	20	3.14	1.36809		273.62	si		
42	-2650.	67.6	20	3.14	1.36809		273.62	si		
43	-2660.	67.6	20	3.14	1.36809		273.62	si		
44	-2670.	67.6	20	3.14	1.36809		273.62	si		
45	-2456.	-8.4	20	3.14	-.58259		-116.52	si		
46	-2473.	-8.4	20	3.14	-.58259		-116.52	si		
47	-2489.	-8.4	20	3.14	-.58259		-116.52	si		
48	-2505.	-8.4	20	3.14	-.58259		-116.52	si		
49	-2522.	-8.4	20	3.14	-.58259		-116.52	si		
50	-2538.	-8.4	20	3.14	-.58259		-116.52	si		
51	-2555.	-8.4	20	3.14	-.58259		-116.52	si		
52	-2571.	-8.4	20	3.14	-.58259		-116.52	si		
53	-2588.	-8.4	20	3.14	-.58259		-116.52	si		
54	-2604.	-8.4	20	3.14	-.58259		-116.52	si		
55	-2621.	-8.4	20	3.14	-.58259		-116.52	si		
56	-2637.	-8.4	20	3.14	-.58259		-116.52	si		
57	-2654.	-8.4	20	3.14	-.58259		-116.52	si		
58	-2670.	-8.4	20	3.14	-.58259		-116.52	si		

% ARMAT.: tesa = .77; comp. = .24; tot. = 1.01

Ripristino Ponte-Tubo

VERIFICA PULVINO YZ 3

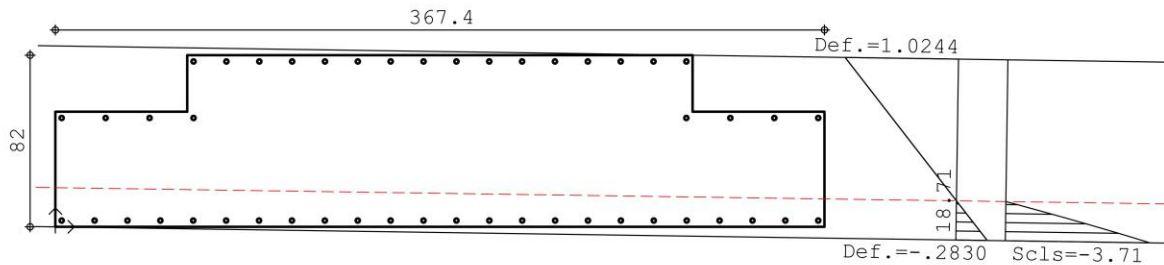
DESCRIZIONI
 Tipo sezione : U Pul
 Tipo verifica: stato limite ultimo

CARATTERISTICHE DEI MATERIALI
 Calcestruzzo: Rck= 30.
 fck= 24.9
 fcd= 14.11 (.35%)
 Acciaio lento: Tipo= B450C
 fyk= 450.
 ftk= 540.
 ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
 eps= muz * y + muy * z + lam
 muz= 1.51230539881345E-05
 muy= 2.21176653333537E-07
 lam=-2.83024445486093E-04

SOLLECITAZIONI AGENTI:
 Nd in z= 183.7; y= 37.5 (baricentro CLS)
 Nd = -40.91
 Mdz= -851.3607
 Mdy= -270.5802

UNITA' DI MISURA:
 kN; cm; kNm; N/mm2.
 Ø in mm; deformazioni*1000.
 SIMBOLI:
 S=sigma (tensioni sui materiali);
 D=deformazioni (epsilon):



TENSIONI NEL CLS:			Dcls	Scls	Vel
ver	Z	Y			
1	0.	55.	.54874	0.	si
2	63.	55.	.56268	0.	si
3	63.	82.	.971	0.	si
4	304.4	82.	1.02439	0.	si
5	304.4	55.	.61607	0.	si
6	367.4	55.	.63	0.	si
7	367.4	0.	-.20176	-2.7	si
8	0.	0.	-.28302	-3.71	si

TENSIONI NEI FERRI:									
Fer	Z	Y	Ø (mm)	Af (cm2)	D	ferri	S	ferri	Vel
1	301.4	79.	20	3.14	.97836	.97836	195.67	si	
2	285.7	79.	20	3.14	.97489	.97489	194.98	si	
3	270.	79.	20	3.14	.97142	.97142	194.28	si	
4	254.3	79.	20	3.14	.96795	.96795	193.59	si	
5	238.6	79.	20	3.14	.96448	.96448	192.9	si	
6	222.9	79.	20	3.14	.961	.961	192.2	si	
7	207.2	79.	20	3.14	.95753	.95753	191.51	si	
8	191.5	79.	20	3.14	.95406	.95406	190.81	si	
9	175.9	79.	20	3.14	.95059	.95059	190.12	si	
10	160.2	79.	20	3.14	.94712	.94712	189.42	si	
11	144.5	79.	20	3.14	.94365	.94365	188.73	si	
12	128.8	79.	20	3.14	.94018	.94018	188.04	si	
13	113.1	79.	20	3.14	.93671	.93671	187.34	si	
14	97.4	79.	20	3.14	.93324	.93324	186.65	si	
15	81.7	79.	20	3.14	.92977	.92977	185.95	si	
16	66.	79.	20	3.14	.92629	.92629	185.26	si	
17	66.	52.	20	3.14	.51797	.51797	103.59	si	
18	45.	52.	20	3.14	.51333	.51333	102.67	si	
19	24.	52.	20	3.14	.50868	.50868	101.74	si	
20	3.	52.	20	3.14	.50404	.50404	100.81	si	
21	364.4	52.	20	3.14	.58397	.58397	116.79	si	
22	343.4	52.	20	3.14	.57933	.57933	115.87	si	
23	322.4	52.	20	3.14	.57468	.57468	114.94	si	
24	301.4	52.	20	3.14	.57004	.57004	114.01	si	
25	364.4	3.	20	3.14	-.15706	-.15706	-31.41	si	
26	348.7	3.	20	3.14	-.16053	-.16053	-32.11	si	
27	333.	3.	20	3.14	-.16401	-.16401	-32.8	si	
28	317.3	3.	20	3.14	-.16748	-.16748	-33.5	si	
29	301.5	3.	20	3.14	-.17096	-.17096	-34.19	si	
30	285.8	3.	20	3.14	-.17444	-.17444	-34.89	si	
31	270.1	3.	20	3.14	-.17791	-.17791	-35.58	si	
32	254.4	3.	20	3.14	-.18139	-.18139	-36.28	si	
33	238.7	3.	20	3.14	-.18486	-.18486	-36.97	si	
34	223.	3.	20	3.14	-.18834	-.18834	-37.67	si	
35	207.3	3.	20	3.14	-.19181	-.19181	-38.36	si	
36	191.6	3.	20	3.14	-.19529	-.19529	-39.06	si	
37	175.8	3.	20	3.14	-.19876	-.19876	-39.75	si	
38	160.1	3.	20	3.14	-.20224	-.20224	-40.45	si	
39	144.4	3.	20	3.14	-.20571	-.20571	-41.14	si	
40	128.7	3.	20	3.14	-.20919	-.20919	-41.84	si	
41	113.	3.	20	3.14	-.21266	-.21266	-42.53	si	
42	97.3	3.	20	3.14	-.21614	-.21614	-43.23	si	
43	81.6	3.	20	3.14	-.21962	-.21962	-43.92	si	
44	65.9	3.	20	3.14	-.22309	-.22309	-44.62	si	
45	50.1	3.	20	3.14	-.22657	-.22657	-45.31	si	
46	34.4	3.	20	3.14	-.23004	-.23004	-46.01	si	
47	18.7	3.	20	3.14	-.23352	-.23352	-46.7	si	
48	3.	3.	20	3.14	-.23699	-.23699	-47.4	si	

% ARMAT.: tesa= .28; comp.= .28; tot.= .56

Ripristino Ponte-Tubo
VERIFICA PULVINO XZ 4

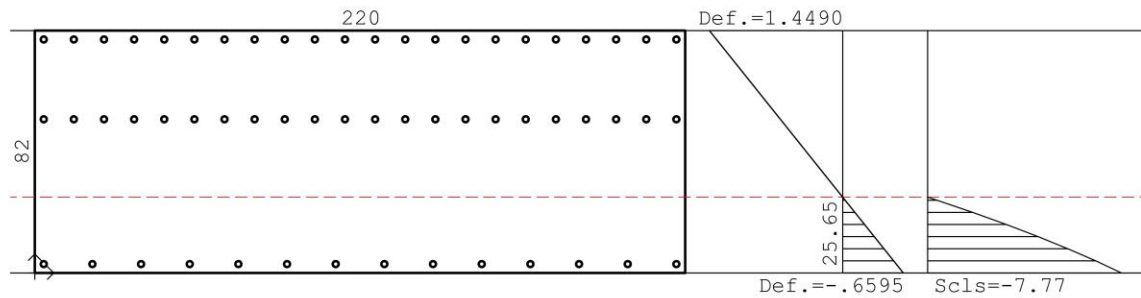
DESCRIZIONI
Tipo sezione : RETTANGOLARE
Tipo verifica: stato limite ultimo

CARATTERISTICHE DEI MATERIALI
Calcestruzzo: Rck= 30.
fck= 24.9
fcd= 14.11 (.35%)
Acciaio lento: Tipo= B450C
fyk= 450.
ftk= 540.
ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
eps= muz * y +muy * z + lam
muz= 2.57128507926903E-05
muy= 0
lam=-3.65049808951236E-04

SOLLECITAZIONI AGENTI:
Nd in y= 29.6 (baricentro CLS)
Nd = -15.86
Mdz=-1770.3612
verifica in pressoflessione retta

UNITA' DI MISURA:
kN; cm; kNm; N/mm2.
Ø in mm; deformazioni*1000.
SIMBOLI:
S=sigma (tensioni sui materiali);
D=deformazioni (epsilon):



TENSIONI NEL CLS:					
ver	Z	Y	Dcls	Scls	Ve
1	-2673.	70.6	1.44899	0.	si
2	-2453.	70.6	1.44899	0.	si
3	-2453.	-11.4	-6.5946	-7.77	si
4	-2673.	-11.4	-6.5946	-7.77	si

TENSIONI NEI FERRI:										
Fer	Z	Y	Ø (mm)	Af (cm2)	D	ferr	S	ferr	Ve	
1	-2456.	40.6	20	3.14		.67761		135.52	si	
3	-2466.	40.6	20	3.14		.67761		135.52	si	
3	-2476.	40.6	20	3.14		.67761		135.52	si	
4	-2487.	40.6	20	3.14		.67761		135.52	si	
5	-2497.	40.6	20	3.14		.67761		135.52	si	
6	-2507.	40.6	20	3.14		.67761		135.52	si	
7	-2517.	40.6	20	3.14		.67761		135.52	si	
8	-2527.	40.6	20	3.14		.67761		135.52	si	
9	-2538.	40.6	20	3.14		.67761		135.52	si	
10	-2548.	40.6	20	3.14		.67761		135.52	si	
11	-2558.	40.6	20	3.14		.67761		135.52	si	
12	-2568.	40.6	20	3.14		.67761		135.52	si	
13	-2578.	40.6	20	3.14		.67761		135.52	si	
14	-2589.	40.6	20	3.14		.67761		135.52	si	
15	-2599.	40.6	20	3.14		.67761		135.52	si	
16	-2609.	40.6	20	3.14		.67761		135.52	si	
17	-2619.	40.6	20	3.14		.67761		135.52	si	
18	-2629.	40.6	20	3.14		.67761		135.52	si	
19	-2639.	40.6	20	3.14		.67761		135.52	si	
20	-2650.	40.6	20	3.14		.67761		135.52	si	
21	-2660.	40.6	20	3.14		.67761		135.52	si	
22	-2670.	40.6	20	3.14		.67761		135.52	si	
23	-2456.	67.6	20	3.14	1.37185		274.37	si		
24	-2466.	67.6	20	3.14	1.37185		274.37	si		
25	-2476.	67.6	20	3.14	1.37185		274.37	si		
26	-2487.	67.6	20	3.14	1.37185		274.37	si		
27	-2497.	67.6	20	3.14	1.37185		274.37	si		
28	-2507.	67.6	20	3.14	1.37185		274.37	si		
29	-2517.	67.6	20	3.14	1.37185		274.37	si		
30	-2527.	67.6	20	3.14	1.37185		274.37	si		
31	-2538.	67.6	20	3.14	1.37185		274.37	si		
32	-2548.	67.6	20	3.14	1.37185		274.37	si		
33	-2558.	67.6	20	3.14	1.37185		274.37	si		
34	-2568.	67.6	20	3.14	1.37185		274.37	si		
35	-2578.	67.6	20	3.14	1.37185		274.37	si		
36	-2589.	67.6	20	3.14	1.37185		274.37	si		
37	-2599.	67.6	20	3.14	1.37185		274.37	si		
38	-2609.	67.6	20	3.14	1.37185		274.37	si		
39	-2619.	67.6	20	3.14	1.37185		274.37	si		
40	-2629.	67.6	20	3.14	1.37185		274.37	si		
41	-2639.	67.6	20	3.14	1.37185		274.37	si		
42	-2650.	67.6	20	3.14	1.37185		274.37	si		
43	-2660.	67.6	20	3.14	1.37185		274.37	si		
44	-2670.	67.6	20	3.14	1.37185		274.37	si		
45	-2456.	-8.4	20	3.14	-58232		-116.46	si		
46	-2473.	-8.4	20	3.14	-58232		-116.46	si		
47	-2489.	-8.4	20	3.14	-58232		-116.46	si		
48	-2505.	-8.4	20	3.14	-58232		-116.46	si		
49	-2522.	-8.4	20	3.14	-58232		-116.46	si		
50	-2538.	-8.4	20	3.14	-58232		-116.46	si		
51	-2555.	-8.4	20	3.14	-58232		-116.46	si		
52	-2571.	-8.4	20	3.14	-58232		-116.46	si		
53	-2588.	-8.4	20	3.14	-58232		-116.46	si		
54	-2604.	-8.4	20	3.14	-58232		-116.46	si		
55	-2621.	-8.4	20	3.14	-58232		-116.46	si		
56	-2637.	-8.4	20	3.14	-58232		-116.46	si		
57	-2654.	-8.4	20	3.14	-58232		-116.46	si		
58	-2670.	-8.4	20	3.14	-58232		-116.46	si		

% ARMAT.: tesa = .77; comp. = .24; tot. = 1.01

Ripristino Ponte-Tubo

VERIFICA PULVINO YZ 4

DESCRIZIONI
 Tipo sezione : U Pul
 Tipo verifica: sFato limite ultimo

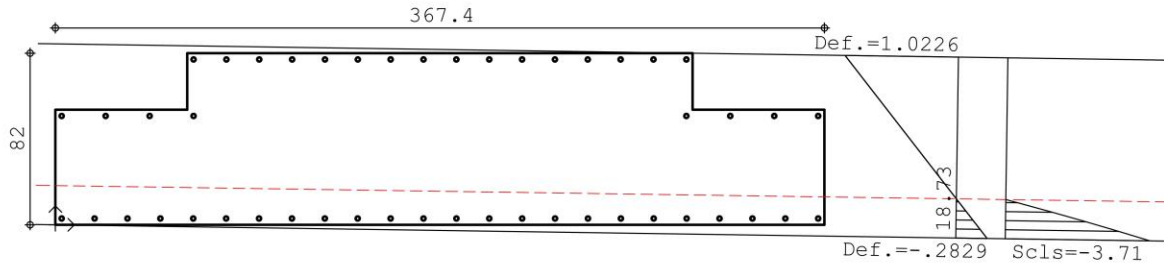
CARATTERISTICHE DEI MATERIALI
 Calcestruzzo: Rck= 30.
 fck= 24.9
 fcd= 14.11 (.35%)
 Acciaio lento: Tipo= B450C
 fyk= 450.
 ftk= 540.
 ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
 eps= muz * y +muy * z + lam
 muz= 1.50972336329232E-05
 muy= 2.21841144762878E-07
 lam=-2.82861155901715E-04

SOLLECITAZIONI AGENTI:
 Nd in z= 183.7; y= 37.5 (baricentro CLS)
 Nd = -42.38
 Mdz= -850.2439
 Mdy= -271.5108

UNITA' DI MISURA:
 kN; cm; kNm; N/mm2.
 Ø in mm; deformazioni*1000.

SIMBOLI:
 S=sigma (tensioni sui materiali);
 D=deformazioni (epsilon):



TENSIONI NEL CLS:			Dcls	Scls	Vel
ver	Z	Y			
1	0.	55.	.54749	0.	si
2	63.	55.	.56146	0.	si
3	63.	82.	.96909	0.	si
4	304.4	82.	1.02264	0.	si
5	304.4	55.	.61502	0.	si
6	367.4	55.	.62899	0.	si
7	367.4	0.	-.20136	-2.7	si
8	0.	0.	-.28286	-3.71	si

TENSIONI NEI FERRI:									
Fer	Z	Y	Ø (mm)	Af (cm2)	D	ferri	S	ferri	Vel
1	301.4	79.	20	3.14	.97668	195.34	si		
2	285.7	79.	20	3.14	.9732	194.64	si		
3	270.	79.	20	3.14	.96972	193.94	si		
4	254.3	79.	20	3.14	.96624	193.25	si		
5	238.6	79.	20	3.14	.96276	192.55	si		
6	222.9	79.	20	3.14	.95928	191.86	si		
7	207.2	79.	20	3.14	.95579	191.16	si		
8	191.5	79.	20	3.14	.95231	190.46	si		
9	175.9	79.	20	3.14	.94883	189.77	si		
10	160.2	79.	20	3.14	.94535	189.07	si		
11	144.5	79.	20	3.14	.94187	188.37	si		
12	128.8	79.	20	3.14	.93839	187.68	si		
13	113.1	79.	20	3.14	.93491	186.98	si		
14	97.4	79.	20	3.14	.93142	186.28	si		
15	81.7	79.	20	3.14	.92794	185.59	si		
16	66.	79.	20	3.14	.92446	184.89	si		
17	66.	52.	20	3.14	.51684	103.37	si		
18	45.	52.	20	3.14	.51218	102.44	si		
19	24.	52.	20	3.14	.50752	101.5	si		
20	3.	52.	20	3.14	.50286	100.57	si		
21	364.4	52.	20	3.14	.58303	116.61	si		
22	343.4	52.	20	3.14	.57838	115.68	si		
23	322.4	52.	20	3.14	.57372	114.74	si		
24	301.4	52.	20	3.14	.56906	113.81	si		
25	364.4	3.	20	3.14	-.15673	-31.35	si		
26	348.7	3.	20	3.14	-.16022	-32.04	si		
27	333.	3.	20	3.14	-.1637	-32.74	si		
28	317.3	3.	20	3.14	-.16719	-33.44	si		
29	301.5	3.	20	3.14	-.17067	-34.13	si		
30	285.8	3.	20	3.14	-.17416	-34.83	si		
31	270.1	3.	20	3.14	-.17765	-35.53	si		
32	254.4	3.	20	3.14	-.18113	-36.23	si		
33	238.7	3.	20	3.14	-.18462	-36.92	si		
34	223.	3.	20	3.14	-.1881	-37.62	si		
35	207.3	3.	20	3.14	-.19159	-38.32	si		
36	191.6	3.	20	3.14	-.19507	-39.01	si		
37	175.8	3.	20	3.14	-.19856	-39.71	si		
38	160.1	3.	20	3.14	-.20205	-40.41	si		
39	144.4	3.	20	3.14	-.20553	-41.11	si		
40	128.7	3.	20	3.14	-.20902	-41.8	si		
41	113.	3.	20	3.14	-.2125	-42.5	si		
42	97.3	3.	20	3.14	-.21599	-43.2	si		
43	81.6	3.	20	3.14	-.21947	-43.89	si		
44	65.9	3.	20	3.14	-.22296	-44.59	si		
45	50.1	3.	20	3.14	-.22645	-45.29	si		
46	34.4	3.	20	3.14	-.22993	-45.99	si		
47	18.7	3.	20	3.14	-.23342	-46.68	si		
48	3.	3.	20	3.14	-.2369	-47.38	si		

% ARMAT.: tesa= .28; comp.= .28; tot.= .56

Ripristino Ponte-Tubo

VERIFICA PULVINO XZ 5

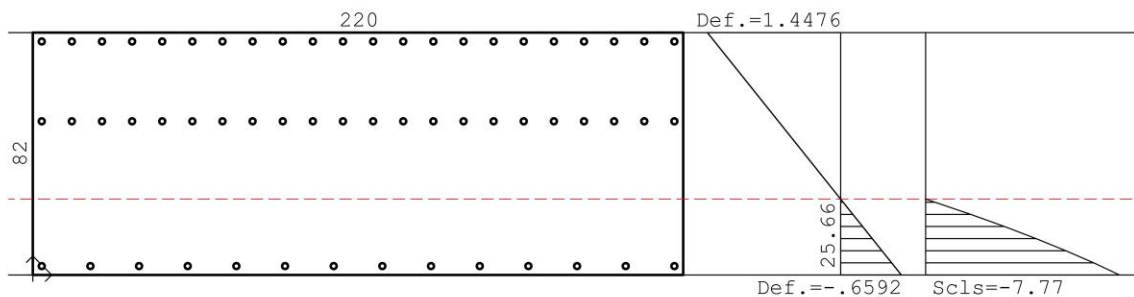
DESCRIZIONI
 Tipo sezione : RETTANGOLARE
 Tipo verifica: stato limite ultimo

CARATTERISTICHE DEI MATERIALI
 Calcestruzzo: Rck= 30.
 fck= 24.9
 fcd= 14.11 (.35%)
 Acciaio lento: Tipo= B450C
 fyk= 450.
 ftk= 540.
 ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
 eps= muz * y +muy * z + lam
 muz= 2.56922299508842E-05
 muy= 0
 lam=-3.64981578231377E-04

SOLLECITAZIONI AGENTI:
 Nd in y= 29.6 (baricentro CLS)
 Nd = -18.39
 Mdz=-1769.3525
 verifica in pressoflessione retta

UNITA' DI MISURA:
 kN; cm; kNm; N/mm2.
 Ø in mm; deformazioni*1000.
 SIMBOLI:
 S=sigma (tensioni sui materiali);
 D=deformazioni (epsilon):



TENSIONI NEL CLS:					
ver	Z	Y	Dcls	Scls	Vel
1	-2673.	70.6	1.44761	0.	si
2	-2453.	70.6	1.44761	0.	si
3	-2453.	-11.4	-.65916	-7.77	si
4	-2673.	-11.4	-.65916	-7.77	si

TENSIONI NEI FERRI:										
Fer	Z	Y	Ø (mm)	Af (cm2)	D	ferri	S	ferri	Vel	
1	-2456.	40.6	20	3.14		.67684	135.37	si		
2	-2456.	40.6	20	3.14		.67684	135.37	si		
3	-2476.	40.6	20	3.14		.67684	135.37	si		
4	-2487.	40.6	20	3.14		.67684	135.37	si		
5	-2497.	40.6	20	3.14		.67684	135.37	si		
6	-2507.	40.6	20	3.14		.67684	135.37	si		
7	-2517.	40.6	20	3.14		.67684	135.37	si		
8	-2527.	40.6	20	3.14		.67684	135.37	si		
9	-2538.	40.6	20	3.14		.67684	135.37	si		
10	-2548.	40.6	20	3.14		.67684	135.37	si		
11	-2558.	40.6	20	3.14		.67684	135.37	si		
12	-2568.	40.6	20	3.14		.67684	135.37	si		
13	-2578.	40.6	20	3.14		.67684	135.37	si		
14	-2589.	40.6	20	3.14		.67684	135.37	si		
15	-2599.	40.6	20	3.14		.67684	135.37	si		
16	-2609.	40.6	20	3.14		.67684	135.37	si		
17	-2619.	40.6	20	3.14		.67684	135.37	si		
18	-2629.	40.6	20	3.14		.67684	135.37	si		
19	-2639.	40.6	20	3.14		.67684	135.37	si		
20	-2650.	40.6	20	3.14		.67684	135.37	si		
21	-2660.	40.6	20	3.14		.67684	135.37	si		
22	-2670.	40.6	20	3.14		.67684	135.37	si		
23	-2456.	67.6	20	3.14	1.37053	274.11	si			
24	-2466.	67.6	20	3.14	1.37053	274.11	si			
25	-2476.	67.6	20	3.14	1.37053	274.11	si			
26	-2487.	67.6	20	3.14	1.37053	274.11	si			
27	-2497.	67.6	20	3.14	1.37053	274.11	si			
28	-2507.	67.6	20	3.14	1.37053	274.11	si			
29	-2517.	67.6	20	3.14	1.37053	274.11	si			
30	-2527.	67.6	20	3.14	1.37053	274.11	si			
31	-2538.	67.6	20	3.14	1.37053	274.11	si			
32	-2548.	67.6	20	3.14	1.37053	274.11	si			
33	-2558.	67.6	20	3.14	1.37053	274.11	si			
34	-2568.	67.6	20	3.14	1.37053	274.11	si			
35	-2578.	67.6	20	3.14	1.37053	274.11	si			
36	-2589.	67.6	20	3.14	1.37053	274.11	si			
37	-2599.	67.6	20	3.14	1.37053	274.11	si			
38	-2609.	67.6	20	3.14	1.37053	274.11	si			
39	-2619.	67.6	20	3.14	1.37053	274.11	si			
40	-2629.	67.6	20	3.14	1.37053	274.11	si			
41	-2639.	67.6	20	3.14	1.37053	274.11	si			
42	-2650.	67.6	20	3.14	1.37053	274.11	si			
43	-2660.	67.6	20	3.14	1.37053	274.11	si			
44	-2670.	67.6	20	3.14	1.37053	274.11	si			
45	-2456.	-8.4	20	3.14	-.58208	-116.42	si			
46	-2473.	-8.4	20	3.14	-.58208	-116.42	si			
47	-2489.	-8.4	20	3.14	-.58208	-116.42	si			
48	-2505.	-8.4	20	3.14	-.58208	-116.42	si			
49	-2522.	-8.4	20	3.14	-.58208	-116.42	si			
50	-2538.	-8.4	20	3.14	-.58208	-116.42	si			
51	-2555.	-8.4	20	3.14	-.58208	-116.42	si			
52	-2571.	-8.4	20	3.14	-.58208	-116.42	si			
53	-2588.	-8.4	20	3.14	-.58208	-116.42	si			
54	-2604.	-8.4	20	3.14	-.58208	-116.42	si			
55	-2621.	-8.4	20	3.14	-.58208	-116.42	si			
56	-2637.	-8.4	20	3.14	-.58208	-116.42	si			
57	-2654.	-8.4	20	3.14	-.58208	-116.42	si			
58	-2670.	-8.4	20	3.14	-.58208	-116.42	si			

% ARMAT.: tesa = .77; comp. = .24; tot. = 1.01

Ripristino Ponte-Tubo
VERIFICA PULVINO YZ 5

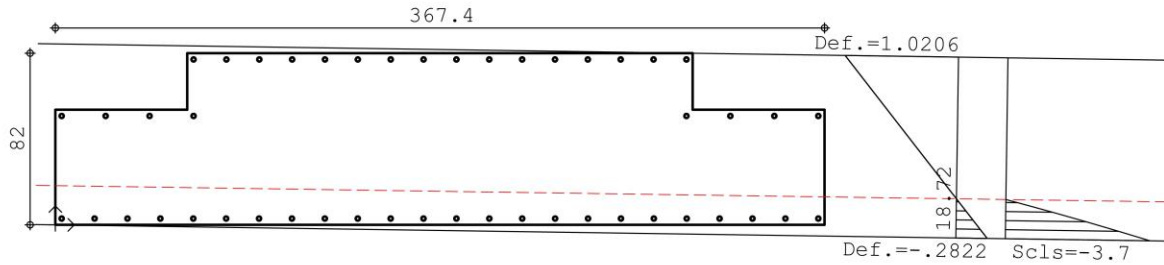
DESCRIZIONI
Tipo sezione : U Pul
Tipo verifica: sFato limite ultimo

CARATTERISTICHE DEI MATERIALI
Calcestruzzo: Rck= 30.
fck= 24.9
fcd= 14.11 (.35%)
Acciaio lento: Tipo= B450C
fyk= 450.
ftk= 540.
ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
eps= muz * y +muy * z + lam
muz= 1.50715591725263E-05
muy= 2.19774326160023E-07
lam=-2.82171188442576E-04

SOLLECITAZIONI AGENTI:
Nd in z= 183.7; y= 37.5 (baricentro CLS)
Nd = -43.35
Mdz= -849.0304
Mdy= -269.0794

UNITA' DI MISURA:
kN; cm; kNm; N/mm2.
Ø in mm; deformazioni*1000.
SIMBOLI:
S=sigma (tensioni sui materiali);
D=deformazioni (epsilon):



TENSIONI NEL CLS:			Dcls	Scfs	Vel
ver	Z	Y			
1	0.	55.	.54676	0.	si
2	63.	55.	.56061	0.	si
3	63.	82.	.96754	0.	si
4	304.4	82.	1.0206	0.	si
5	304.4	55.	.61366	0.	si
6	367.4	55.	.62751	0.	si
7	367.4	0.	-.20143	-2.7	si
8	0.	0.	-.28217	-3.7	si

TENSIONI NEI FERRI:									
Fer	Z	Y	Ø (mm)	Af (cm2)	D	ferri	S	ferri	Vel
1	301.4	79.	20	3.14	3.14	.97472		194.94	si
2	285.7	79.	20	3.14	3.14	.97127		194.25	si
3	270.	79.	20	3.14	3.14	.96782		193.56	si
4	254.3	79.	20	3.14	3.14	.96437		192.87	si
5	238.6	79.	20	3.14	3.14	.96093		192.19	si
6	222.9	79.	20	3.14	3.14	.95748		191.5	si
7	207.2	79.	20	3.14	3.14	.95403		190.81	si
8	191.5	79.	20	3.14	3.14	.95058		190.12	si
9	175.9	79.	20	3.14	3.14	.94713		189.43	si
10	160.2	79.	20	3.14	3.14	.94368		188.74	si
11	144.5	79.	20	3.14	3.14	.94023		188.05	si
12	128.8	79.	20	3.14	3.14	.93678		187.36	si
13	113.1	79.	20	3.14	3.14	.93333		186.67	si
14	97.4	79.	20	3.14	3.14	.92989		185.98	si
15	81.7	79.	20	3.14	3.14	.92644		185.29	si
16	66.	79.	20	3.14	3.14	.92299		184.6	si
17	66.	52.	20	3.14	3.14	.51605		103.21	si
18	45.	52.	20	3.14	3.14	.51144		102.29	si
19	24.	52.	20	3.14	3.14	.50682		101.36	si
20	3.	52.	20	3.14	3.14	.50221		100.44	si
21	364.4	52.	20	3.14	3.14	.58164		116.33	si
22	343.4	52.	20	3.14	3.14	.57702		115.4	si
23	322.4	52.	20	3.14	3.14	.57241		114.48	si
24	301.4	52.	20	3.14	3.14	.56779		113.56	si
25	364.4	3.	20	3.14	3.14	-.15687		-31.37	si
26	348.7	3.	20	3.14	3.14	-.16032		-32.06	si
27	333.	3.	20	3.14	3.14	-.16378		-32.76	si
28	317.3	3.	20	3.14	3.14	-.16723		-33.45	si
29	301.5	3.	20	3.14	3.14	-.17068		-34.14	si
30	285.8	3.	20	3.14	3.14	-.17414		-34.83	si
31	270.1	3.	20	3.14	3.14	-.17759		-35.52	si
32	254.4	3.	20	3.14	3.14	-.18104		-36.21	si
33	238.7	3.	20	3.14	3.14	-.1845		-36.9	si
34	223.	3.	20	3.14	3.14	-.18795		-37.59	si
35	207.3	3.	20	3.14	3.14	-.1914		-38.28	si
36	191.6	3.	20	3.14	3.14	-.19486		-38.97	si
37	175.8	3.	20	3.14	3.14	-.19831		-39.66	si
38	160.1	3.	20	3.14	3.14	-.20176		-40.35	si
39	144.4	3.	20	3.14	3.14	-.20522		-41.04	si
40	128.7	3.	20	3.14	3.14	-.20867		-41.73	si
41	113.	3.	20	3.14	3.14	-.21212		-42.42	si
42	97.3	3.	20	3.14	3.14	-.21558		-43.12	si
43	81.6	3.	20	3.14	3.14	-.21903		-43.81	si
44	65.9	3.	20	3.14	3.14	-.22248		-44.5	si
45	50.1	3.	20	3.14	3.14	-.22594		-45.19	si
46	34.4	3.	20	3.14	3.14	-.22939		-45.88	si
47	18.7	3.	20	3.14	3.14	-.23284		-46.57	si
48	3.	3.	20	3.14	3.14	-.2363		-47.26	si

% ARMAT.: tesa= .28; comp.= .28; tot.= .56

Ripristino Ponte-Tubo
VERIFICA PULVINO XZ 6

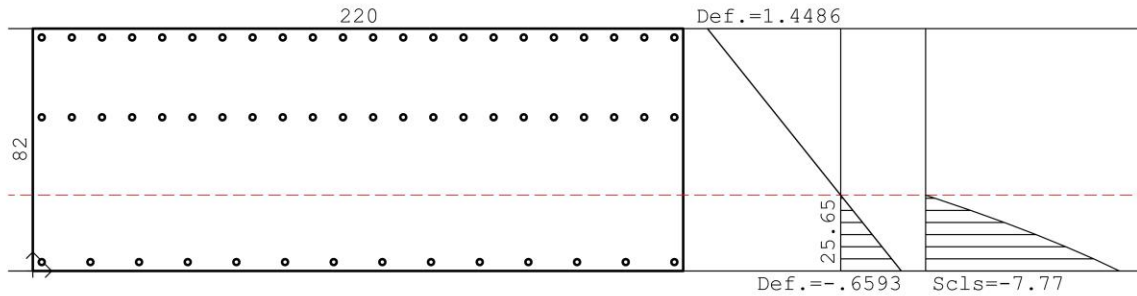
DESCRIZIONI
Tipo sezione : RETTANGOLARE
Tipo verifica: stato limite ultimo

CARATTERISTICHE DEI MATERIALI
Calcestruzzo: Rck= 30.
fck= 24.9
fcd= 14.11 (.35%)
Acciaio lento: Tipo= B450C
fyk= 450.
ftk= 540.
ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
eps= muz * y +muy * z + lam
muz= 2.57064866826944E-05
muy= 0
lam=-3.64972331791936E-04

SOLLECITAZIONI AGENTI:
Nd in y= 29.6 (baricentro CLS)
Nd = -16.06
Mdz=-1769.9667
verifica in pressoflessione retta

UNITA' DI MISURA:
kN; cm; kNm; N/mm2.
Ø in mm; deformazioni*1000.
SIMBOLI:
S=sigma (tensioni sui materiali);
D=deformazioni (epsilon):



TENSIONI NEL CLS:					
ver	Z	Y	Dcls	Scls	Vel
1	-2673.	70.6	1.44862	0.	si
2	-2453.	70.6	1.44862	0.	si
3	-2453.	-11.4	-.65931	-7.77	si
4	-2673.	-11.4	-.65931	-7.77	si

TENSIONI NEI FERRI:										
Fer	Z	Y	Ø (mm)	Af (cm2)	D	ferri	S	ferri	Vel	
1	-2456.	40.6	20	3.14		.67743		135.49	si	
3	-2466.	40.6	20	3.14		.67743		135.49	si	
3	-2476.	40.6	20	3.14		.67743		135.49	si	
4	-2487.	40.6	20	3.14		.67743		135.49	si	
5	-2497.	40.6	20	3.14		.67743		135.49	si	
6	-2507.	40.6	20	3.14		.67743		135.49	si	
7	-2517.	40.6	20	3.14		.67743		135.49	si	
8	-2527.	40.6	20	3.14		.67743		135.49	si	
9	-2538.	40.6	20	3.14		.67743		135.49	si	
10	-2548.	40.6	20	3.14		.67743		135.49	si	
11	-2558.	40.6	20	3.14		.67743		135.49	si	
12	-2568.	40.6	20	3.14		.67743		135.49	si	
13	-2578.	40.6	20	3.14		.67743		135.49	si	
14	-2589.	40.6	20	3.14		.67743		135.49	si	
15	-2599.	40.6	20	3.14		.67743		135.49	si	
16	-2609.	40.6	20	3.14		.67743		135.49	si	
17	-2619.	40.6	20	3.14		.67743		135.49	si	
18	-2629.	40.6	20	3.14		.67743		135.49	si	
19	-2639.	40.6	20	3.14		.67743		135.49	si	
20	-2650.	40.6	20	3.14		.67743		135.49	si	
21	-2660.	40.6	20	3.14		.67743		135.49	si	
22	-2670.	40.6	20	3.14		.67743		135.49	si	
23	-2456.	67.6	20	3.14	1.3715		274.3	si		
24	-2466.	67.6	20	3.14	1.3715		274.3	si		
25	-2476.	67.6	20	3.14	1.3715		274.3	si		
26	-2487.	67.6	20	3.14	1.3715		274.3	si		
27	-2497.	67.6	20	3.14	1.3715		274.3	si		
28	-2507.	67.6	20	3.14	1.3715		274.3	si		
29	-2517.	67.6	20	3.14	1.3715		274.3	si		
30	-2527.	67.6	20	3.14	1.3715		274.3	si		
31	-2538.	67.6	20	3.14	1.3715		274.3	si		
32	-2548.	67.6	20	3.14	1.3715		274.3	si		
33	-2558.	67.6	20	3.14	1.3715		274.3	si		
34	-2568.	67.6	20	3.14	1.3715		274.3	si		
35	-2578.	67.6	20	3.14	1.3715		274.3	si		
36	-2589.	67.6	20	3.14	1.3715		274.3	si		
37	-2599.	67.6	20	3.14	1.3715		274.3	si		
38	-2609.	67.6	20	3.14	1.3715		274.3	si		
39	-2619.	67.6	20	3.14	1.3715		274.3	si		
40	-2629.	67.6	20	3.14	1.3715		274.3	si		
41	-2639.	67.6	20	3.14	1.3715		274.3	si		
42	-2650.	67.6	20	3.14	1.3715		274.3	si		
43	-2660.	67.6	20	3.14	1.3715		274.3	si		
44	-2670.	67.6	20	3.14	1.3715		274.3	si		
45	-2456.	-8.4	20	3.14		-.58219		-116.44	si	
46	-2473.	-8.4	20	3.14		-.58219		-116.44	si	
47	-2489.	-8.4	20	3.14		-.58219		-116.44	si	
48	-2505.	-8.4	20	3.14		-.58219		-116.44	si	
49	-2522.	-8.4	20	3.14		-.58219		-116.44	si	
50	-2538.	-8.4	20	3.14		-.58219		-116.44	si	
51	-2555.	-8.4	20	3.14		-.58219		-116.44	si	
52	-2571.	-8.4	20	3.14		-.58219		-116.44	si	
53	-2588.	-8.4	20	3.14		-.58219		-116.44	si	
54	-2604.	-8.4	20	3.14		-.58219		-116.44	si	
55	-2621.	-8.4	20	3.14		-.58219		-116.44	si	
56	-2637.	-8.4	20	3.14		-.58219		-116.44	si	
57	-2654.	-8.4	20	3.14		-.58219		-116.44	si	
58	-2670.	-8.4	20	3.14		-.58219		-116.44	si	

% ARMAT.: tesa = .77; comp. = .24; tot. = 1.01

Ripristino Ponte-Tubo

VERIFICA PULVINO YZ 6

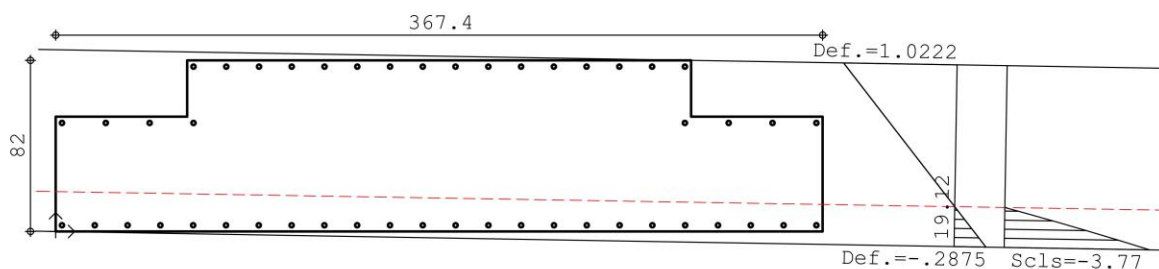
DESCRIZIONI
 Tipo sezione : U Pul
 Tipo verifica: sFato limite ultimo

CARATTERISTICHE DEI MATERIALI
 Calcestruzzo: Rck= 30.
 fck= 24.9
 fcd= 14.11 (.35%)
 Acciaio lento: Tipo= B450C
 fyk= 450.
 ftk= 540.
 ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
 eps= muz * y +muy * z + lam
 muz= 1.50369149148332E-05
 muy= 2.52028211707263E-07
 lam=-2.87535019021515E-04

SOLLECITAZIONI AGENTI:
 Nd in z= 183.7; y= 37.5
 Nd = -45.92
 Mdz= -847.6341
 Mdy= -308.5721

UNITA' DI MISURA:
 kN; cm; kNm; N/mm2.
 Ø in mm; deformazioni*1000.
 SIMBOLI:
 S=sigma (tensioni sui materiali);
 D=deformazioni (epsilon):



TENSIONI NEL CLS:			Dcls	Scls	Ve
ver	Z	Y			
1	0.	55.	.5395	0.	si
2	63.	55.	.55537	0.	si
3	63.	82.	.96137	0.	si
4	304.4	82.	1.02221	0.	si
5	304.4	55.	.61621	0.	si
6	367.4	55.	.63209	0.	si
7	367.4	0.	-.19494	-2.62	si
8	0.	0.	-.28754	-3.77	si

TENSIONI NEI FERRI:									
Fer	Z	Y	Ø (mm)	Af (cm2)	D	ferri	S	ferri	Ve
1	301.4	79.	20	3.14	3.14	.97634		195.27	si
2	285.7	79.	20	3.14	3.14	.97239		194.48	si
3	270.	79.	20	3.14	3.14	.96843		193.69	si
4	254.3	79.	20	3.14	3.14	.96448		192.9	si
5	238.6	79.	20	3.14	3.14	.96052		192.1	si
6	222.9	79.	20	3.14	3.14	.95657		191.31	si
7	207.2	79.	20	3.14	3.14	.95261		190.52	si
8	191.5	79.	20	3.14	3.14	.94866		189.73	si
9	175.9	79.	20	3.14	3.14	.9447		188.94	si
10	160.2	79.	20	3.14	3.14	.94075		188.15	si
11	144.5	79.	20	3.14	3.14	.93679		187.36	si
12	128.8	79.	20	3.14	3.14	.93284		186.57	si
13	113.1	79.	20	3.14	3.14	.92888		185.78	si
14	97.4	79.	20	3.14	3.14	.92493		184.99	si
15	81.7	79.	20	3.14	3.14	.92097		184.19	si
16	66.	79.	20	3.14	3.14	.91702		183.4	si
17	66.	52.	20	3.14	3.14	.51102		102.2	si
18	45.	52.	20	3.14	3.14	.50573		101.15	si
19	24.	52.	20	3.14	3.14	.50043		100.09	si
20	3.	52.	20	3.14	3.14	.49514		99.03	si
21	364.4	52.	20	3.14	3.14	.58622		117.24	si
22	343.4	52.	20	3.14	3.14	.58093		116.19	si
23	322.4	52.	20	3.14	3.14	.57564		115.13	si
24	301.4	52.	20	3.14	3.14	.57035		114.07	si
25	364.4	3.	20	3.14	3.14	-.15059		-30.12	si
26	348.7	3.	20	3.14	3.14	-.15455		-30.91	si
27	333.	3.	20	3.14	3.14	-.15851		-31.7	si
28	317.3	3.	20	3.14	3.14	-.16247		-32.49	si
29	301.5	3.	20	3.14	3.14	-.16643		-33.29	si
30	285.8	3.	20	3.14	3.14	-.17039		-34.08	si
31	270.1	3.	20	3.14	3.14	-.17435		-34.87	si
32	254.4	3.	20	3.14	3.14	-.17831		-35.66	si
33	238.7	3.	20	3.14	3.14	-.18227		-36.45	si
34	223.	3.	20	3.14	3.14	-.18623		-37.25	si
35	207.3	3.	20	3.14	3.14	-.19019		-38.04	si
36	191.6	3.	20	3.14	3.14	-.19415		-38.83	si
37	175.8	3.	20	3.14	3.14	-.19811		-39.62	si
38	160.1	3.	20	3.14	3.14	-.20207		-40.41	si
39	144.4	3.	20	3.14	3.14	-.20603		-41.21	si
40	128.7	3.	20	3.14	3.14	-.20999		-42.	si
41	113.	3.	20	3.14	3.14	-.21395		-42.79	si
42	97.3	3.	20	3.14	3.14	-.21791		-43.58	si
43	81.6	3.	20	3.14	3.14	-.22187		-44.37	si
44	65.9	3.	20	3.14	3.14	-.22583		-45.17	si
45	50.1	3.	20	3.14	3.14	-.22979		-45.96	si
46	34.4	3.	20	3.14	3.14	-.23375		-46.75	si
47	18.7	3.	20	3.14	3.14	-.23771		-47.54	si
48	3.	3.	20	3.14	3.14	-.24167		-48.33	si

% ARMAT.: tesa= .28; comp.= .28; tot.= .56

Ripristino Ponte-Tubo

VERIFICA PULVINO XZ 7

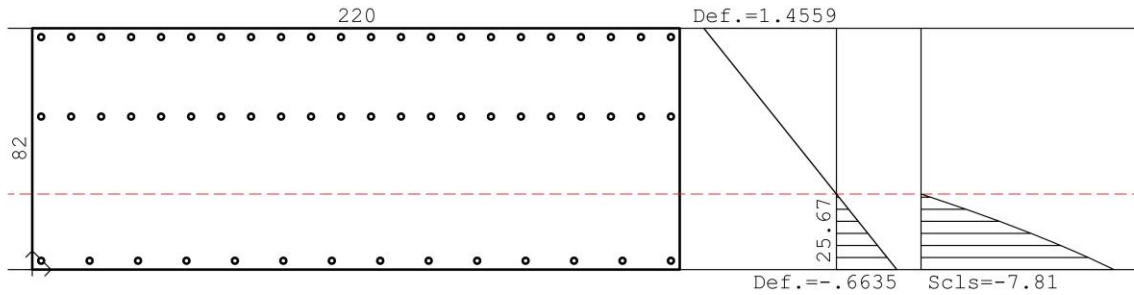
DESCRIZIONI
 Tipo sezione : RETTANGOLARE
 Tipo verifica: stato limite ultimo

CARATTERISTICHE DEI MATERIALI
 Calcestruzzo: Rck= 30.
 fck= 24.9
 fcd= 14.11 (.35%)
 Acciaio lento: Tipo= B450C
 fyk= 450.
 ftk= 540.
 ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
 eps= muz * y + muy * z + lam
 muz= 2.5846098503605E-05
 muy= 0
 lam=-3.67562688065386E-04

SOLLECITAZIONI AGENTI:
 Nd in y= 29.6 (baricentro CLS)
 Nd = -20.83
 Mdz=-1779.9301
 verifica in pressoflessione retta

UNITA' DI MISURA:
 kN; cm; kNm; N/mm2.
 Ø in mm; deformazioni*1000.
 SIMBOLI:
 S=sigma (tensioni sui materiali);
 D=deformazioni (epsilon):



ver	Z	Y	Dcls	Scls	Vel
1	-2673.	70.6	1.45588	0.	si
2	-2453.	70.6	1.45588	0.	si
3	-2453.	-11.4	-.6635	-7.81	si
4	-2673.	-11.4	-.6635	-7.81	si

Fer	Z	Y	Ø (mm)	Af (cm2)	D ferri	S ferri	Vel
1	-2456.	40.6	20	3.14	.6805	136.1	si
2	-2466.	40.6	20	3.14	.6805	136.1	si
3	-2476.	40.6	20	3.14	.6805	136.1	si
4	-2487.	40.6	20	3.14	.6805	136.1	si
5	-2497.	40.6	20	3.14	.6805	136.1	si
6	-2507.	40.6	20	3.14	.6805	136.1	si
7	-2517.	40.6	20	3.14	.6805	136.1	si
8	-2527.	40.6	20	3.14	.6805	136.1	si
9	-2538.	40.6	20	3.14	.6805	136.1	si
10	-2548.	40.6	20	3.14	.6805	136.1	si
11	-2558.	40.6	20	3.14	.6805	136.1	si
12	-2568.	40.6	20	3.14	.6805	136.1	si
13	-2578.	40.6	20	3.14	.6805	136.1	si
14	-2589.	40.6	20	3.14	.6805	136.1	si
15	-2599.	40.6	20	3.14	.6805	136.1	si
16	-2609.	40.6	20	3.14	.6805	136.1	si
17	-2619.	40.6	20	3.14	.6805	136.1	si
18	-2629.	40.6	20	3.14	.6805	136.1	si
19	-2639.	40.6	20	3.14	.6805	136.1	si
20	-2650.	40.6	20	3.14	.6805	136.1	si
21	-2660.	40.6	20	3.14	.6805	136.1	si
22	-2670.	40.6	20	3.14	.6805	136.1	si
23	-2456.	67.6	20	3.14	1.37834	275.67	si
24	-2466.	67.6	20	3.14	1.37834	275.67	si
25	-2476.	67.6	20	3.14	1.37834	275.67	si
26	-2487.	67.6	20	3.14	1.37834	275.67	si
27	-2497.	67.6	20	3.14	1.37834	275.67	si
28	-2507.	67.6	20	3.14	1.37834	275.67	si
29	-2517.	67.6	20	3.14	1.37834	275.67	si
30	-2527.	67.6	20	3.14	1.37834	275.67	si
31	-2538.	67.6	20	3.14	1.37834	275.67	si
32	-2548.	67.6	20	3.14	1.37834	275.67	si
33	-2558.	67.6	20	3.14	1.37834	275.67	si
34	-2568.	67.6	20	3.14	1.37834	275.67	si
35	-2578.	67.6	20	3.14	1.37834	275.67	si
36	-2589.	67.6	20	3.14	1.37834	275.67	si
37	-2599.	67.6	20	3.14	1.37834	275.67	si
38	-2609.	67.6	20	3.14	1.37834	275.67	si
39	-2619.	67.6	20	3.14	1.37834	275.67	si
40	-2629.	67.6	20	3.14	1.37834	275.67	si
41	-2639.	67.6	20	3.14	1.37834	275.67	si
42	-2650.	67.6	20	3.14	1.37834	275.67	si
43	-2660.	67.6	20	3.14	1.37834	275.67	si
44	-2670.	67.6	20	3.14	1.37834	275.67	si
45	-2456.	-8.4	20	3.14	-.58596	-117.19	si
46	-2473.	-8.4	20	3.14	-.58596	-117.19	si
47	-2489.	-8.4	20	3.14	-.58596	-117.19	si
48	-2505.	-8.4	20	3.14	-.58596	-117.19	si
49	-2522.	-8.4	20	3.14	-.58596	-117.19	si
50	-2538.	-8.4	20	3.14	-.58596	-117.19	si
51	-2555.	-8.4	20	3.14	-.58596	-117.19	si
52	-2571.	-8.4	20	3.14	-.58596	-117.19	si
53	-2588.	-8.4	20	3.14	-.58596	-117.19	si
54	-2604.	-8.4	20	3.14	-.58596	-117.19	si
55	-2621.	-8.4	20	3.14	-.58596	-117.19	si
56	-2637.	-8.4	20	3.14	-.58596	-117.19	si
57	-2654.	-8.4	20	3.14	-.58596	-117.19	si
58	-2670.	-8.4	20	3.14	-.58596	-117.19	si

% ARMAT.: tesa = .77; comp. = .24; tot. = 1.01

Ripristino Ponte-Tubo

VERIFICA PULVINO YZ 7

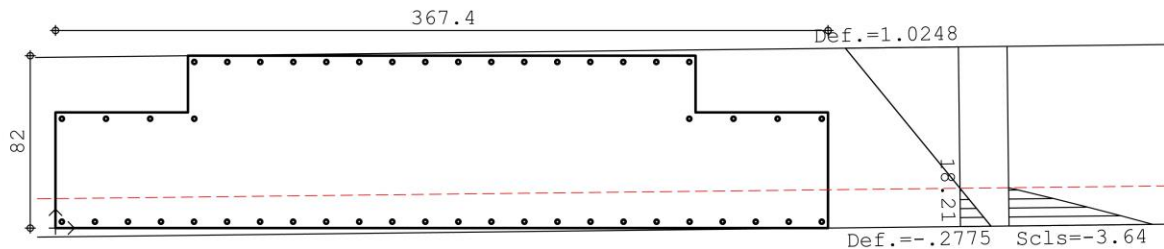
DESCRIZIONI
 Tipo sezione : U Pul
 Tipo verifica: sTato limite ultimo

CARATTERISTICHE DEI MATERIALI
 Calcestruzzo: Rck= 30.
 fck= 24.9
 fcd= 14.11 (.35%)
 Acciaio lento: Tipo= B450C
 fyk= 450.
 ftk= 540.
 ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
 eps= muz * y + muy * z + lam
 muz= 1.52362531246454E-05
 muy= -1.73734573043911E-07
 lam= -2.13658640822338E-04

SOLLECITAZIONI AGENTI:
 Nd in z= 183.7; y= 37.5 (baricentro CLS)
 Nd = -52.42
 Mdz= -860.1243
 Mdy= 213.2854

UNITA' DI MISURA:
 kN; cm; kNm; N/mm2.
 Ø in mm; deformazioni*1000.
 SIMBOLI:
 S=sigma (tensioni sui materiali);
 D=deformazioni (epsilon):



TENSIONI NEL CLS:			Dcls	Scls	Vel
ver	Z	Y			
1	0.	55.	.62434	0.	si
2	63.	55.	.61339	0.	si
3	63.	82.	1.02477	0.	si
4	304.4	82.	.98283	0.	si
5	304.4	55.	.57145	0.	si
6	367.4	55.	.56051	0.	si
7	367.4	0.	-.27749	-3.64	si
8	0.	0.	-.21366	-2.85	si

TENSIONI NEI FERRI:									
Fer	Z	Y	Ø (mm)	Af (cm2)	D	ferri	S	ferri	Vel
1	301.4	79.	20	3.14	3.14	.93764		187.53	si
2	285.7	79.	20	3.14	3.14	.94037		188.07	si
3	270.	79.	20	3.14	3.14	.94309		188.62	si
4	254.3	79.	20	3.14	3.14	.94582		189.16	si
5	238.6	79.	20	3.14	3.14	.94855		189.71	si
6	222.9	79.	20	3.14	3.14	.95127		190.25	si
7	207.2	79.	20	3.14	3.14	.954		190.8	si
8	191.5	79.	20	3.14	3.14	.95673		191.35	si
9	175.9	79.	20	3.14	3.14	.95945		191.89	si
10	160.2	79.	20	3.14	3.14	.96218		192.44	si
11	144.5	79.	20	3.14	3.14	.96491		192.98	si
12	128.8	79.	20	3.14	3.14	.96763		193.53	si
13	113.1	79.	20	3.14	3.14	.97036		194.07	si
14	97.4	79.	20	3.14	3.14	.97309		194.62	si
15	81.7	79.	20	3.14	3.14	.97581		195.16	si
16	66.	79.	20	3.14	3.14	.97854		195.71	si
17	66.	52.	20	3.14	3.14	.56716		113.43	si
18	45.	52.	20	3.14	3.14	.57081		114.16	si
19	24.	52.	20	3.14	3.14	.57446		114.89	si
20	3.	52.	20	3.14	3.14	.57811		115.62	si
21	364.4	52.	20	3.14	3.14	.51532		103.06	si
22	343.4	52.	20	3.14	3.14	.51897		103.79	si
23	322.4	52.	20	3.14	3.14	.52261		104.52	si
24	301.4	52.	20	3.14	3.14	.52626		105.25	si
25	364.4	3.	20	3.14	3.14	-.23126		-46.25	si
26	348.7	3.	20	3.14	3.14	-.22853		-45.71	si
27	333.	3.	20	3.14	3.14	-.2258		-45.16	si
28	317.3	3.	20	3.14	3.14	-.22307		-44.61	si
29	301.5	3.	20	3.14	3.14	-.22034		-44.07	si
30	285.8	3.	20	3.14	3.14	-.21761		-43.52	si
31	270.1	3.	20	3.14	3.14	-.21488		-42.98	si
32	254.4	3.	20	3.14	3.14	-.21215		-42.43	si
33	238.7	3.	20	3.14	3.14	-.20942		-41.88	si
34	223.	3.	20	3.14	3.14	-.20669		-41.34	si
35	207.3	3.	20	3.14	3.14	-.20396		-40.79	si
36	191.6	3.	20	3.14	3.14	-.20123		-40.25	si
37	175.8	3.	20	3.14	3.14	-.1985		-39.7	si
38	160.1	3.	20	3.14	3.14	-.19577		-39.15	si
39	144.4	3.	20	3.14	3.14	-.19304		-38.61	si
40	128.7	3.	20	3.14	3.14	-.19031		-38.06	si
41	113.	3.	20	3.14	3.14	-.18758		-37.52	si
42	97.3	3.	20	3.14	3.14	-.18485		-36.97	si
43	81.6	3.	20	3.14	3.14	-.18212		-36.42	si
44	65.9	3.	20	3.14	3.14	-.17939		-35.88	si
45	50.1	3.	20	3.14	3.14	-.17666		-35.33	si
46	34.4	3.	20	3.14	3.14	-.17393		-34.79	si
47	18.7	3.	20	3.14	3.14	-.1712		-34.24	si
48	3.	3.	20	3.14	3.14	-.16847		-33.69	si

% ARMAT.: tesa= .28; comp.= .28; tot.= .56

Ripristino Ponte-Tubo
VERIFICA PULVINO XZ 8

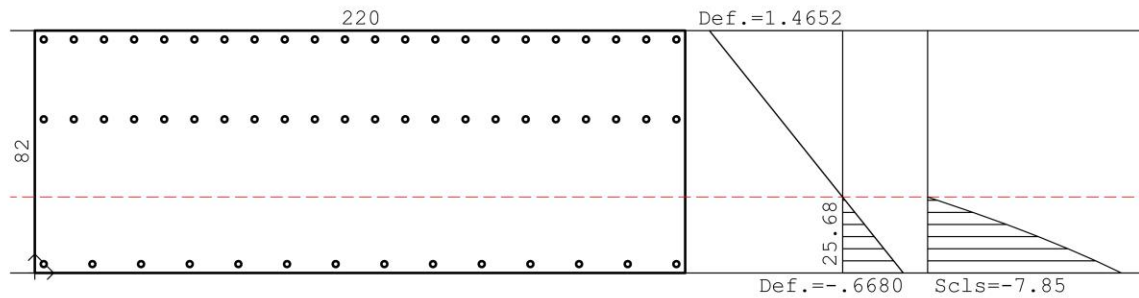
DESCRIZIONI
Tipo sezione : RETTANGOLARE
Tipo verifica: stato limite ultimo

CARATTERISTICHE DEI MATERIALI
Calcestruzzo: Rck= 30.
fck= 24.9
fcd= 14.11 (.35%)
Acciaio lento: Tipo= B450C
fyk= 450.
ftk= 540.
ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
eps= muz * y +muy * z + lam
muz= 2.60149923796162E-05
muy= 0
lam=-3.70153871160676E-04

SOLLECITAZIONI AGENTI:
Nd in y= 29.6 (baricentro CLS)
Nd = -20.99
Mdz=-1791.1745
verifica in pressoflessione retta

UNITA' DI MISURA:
kN; cm; kNm; N/mm2.
Ø in mm; deformazioni*1000.
SIMBOLI:
S=sigma (tensioni sui materiali);
D=deformazioni (epsilon):



TENSIONI NEL CLS:					
ver	Z	Y	Dcls	Scls	Vel
1	-2673.	70.6	1.4652	0.	si
2	-2453.	70.6	1.4652	0.	si
3	-2453.	-11.4	-6.6803	-7.85	si
4	-2673.	-11.4	-6.6803	-7.85	si

TENSIONI NEI FERRI:										
fer	Z	Y	Ø (mm)	Af (cm2)	D	ferri	S	ferri	Vel	
1	-2456.	40.6	20	3.14		.68475		136.95	si	
2	-2456.	40.6	20	3.14		.68475		136.95	si	
3	-2476.	40.6	20	3.14		.68475		136.95	si	
4	-2487.	40.6	20	3.14		.68475		136.95	si	
5	-2497.	40.6	20	3.14		.68475		136.95	si	
6	-2507.	40.6	20	3.14		.68475		136.95	si	
7	-2517.	40.6	20	3.14		.68475		136.95	si	
8	-2527.	40.6	20	3.14		.68475		136.95	si	
9	-2538.	40.6	20	3.14		.68475		136.95	si	
10	-2548.	40.6	20	3.14		.68475		136.95	si	
11	-2558.	40.6	20	3.14		.68475		136.95	si	
12	-2568.	40.6	20	3.14		.68475		136.95	si	
13	-2578.	40.6	20	3.14		.68475		136.95	si	
14	-2589.	40.6	20	3.14		.68475		136.95	si	
15	-2599.	40.6	20	3.14		.68475		136.95	si	
16	-2609.	40.6	20	3.14		.68475		136.95	si	
17	-2619.	40.6	20	3.14		.68475		136.95	si	
18	-2629.	40.6	20	3.14		.68475		136.95	si	
19	-2639.	40.6	20	3.14		.68475		136.95	si	
20	-2650.	40.6	20	3.14		.68475		136.95	si	
21	-2660.	40.6	20	3.14		.68475		136.95	si	
22	-2670.	40.6	20	3.14		.68475		136.95	si	
23	-2456.	67.6	20	3.14	1.38716			277.43	si	
24	-2466.	67.6	20	3.14	1.38716			277.43	si	
25	-2476.	67.6	20	3.14	1.38716			277.43	si	
26	-2487.	67.6	20	3.14	1.38716			277.43	si	
27	-2497.	67.6	20	3.14	1.38716			277.43	si	
28	-2507.	67.6	20	3.14	1.38716			277.43	si	
29	-2517.	67.6	20	3.14	1.38716			277.43	si	
30	-2527.	67.6	20	3.14	1.38716			277.43	si	
31	-2538.	67.6	20	3.14	1.38716			277.43	si	
32	-2548.	67.6	20	3.14	1.38716			277.43	si	
33	-2558.	67.6	20	3.14	1.38716			277.43	si	
34	-2568.	67.6	20	3.14	1.38716			277.43	si	
35	-2578.	67.6	20	3.14	1.38716			277.43	si	
36	-2589.	67.6	20	3.14	1.38716			277.43	si	
37	-2599.	67.6	20	3.14	1.38716			277.43	si	
38	-2609.	67.6	20	3.14	1.38716			277.43	si	
39	-2619.	67.6	20	3.14	1.38716			277.43	si	
40	-2629.	67.6	20	3.14	1.38716			277.43	si	
41	-2639.	67.6	20	3.14	1.38716			277.43	si	
42	-2650.	67.6	20	3.14	1.38716			277.43	si	
43	-2660.	67.6	20	3.14	1.38716			277.43	si	
44	-2670.	67.6	20	3.14	1.38716			277.43	si	
45	-2456.	-8.4	20	3.14		-.58998		-118.	si	
46	-2473.	-8.4	20	3.14		-.58998		-118.	si	
47	-2489.	-8.4	20	3.14		-.58998		-118.	si	
48	-2505.	-8.4	20	3.14		-.58998		-118.	si	
49	-2522.	-8.4	20	3.14		-.58998		-118.	si	
50	-2538.	-8.4	20	3.14		-.58998		-118.	si	
51	-2555.	-8.4	20	3.14		-.58998		-118.	si	
52	-2571.	-8.4	20	3.14		-.58998		-118.	si	
53	-2588.	-8.4	20	3.14		-.58998		-118.	si	
54	-2604.	-8.4	20	3.14		-.58998		-118.	si	
55	-2621.	-8.4	20	3.14		-.58998		-118.	si	
56	-2637.	-8.4	20	3.14		-.58998		-118.	si	
57	-2654.	-8.4	20	3.14		-.58998		-118.	si	
58	-2670.	-8.4	20	3.14		-.58998		-118.	si	

% ARMAT.: tesa = .77; comp. = .24; tot. = 1.01

Ripristino Ponte-Tubo

VERIFICA PULVINO YZ 8

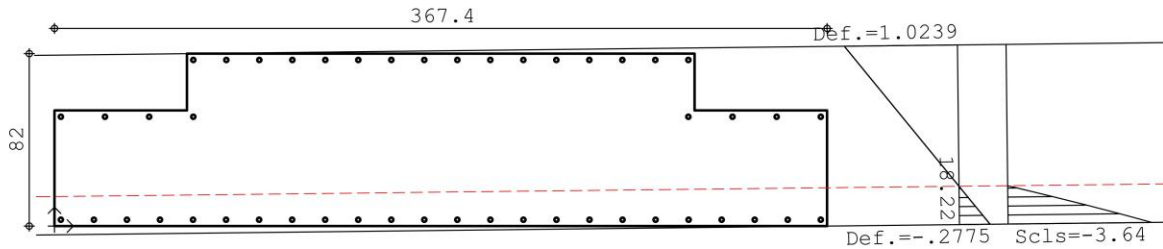
DESCRIZIONI
 Tipo sezione : U Pul
 Tipo verifica: sTato limite ultimo

CARATTERISTICHE DEI MATERIALI
 Calcestruzzo: Rck= 30.
 fck= 24.9
 fcd= 14.11 (.35%)
 Acciaio lento: Tipo= B450C
 fyk= 450.
 ftk= 540.
 ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
 eps= muz * y + muy * z + lam
 muz= 1.52290513204636E-05
 muy= -1.72813096668434E-07
 lam= -2.14022457526061E-04

SOLLECITAZIONI AGENTI:
 Nd in z= 183.7; y= 37.5 (baricentro CLS)
 Nd = -55.74
 Mdz= -860.4358
 Mdy= 212.3395

UNITA' DI MISURA:
 kN; cm; kNm; N/mm2.
 Ø in mm; deformazioni*1000.
 SIMBOLI:
 S=sigma (tensioni sui materiali);
 D=deformazioni (epsilon):



TENSIONI NEL CLS:			Dcls	Scls	Vel
ver	Z	Y			
1	0.	55.	.62358	0.	si
2	63.	55.	.61269	0.	si
3	63.	82.	1.02387	0.	si
4	304.4	82.	.98216	0.	si
5	304.4	55.	.57097	0.	si
6	367.4	55.	.56008	0.	si
7	367.4	0.	-.27751	-3.64	si
8	0.	0.	-.21402	-2.86	si

TENSIONI NEI FERRI:									
Fer	Z	Y	Ø (mm)	Af (cm2)	D	ferri	S	ferri	Vel
1	301.4	79.	20	3.14	3.14	.93699		187.4	si
2	285.7	79.	20	3.14	3.14	.9397		187.94	si
3	270.	79.	20	3.14	3.14	.94241		188.48	si
4	254.3	79.	20	3.14	3.14	.94512		189.02	si
5	238.6	79.	20	3.14	3.14	.94783		189.57	si
6	222.9	79.	20	3.14	3.14	.95055		190.11	si
7	207.2	79.	20	3.14	3.14	.95326		190.65	si
8	191.5	79.	20	3.14	3.14	.95597		191.19	si
9	175.9	79.	20	3.14	3.14	.95868		191.74	si
10	160.2	79.	20	3.14	3.14	.96139		192.28	si
11	144.5	79.	20	3.14	3.14	.96411		192.82	si
12	128.8	79.	20	3.14	3.14	.96682		193.36	si
13	113.1	79.	20	3.14	3.14	.96953		193.91	si
14	97.4	79.	20	3.14	3.14	.97224		194.45	si
15	81.7	79.	20	3.14	3.14	.97495		194.99	si
16	66.	79.	20	3.14	3.14	.97767		195.53	si
17	66.	52.	20	3.14	3.14	.56648		113.3	si
18	45.	52.	20	3.14	3.14	.57011		114.02	si
19	24.	52.	20	3.14	3.14	.57374		114.75	si
20	3.	52.	20	3.14	3.14	.57737		115.47	si
21	364.4	52.	20	3.14	3.14	.51492		102.98	si
22	343.4	52.	20	3.14	3.14	.51854		103.71	si
23	322.4	52.	20	3.14	3.14	.52217		104.43	si
24	301.4	52.	20	3.14	3.14	.5258		105.16	si
25	364.4	3.	20	3.14	3.14	-.23131		-46.26	si
26	348.7	3.	20	3.14	3.14	-.22859		-45.72	si
27	333.	3.	20	3.14	3.14	-.22588		-45.18	si
28	317.3	3.	20	3.14	3.14	-.22316		-44.63	si
29	301.5	3.	20	3.14	3.14	-.22045		-44.09	si
30	285.8	3.	20	3.14	3.14	-.21773		-43.55	si
31	270.1	3.	20	3.14	3.14	-.21502		-43.	si
32	254.4	3.	20	3.14	3.14	-.2123		-42.46	si
33	238.7	3.	20	3.14	3.14	-.20959		-41.92	si
34	223.	3.	20	3.14	3.14	-.20687		-41.37	si
35	207.3	3.	20	3.14	3.14	-.20415		-40.83	si
36	191.6	3.	20	3.14	3.14	-.20144		-40.29	si
37	175.8	3.	20	3.14	3.14	-.19872		-39.74	si
38	160.1	3.	20	3.14	3.14	-.19601		-39.2	si
39	144.4	3.	20	3.14	3.14	-.19329		-38.66	si
40	128.7	3.	20	3.14	3.14	-.19058		-38.12	si
41	113.	3.	20	3.14	3.14	-.18786		-37.57	si
42	97.3	3.	20	3.14	3.14	-.18515		-37.03	si
43	81.6	3.	20	3.14	3.14	-.18243		-36.49	si
44	65.9	3.	20	3.14	3.14	-.17972		-35.94	si
45	50.1	3.	20	3.14	3.14	-.177		-35.4	si
46	34.4	3.	20	3.14	3.14	-.17428		-34.86	si
47	18.7	3.	20	3.14	3.14	-.17157		-34.31	si
48	3.	3.	20	3.14	3.14	-.16885		-33.77	si

% ARMAT.: tesa= .28; comp.= .28; tot.= .56

Ripristino Ponte-Tubo
VERIFICA PULVINO XZ 9

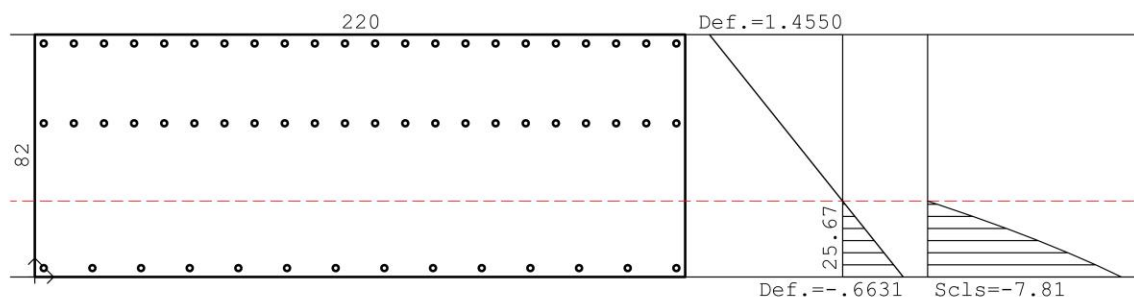
DESCRIZIONI
Tipo sezione : RETTANGOLARE
Tipo verifica: stato limite ultimo

CARATTERISTICHE DEI MATERIALI
Calcestruzzo: Rck= 30.
fck= 24.9
fcd= 14.11 (.35%)
Acciaio lento: Tipo= B450C
fyk= 450.
ftk= 540.
ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
eps= muz * y +muy * z + lam
muz= 2.58298584086149E-05
muy= 0
lam=-3.67324885511883E-04

SOLLECITAZIONI AGENTI:
Nd in y= 29.6 (baricentro CLS)
Nd = -20.93
Mdz=-1778.8651
verifica in pressoflessione retta

UNITA' DI MISURA:
kN; cm; kNm; N/mm2.
Ø in mm; deformazioni*1000.
SIMBOLI:
S=sigma (tensioni sui materiali);
D=deformazioni (epsilon):



TENSIONI NEL CLS:					
ver	Z	Y	Dcls	Scls	Ve
1	-2673.	70.6	1.45497	0.	si
2	-2453.	70.6	1.45497	0.	si
3	-2453.	-11.4	-.66308	-7.81	si
4	-2673.	-11.4	-.66308	-7.81	si

TENSIONI NEI FERRI:										
Fer	Z	Y	Ø (mm)	Af (cm2)	D	ferri	S	ferri	Ve	
1	-2456.	40.6	20	3.14		.68008		136.02	si	
3	-2466.	40.6	20	3.14		.68008		136.02	si	
3	-2476.	40.6	20	3.14		.68008		136.02	si	
4	-2487.	40.6	20	3.14		.68008		136.02	si	
5	-2497.	40.6	20	3.14		.68008		136.02	si	
6	-2507.	40.6	20	3.14		.68008		136.02	si	
7	-2517.	40.6	20	3.14		.68008		136.02	si	
8	-2527.	40.6	20	3.14		.68008		136.02	si	
9	-2538.	40.6	20	3.14		.68008		136.02	si	
10	-2548.	40.6	20	3.14		.68008		136.02	si	
11	-2558.	40.6	20	3.14		.68008		136.02	si	
12	-2568.	40.6	20	3.14		.68008		136.02	si	
13	-2578.	40.6	20	3.14		.68008		136.02	si	
14	-2589.	40.6	20	3.14		.68008		136.02	si	
15	-2599.	40.6	20	3.14		.68008		136.02	si	
16	-2609.	40.6	20	3.14		.68008		136.02	si	
17	-2619.	40.6	20	3.14		.68008		136.02	si	
18	-2629.	40.6	20	3.14		.68008		136.02	si	
19	-2639.	40.6	20	3.14		.68008		136.02	si	
20	-2650.	40.6	20	3.14		.68008		136.02	si	
21	-2660.	40.6	20	3.14		.68008		136.02	si	
22	-2670.	40.6	20	3.14		.68008		136.02	si	
23	-2456.	67.6	20	3.14	1.37748		275.5	si		
24	-2466.	67.6	20	3.14	1.37748		275.5	si		
25	-2476.	67.6	20	3.14	1.37748		275.5	si		
26	-2487.	67.6	20	3.14	1.37748		275.5	si		
27	-2497.	67.6	20	3.14	1.37748		275.5	si		
28	-2507.	67.6	20	3.14	1.37748		275.5	si		
29	-2517.	67.6	20	3.14	1.37748		275.5	si		
30	-2527.	67.6	20	3.14	1.37748		275.5	si		
31	-2538.	67.6	20	3.14	1.37748		275.5	si		
32	-2548.	67.6	20	3.14	1.37748		275.5	si		
33	-2558.	67.6	20	3.14	1.37748		275.5	si		
34	-2568.	67.6	20	3.14	1.37748		275.5	si		
35	-2578.	67.6	20	3.14	1.37748		275.5	si		
36	-2589.	67.6	20	3.14	1.37748		275.5	si		
37	-2599.	67.6	20	3.14	1.37748		275.5	si		
38	-2609.	67.6	20	3.14	1.37748		275.5	si		
39	-2619.	67.6	20	3.14	1.37748		275.5	si		
40	-2629.	67.6	20	3.14	1.37748		275.5	si		
41	-2639.	67.6	20	3.14	1.37748		275.5	si		
42	-2650.	67.6	20	3.14	1.37748		275.5	si		
43	-2660.	67.6	20	3.14	1.37748		275.5	si		
44	-2670.	67.6	20	3.14	1.37748		275.5	si		
45	-2456.	-8.4	20	3.14	-.58559		-117.12	si		
46	-2473.	-8.4	20	3.14	-.58559		-117.12	si		
47	-2489.	-8.4	20	3.14	-.58559		-117.12	si		
48	-2505.	-8.4	20	3.14	-.58559		-117.12	si		
49	-2522.	-8.4	20	3.14	-.58559		-117.12	si		
50	-2538.	-8.4	20	3.14	-.58559		-117.12	si		
51	-2555.	-8.4	20	3.14	-.58559		-117.12	si		
52	-2571.	-8.4	20	3.14	-.58559		-117.12	si		
53	-2588.	-8.4	20	3.14	-.58559		-117.12	si		
54	-2604.	-8.4	20	3.14	-.58559		-117.12	si		
55	-2621.	-8.4	20	3.14	-.58559		-117.12	si		
56	-2637.	-8.4	20	3.14	-.58559		-117.12	si		
57	-2654.	-8.4	20	3.14	-.58559		-117.12	si		
58	-2670.	-8.4	20	3.14	-.58559		-117.12	si		

% ARMAT.: tesa = .77; comp. = .24; tot. = 1.01

Ripristino Ponte-Tubo
VERIFICA PULVINO YZ 9

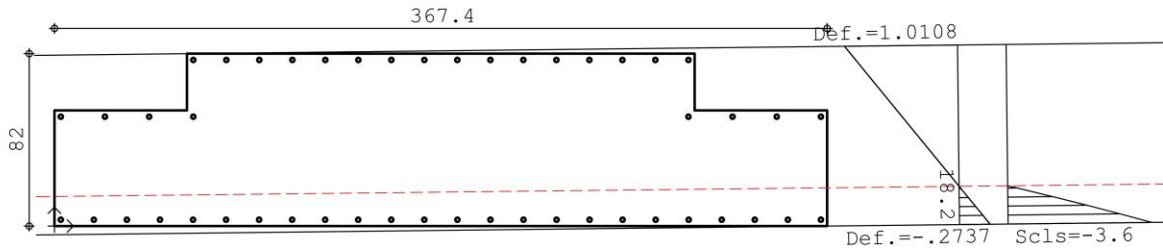
DESCRIZIONI
Tipo sezione : U Pul
Tipo verifica: stato limite ultimo

CARATTERISTICHE DEI MATERIALI
Calcestruzzo: Rck= 30.
fck= 24.9
fcd= 14.11 (.35%)
Acciaio lento: Tipo= B450C
fyk= 450.
ftk= 540.
ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
eps= muz * y + muy * z + lam
muz= 1.50366610154372E-05
muy=-1.69162046405504E-07
lam=-2.11589728839451E-04

SOLLECITAZIONI AGENTI:
Nd in z= 183.7; y= 37.5 (baricentro CLS)
Nd = -55.5
Mdz= -849.7302
Mdy= 207.9787

UNITA' DI MISURA:
kN; cm; kNm; N/mm2.
Ø in mm; deformazioni*1000.
SIMBOLI:
S=sigma (tensioni sui materiali);
D=deformazioni (epsilon):



TENSIONI NEL CLS:			Dcls	Scsls	Vel
ver	Z	Y			
1	0.	55.	.61543	0.	si
2	63.	55.	.60477	0.	si
3	63.	82.	1.01076	0.	si
4	304.4	82.	.96992	0.	si
5	304.4	55.	.56393	0.	si
6	367.4	55.	.55328	0.	si
7	367.4	0.	-.27374	-3.6	si
8	0.	0.	-.21159	-2.83	si

TENSIONI NEI FERRI:									
Fer	Z	Y	Ø (mm)	Af (cm2)	D	ferri	S	ferri	Vel
1	301.4	79.	20	3.14	3.14	.92532	185.06	185.06	si
2	285.7	79.	20	3.14	3.14	.92798	185.6	185.6	si
3	270.	79.	20	3.14	3.14	.93063	186.13	186.13	si
4	254.3	79.	20	3.14	3.14	.93329	186.66	186.66	si
5	238.6	79.	20	3.14	3.14	.93594	187.19	187.19	si
6	222.9	79.	20	3.14	3.14	.93859	187.72	187.72	si
7	207.2	79.	20	3.14	3.14	.94125	188.25	188.25	si
8	191.5	79.	20	3.14	3.14	.9439	188.78	188.78	si
9	175.9	79.	20	3.14	3.14	.94656	189.31	189.31	si
10	160.2	79.	20	3.14	3.14	.94921	189.84	189.84	si
11	144.5	79.	20	3.14	3.14	.95187	190.37	190.37	si
12	128.8	79.	20	3.14	3.14	.95452	190.9	190.9	si
13	113.1	79.	20	3.14	3.14	.95718	191.44	191.44	si
14	97.4	79.	20	3.14	3.14	.95983	191.97	191.97	si
15	81.7	79.	20	3.14	3.14	.96249	192.5	192.5	si
16	66.	79.	20	3.14	3.14	.96514	193.03	193.03	si
17	66.	52.	20	3.14	3.14	.55915	111.83	111.83	si
18	45.	52.	20	3.14	3.14	.5627	112.54	112.54	si
19	24.	52.	20	3.14	3.14	.56626	113.25	113.25	si
20	3.	52.	20	3.14	3.14	.56981	113.96	113.96	si
21	364.4	52.	20	3.14	3.14	.50867	101.73	101.73	si
22	343.4	52.	20	3.14	3.14	.51223	102.45	102.45	si
23	322.4	52.	20	3.14	3.14	.51578	103.16	103.16	si
24	301.4	52.	20	3.14	3.14	.51933	103.87	103.87	si
25	364.4	3.	20	3.14	3.14	-.22812	-45.62	-45.62	si
26	348.7	3.	20	3.14	3.14	-.22546	-45.09	-45.09	si
27	333.	3.	20	3.14	3.14	-.22281	-44.56	-44.56	si
28	317.3	3.	20	3.14	3.14	-.22015	-44.03	-44.03	si
29	301.5	3.	20	3.14	3.14	-.21749	-43.5	-43.5	si
30	285.8	3.	20	3.14	3.14	-.21483	-42.97	-42.97	si
31	270.1	3.	20	3.14	3.14	-.21217	-42.43	-42.43	si
32	254.4	3.	20	3.14	3.14	-.20952	-41.9	-41.9	si
33	238.7	3.	20	3.14	3.14	-.20686	-41.37	-41.37	si
34	223.	3.	20	3.14	3.14	-.2042	-40.84	-40.84	si
35	207.3	3.	20	3.14	3.14	-.20154	-40.31	-40.31	si
36	191.6	3.	20	3.14	3.14	-.19888	-39.78	-39.78	si
37	175.8	3.	20	3.14	3.14	-.19623	-39.25	-39.25	si
38	160.1	3.	20	3.14	3.14	-.19357	-38.71	-38.71	si
39	144.4	3.	20	3.14	3.14	-.19091	-38.18	-38.18	si
40	128.7	3.	20	3.14	3.14	-.18825	-37.65	-37.65	si
41	113.	3.	20	3.14	3.14	-.18559	-37.12	-37.12	si
42	97.3	3.	20	3.14	3.14	-.18294	-36.59	-36.59	si
43	81.6	3.	20	3.14	3.14	-.18028	-36.06	-36.06	si
44	65.9	3.	20	3.14	3.14	-.17762	-35.52	-35.52	si
45	50.1	3.	20	3.14	3.14	-.17496	-34.99	-34.99	si
46	34.4	3.	20	3.14	3.14	-.1723	-34.46	-34.46	si
47	18.7	3.	20	3.14	3.14	-.16965	-33.93	-33.93	si
48	3.	3.	20	3.14	3.14	-.16699	-33.4	-33.4	si

% ARMAT.: tesa= .28; comp.= .28; tot.= .56

Ripristino Ponte-Tubo

VERIFICA PULVINO XZ 10

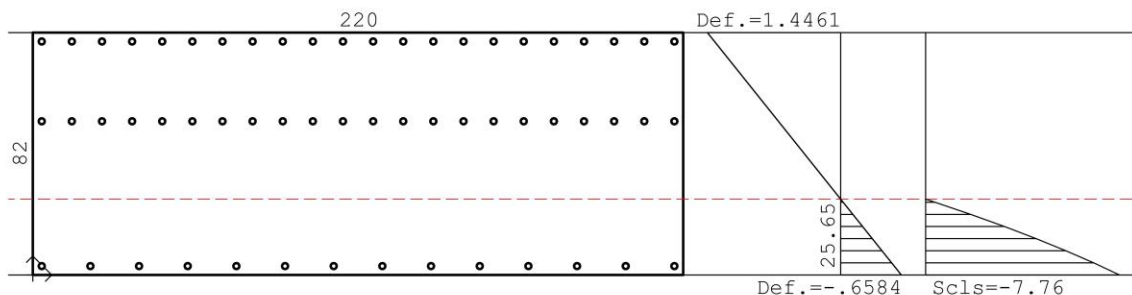
DESCRIZIONI
 Tipo sezione : RETTANGOLARE
 Tipo verifica: stato limite ultimo

CARATTERISTICHE DEI MATERIALI
 Calcestruzzo: Rck= 30.
 fck= 24.9
 fcd= 14.11 (.35%)
 Acciaio lento: Tipo= B450C
 fyk= 450.
 ftk= 540.
 ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
 eps= muz * y +muy * z + lam
 muz= 2.56646260999985E-05
 muy= 0
 lam=-3.64512746188839E-04

SOLLECITAZIONI AGENTI:
 Nd in y= 29.6 (baricentro CLS)
 Nd = -17.89
 Mdz=-1767.4454
 verifica in pressoflessione retta

UNITA' DI MISURA:
 kN; cm; kNm; N/mm2.
 Ø in mm; deformazioni*1000.
 SIMBOLI:
 S=sigma (tensioni sui materiali);
 D=deformazioni (epsilon):



TENSIONI NEL CLS:					
ver	Z	Y	Dcls	Scls	Ve
1	-2673.	70.6	1.44613	0.	si
2	-2453.	70.6	1.44613	0.	si
3	-2453.	-11.4	-.65837	-7.76	si
4	-2673.	-11.4	-.65837	-7.76	si

TENSIONI NEI FERRI:										
Fer	Z	Y	Ø (mm)	Af (cm2)	D	ferri	S	ferri	Ve	
1	-2456.	40.6	20	3.14		.67619		135.24	si	
3	-2466.	40.6	20	3.14		.67619		135.24	si	
3	-2476.	40.6	20	3.14		.67619		135.24	si	
4	-2487.	40.6	20	3.14		.67619		135.24	si	
5	-2497.	40.6	20	3.14		.67619		135.24	si	
6	-2507.	40.6	20	3.14		.67619		135.24	si	
7	-2517.	40.6	20	3.14		.67619		135.24	si	
8	-2527.	40.6	20	3.14		.67619		135.24	si	
9	-2538.	40.6	20	3.14		.67619		135.24	si	
10	-2548.	40.6	20	3.14		.67619		135.24	si	
11	-2558.	40.6	20	3.14		.67619		135.24	si	
12	-2568.	40.6	20	3.14		.67619		135.24	si	
13	-2578.	40.6	20	3.14		.67619		135.24	si	
14	-2589.	40.6	20	3.14		.67619		135.24	si	
15	-2599.	40.6	20	3.14		.67619		135.24	si	
16	-2609.	40.6	20	3.14		.67619		135.24	si	
17	-2619.	40.6	20	3.14		.67619		135.24	si	
18	-2629.	40.6	20	3.14		.67619		135.24	si	
19	-2639.	40.6	20	3.14		.67619		135.24	si	
20	-2650.	40.6	20	3.14		.67619		135.24	si	
21	-2660.	40.6	20	3.14		.67619		135.24	si	
22	-2670.	40.6	20	3.14		.67619		135.24	si	
23	-2456.	67.6	20	3.14	1.36913			273.83	si	
24	-2466.	67.6	20	3.14	1.36913			273.83	si	
25	-2476.	67.6	20	3.14	1.36913			273.83	si	
26	-2487.	67.6	20	3.14	1.36913			273.83	si	
27	-2497.	67.6	20	3.14	1.36913			273.83	si	
28	-2507.	67.6	20	3.14	1.36913			273.83	si	
29	-2517.	67.6	20	3.14	1.36913			273.83	si	
30	-2527.	67.6	20	3.14	1.36913			273.83	si	
31	-2538.	67.6	20	3.14	1.36913			273.83	si	
32	-2548.	67.6	20	3.14	1.36913			273.83	si	
33	-2558.	67.6	20	3.14	1.36913			273.83	si	
34	-2568.	67.6	20	3.14	1.36913			273.83	si	
35	-2578.	67.6	20	3.14	1.36913			273.83	si	
36	-2589.	67.6	20	3.14	1.36913			273.83	si	
37	-2599.	67.6	20	3.14	1.36913			273.83	si	
38	-2609.	67.6	20	3.14	1.36913			273.83	si	
39	-2619.	67.6	20	3.14	1.36913			273.83	si	
40	-2629.	67.6	20	3.14	1.36913			273.83	si	
41	-2639.	67.6	20	3.14	1.36913			273.83	si	
42	-2650.	67.6	20	3.14	1.36913			273.83	si	
43	-2660.	67.6	20	3.14	1.36913			273.83	si	
44	-2670.	67.6	20	3.14	1.36913			273.83	si	
45	-2456.	-8.4	20	3.14		-.58138		-116.28	si	
46	-2473.	-8.4	20	3.14		-.58138		-116.28	si	
47	-2489.	-8.4	20	3.14		-.58138		-116.28	si	
48	-2505.	-8.4	20	3.14		-.58138		-116.28	si	
49	-2522.	-8.4	20	3.14		-.58138		-116.28	si	
50	-2538.	-8.4	20	3.14		-.58138		-116.28	si	
51	-2555.	-8.4	20	3.14		-.58138		-116.28	si	
52	-2571.	-8.4	20	3.14		-.58138		-116.28	si	
53	-2588.	-8.4	20	3.14		-.58138		-116.28	si	
54	-2604.	-8.4	20	3.14		-.58138		-116.28	si	
55	-2621.	-8.4	20	3.14		-.58138		-116.28	si	
56	-2637.	-8.4	20	3.14		-.58138		-116.28	si	
57	-2654.	-8.4	20	3.14		-.58138		-116.28	si	
58	-2670.	-8.4	20	3.14		-.58138		-116.28	si	

% ARMAT.: tesa = .77; comp. = .24; tot. = 1.01

Ripristino Ponte-Tubo

VERIFICA PULVINO YZ 10

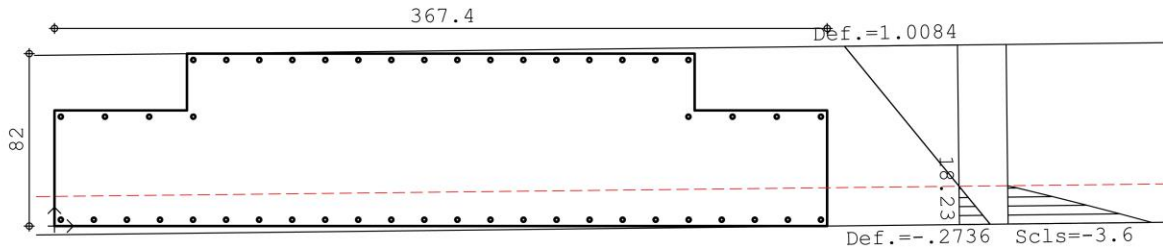
DESCRIZIONI
 Tipo sezione : U Pul
 Tipo verifica: sTato limite ultimo

CARATTERISTICHE DEI MATERIALI
 Calcestruzzo: Rck= 30.
 fck= 24.9
 fcd= 14.11 (.35%)
 Acciaio lento: Tipo= B450C
 fyk= 450.
 ftk= 540.
 ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
 eps= muz * y +muy * z + lam
 muz= 1.50073671779657E-05
 muy=-1.68869044479765E-07
 lam=-2.11527013082705E-04

SOLLECITAZIONI AGENTI:
 Nd in z= 183.7; y= 37.5 (baricentro CLS)
 Nd = -59.35
 Mdz= -848.931
 Mdy= 207.8427

UNITA' DI MISURA:
 kN; cm; kNm; N/mm2.
 Ø in mm; deformazioni*1000.
 SIMBOLI:
 S=sigma (tensioni sui materiali);
 D=deformazioni (epsilon):



TENSIONI NEL CLS:			Dcls	Scls	Vel
ver	Z	Y			
1	0.	55.	.61388	0.	si
2	63.	55.	.60324	0.	si
3	63.	82.	1.00844	0.	si
4	304.4	82.	.96767	0.	si
5	304.4	55.	.56247	0.	si
6	367.4	55.	.55184	0.	si
7	367.4	0.	-.27357	-3.6	si
8	0.	0.	-.21153	-2.83	si

TENSIONI NEI FERRI:									
Fer	Z	Y	Ø (mm)	Af (cm2)	D	ferri	S	ferri	Vel
1	301.4	79.	20	3.14	3.14	.92316		184.63	si
2	285.7	79.	20	3.14	3.14	.92581		185.16	si
3	270.	79.	20	3.14	3.14	.92846		185.69	si
4	254.3	79.	20	3.14	3.14	.93111		186.22	si
5	238.6	79.	20	3.14	3.14	.93376		186.75	si
6	222.9	79.	20	3.14	3.14	.93641		187.28	si
7	207.2	79.	20	3.14	3.14	.93906		187.81	si
8	191.5	79.	20	3.14	3.14	.94171		188.34	si
9	175.9	79.	20	3.14	3.14	.94436		188.87	si
10	160.2	79.	20	3.14	3.14	.94701		189.4	si
11	144.5	79.	20	3.14	3.14	.94966		189.93	si
12	128.8	79.	20	3.14	3.14	.95231		190.46	si
13	113.1	79.	20	3.14	3.14	.95496		190.99	si
14	97.4	79.	20	3.14	3.14	.95761		191.52	si
15	81.7	79.	20	3.14	3.14	.96026		192.05	si
16	66.	79.	20	3.14	3.14	.96291		192.58	si
17	66.	52.	20	3.14	3.14	.55771		111.54	si
18	45.	52.	20	3.14	3.14	.56126		112.25	si
19	24.	52.	20	3.14	3.14	.5648		112.96	si
20	3.	52.	20	3.14	3.14	.56835		113.67	si
21	364.4	52.	20	3.14	3.14	.50732		101.46	si
22	343.4	52.	20	3.14	3.14	.51087		102.17	si
23	322.4	52.	20	3.14	3.14	.51441		102.88	si
24	301.4	52.	20	3.14	3.14	.51796		103.59	si
25	364.4	3.	20	3.14	3.14	-.22804		-45.61	si
26	348.7	3.	20	3.14	3.14	-.22539		-45.08	si
27	333.	3.	20	3.14	3.14	-.22273		-44.55	si
28	317.3	3.	20	3.14	3.14	-.22008		-44.02	si
29	301.5	3.	20	3.14	3.14	-.21743		-43.49	si
30	285.8	3.	20	3.14	3.14	-.21477		-42.95	si
31	270.1	3.	20	3.14	3.14	-.21212		-42.42	si
32	254.4	3.	20	3.14	3.14	-.20947		-41.89	si
33	238.7	3.	20	3.14	3.14	-.20681		-41.36	si
34	223.	3.	20	3.14	3.14	-.20416		-40.83	si
35	207.3	3.	20	3.14	3.14	-.20151		-40.3	si
36	191.6	3.	20	3.14	3.14	-.19885		-39.77	si
37	175.8	3.	20	3.14	3.14	-.1962		-39.24	si
38	160.1	3.	20	3.14	3.14	-.19355		-38.71	si
39	144.4	3.	20	3.14	3.14	-.19089		-38.18	si
40	128.7	3.	20	3.14	3.14	-.18824		-37.65	si
41	113.	3.	20	3.14	3.14	-.18559		-37.12	si
42	97.3	3.	20	3.14	3.14	-.18293		-36.59	si
43	81.6	3.	20	3.14	3.14	-.18028		-36.06	si
44	65.9	3.	20	3.14	3.14	-.17763		-35.53	si
45	50.1	3.	20	3.14	3.14	-.17497		-34.99	si
46	34.4	3.	20	3.14	3.14	-.17232		-34.46	si
47	18.7	3.	20	3.14	3.14	-.16966		-33.93	si
48	3.	3.	20	3.14	3.14	-.16701		-33.4	si

% ARMAT.: tesa= .28; comp.= .28; tot.= .56

Ripristino Ponte-Tubo
VERIFICA PULVINO XZ 11

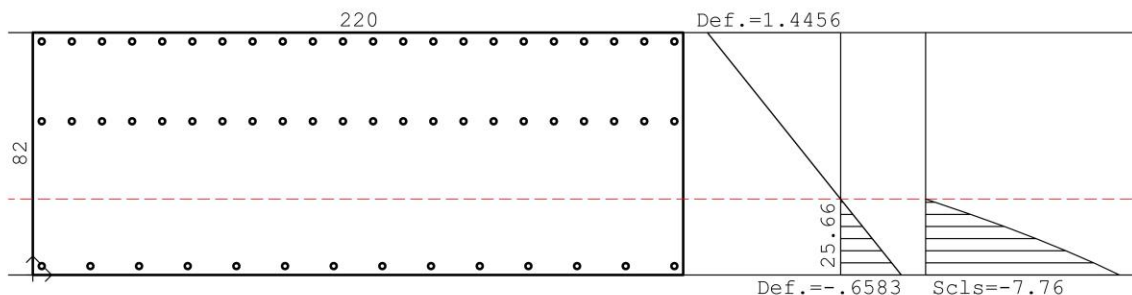
DESCRIZIONI
Tipo sezione : RETTANGOLARE
Tipo verifica: stato limite ultimo

CARATTERISTICHE DEI MATERIALI
Calcestruzzo: Rck= 30.
fck= 24.9
fcd= 14.11 (.35%)
Acciaio lento: Tipo= B450C
fyk= 450.
ftk= 540.
ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
eps= muz * y +muy * z + lam
muz= 2.56576499112399E-05
muy= 0
lam=-3.64510454225526E-04

SOLLECITAZIONI AGENTI:
Nd in y= 29.6 (baricentro CLS)
Nd = -18.96
Mdz=-1767.1348
verifica in pressoflessione retta

UNITA' DI MISURA:
kN; cm; kNm; N/mm2.
Ø in mm; deformazioni*1000.
SIMBOLI:
S=sigma (tensioni sui materiali);
D=deformazioni (epsilon):



TENSIONI NEL CLS:					
ver	Z	Y	Dcls	Scls	Vel
1	-2673.	70.6	1.44564	0.	si
2	-2453.	70.6	1.44564	0.	si
3	-2453.	-11.4	-.65829	-7.76	si
4	-2673.	-11.4	-.65829	-7.76	si

TENSIONI NEI FERRI:											
Fer	Z	Y	Ø (mm)	Af (cm2)	D	ferri	S	ferri	Vel		
1	-2456.	40.6	20	3.14		.67591		135.18	si		
2	-2456.	40.6	20	3.14		.67591		135.18	si		
3	-2476.	40.6	20	3.14		.67591		135.18	si		
4	-2487.	40.6	20	3.14		.67591		135.18	si		
5	-2497.	40.6	20	3.14		.67591		135.18	si		
6	-2507.	40.6	20	3.14		.67591		135.18	si		
7	-2517.	40.6	20	3.14		.67591		135.18	si		
8	-2527.	40.6	20	3.14		.67591		135.18	si		
9	-2538.	40.6	20	3.14		.67591		135.18	si		
10	-2548.	40.6	20	3.14		.67591		135.18	si		
11	-2558.	40.6	20	3.14		.67591		135.18	si		
12	-2568.	40.6	20	3.14		.67591		135.18	si		
13	-2578.	40.6	20	3.14		.67591		135.18	si		
14	-2589.	40.6	20	3.14		.67591		135.18	si		
15	-2599.	40.6	20	3.14		.67591		135.18	si		
16	-2609.	40.6	20	3.14		.67591		135.18	si		
17	-2619.	40.6	20	3.14		.67591		135.18	si		
18	-2629.	40.6	20	3.14		.67591		135.18	si		
19	-2639.	40.6	20	3.14		.67591		135.18	si		
20	-2650.	40.6	20	3.14		.67591		135.18	si		
21	-2660.	40.6	20	3.14		.67591		135.18	si		
22	-2670.	40.6	20	3.14		.67591		135.18	si		
23	-2456.	67.6	20	3.14	1.36866		273.73	si			
24	-2466.	67.6	20	3.14	1.36866		273.73	si			
25	-2476.	67.6	20	3.14	1.36866		273.73	si			
26	-2487.	67.6	20	3.14	1.36866		273.73	si			
27	-2497.	67.6	20	3.14	1.36866		273.73	si			
28	-2507.	67.6	20	3.14	1.36866		273.73	si			
29	-2517.	67.6	20	3.14	1.36866		273.73	si			
30	-2527.	67.6	20	3.14	1.36866		273.73	si			
31	-2538.	67.6	20	3.14	1.36866		273.73	si			
32	-2548.	67.6	20	3.14	1.36866		273.73	si			
33	-2558.	67.6	20	3.14	1.36866		273.73	si			
34	-2568.	67.6	20	3.14	1.36866		273.73	si			
35	-2578.	67.6	20	3.14	1.36866		273.73	si			
36	-2589.	67.6	20	3.14	1.36866		273.73	si			
37	-2599.	67.6	20	3.14	1.36866		273.73	si			
38	-2609.	67.6	20	3.14	1.36866		273.73	si			
39	-2619.	67.6	20	3.14	1.36866		273.73	si			
40	-2629.	67.6	20	3.14	1.36866		273.73	si			
41	-2639.	67.6	20	3.14	1.36866		273.73	si			
42	-2650.	67.6	20	3.14	1.36866		273.73	si			
43	-2660.	67.6	20	3.14	1.36866		273.73	si			
44	-2670.	67.6	20	3.14	1.36866		273.73	si			
45	-2456.	-8.4	20	3.14	-.58132		-116.26	si			
46	-2473.	-8.4	20	3.14	-.58132		-116.26	si			
47	-2489.	-8.4	20	3.14	-.58132		-116.26	si			
48	-2505.	-8.4	20	3.14	-.58132		-116.26	si			
49	-2522.	-8.4	20	3.14	-.58132		-116.26	si			
50	-2538.	-8.4	20	3.14	-.58132		-116.26	si			
51	-2555.	-8.4	20	3.14	-.58132		-116.26	si			
52	-2571.	-8.4	20	3.14	-.58132		-116.26	si			
53	-2588.	-8.4	20	3.14	-.58132		-116.26	si			
54	-2604.	-8.4	20	3.14	-.58132		-116.26	si			
55	-2621.	-8.4	20	3.14	-.58132		-116.26	si			
56	-2637.	-8.4	20	3.14	-.58132		-116.26	si			
57	-2654.	-8.4	20	3.14	-.58132		-116.26	si			
58	-2670.	-8.4	20	3.14	-.58132		-116.26	si			

% ARMAT.: tesa = .77; comp. = .24; tot. = 1.01

Ripristino Ponte-Tubo VERIFICA PULVINO YZ 11

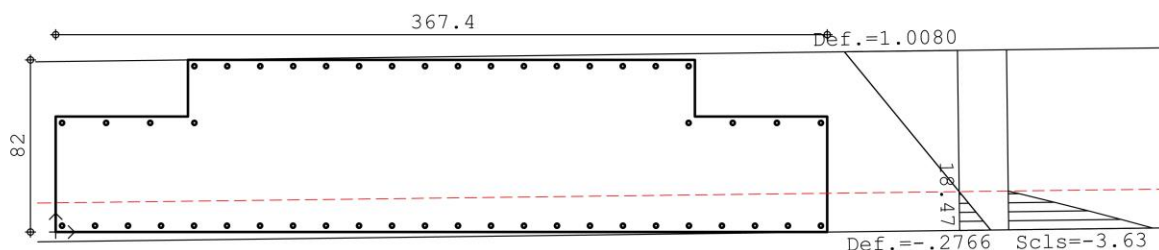
DESCRIZIONI
 Tipo sezione : U Pul
 Tipo verifica: sStato limite ultimo

CARATTERISTICHE DEI MATERIALI
 Calcestruzzo: Rck= 30.
 fck= 24.9
 fcd= 14.11 (.35%)
 Acciaio lento: Tipo= B450C
 fyk= 450.
 ftk= 540.
 ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
 eps= muz * y +muy * z + lam
 muz= 1.49760591287142E-05
 muy=-1.85599010968109E-07
 lam=-2.0839229463346E-04

SOLLECITAZIONI AGENTI:
 Nd in z= 183.7; y= 37.5 (baricentro CLS)
 Nd = -65.19
 Mdz= -848.4335
 Mdy= 228.731

UNITA' DI MISURA:
 kN; cm; kNm; N/mm2.
 Ø in mm; deformazioni*1000.
 SIMBOLI:
 S=sigma (tensioni sui materiali);
 D=deformazioni (epsilon):



TENSIONI NEL CLS:			Dcls	Scls	Vel
ver	Z	Y			
1	0.	55.	.61529	0.	si
2	63.	55.	.6036	0.	si
3	63.	82.	1.00795	0.	si
4	304.4	82.	.96315	0.	si
5	304.4	55.	.55879	0.	si
6	367.4	55.	.5471	0.	si
7	367.4	0.	-.27658	-3.63	si
8	0.	0.	-.20839	-2.79	si

TENSIONI NEI FERRI:									
Fer	Z	Y	Ø (mm)	Af (cm2)	D	ferri	S	ferri	Vel
1	301.4	79.	20	3.14	3.14	.91878		133.76	si
2	285.7	79.	20	3.14	3.14	.92169		184.34	si
3	270.	79.	20	3.14	3.14	.9246		184.92	si
4	254.3	79.	20	3.14	3.14	.92751		185.5	si
5	238.6	79.	20	3.14	3.14	.93043		186.09	si
6	222.9	79.	20	3.14	3.14	.93334		186.67	si
7	207.2	79.	20	3.14	3.14	.93625		187.25	si
8	191.5	79.	20	3.14	3.14	.93917		187.83	si
9	175.9	79.	20	3.14	3.14	.94208		188.42	si
10	160.2	79.	20	3.14	3.14	.94499		189.	si
11	144.5	79.	20	3.14	3.14	.9479		189.58	si
12	128.8	79.	20	3.14	3.14	.95082		190.16	si
13	113.1	79.	20	3.14	3.14	.95373		190.75	si
14	97.4	79.	20	3.14	3.14	.95664		191.33	si
15	81.7	79.	20	3.14	3.14	.95955		191.91	si
16	66.	79.	20	3.14	3.14	.96247		192.49	si
17	66.	52.	20	3.14	3.14	.55811		111.62	si
18	45.	52.	20	3.14	3.14	.56201		112.4	si
19	24.	52.	20	3.14	3.14	.56591		113.18	si
20	3.	52.	20	3.14	3.14	.56981		113.96	si
21	364.4	52.	20	3.14	3.14	.50273		100.55	si
22	343.4	52.	20	3.14	3.14	.50663		101.33	si
23	322.4	52.	20	3.14	3.14	.51053		102.11	si
24	301.4	52.	20	3.14	3.14	.51442		102.88	si
25	364.4	3.	20	3.14	3.14	-.2311		-46.22	si
26	348.7	3.	20	3.14	3.14	-.22818		-45.64	si
27	333.	3.	20	3.14	3.14	-.22526		-45.05	si
28	317.3	3.	20	3.14	3.14	-.22235		-44.47	si
29	301.5	3.	20	3.14	3.14	-.21943		-43.89	si
30	285.8	3.	20	3.14	3.14	-.21651		-43.3	si
31	270.1	3.	20	3.14	3.14	-.2136		-42.72	si
32	254.4	3.	20	3.14	3.14	-.21068		-42.14	si
33	238.7	3.	20	3.14	3.14	-.20777		-41.55	si
34	223.	3.	20	3.14	3.14	-.20485		-40.97	si
35	207.3	3.	20	3.14	3.14	-.20193		-40.39	si
36	191.6	3.	20	3.14	3.14	-.19902		-39.8	si
37	175.8	3.	20	3.14	3.14	-.1961		-39.22	si
38	160.1	3.	20	3.14	3.14	-.19318		-38.64	si
39	144.4	3.	20	3.14	3.14	-.19027		-38.05	si
40	128.7	3.	20	3.14	3.14	-.18735		-37.47	si
41	113.	3.	20	3.14	3.14	-.18444		-36.89	si
42	97.3	3.	20	3.14	3.14	-.18152		-36.3	si
43	81.6	3.	20	3.14	3.14	-.1786		-35.72	si
44	65.9	3.	20	3.14	3.14	-.17569		-35.14	si
45	50.1	3.	20	3.14	3.14	-.17277		-34.55	si
46	34.4	3.	20	3.14	3.14	-.16985		-33.97	si
47	18.7	3.	20	3.14	3.14	-.16694		-33.39	si
48	3.	3.	20	3.14	3.14	-.16402		-32.8	si

% ARMAT.: tesa = .28; comp. = .28; tot. = .56

Ripristino Ponte-Tubo
VERIFICA PULVINO XZ 12

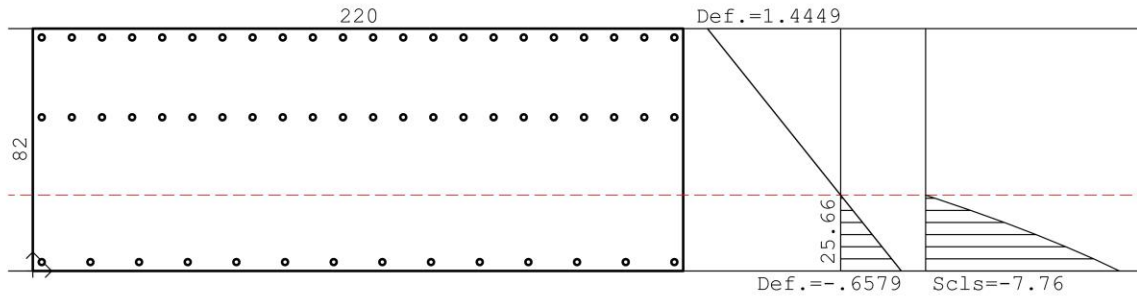
DESCRIZIONI
Tipo sezione : RETTANGOLARE
Tipo verifica: stato limite ultimo

CARATTERISTICHE DEI MATERIALI
Calcestruzzo: Rck= 30.
fck= 24.9
fcd= 14.11 (.35%)
Acciaio lento: Tipo= B450C
fyk= 450.
ftk= 540.
ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
eps= muz * y +muy * z + lam
muz= 2.56432237818568E-05
muy= 0
lam=-3.64270456849552E-04

SOLLECITAZIONI AGENTI:
Nd in y= 29.6 (baricentro CLS)
Nd = -18.75
Mdz=-1766.1454
verifica in pressoflessione retta

UNITA' DI MISURA:
kN; cm; kNm; N/mm2.
Ø in mm; deformazioni*1000.
SIMBOLI:
S=sigma (tensioni sui materiali);
D=deformazioni (epsilon):



TENSIONI NEL CLS:					
ver	Z	Y	Dcls	Scls	Ve
1	-2673.	70.6	1.44486	0.	si
2	-2453.	70.6	1.44486	0.	si
3	-2453.	-11.4	-6.5789	-7.76	si
4	-2673.	-11.4	-6.5789	-7.76	si

TENSIONI NEI FERRI:										
Fer	Z	Y	Ø (mm)	Af (cm2)	D	ferri	S	ferri	Ve	
1	-2456.	40.6	20	3.14		.67556		135.11	si	
2	-2456.	40.6	20	3.14		.67556		135.11	si	
3	-2476.	40.6	20	3.14		.67556		135.11	si	
4	-2487.	40.6	20	3.14		.67556		135.11	si	
5	-2497.	40.6	20	3.14		.67556		135.11	si	
6	-2507.	40.6	20	3.14		.67556		135.11	si	
7	-2517.	40.6	20	3.14		.67556		135.11	si	
8	-2527.	40.6	20	3.14		.67556		135.11	si	
9	-2538.	40.6	20	3.14		.67556		135.11	si	
10	-2548.	40.6	20	3.14		.67556		135.11	si	
11	-2558.	40.6	20	3.14		.67556		135.11	si	
12	-2568.	40.6	20	3.14		.67556		135.11	si	
13	-2578.	40.6	20	3.14		.67556		135.11	si	
14	-2589.	40.6	20	3.14		.67556		135.11	si	
15	-2599.	40.6	20	3.14		.67556		135.11	si	
16	-2609.	40.6	20	3.14		.67556		135.11	si	
17	-2619.	40.6	20	3.14		.67556		135.11	si	
18	-2629.	40.6	20	3.14		.67556		135.11	si	
19	-2639.	40.6	20	3.14		.67556		135.11	si	
20	-2650.	40.6	20	3.14		.67556		135.11	si	
21	-2660.	40.6	20	3.14		.67556		135.11	si	
22	-2670.	40.6	20	3.14		.67556		135.11	si	
23	-2456.	67.6	20	3.14	1.36793		273.59	si		
24	-2466.	67.6	20	3.14	1.36793		273.59	si		
25	-2476.	67.6	20	3.14	1.36793		273.59	si		
26	-2487.	67.6	20	3.14	1.36793		273.59	si		
27	-2497.	67.6	20	3.14	1.36793		273.59	si		
28	-2507.	67.6	20	3.14	1.36793		273.59	si		
29	-2517.	67.6	20	3.14	1.36793		273.59	si		
30	-2527.	67.6	20	3.14	1.36793		273.59	si		
31	-2538.	67.6	20	3.14	1.36793		273.59	si		
32	-2548.	67.6	20	3.14	1.36793		273.59	si		
33	-2558.	67.6	20	3.14	1.36793		273.59	si		
34	-2568.	67.6	20	3.14	1.36793		273.59	si		
35	-2578.	67.6	20	3.14	1.36793		273.59	si		
36	-2589.	67.6	20	3.14	1.36793		273.59	si		
37	-2599.	67.6	20	3.14	1.36793		273.59	si		
38	-2609.	67.6	20	3.14	1.36793		273.59	si		
39	-2619.	67.6	20	3.14	1.36793		273.59	si		
40	-2629.	67.6	20	3.14	1.36793		273.59	si		
41	-2639.	67.6	20	3.14	1.36793		273.59	si		
42	-2650.	67.6	20	3.14	1.36793		273.59	si		
43	-2660.	67.6	20	3.14	1.36793		273.59	si		
44	-2670.	67.6	20	3.14	1.36793		273.59	si		
45	-2456.	-8.4	20	3.14	-58096		-116.19	si		
46	-2473.	-8.4	20	3.14	-58096		-116.19	si		
47	-2489.	-8.4	20	3.14	-58096		-116.19	si		
48	-2505.	-8.4	20	3.14	-58096		-116.19	si		
49	-2522.	-8.4	20	3.14	-58096		-116.19	si		
50	-2538.	-8.4	20	3.14	-58096		-116.19	si		
51	-2555.	-8.4	20	3.14	-58096		-116.19	si		
52	-2571.	-8.4	20	3.14	-58096		-116.19	si		
53	-2588.	-8.4	20	3.14	-58096		-116.19	si		
54	-2604.	-8.4	20	3.14	-58096		-116.19	si		
55	-2621.	-8.4	20	3.14	-58096		-116.19	si		
56	-2637.	-8.4	20	3.14	-58096		-116.19	si		
57	-2654.	-8.4	20	3.14	-58096		-116.19	si		
58	-2670.	-8.4	20	3.14	-58096		-116.19	si		

% ARMAT.: tesa = .77; comp. = .24; tot. = 1.01

Ripristino Ponte-Tubo

VERIFICA PULVINO YZ 12

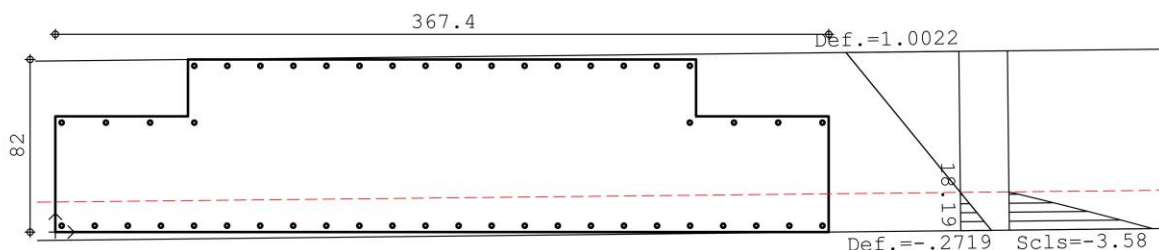
DESCRIZIONI
 Tipo sezione : U Pul
 Tipo verifica: sFato limite ultimo

CARATTERISTICHE DEI MATERIALI
 Calcestruzzo: Rck= 30.
 fck= 24.9
 fcd= 14.11 (.35%)
 Acciaio lento: Tipo= B450C
 fyk= 450.
 ftk= 540.
 ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
 eps= muz * y + muy * z + lam
 muz= 1.4947540429251E-05
 muy= -1.58908128337273E-07
 lam= -2.13483414556776E-04

SOLLECITAZIONI AGENTI:
 Nd in z= 183.7; y= 37.5 (baricentro CLS)
 Nd = -70.68
 Mdz= -848.0467
 Mdy= 196.2182

UNITA' DI MISURA:
 kN; cm; kNm; N/mm2.
 Ø in mm; deformazioni*1000.
 SIMBOLI:
 S=sigma (tensioni sui materiali);
 D=deformazioni (epsilon):



TENSIONI NEL CLS:			Dcls	Scls	Vel
ver	Z	Y			
1	0.	55.	.60863	0.	si
2	63.	55.	.59862	0.	si
3	63.	82.	1.0022	0.	si
4	304.4	82.	.96384	0.	si
5	304.4	55.	.56026	0.	si
6	367.4	55.	.55025	0.	si
7	367.4	0.	-.27187	-3.58	si
8	0.	0.	-.21348	-2.85	si

TENSIONI NEI FERRI:									
Fer	Z	Y	Ø (mm)	Af (cm2)	D	ferri	S	ferri	Vel
1	301.4	79.	20	3.14	3.14	.91948		183.9	si
2	285.7	79.	20	3.14	3.14	.92197		184.39	si
3	270.	79.	20	3.14	3.14	.92447		184.89	si
4	254.3	79.	20	3.14	3.14	.92696		185.39	si
5	238.6	79.	20	3.14	3.14	.92945		185.89	si
6	222.9	79.	20	3.14	3.14	.93195		186.39	si
7	207.2	79.	20	3.14	3.14	.93444		186.89	si
8	191.5	79.	20	3.14	3.14	.93693		187.39	si
9	175.9	79.	20	3.14	3.14	.93943		187.89	si
10	160.2	79.	20	3.14	3.14	.94192		188.38	si
11	144.5	79.	20	3.14	3.14	.94442		188.88	si
12	128.8	79.	20	3.14	3.14	.94691		189.38	si
13	113.1	79.	20	3.14	3.14	.9494		189.88	si
14	97.4	79.	20	3.14	3.14	.9519		190.38	si
15	81.7	79.	20	3.14	3.14	.95439		190.88	si
16	66.	79.	20	3.14	3.14	.95688		191.38	si
17	66.	52.	20	3.14	3.14	.5533		110.66	si
18	45.	52.	20	3.14	3.14	.55664		111.33	si
19	24.	52.	20	3.14	3.14	.55997		111.99	si
20	3.	52.	20	3.14	3.14	.56331		112.66	si
21	364.4	52.	20	3.14	3.14	.50588		101.18	si
22	343.4	52.	20	3.14	3.14	.50922		101.84	si
23	322.4	52.	20	3.14	3.14	.51256		102.51	si
24	301.4	52.	20	3.14	3.14	.51589		103.18	si
25	364.4	3.	20	3.14	3.14	-.22655		-45.31	si
26	348.7	3.	20	3.14	3.14	-.22405		-44.81	si
27	333.	3.	20	3.14	3.14	-.22155		-44.31	si
28	317.3	3.	20	3.14	3.14	-.21906		-43.81	si
29	301.5	3.	20	3.14	3.14	-.21656		-43.31	si
30	285.8	3.	20	3.14	3.14	-.21406		-42.81	si
31	270.1	3.	20	3.14	3.14	-.21157		-42.31	si
32	254.4	3.	20	3.14	3.14	-.20907		-41.81	si
33	238.7	3.	20	3.14	3.14	-.20657		-41.31	si
34	223.	3.	20	3.14	3.14	-.20407		-40.81	si
35	207.3	3.	20	3.14	3.14	-.20158		-40.32	si
36	191.6	3.	20	3.14	3.14	-.19908		-39.82	si
37	175.8	3.	20	3.14	3.14	-.19658		-39.32	si
38	160.1	3.	20	3.14	3.14	-.19409		-38.82	si
39	144.4	3.	20	3.14	3.14	-.19159		-38.32	si
40	128.7	3.	20	3.14	3.14	-.18909		-37.82	si
41	113.	3.	20	3.14	3.14	-.1866		-37.32	si
42	97.3	3.	20	3.14	3.14	-.1841		-36.82	si
43	81.6	3.	20	3.14	3.14	-.1816		-36.32	si
44	65.9	3.	20	3.14	3.14	-.17911		-35.82	si
45	50.1	3.	20	3.14	3.14	-.17661		-35.32	si
46	34.4	3.	20	3.14	3.14	-.17411		-34.82	si
47	18.7	3.	20	3.14	3.14	-.17161		-34.32	si
48	3.	3.	20	3.14	3.14	-.16912		-33.82	si

% ARMAT.: tesa= .28; comp.= .28; tot.= .56

Ripristino Ponte-Tubo

VERIFICA PULVINO XZ 13

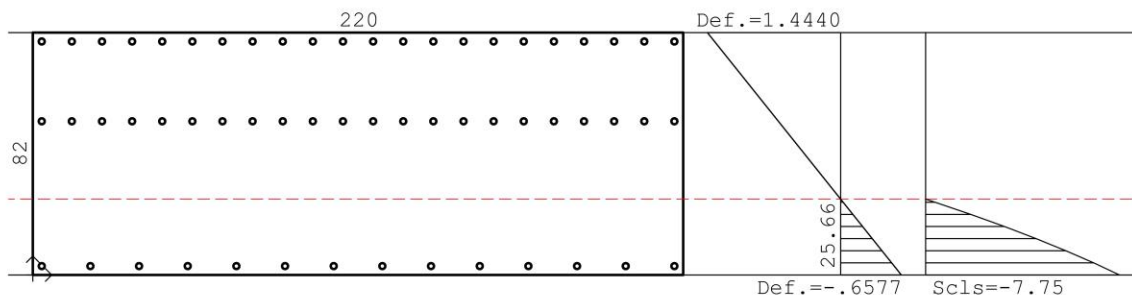
DESCRIZIONI
 Tipo sezione : RETTANGOLARE
 Tipo verifica: stato limite ultimo

CARATTERISTICHE DEI MATERIALI
 Calcestruzzo: Rck= 30.
 fck= 24.9
 fcd= 14.11 (.35%)
 Acciaio lento: Tipo= B450C
 fyk= 450.
 ftk= 540.
 ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
 eps= muz * y +muy * z + lam
 muz= 2.56299812801571E-05
 muy= 0
 lam=-3.64199962552355E-04

SOLLECITAZIONI AGENTI:
 Nd in y= 29.6 (baricentro CLS)
 Nd = -20.1
 Mdz=-1765.4582
 verifica in pressoflessione retta

UNITA' DI MISURA:
 kN; cm; kNm; N/mm2.
 Ø in mm; deformazioni*1000.
 SIMBOLI:
 S=sigma (tensioni sui materiali);
 D=deformazioni (epsilon):



TENSIONI NEL CLS:					
ver	Z	Y	Dcls	Scls	Vel
1	-2673.	70.6	1.444	0.	si
2	-2453.	70.6	1.444	0.	si
3	-2453.	-11.4	-6.5766	-7.75	si
4	-2673.	-11.4	-6.5766	-7.75	si

TENSIONI NEI FERRI:										
Fer	Z	Y	Ø (mm)	Af (cm2)	D	ferri	S	ferri	Vel	
1	-2456.	40.6	20	3.14		.6751		135.02	si	
3	-2466.	40.6	20	3.14		.6751		135.02	si	
3	-2476.	40.6	20	3.14		.6751		135.02	si	
4	-2487.	40.6	20	3.14		.6751		135.02	si	
5	-2497.	40.6	20	3.14		.6751		135.02	si	
6	-2507.	40.6	20	3.14		.6751		135.02	si	
7	-2517.	40.6	20	3.14		.6751		135.02	si	
8	-2527.	40.6	20	3.14		.6751		135.02	si	
9	-2538.	40.6	20	3.14		.6751		135.02	si	
10	-2548.	40.6	20	3.14		.6751		135.02	si	
11	-2558.	40.6	20	3.14		.6751		135.02	si	
12	-2568.	40.6	20	3.14		.6751		135.02	si	
13	-2578.	40.6	20	3.14		.6751		135.02	si	
14	-2589.	40.6	20	3.14		.6751		135.02	si	
15	-2599.	40.6	20	3.14		.6751		135.02	si	
16	-2609.	40.6	20	3.14		.6751		135.02	si	
17	-2619.	40.6	20	3.14		.6751		135.02	si	
18	-2629.	40.6	20	3.14		.6751		135.02	si	
19	-2639.	40.6	20	3.14		.6751		135.02	si	
20	-2650.	40.6	20	3.14		.6751		135.02	si	
21	-2660.	40.6	20	3.14		.6751		135.02	si	
22	-2670.	40.6	20	3.14		.6751		135.02	si	
23	-2456.	67.6	20	3.14	1.36711		273.42	si		
24	-2466.	67.6	20	3.14	1.36711		273.42	si		
25	-2476.	67.6	20	3.14	1.36711		273.42	si		
26	-2487.	67.6	20	3.14	1.36711		273.42	si		
27	-2497.	67.6	20	3.14	1.36711		273.42	si		
28	-2507.	67.6	20	3.14	1.36711		273.42	si		
29	-2517.	67.6	20	3.14	1.36711		273.42	si		
30	-2527.	67.6	20	3.14	1.36711		273.42	si		
31	-2538.	67.6	20	3.14	1.36711		273.42	si		
32	-2548.	67.6	20	3.14	1.36711		273.42	si		
33	-2558.	67.6	20	3.14	1.36711		273.42	si		
34	-2568.	67.6	20	3.14	1.36711		273.42	si		
35	-2578.	67.6	20	3.14	1.36711		273.42	si		
36	-2589.	67.6	20	3.14	1.36711		273.42	si		
37	-2599.	67.6	20	3.14	1.36711		273.42	si		
38	-2609.	67.6	20	3.14	1.36711		273.42	si		
39	-2619.	67.6	20	3.14	1.36711		273.42	si		
40	-2629.	67.6	20	3.14	1.36711		273.42	si		
41	-2639.	67.6	20	3.14	1.36711		273.42	si		
42	-2650.	67.6	20	3.14	1.36711		273.42	si		
43	-2660.	67.6	20	3.14	1.36711		273.42	si		
44	-2670.	67.6	20	3.14	1.36711		273.42	si		
45	-2456.	-8.4	20	3.14	-5.8077		-116.15	si		
46	-2473.	-8.4	20	3.14	-5.8077		-116.15	si		
47	-2489.	-8.4	20	3.14	-5.8077		-116.15	si		
48	-2505.	-8.4	20	3.14	-5.8077		-116.15	si		
49	-2522.	-8.4	20	3.14	-5.8077		-116.15	si		
50	-2538.	-8.4	20	3.14	-5.8077		-116.15	si		
51	-2555.	-8.4	20	3.14	-5.8077		-116.15	si		
52	-2571.	-8.4	20	3.14	-5.8077		-116.15	si		
53	-2588.	-8.4	20	3.14	-5.8077		-116.15	si		
54	-2604.	-8.4	20	3.14	-5.8077		-116.15	si		
55	-2621.	-8.4	20	3.14	-5.8077		-116.15	si		
56	-2637.	-8.4	20	3.14	-5.8077		-116.15	si		
57	-2654.	-8.4	20	3.14	-5.8077		-116.15	si		
58	-2670.	-8.4	20	3.14	-5.8077		-116.15	si		

% ARMAT.: tesa = .77; comp. = .24; tot. = 1.01

Ripristino Ponte-Tubo

VERIFICA PULVINO YZ 13

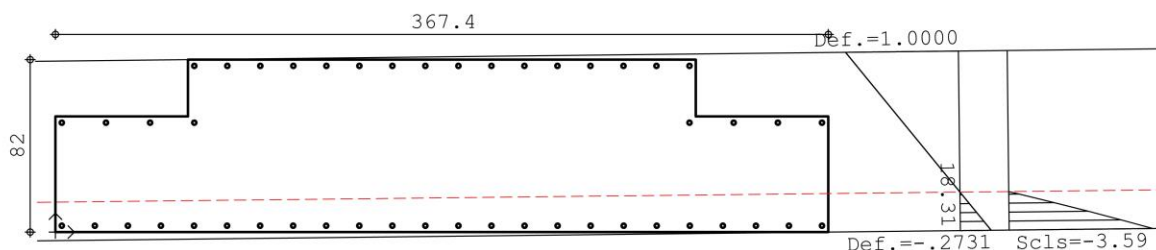
DESCRIZIONI
 Tipo sezione : U Pul
 Tipo verifica: stato limite ultimo

CARATTERISTICHE DEI MATERIALI
 Calcestruzzo: Rck= 30.
 fck= 24.9
 fcd= 14.11 (.35%)
 Acciaio lento: Tipo= B450C
 fyk= 450.
 ftk= 540.
 ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
 eps= muz * y + muy * z + lam
 muz= 1.49112852024972E-05
 muy= -1.65657212406477E-07
 lam= -2.12243567634978E-04

SOLLECITAZIONI AGENTI:
 Nd in z= 183.7; y= 37.5 (baricentro CLS)
 Nd = -77.44
 Mdz= -847.4793
 Mdy= 204.9076

UNITA' DI MISURA:
 kN; cm; kNm; N/mm2.
 Ø in mm; deformazioni*1000.
 SIMBOLI:
 S=sigma (tensioni sui materiali);
 D=deformazioni (epsilon):



TENSIONI NEL CLS:			Dcls	Scsls	Vel
ver	Z	Y			
1	0.	55.	.60788	0.	si
2	63.	55.	.59744	0.	si
3	63.	82.	1.00005	0.	si
4	304.4	82.	.96006	0.	si
5	304.4	55.	.55745	0.	si
6	367.4	55.	.54701	0.	si
7	367.4	0.	-.27311	-3.59	si
8	0.	0.	-.21224	-2.84	si

TENSIONI NEI FERRI:									
Fer	Z	Y	Ø (mm)	Af (cm2)	D	ferr	S	ferr	Vel
1	301.4	79.	20	3.14	3.14	.91582		183.16	si
2	285.7	79.	20	3.14	3.14	.91842		183.68	si
3	270.	79.	20	3.14	3.14	.92102		184.2	si
4	254.3	79.	20	3.14	3.14	.92362		184.72	si
5	238.6	79.	20	3.14	3.14	.92622		185.24	si
6	222.9	79.	20	3.14	3.14	.92882		185.76	si
7	207.2	79.	20	3.14	3.14	.93142		186.28	si
8	191.5	79.	20	3.14	3.14	.93402		186.8	si
9	175.9	79.	20	3.14	3.14	.93662		187.32	si
10	160.2	79.	20	3.14	3.14	.93922		187.84	si
11	144.5	79.	20	3.14	3.14	.94182		188.36	si
12	128.8	79.	20	3.14	3.14	.94442		188.88	si
13	113.1	79.	20	3.14	3.14	.94702		189.4	si
14	97.4	79.	20	3.14	3.14	.94962		189.92	si
15	81.7	79.	20	3.14	3.14	.95222		190.44	si
16	66.	79.	20	3.14	3.14	.95481		190.96	si
17	66.	52.	20	3.14	3.14	.55221		110.44	si
18	45.	52.	20	3.14	3.14	.55569		111.14	si
19	24.	52.	20	3.14	3.14	.55917		111.83	si
20	3.	52.	20	3.14	3.14	.56265		112.53	si
21	364.4	52.	20	3.14	3.14	.50278		100.56	si
22	343.4	52.	20	3.14	3.14	.50626		101.25	si
23	322.4	52.	20	3.14	3.14	.50974		101.95	si
24	301.4	52.	20	3.14	3.14	.51321		102.64	si
25	364.4	3.	20	3.14	3.14	-.22788		-45.58	si
26	348.7	3.	20	3.14	3.14	-.22527		-45.05	si
27	333.	3.	20	3.14	3.14	-.22267		-44.53	si
28	317.3	3.	20	3.14	3.14	-.22007		-44.01	si
29	301.5	3.	20	3.14	3.14	-.21746		-43.49	si
30	285.8	3.	20	3.14	3.14	-.21486		-42.97	si
31	270.1	3.	20	3.14	3.14	-.21226		-42.45	si
32	254.4	3.	20	3.14	3.14	-.20965		-41.93	si
33	238.7	3.	20	3.14	3.14	-.20705		-41.41	si
34	223.	3.	20	3.14	3.14	-.20445		-40.89	si
35	207.3	3.	20	3.14	3.14	-.20185		-40.37	si
36	191.6	3.	20	3.14	3.14	-.19924		-39.85	si
37	175.8	3.	20	3.14	3.14	-.19664		-39.33	si
38	160.1	3.	20	3.14	3.14	-.19404		-38.81	si
39	144.4	3.	20	3.14	3.14	-.19143		-38.29	si
40	128.7	3.	20	3.14	3.14	-.18883		-37.77	si
41	113.	3.	20	3.14	3.14	-.18623		-37.25	si
42	97.3	3.	20	3.14	3.14	-.18362		-36.72	si
43	81.6	3.	20	3.14	3.14	-.18102		-36.2	si
44	65.9	3.	20	3.14	3.14	-.17842		-35.68	si
45	50.1	3.	20	3.14	3.14	-.17582		-35.16	si
46	34.4	3.	20	3.14	3.14	-.17321		-34.64	si
47	18.7	3.	20	3.14	3.14	-.17061		-34.12	si
48	3.	3.	20	3.14	3.14	-.16801		-33.6	si

% ARMAT.: tesa= .28; comp.= .28; tot.= .56

Ripristino Ponte-Tubo

VERIFICA PULVINO XZ 14

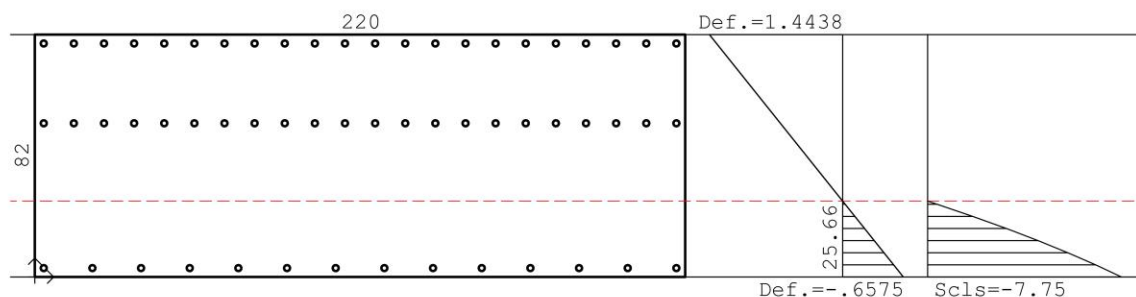
DESCRIZIONI
 Tipo sezione : RETTANGOLARE
 Tipo verifica: stato limite ultimo

CARATTERISTICHE DEI MATERIALI
 Calcestruzzo: Rck= 30.
 fck= 24.9
 fcd= 14.11 (.35%)
 Acciaio lento: Tipo= B450C
 fyk= 450.
 ftk= 540.
 ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
 eps= muz * y +muy * z + lam
 muz= 2.56258281680818E-05
 muy= 0
 lam=-3.64086261785591E-04

SOLLECITAZIONI AGENTI:
 Nd in y= 29.6 (baricentro CLS)
 Nd = -19.58
 Mdz=-1765.1075
 verifica in pressoflessione retta

UNITA' DI MISURA:
 kN; cm; kNm; N/mm2.
 Ø in mm; deformazioni*1000.
 SIMBOLI:
 S=sigma (tensioni sui materiali);
 D=deformazioni (epsilon):



TENSIONI NEL CLS:					
ver	Z	Y	Dcls	Scls	Vel
1	-2673.	70.6	1.44382	0.	si
2	-2453.	70.6	1.44382	0.	si
3	-2453.	-11.4	-.6575	-7.75	si
4	-2673.	-11.4	-.6575	-7.75	si

TENSIONI NEI FERRI:										
Fer	Z	Y	Ø (mm)	Af (cm2)	D	ferri	S	ferri	Vel	
1	-2456.	40.6	20	3.14		.67504		135.01	si	
2	-2456.	40.6	20	3.14		.67504		135.01	si	
3	-2476.	40.6	20	3.14		.67504		135.01	si	
4	-2487.	40.6	20	3.14		.67504		135.01	si	
5	-2497.	40.6	20	3.14		.67504		135.01	si	
6	-2507.	40.6	20	3.14		.67504		135.01	si	
7	-2517.	40.6	20	3.14		.67504		135.01	si	
8	-2527.	40.6	20	3.14		.67504		135.01	si	
9	-2538.	40.6	20	3.14		.67504		135.01	si	
10	-2548.	40.6	20	3.14		.67504		135.01	si	
11	-2558.	40.6	20	3.14		.67504		135.01	si	
12	-2568.	40.6	20	3.14		.67504		135.01	si	
13	-2578.	40.6	20	3.14		.67504		135.01	si	
14	-2589.	40.6	20	3.14		.67504		135.01	si	
15	-2599.	40.6	20	3.14		.67504		135.01	si	
16	-2609.	40.6	20	3.14		.67504		135.01	si	
17	-2619.	40.6	20	3.14		.67504		135.01	si	
18	-2629.	40.6	20	3.14		.67504		135.01	si	
19	-2639.	40.6	20	3.14		.67504		135.01	si	
20	-2650.	40.6	20	3.14		.67504		135.01	si	
21	-2660.	40.6	20	3.14		.67504		135.01	si	
22	-2670.	40.6	20	3.14		.67504		135.01	si	
23	-2456.	67.6	20	3.14	1.36694		273.39	si		
24	-2466.	67.6	20	3.14	1.36694		273.39	si		
25	-2476.	67.6	20	3.14	1.36694		273.39	si		
26	-2487.	67.6	20	3.14	1.36694		273.39	si		
27	-2497.	67.6	20	3.14	1.36694		273.39	si		
28	-2507.	67.6	20	3.14	1.36694		273.39	si		
29	-2517.	67.6	20	3.14	1.36694		273.39	si		
30	-2527.	67.6	20	3.14	1.36694		273.39	si		
31	-2538.	67.6	20	3.14	1.36694		273.39	si		
32	-2548.	67.6	20	3.14	1.36694		273.39	si		
33	-2558.	67.6	20	3.14	1.36694		273.39	si		
34	-2568.	67.6	20	3.14	1.36694		273.39	si		
35	-2578.	67.6	20	3.14	1.36694		273.39	si		
36	-2589.	67.6	20	3.14	1.36694		273.39	si		
37	-2599.	67.6	20	3.14	1.36694		273.39	si		
38	-2609.	67.6	20	3.14	1.36694		273.39	si		
39	-2619.	67.6	20	3.14	1.36694		273.39	si		
40	-2629.	67.6	20	3.14	1.36694		273.39	si		
41	-2639.	67.6	20	3.14	1.36694		273.39	si		
42	-2650.	67.6	20	3.14	1.36694		273.39	si		
43	-2660.	67.6	20	3.14	1.36694		273.39	si		
44	-2670.	67.6	20	3.14	1.36694		273.39	si		
45	-2456.	-8.4	20	3.14	-.58062		-116.12	si		
46	-2473.	-8.4	20	3.14	-.58062		-116.12	si		
47	-2489.	-8.4	20	3.14	-.58062		-116.12	si		
48	-2505.	-8.4	20	3.14	-.58062		-116.12	si		
49	-2522.	-8.4	20	3.14	-.58062		-116.12	si		
50	-2538.	-8.4	20	3.14	-.58062		-116.12	si		
51	-2555.	-8.4	20	3.14	-.58062		-116.12	si		
52	-2571.	-8.4	20	3.14	-.58062		-116.12	si		
53	-2588.	-8.4	20	3.14	-.58062		-116.12	si		
54	-2604.	-8.4	20	3.14	-.58062		-116.12	si		
55	-2621.	-8.4	20	3.14	-.58062		-116.12	si		
56	-2637.	-8.4	20	3.14	-.58062		-116.12	si		
57	-2654.	-8.4	20	3.14	-.58062		-116.12	si		
58	-2670.	-8.4	20	3.14	-.58062		-116.12	si		

% ARMAT.: tesa = .77; comp. = .24; tot. = 1.01

Ripristino Ponte-Tubo

VERIFICA PULVINO YZ 14

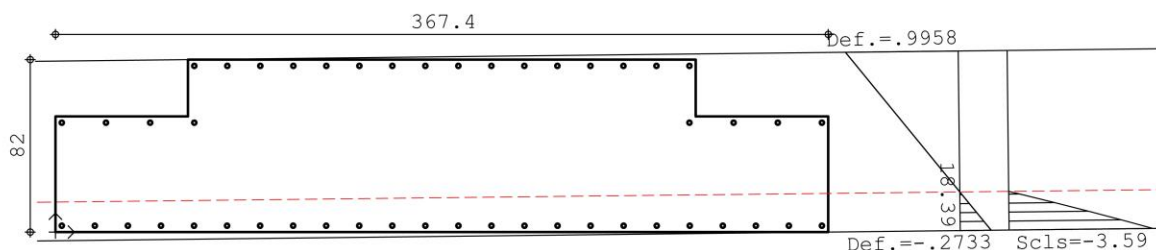
DESCRIZIONI
 Tipo sezione : U Pul
 Tipo verifica: sFato limite ultimo

CARATTERISTICHE DEI MATERIALI
 Calcestruzzo: Rck= 30.
 fck= 24.9
 fcd= 14.11 (.35%)
 Acciaio lento: Tipo= B450C
 fyk= 450.
 ftk= 540.
 ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
 eps= muz * y +muy * z + lam
 muz= 1.48594883671033E-05
 muy=-1.66478036928512E-07
 lam=-2.12161229763267E-04

SOLLECITAZIONI AGENTI:
 Nd in z= 183.7; y= 37.5 (baricentro CLS)
 Nd = -87.38
 Mdz= -846.7349
 Mdy= 206.4791

UNITA' DI MISURA:
 kN; cm; kNm; N/mm2.
 Ø in mm; deformazioni*1000.
 SIMBOLI:
 S=sigma (tensioni sui materiali);
 D=deformazioni (epsilon):



TENSIONI NEL CLS:			Dcls	Scsls	Vel
ver	Z	Y			
1	0.	55.	.60511	0.	si
2	63.	55.	.59462	0.	si
3	63.	82.	.99583	0.	si
4	304.4	82.	.95564	0.	si
5	304.4	55.	.55443	0.	si
6	367.4	55.	.54395	0.	si
7	367.4	0.	-.27333	-3.59	si
8	0.	0.	-.21216	-2.83	si

TENSIONI NEI FERRI:									
Fer	Z	Y	Ø (mm)	Af (cm2)	D	ferri	S	ferri	Vel
1	301.4	79.	20	3.14	3.14	.91156		182.31	si
2	285.7	79.	20	3.14	3.14	.91417		182.83	si
3	270.	79.	20	3.14	3.14	.91679		183.36	si
4	254.3	79.	20	3.14	3.14	.9194		183.88	si
5	238.6	79.	20	3.14	3.14	.92201		184.4	si
6	222.9	79.	20	3.14	3.14	.92462		184.92	si
7	207.2	79.	20	3.14	3.14	.92724		185.45	si
8	191.5	79.	20	3.14	3.14	.92985		185.97	si
9	175.9	79.	20	3.14	3.14	.93246		186.49	si
10	160.2	79.	20	3.14	3.14	.93508		187.02	si
11	144.5	79.	20	3.14	3.14	.93769		187.54	si
12	128.8	79.	20	3.14	3.14	.9403		188.06	si
13	113.1	79.	20	3.14	3.14	.94291		188.58	si
14	97.4	79.	20	3.14	3.14	.94553		189.11	si
15	81.7	79.	20	3.14	3.14	.94814		189.63	si
16	66.	79.	20	3.14	3.14	.95075		190.15	si
17	66.	52.	20	3.14	3.14	.54954		109.91	si
18	45.	52.	20	3.14	3.14	.55304		110.61	si
19	24.	52.	20	3.14	3.14	.55654		111.31	si
20	3.	52.	20	3.14	3.14	.56003		112.01	si
21	364.4	52.	20	3.14	3.14	.49987		99.97	si
22	343.4	52.	20	3.14	3.14	.50336		100.67	si
23	322.4	52.	20	3.14	3.14	.50686		101.37	si
24	301.4	52.	20	3.14	3.14	.51036		102.07	si
25	364.4	3.	20	3.14	3.14	-.22825		-45.65	si
26	348.7	3.	20	3.14	3.14	-.22563		-45.13	si
27	333.	3.	20	3.14	3.14	-.22302		-44.6	si
28	317.3	3.	20	3.14	3.14	-.2204		-44.08	si
29	301.5	3.	20	3.14	3.14	-.21778		-43.56	si
30	285.8	3.	20	3.14	3.14	-.21517		-43.03	si
31	270.1	3.	20	3.14	3.14	-.21255		-42.51	si
32	254.4	3.	20	3.14	3.14	-.20994		-41.99	si
33	238.7	3.	20	3.14	3.14	-.20732		-41.46	si
34	223.	3.	20	3.14	3.14	-.2047		-40.94	si
35	207.3	3.	20	3.14	3.14	-.20209		-40.42	si
36	191.6	3.	20	3.14	3.14	-.19947		-39.89	si
37	175.8	3.	20	3.14	3.14	-.19686		-39.37	si
38	160.1	3.	20	3.14	3.14	-.19424		-38.85	si
39	144.4	3.	20	3.14	3.14	-.19163		-38.33	si
40	128.7	3.	20	3.14	3.14	-.18901		-37.8	si
41	113.	3.	20	3.14	3.14	-.18639		-37.28	si
42	97.3	3.	20	3.14	3.14	-.18378		-36.76	si
43	81.6	3.	20	3.14	3.14	-.18116		-36.23	si
44	65.9	3.	20	3.14	3.14	-.17855		-35.71	si
45	50.1	3.	20	3.14	3.14	-.17593		-35.19	si
46	34.4	3.	20	3.14	3.14	-.17331		-34.66	si
47	18.7	3.	20	3.14	3.14	-.1707		-34.14	si
48	3.	3.	20	3.14	3.14	-.16808		-33.62	si

% ARMAT.: tesa = .28; comp. = .28; tot. = .56

Ripristino Ponte-Tubo
VERIFICA PULVINO XZ 15

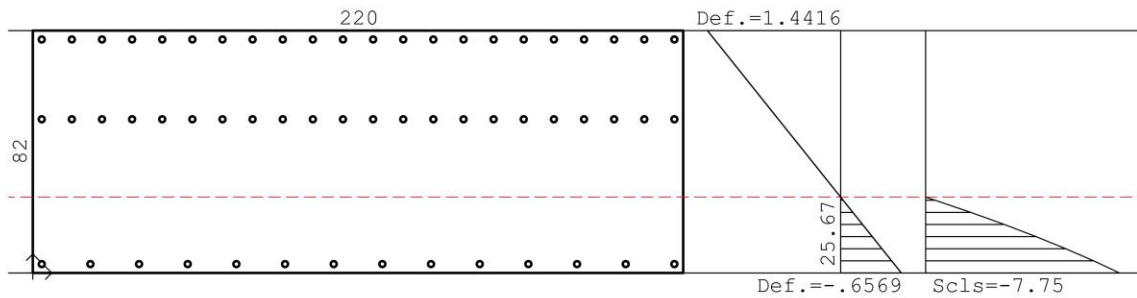
DESCRIZIONI
Tipo sezione : RETTANGOLARE
Tipo verifica: stato limite ultimo

CARATTERISTICHE DEI MATERIALI
Calcestruzzo: Rck= 30.
fck= 24.9
fcd= 14.11 (.35%)
Acciaio lento: Tipo= B450C
fyk= 450.
ftk= 540.
ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
eps= muz * y +muy * z + lam
muz= 2.55919631625576E-05
muy= 0
lam=-3.63884383079103E-04

SOLLECITAZIONI AGENTI:
Nd in y= 29.6 (baricentro CLS)
Nd = -22.81
Mdz=-1763.3182
verifica in pressoflessione retta

UNITA' DI MISURA:
kN; cm; kNm; N/mm2.
Ø in mm; deformazioni*1000.
SIMBOLI:
S=sigma (tensioni sui materiali);
D=deformazioni (epsilon):



TENSIONI NEL CLS:					
ver	Z	Y	Dcls	Scls	Vel
1	-2673.	70.6	1.44163	0.	si
2	-2453.	70.6	1.44163	0.	si
3	-2453.	-11.4	-65691	-7.75	si
4	-2673.	-11.4	-65691	-7.75	si

TENSIONI NEI FERRI:										
Fer	Z	Y	Ø (mm)	Af (cm2)	D	ferri	S	ferri	Vel	
1	-2456.	40.6	20	3.14		.67387		134.77	si	
3	-2466.	40.6	20	3.14		.67387		134.77	si	
3	-2476.	40.6	20	3.14		.67387		134.77	si	
4	-2487.	40.6	20	3.14		.67387		134.77	si	
5	-2497.	40.6	20	3.14		.67387		134.77	si	
6	-2507.	40.6	20	3.14		.67387		134.77	si	
7	-2517.	40.6	20	3.14		.67387		134.77	si	
8	-2527.	40.6	20	3.14		.67387		134.77	si	
9	-2538.	40.6	20	3.14		.67387		134.77	si	
10	-2548.	40.6	20	3.14		.67387		134.77	si	
11	-2558.	40.6	20	3.14		.67387		134.77	si	
12	-2568.	40.6	20	3.14		.67387		134.77	si	
13	-2578.	40.6	20	3.14		.67387		134.77	si	
14	-2589.	40.6	20	3.14		.67387		134.77	si	
15	-2599.	40.6	20	3.14		.67387		134.77	si	
16	-2609.	40.6	20	3.14		.67387		134.77	si	
17	-2619.	40.6	20	3.14		.67387		134.77	si	
18	-2629.	40.6	20	3.14		.67387		134.77	si	
19	-2639.	40.6	20	3.14		.67387		134.77	si	
20	-2650.	40.6	20	3.14		.67387		134.77	si	
21	-2660.	40.6	20	3.14		.67387		134.77	si	
22	-2670.	40.6	20	3.14		.67387		134.77	si	
23	-2456.	67.6	20	3.14	1.36485		272.97	si		
24	-2466.	67.6	20	3.14	1.36485		272.97	si		
25	-2476.	67.6	20	3.14	1.36485		272.97	si		
26	-2487.	67.6	20	3.14	1.36485		272.97	si		
27	-2497.	67.6	20	3.14	1.36485		272.97	si		
28	-2507.	67.6	20	3.14	1.36485		272.97	si		
29	-2517.	67.6	20	3.14	1.36485		272.97	si		
30	-2527.	67.6	20	3.14	1.36485		272.97	si		
31	-2538.	67.6	20	3.14	1.36485		272.97	si		
32	-2548.	67.6	20	3.14	1.36485		272.97	si		
33	-2558.	67.6	20	3.14	1.36485		272.97	si		
34	-2568.	67.6	20	3.14	1.36485		272.97	si		
35	-2578.	67.6	20	3.14	1.36485		272.97	si		
36	-2589.	67.6	20	3.14	1.36485		272.97	si		
37	-2599.	67.6	20	3.14	1.36485		272.97	si		
38	-2609.	67.6	20	3.14	1.36485		272.97	si		
39	-2619.	67.6	20	3.14	1.36485		272.97	si		
40	-2629.	67.6	20	3.14	1.36485		272.97	si		
41	-2639.	67.6	20	3.14	1.36485		272.97	si		
42	-2650.	67.6	20	3.14	1.36485		272.97	si		
43	-2660.	67.6	20	3.14	1.36485		272.97	si		
44	-2670.	67.6	20	3.14	1.36485		272.97	si		
45	-2456.	-8.4	20	3.14	-58014		-116.03	si		
46	-2473.	-8.4	20	3.14	-58014		-116.03	si		
47	-2489.	-8.4	20	3.14	-58014		-116.03	si		
48	-2505.	-8.4	20	3.14	-58014		-116.03	si		
49	-2522.	-8.4	20	3.14	-58014		-116.03	si		
50	-2538.	-8.4	20	3.14	-58014		-116.03	si		
51	-2555.	-8.4	20	3.14	-58014		-116.03	si		
52	-2571.	-8.4	20	3.14	-58014		-116.03	si		
53	-2588.	-8.4	20	3.14	-58014		-116.03	si		
54	-2604.	-8.4	20	3.14	-58014		-116.03	si		
55	-2621.	-8.4	20	3.14	-58014		-116.03	si		
56	-2637.	-8.4	20	3.14	-58014		-116.03	si		
57	-2654.	-8.4	20	3.14	-58014		-116.03	si		
58	-2670.	-8.4	20	3.14	-58014		-116.03	si		

% ARMAT.: tesa = .77; comp. = .24; tot. = 1.01

Ripristino Ponte-Tubo

VERIFICA PULVINO YZ 15

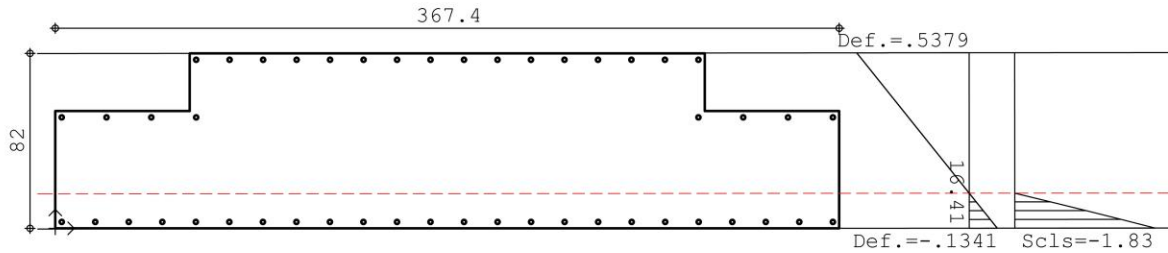
DESCRIZIONI
 Tipo sezione : U Pul
 Tipo verifica: sFato limite ultimo

CARATTERISTICHE DEI MATERIALI
 Calcestruzzo: Rck= 30.
 fck= 24.9
 fcd= 14.11 (.35%)
 Acciaio lento: Tipo= B450C
 fyk= 450.
 ftk= 540.
 ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
 eps= muz * y +muy * z + lam
 muz= 8.16868130803163E-06
 muy=-7.03312576293977E-09
 lam=-1.31489251673642E-04

SOLLECITAZIONI AGENTI:
 Nd in z= 183.7; y= 37.5 (baricentro CLS)
 Nd = -48.32
 Mdz= -466.79
 Mdy= 8.8764

UNITA' DI MISURA:
 kN; cm; kNm; N/mm2.
 Ø in mm; deformazioni*1000.
 SIMBOLI:
 S=sigma (tensioni sui materiali);
 D=deformazioni (epsilon):



TENSIONI NEL CLS:			Dcls	Scs	Ve
ver	Z	Y			
1	0.	55.	.31779	0.	si
2	63.	55.	.31735	0.	si
3	63.	82.	.5379	0.	si
4	304.4	82.	.5362	0.	si
5	304.4	55.	.31565	0.	si
6	367.4	55.	.3152	0.	si
7	367.4	0.	-.13407	-1.83	si
8	0.	0.	-.13149	-1.79	si

TENSIONI NEI FERRI:									
Fer	Z	Y	Ø (mm)	Af (cm2)	D	ferri	S	ferri	Ve
1	301.4	79.	20	3.14	3.14	.51172		102.34	si
2	285.7	79.	20	3.14	3.14	.51183		102.37	si
3	270.	79.	20	3.14	3.14	.51194		102.39	si
4	254.3	79.	20	3.14	3.14	.51205		102.41	si
5	238.6	79.	20	3.14	3.14	.51216		102.43	si
6	222.9	79.	20	3.14	3.14	.51227		102.45	si
7	207.2	79.	20	3.14	3.14	.51238		102.48	si
8	191.5	79.	20	3.14	3.14	.51249		102.5	si
9	175.9	79.	20	3.14	3.14	.5126		102.52	si
10	160.2	79.	20	3.14	3.14	.51271		102.54	si
11	144.5	79.	20	3.14	3.14	.51282		102.56	si
12	128.8	79.	20	3.14	3.14	.51293		102.59	si
13	113.1	79.	20	3.14	3.14	.51304		102.61	si
14	97.4	79.	20	3.14	3.14	.51315		102.63	si
15	81.7	79.	20	3.14	3.14	.51326		102.65	si
16	66.	79.	20	3.14	3.14	.51337		102.67	si
17	66.	52.	20	3.14	3.14	.29282		58.56	si
18	45.	52.	20	3.14	3.14	.29297		58.59	si
19	24.	52.	20	3.14	3.14	.29311		58.62	si
20	3.	52.	20	3.14	3.14	.29326		58.65	si
21	364.4	52.	20	3.14	3.14	.29072		58.14	si
22	343.4	52.	20	3.14	3.14	.29087		58.17	si
23	322.4	52.	20	3.14	3.14	.29101		58.2	si
24	301.4	52.	20	3.14	3.14	.29116		58.23	si
25	364.4	3.	20	3.14	3.14	-.10955		-21.91	si
26	348.7	3.	20	3.14	3.14	-.10944		-21.89	si
27	333.	3.	20	3.14	3.14	-.10933		-21.87	si
28	317.3	3.	20	3.14	3.14	-.10921		-21.84	si
29	301.5	3.	20	3.14	3.14	-.1091		-21.82	si
30	285.8	3.	20	3.14	3.14	-.10899		-21.8	si
31	270.1	3.	20	3.14	3.14	-.10888		-21.78	si
32	254.4	3.	20	3.14	3.14	-.10877		-21.75	si
33	238.7	3.	20	3.14	3.14	-.10866		-21.73	si
34	223.	3.	20	3.14	3.14	-.10855		-21.71	si
35	207.3	3.	20	3.14	3.14	-.10844		-21.69	si
36	191.6	3.	20	3.14	3.14	-.10833		-21.67	si
37	175.8	3.	20	3.14	3.14	-.10822		-21.64	si
38	160.1	3.	20	3.14	3.14	-.10811		-21.62	si
39	144.4	3.	20	3.14	3.14	-.108		-21.6	si
40	128.7	3.	20	3.14	3.14	-.10789		-21.58	si
41	113.	3.	20	3.14	3.14	-.10778		-21.56	si
42	97.3	3.	20	3.14	3.14	-.10767		-21.53	si
43	81.6	3.	20	3.14	3.14	-.10756		-21.51	si
44	65.9	3.	20	3.14	3.14	-.10745		-21.49	si
45	50.1	3.	20	3.14	3.14	-.10734		-21.47	si
46	34.4	3.	20	3.14	3.14	-.10723		-21.45	si
47	18.7	3.	20	3.14	3.14	-.10711		-21.42	si
48	3.	3.	20	3.14	3.14	-.107		-21.4	si

% ARMAT.: tesa= .28; comp.= .28; tot.= .56