

CONSORZIO DI BONIFICA STORNARA E TARA

viale Magna Grecia, 240 - 74121 TARANTO

*"RIPRISTINO DEL PONTE TUBO DELL'IMPIANTO IRRIGUO CONSORTILE
SX BRADANO UBICATO IN ATTRAVERSAMENTO DELLA LAMA DI LATERZA"*
COMUNE DI CASTELLANETA (TARANTO)

PROGETTO DEFINITIVO

CIG 7845120DD0



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ELABORATO	DATA	SCALA	ALLEGATO
Verifica strutturale dei pulvini (stato di fatto)	02/2021	-	R.6.s.3

AGGIORNAMENTO	DATA	DESCRIZIONE

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VERIFICA PULVINI (armature effetto piastra):

PARAMETRI GENERALI

CASI DI CARICO:

Nome	Descrizione
1	SLU
2	SLU VENTOY
6	SLU con SISMAX PRINC
7	SLU con SISMAX PRINC
8	SLU con SISMAZ PRINC
13	SLU Solo Perm.

DATI:

tensione di snervamento acciaio (fyk):	450	N/mm ²
coefficiente sicurezza acciaio	: 1.15	
deformazione ultima acciaio	: 1.86	per mille
deformazione ultima cls	: 3.5	per mille
rapporto rottura/snervamento (k):	1	
resistenza cilindrica cls (fck):	24.9	N/mm ²
coefficiente sicurezza cls	: 1.5	
coefficiente riduttivo (alfa):	0.85	
copri ferro inferiore (asse armatura):	3	cm
copri ferro superiore (asse armatura):	3	cm

LEGENDA:

spess	= spessore guscio. Verifica effettuata su sezione BxH, con B=1 cm e H="spess" cm
Af	= area disposta al lembo teso, in cm ² al metro
Afc	= area disposta al lembo compresso, in cm ² al metro
Mom	= momento flettente [kNm/m]
Nor	= sforzo normale [kN]
epsC	= deformazione cls [per mille]
epsF	= deformazione acciaio [per mille]

NOTA:

Per gli elementi non dissipativi la permanenza in campo elastico è ottenuta limitando la deformazione dell'acciaio alla deformazione di snervamento (1.86 per mille) e quella del calcestruzzo al 2 per mille.

MACROGUSCIO: Pulvi no1

GUSCI	spess	INFERIORE ORIZZONTALE						INFERIORE VERTICALE							
		Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF		
101	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	3.	0.	0.00	0.01		
102	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01		
103	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01		
104	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	3.	0.	0.00	0.01		
105	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00		
106	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00		
107	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00		
108	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00		
109	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00		
110	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00		
111	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00		
112	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00		
113	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00		
114	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00		
115	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00		
116	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00		
117	55	20.52	20.52	9.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00		
118	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00		
119	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00		
120	55	20.52	20.52	9.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00		
121	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	3.	0.	0.00	0.01		
122	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	3.	0.	0.00	0.01		
123	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	3.	0.	0.00	0.01		
124	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	3.	0.	0.00	0.01		
GUSCI	spess	SUPERIORE ORIZZONTALE						SUPERIORE VERTICALE							
		Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF		
101	55	20.52	20.52	21.	0.	0.03	0.10	34.27	19.99	10.	0.	0.01	0.03		
102	55	20.52	20.52	203.	0.	0.33	0.98	34.27	19.99	8.	0.	0.01	0.02		
103	55	20.52	20.52	215.	0.	0.35	1.04	34.27	19.99	8.	0.	0.01	0.02		
104	55	20.52	20.52	20.	0.	0.03	0.10	34.27	19.99	10.	0.	0.01	0.03		
105	55	20.52	20.52	18.	0.	0.03	0.09	34.27	19.99	133.	0.	0.19	0.39		
106	55	20.52	20.52	209.	0.	0.34	1.01	34.27	19.99	128.	0.	0.18	0.38		
107	55	20.52	20.52	225.	0.	0.37	1.09	34.27	19.99	129.	0.	0.18	0.38		
108	55	20.52	20.52	17.	0.	0.03	0.08	34.27	19.99	137.	0.	0.19	0.41		
109	82	20.52	20.52	20.	0.	0.02	0.06	34.27	19.99	723.	0.	0.53	1.38		
110	82	20.52	20.52	225.	0.	0.19	0.71	34.27	19.99	722.	0.	0.52	1.38		
111	82	20.52	20.52	225.	0.	0.20	0.71	34.27	19.99	722.	0.	0.52	1.38		
112	82	20.52	20.52	19.	0.	0.02	0.06	34.27	19.99	722.	0.	0.52	1.38		
113	82	20.52	20.52	17.	0.	0.01	0.05	34.27	19.99	723.	0.	0.53	1.38		
114	82	20.52	20.52	224.	0.	0.19	0.70	34.27	19.99	722.	0.	0.52	1.38		
115	82	20.52	20.52	224.	0.	0.19	0.70	34.27	19.99	722.	0.	0.52	1.38		
116	82	20.52	20.52	16.	0.	0.01	0.05	34.27	19.99	723.	0.	0.53	1.38		
117	55	20.52	20.52	21.	0.	0.03	0.10	34.27	19.99	133.	0.	0.19	0.39		
118	55	20.52	20.52	215.	0.	0.35	1.04	34.27	19.99	127.	0.	0.18	0.38		
119	55	20.52	20.52	219.	0.	0.36	1.06	34.27	19.99	128.	0.	0.18	0.38		
120	55	20.52	20.52	19.	0.	0.03	0.09	34.27	19.99	137.	0.	0.19	0.40		
121	55	20.52	20.52	20.	0.	0.03	0.10	34.27	19.99	10.	0.	0.01	0.03		
122	55	20.52	20.52	203.	0.	0.33	0.98	34.27	19.99	8.	0.	0.01	0.02		
123	55	20.52	20.52	215.	0.	0.35	1.04	34.27	19.99	7.	0.	0.01	0.02		
124	55	20.52	20.52	19.	0.	0.03	0.09	34.27	19.99	10.	0.	0.01	0.03		
***** TAGLIO PERPENDI COLARE															
GUSCI	τx	τy	τt	GUSCI	τx	τy	τt	GUSCI	τx	τy	τt	GUSCI	τx	τy	τt
101	0.5	0.3	0.4	102	0.5	0.4	0.5	103	0.5	0.4	0.5	104	0.5	1.5	1.1
104	0.4	0.4	0.4	105	0.5	1.7	1.6	106	0.5	1.5	1.1	107	0.5	1.5	1.1
107	0.5	1.5	1.2	108	0.5	1.6	1.5	109	0.4	0.8	0.7	110	0.8	0.9	0.9
110	0.8	0.9	0.9	111	0.8	0.9	0.9	112	0.4	0.7	0.7				

113	0.4	0.7	0.7	114	0.8	0.9	0.9	115	0.8	0.9	0.9
116	0.4	0.7	0.7	117	0.5	1.6	1.5	118	0.5	1.5	1.1
119	0.5	1.5	1.1	120	0.5	1.6	1.5	121	0.5	0.3	0.4
122	0.4	0.3	0.5	123	0.5	0.4	0.5	124	0.5	0.3	0.4

VERIFICHE A PUNZONAMENTO

	Norm [kN]	beta	sigT [N/mm2]	Pcrit [cm]	Ro [%]	Acrit [cm2]	VRd, c [kN]	VEd [kN]	A staffe [cm2]	VRd, cs [kN]		
A	1	-2799.443	1.47	0.010	610.4	0.26	108271.4	1620.910	3628.900	73.0	-0.010	Sì

MACROGUSCIO: Pulvi no2

GUSCI	spess	INFERIORE ORIZZONTALE						INFERIORE VERTICALE					
		Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
201	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	33.	0.	0.05	0.16
202	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	27.	0.	0.04	0.13
203	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	24.	0.	0.04	0.12
204	55	20.52	20.52	21.	0.	0.03	0.10	19.99	34.27	30.	0.	0.04	0.15
205	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	18.	0.	0.03	0.09
206	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	35.	0.	0.05	0.17
207	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	38.	0.	0.06	0.19
208	55	20.52	20.52	20.	0.	0.03	0.10	19.99	34.27	47.	0.	0.07	0.23
209	82	20.52	20.52	9.	0.	0.01	0.03	19.99	34.27	0.	0.	0.00	0.00
210	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
211	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
212	82	20.52	20.52	18.	0.	0.02	0.06	19.99	34.27	0.	0.	0.00	0.00
213	82	20.52	20.52	9.	0.	0.01	0.03	19.99	34.27	0.	0.	0.00	0.00
214	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
215	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
216	82	20.52	20.52	18.	0.	0.02	0.06	19.99	34.27	0.	0.	0.00	0.00
217	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	16.	0.	0.02	0.08
218	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	33.	0.	0.05	0.16
219	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	36.	0.	0.05	0.18
220	55	20.52	20.52	20.	0.	0.03	0.09	19.99	34.27	46.	0.	0.07	0.23
221	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	32.	0.	0.05	0.16
222	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	26.	0.	0.04	0.13
223	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	23.	0.	0.03	0.11
224	55	20.52	20.52	20.	0.	0.03	0.10	19.99	34.27	30.	0.	0.04	0.15

GUSCI	spess	SUPERIORE ORIZZONTALE						SUPERIORE VERTICALE					
		Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
201	55	20.52	20.52	22.	0.	0.04	0.11	34.27	19.99	30.	0.	0.04	0.09
202	55	20.52	20.52	210.	0.	0.35	1.01	34.27	19.99	31.	0.	0.04	0.09
203	55	20.52	20.52	250.	0.	0.41	1.21	34.27	19.99	34.	0.	0.05	0.10
204	55	20.52	20.52	53.	0.	0.09	0.26	34.27	19.99	42.	0.	0.06	0.12
205	55	20.52	20.52	20.	0.	0.03	0.10	34.27	19.99	129.	0.	0.18	0.38
206	55	20.52	20.52	215.	0.	0.35	1.04	34.27	19.99	145.	0.	0.20	0.43
207	55	20.52	20.52	264.	0.	0.43	1.28	34.27	19.99	152.	0.	0.21	0.45
208	55	20.52	20.52	53.	0.	0.09	0.26	34.27	19.99	168.	0.	0.24	0.50
209	82	20.52	20.52	18.	0.	0.02	0.06	34.27	19.99	723.	0.	0.53	1.38
210	82	20.52	20.52	225.	0.	0.20	0.71	34.27	19.99	722.	0.	0.52	1.38
211	82	20.52	20.52	241.	0.	0.21	0.76	34.27	19.99	722.	0.	0.52	1.38
212	82	20.52	20.52	24.	0.	0.02	0.07	34.27	19.99	723.	0.	0.53	1.38
213	82	20.52	20.52	17.	0.	0.01	0.05	34.27	19.99	721.	0.	0.52	1.38
214	82	20.52	20.52	223.	0.	0.19	0.70	34.27	19.99	721.	0.	0.52	1.38
215	82	20.52	20.52	232.	0.	0.20	0.73	34.27	19.99	721.	0.	0.52	1.38
216	82	20.52	20.52	28.	0.	0.02	0.09	34.27	19.99	721.	0.	0.52	1.38
217	55	20.52	20.52	21.	0.	0.03	0.10	34.27	19.99	129.	0.	0.18	0.38
218	55	20.52	20.52	221.	0.	0.36	1.07	34.27	19.99	142.	0.	0.20	0.42
219	55	20.52	20.52	247.	0.	0.41	1.19	34.27	19.99	149.	0.	0.21	0.44
220	55	20.52	20.52	57.	0.	0.09	0.27	34.27	19.99	165.	0.	0.23	0.49
221	55	20.52	20.52	21.	0.	0.04	0.10	34.27	19.99	28.	0.	0.04	0.08
222	55	20.52	20.52	210.	0.	0.35	1.02	34.27	19.99	30.	0.	0.04	0.09
223	55	20.52	20.52	238.	0.	0.39	1.15	34.27	19.99	33.	0.	0.05	0.10
224	55	20.52	20.52	56.	0.	0.09	0.27	34.27	19.99	41.	0.	0.06	0.12

***** TAGLIO PERPENDI COLARE

GUSCI	tx	ty	tz	GUSCI	tx	ty	tz	GUSCI	tx	ty	tz
201	0.5	0.3	0.4	202	0.5	0.4	0.5	203	0.5	0.4	0.5
204	0.4	0.4	0.4	205	0.5	1.7	1.6	206	0.5	1.5	1.2
207	0.5	1.5	1.1	208	0.5	1.6	1.5	209	0.4	0.8	0.7
210	0.8	0.9	0.9	211	0.8	0.9	0.9	212	0.4	0.7	0.7
213	0.4	0.7	0.7	214	0.8	0.9	0.9	215	0.8	0.9	0.9
216	0.4	0.7	0.7	217	0.5	1.6	1.5	218	0.5	1.5	1.1
219	0.5	1.5	1.1	220	0.5	1.6	1.5	221	0.5	0.3	0.4
222	0.5	0.4	0.5	223	0.5	0.3	0.5	224	0.5	0.3	0.4

VERIFICHE A PUNZONAMENTO

	Norm [kN]	beta	sigT [N/mm2]	Pcrit [cm]	Ro [%]	Acrit [cm2]	VRd, c [kN]	VEd [kN]	A staffe [cm2]	VRd, cs [kN]		
A	2	-2799.310	1.47	0.010	610.4	0.26	108271.4	1620.910	3628.680	73.0	-0.010	Sì

MACROGUSCIO: Pulvi no3

GUSCI	spess	INFERIORE ORIZZONTALE						INFERIORE VERTICALE					
		Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
301	55	20.52	20.52	12.	0.	0.02	0.06	19.99	34.27	5.	0.	0.01	0.03
302	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	3.	0.	0.01	0.02
303	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	3.	0.	0.01	0.02
304	55	20.52	20.52	11.	0.	0.02	0.06	19.99	34.27	4.	0.	0.01	0.02
305	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
306	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
307	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
308	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
309	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
310	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
311	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
312	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00

313	82	20.52	20.52	6.	0.	0.01	0.02	19.99	34.27	0.	0.	0.00	0.00
314	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
315	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
316	82	20.52	20.52	6.	0.	0.01	0.02	19.99	34.27	0.	0.	0.00	0.00
317	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
318	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
319	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
320	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
321	55	20.52	20.52	12.	0.	0.02	0.06	19.99	34.27	5.	0.	0.01	0.02
322	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	3.	0.	0.00	0.02
323	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	3.	0.	0.00	0.02
324	55	20.52	20.52	11.	0.	0.02	0.06	19.99	34.27	4.	0.	0.01	0.02

SUPERIORE ORIZZONTALE

SUPERIORE VERTICALE

GUSCI	spess	Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
301	55	20.52	20.52	21.	0.	0.03	0.10	34.27	19.99	12.	0.	0.02	0.03
302	55	20.52	20.52	220.	0.	0.36	1.06	34.27	19.99	10.	0.	0.01	0.03
303	55	20.52	20.52	207.	0.	0.34	1.00	34.27	19.99	7.	0.	0.01	0.02
304	55	20.52	20.52	19.	0.	0.03	0.09	34.27	19.99	8.	0.	0.01	0.02
305	55	20.52	20.52	18.	0.	0.03	0.09	34.27	19.99	136.	0.	0.19	0.40
306	55	20.52	20.52	230.	0.	0.38	1.11	34.27	19.99	128.	0.	0.18	0.38
307	55	20.52	20.52	219.	0.	0.36	1.06	34.27	19.99	126.	0.	0.18	0.37
308	55	20.52	20.52	18.	0.	0.03	0.09	34.27	19.99	133.	0.	0.19	0.39
309	82	20.52	20.52	15.	0.	0.01	0.05	34.27	19.99	736.	0.	0.53	1.41
310	82	20.52	20.52	230.	0.	0.20	0.72	34.27	19.99	735.	0.	0.53	1.41
311	82	20.52	20.52	229.	0.	0.20	0.72	34.27	19.99	735.	0.	0.53	1.41
312	82	20.52	20.52	15.	0.	0.01	0.05	34.27	19.99	736.	0.	0.53	1.41
313	82	20.52	20.52	18.	0.	0.02	0.06	34.27	19.99	730.	0.	0.53	1.40
314	82	20.52	20.52	228.	0.	0.20	0.72	34.27	19.99	729.	0.	0.53	1.40
315	82	20.52	20.52	229.	0.	0.20	0.72	34.27	19.99	729.	0.	0.53	1.40
316	82	20.52	20.52	18.	0.	0.02	0.06	34.27	19.99	729.	0.	0.53	1.40
317	55	20.52	20.52	20.	0.	0.03	0.10	34.27	19.99	136.	0.	0.19	0.40
318	55	20.52	20.52	224.	0.	0.37	1.08	34.27	19.99	127.	0.	0.18	0.38
319	55	20.52	20.52	214.	0.	0.35	1.03	34.27	19.99	126.	0.	0.18	0.37
320	55	20.52	20.52	18.	0.	0.03	0.09	34.27	19.99	133.	0.	0.19	0.39
321	55	20.52	20.52	22.	0.	0.04	0.11	34.27	19.99	11.	0.	0.02	0.03
322	55	20.52	20.52	220.	0.	0.36	1.06	34.27	19.99	9.	0.	0.01	0.03
323	55	20.52	20.52	207.	0.	0.34	1.00	34.27	19.99	6.	0.	0.01	0.02
324	55	20.52	20.52	21.	0.	0.03	0.10	34.27	19.99	9.	0.	0.01	0.03

***** TAGLIO PERPENDI COLARE

GUSCI	tx	ty	tz	GUSCI	tx	ty	tz	GUSCI	tx	ty	tz
301	0.5	0.4	0.4	302	0.5	0.4	0.5	303	0.5	0.4	0.5
304	0.4	0.4	0.4	305	0.5	1.7	1.6	306	0.5	1.5	1.2
307	0.5	1.5	1.1	308	0.5	1.6	1.6	309	0.3	0.8	0.8
310	0.8	0.9	0.9	311	0.8	0.9	0.9	312	0.4	0.7	0.7
313	0.3	0.7	0.7	314	0.8	0.9	0.9	315	0.8	0.9	0.9
316	0.3	0.7	0.7	317	0.5	1.6	1.5	318	0.5	1.5	1.1
319	0.5	1.5	1.1	320	0.5	1.6	1.5	321	0.5	0.3	0.4
322	0.5	0.3	0.5	323	0.5	0.3	0.5	324	0.5	0.3	0.4

VERIFICHE A PUNZONAMENTO

	Norm	beta	sigT	Pcrit	Ro	Acrit	Vrd, c	VEd	A staffe	Vrd, cs		
	[kN]		[N/mm2]	[cm]	[%]	[cm2]	[kN]	[kN]	[cm2]	[kN]		
A	3	-2799.405	1.47	0.010	610.4	0.26	108271.4	1620.910	3628.750	73.0	-0.010	Sì

MACROGUSCI 0: Pulvi no4

INFERIORE ORIZZONTALE

INFERIORE VERTICALE

GUSCI	spess	Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
401	55	20.52	20.52	11.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01
402	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
403	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
404	55	20.52	20.52	11.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01
405	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
406	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
407	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
408	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
409	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
410	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
411	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
412	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
413	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
414	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
415	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
416	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
417	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
418	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
419	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
420	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
421	55	20.52	20.52	11.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01
422	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
423	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
424	55	20.52	20.52	11.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01

SUPERIORE ORIZZONTALE

SUPERIORE VERTICALE

GUSCI	spess	Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
401	55	20.52	20.52	19.	0.	0.03	0.09	34.27	19.99	10.	0.	0.01	0.03
402	55	20.52	20.52	219.	0.	0.36	1.06	34.27	19.99	9.	0.	0.01	0.03
403	55	20.52	20.52	207.	0.	0.34	1.00	34.27	19.99	8.	0.	0.01	0.02
404	55	20.52	20.52	19.	0.	0.03	0.09	34.27	19.99	10.	0.	0.01	0.03
405	55	20.52	20.52	18.	0.	0.03	0.09	34.27	19.99	137.	0.	0.19	0.40
406	55	20.52	20.52	224.	0.	0.37	1.08	34.27	19.99	128.	0.	0.18	0.38
407	55	20.52	20.52	219.	0.	0.36	1.06	34.27	19.99	127.	0.	0.18	0.37
408	55	20.52	20.52	18.	0.	0.03	0.09	34.27	19.99	133.	0.	0.19	0.39
409	82	20.52	20.52	13.	0.	0.01	0.04	34.27	19.99	723.	0.	0.53	1.38
410	82	20.52	20.52	228.	0.	0.20	0.72	34.27	19.99	723.	0.	0.53	1.38
411	82	20.52	20.52	228.	0.	0.20	0.72	34.27	19.99	723.	0.	0.53	1.38
412	82	20.52	20.52	13.	0.	0.01	0.04	34.27	19.99	723.	0.	0.53	1.38

413	82	20.52	20.52	17.	0.	0.01	0.05	34.27	19.99	722.	0.	0.52	1.38
414	82	20.52	20.52	229.	0.	0.20	0.72	34.27	19.99	722.	0.	0.52	1.38
415	82	20.52	20.52	229.	0.	0.20	0.72	34.27	19.99	722.	0.	0.52	1.38
416	82	20.52	20.52	17.	0.	0.01	0.05	34.27	19.99	722.	0.	0.52	1.38
417	55	20.52	20.52	17.	0.	0.03	0.08	34.27	19.99	136.	0.	0.19	0.40
418	55	20.52	20.52	229.	0.	0.38	1.11	34.27	19.99	128.	0.	0.18	0.38
419	55	20.52	20.52	213.	0.	0.35	1.03	34.27	19.99	126.	0.	0.18	0.37
420	55	20.52	20.52	17.	0.	0.03	0.08	34.27	19.99	133.	0.	0.19	0.39
421	55	20.52	20.52	20.	0.	0.03	0.10	34.27	19.99	11.	0.	0.02	0.03
422	55	20.52	20.52	219.	0.	0.36	1.06	34.27	19.99	9.	0.	0.01	0.03
423	55	20.52	20.52	207.	0.	0.34	1.00	34.27	19.99	8.	0.	0.01	0.02
424	55	20.52	20.52	20.	0.	0.03	0.10	34.27	19.99	10.	0.	0.01	0.03

***** TAVOLO PERPENDI COLARE

GUSCI	tx	ty	tt	GUSCI	tx	ty	tt	GUSCI	tx	ty	tt
401	0.5	0.4	0.4	402	0.5	0.4	0.5	403	0.5	0.4	0.5
404	0.4	0.4	0.4	405	0.5	1.7	1.6	406	0.5	1.5	1.2
407	0.5	1.5	1.1	408	0.5	1.6	1.6	409	0.4	0.8	0.7
410	0.8	0.9	0.9	411	0.8	0.9	0.9	412	0.4	0.7	0.7
413	0.3	0.7	0.7	414	0.8	0.9	0.9	415	0.8	0.9	0.9
416	0.3	0.7	0.7	417	0.5	1.6	1.5	418	0.5	1.5	1.1
419	0.5	1.5	1.1	420	0.5	1.6	1.5	421	0.5	0.3	0.4
422	0.5	0.3	0.5	423	0.5	0.3	0.5	424	0.5	0.3	0.4

VERIFICHE A PUNZONAMENTO

	Norm	beta	sigT	Pcrit	Ro	Acrit	VRd, c	VEd	A staffe	VRd, cs		
	[kN]		[N/mm ²]	[cm]	[%]	[cm ²]	[kN]	[kN]	[cm ²]	[kN]		
A	4	-2799.447	1.47	0.010	610.4	0.26	108271.4	1620.910	3628.850	73.0	-0.010	Sì

MACROGUSCIO: Pulvi no5

INFERIORE ORIZZONTALE

GUSCI	spess	Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
501	55	20.52	20.52	11.	0.	0.02	0.05	19.99	34.27	3.	0.	0.00	0.01
502	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
503	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
504	55	20.52	20.52	11.	0.	0.02	0.05	19.99	34.27	3.	0.	0.00	0.01
505	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
506	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
507	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
508	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
509	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
510	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
511	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
512	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
513	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
514	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
515	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
516	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
517	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
518	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
519	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
520	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
521	55	20.52	20.52	11.	0.	0.02	0.05	19.99	34.27	3.	0.	0.00	0.01
522	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
523	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
524	55	20.52	20.52	11.	0.	0.02	0.05	19.99	34.27	3.	0.	0.00	0.01

SUPERIORE VERTICALE

SUPERIORE ORIZZONTALE

GUSCI	spess	Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
501	55	20.52	20.52	19.	0.	0.03	0.09	34.27	19.99	10.	0.	0.01	0.03
502	55	20.52	20.52	219.	0.	0.36	1.06	34.27	19.99	9.	0.	0.01	0.03
503	55	20.52	20.52	207.	0.	0.34	1.00	34.27	19.99	8.	0.	0.01	0.02
504	55	20.52	20.52	19.	0.	0.03	0.09	34.27	19.99	10.	0.	0.01	0.03
505	55	20.52	20.52	18.	0.	0.03	0.09	34.27	19.99	137.	0.	0.19	0.40
506	55	20.52	20.52	223.	0.	0.37	1.08	34.27	19.99	128.	0.	0.18	0.38
507	55	20.52	20.52	219.	0.	0.36	1.06	34.27	19.99	127.	0.	0.18	0.37
508	55	20.52	20.52	18.	0.	0.03	0.09	34.27	19.99	133.	0.	0.19	0.39
509	82	20.52	20.52	13.	0.	0.01	0.04	34.27	19.99	723.	0.	0.53	1.38
510	82	20.52	20.52	228.	0.	0.20	0.72	34.27	19.99	723.	0.	0.53	1.38
511	82	20.52	20.52	228.	0.	0.20	0.72	34.27	19.99	723.	0.	0.53	1.38
512	82	20.52	20.52	13.	0.	0.01	0.04	34.27	19.99	723.	0.	0.53	1.38
513	82	20.52	20.52	17.	0.	0.01	0.05	34.27	19.99	722.	0.	0.52	1.38
514	82	20.52	20.52	229.	0.	0.20	0.72	34.27	19.99	722.	0.	0.52	1.38
515	82	20.52	20.52	229.	0.	0.20	0.72	34.27	19.99	722.	0.	0.52	1.38
516	82	20.52	20.52	17.	0.	0.01	0.05	34.27	19.99	722.	0.	0.52	1.38
517	55	20.52	20.52	17.	0.	0.03	0.08	34.27	19.99	136.	0.	0.19	0.40
518	55	20.52	20.52	229.	0.	0.38	1.11	34.27	19.99	127.	0.	0.18	0.38
519	55	20.52	20.52	213.	0.	0.35	1.03	34.27	19.99	126.	0.	0.18	0.37
520	55	20.52	20.52	17.	0.	0.03	0.08	34.27	19.99	133.	0.	0.19	0.39
521	55	20.52	20.52	20.	0.	0.03	0.10	34.27	19.99	11.	0.	0.02	0.03
522	55	20.52	20.52	219.	0.	0.36	1.06	34.27	19.99	9.	0.	0.01	0.03
523	55	20.52	20.52	207.	0.	0.34	1.00	34.27	19.99	8.	0.	0.01	0.02
524	55	20.52	20.52	20.	0.	0.03	0.10	34.27	19.99	10.	0.	0.01	0.03

***** TAVOLO PERPENDI COLARE

GUSCI	tx	ty	tt	GUSCI	tx	ty	tt	GUSCI	tx	ty	tt
501	0.5	0.4	0.4	502	0.5	0.4	0.5	503	0.5	0.4	0.5
504	0.4	0.4	0.4	505	0.5	1.7	1.6	506	0.5	1.5	1.2
507	0.5	1.5	1.1	508	0.5	1.6	1.6	509	0.4	0.8	0.7
510	0.8	0.9	0.9	511	0.8	0.9	0.9	512	0.4	0.7	0.7
513	0.3	0.7	0.7	514	0.8	0.9	0.9	515	0.8	0.9	0.9
516	0.3	0.7	0.7	517	0.5	1.6	1.5	518	0.5	1.5	1.1
519	0.5	1.5	1.1	520	0.5	1.6	1.5	521	0.5	0.3	0.4
522	0.5	0.3	0.5	523	0.5	0.3	0.5	524	0.5	0.3	0.4

VERIFICHE A PUNZONAMENTO

	Norm	beta	sigT	Pcrit	Ro	Acrit	VRd, c	VEd	A staffe	VRd, cs		
	[kN]		[N/mm ²]	[cm]	[%]	[cm ²]	[kN]	[kN]	[cm ²]	[kN]		
A	5	-2799.461	1.47	0.010	610.4	0.26	108271.4	1620.910	3628.840	73.0	-0.010	Sì

MACROGUSCIO: Pulvi no6

MACROGUSCIO: Pulvi no6															
INFERIORE ORIZZONTALE								INFERIORE VERTICALE							
GUSCI	spess	Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF		
601	55	20.52	20.52	12.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01		
602	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01		
603	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01		
604	55	20.52	20.52	12.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01		
605	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00		
606	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00		
607	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00		
608	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00		
609	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00		
610	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00		
611	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00		
612	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00		
613	82	20.52	20.52	6.	0.	0.01	0.02	19.99	34.27	0.	0.	0.00	0.00		
614	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00		
615	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00		
616	82	20.52	20.52	6.	0.	0.01	0.02	19.99	34.27	0.	0.	0.00	0.00		
617	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00		
618	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00		
619	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00		
620	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00		
621	55	20.52	20.52	12.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01		
622	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01		
623	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01		
624	55	20.52	20.52	12.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01		
SUPERIORE ORIZZONTALE								SUPERIORE VERTICALE							
GUSCI	spess	Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF		
601	55	20.52	20.52	19.	0.	0.03	0.09	34.27	19.99	11.	0.	0.02	0.03		
602	55	20.52	20.52	220.	0.	0.36	1.06	34.27	19.99	9.	0.	0.01	0.03		
603	55	20.52	20.52	207.	0.	0.34	1.00	34.27	19.99	8.	0.	0.01	0.02		
604	55	20.52	20.52	19.	0.	0.03	0.09	34.27	19.99	10.	0.	0.01	0.03		
605	55	20.52	20.52	18.	0.	0.03	0.09	34.27	19.99	137.	0.	0.19	0.40		
606	55	20.52	20.52	224.	0.	0.37	1.08	34.27	19.99	128.	0.	0.18	0.38		
607	55	20.52	20.52	219.	0.	0.36	1.06	34.27	19.99	127.	0.	0.18	0.38		
608	55	20.52	20.52	18.	0.	0.03	0.09	34.27	19.99	133.	0.	0.19	0.39		
609	82	20.52	20.52	13.	0.	0.01	0.04	34.27	19.99	723.	0.	0.53	1.38		
610	82	20.52	20.52	228.	0.	0.20	0.72	34.27	19.99	723.	0.	0.53	1.38		
611	82	20.52	20.52	228.	0.	0.20	0.72	34.27	19.99	723.	0.	0.53	1.38		
612	82	20.52	20.52	13.	0.	0.01	0.04	34.27	19.99	724.	0.	0.53	1.39		
613	82	20.52	20.52	17.	0.	0.01	0.05	34.27	19.99	722.	0.	0.52	1.38		
614	82	20.52	20.52	229.	0.	0.20	0.72	34.27	19.99	722.	0.	0.52	1.38		
615	82	20.52	20.52	229.	0.	0.20	0.72	34.27	19.99	722.	0.	0.52	1.38		
616	82	20.52	20.52	17.	0.	0.01	0.05	34.27	19.99	723.	0.	0.53	1.38		
617	55	20.52	20.52	17.	0.	0.03	0.08	34.27	19.99	137.	0.	0.19	0.40		
618	55	20.52	20.52	230.	0.	0.38	1.11	34.27	19.99	128.	0.	0.18	0.38		
619	55	20.52	20.52	213.	0.	0.35	1.03	34.27	19.99	127.	0.	0.18	0.37		
620	55	20.52	20.52	17.	0.	0.03	0.08	34.27	19.99	133.	0.	0.19	0.39		
621	55	20.52	20.52	20.	0.	0.03	0.10	34.27	19.99	11.	0.	0.02	0.03		
622	55	20.52	20.52	220.	0.	0.36	1.06	34.27	19.99	9.	0.	0.01	0.03		
623	55	20.52	20.52	207.	0.	0.34	1.00	34.27	19.99	8.	0.	0.01	0.02		
624	55	20.52	20.52	20.	0.	0.03	0.10	34.27	19.99	10.	0.	0.01	0.03		
***** TAGLIO PERPENDI COLARE															
GUSCI	tx	ty	tz	GUSCI	tx	ty	tz	GUSCI	tx	ty	tz	GUSCI	tx	ty	tz
601	0.5	0.4	0.4	602	0.5	0.4	0.5	603	0.5	0.4	0.5	604	0.5	0.4	0.5
604	0.4	0.4	0.4	605	0.5	1.7	1.6	606	0.5	1.5	1.2	607	0.5	1.5	1.2
607	0.5	1.5	1.1	608	0.5	1.6	1.6	609	0.4	0.8	0.7	610	0.8	0.9	0.9
610	0.8	0.9	0.9	611	0.8	0.9	0.9	612	0.4	0.7	0.7	613	0.3	0.7	0.7
613	0.3	0.7	0.7	614	0.8	0.9	0.9	615	0.8	0.9	0.9	616	0.3	0.7	0.7
616	0.3	0.7	0.7	617	0.5	1.6	1.5	618	0.5	1.5	1.1	619	0.5	1.5	1.1
619	0.5	1.5	1.1	620	0.5	1.6	1.5	621	0.5	0.3	0.4	622	0.5	0.4	0.5
622	0.5	0.4	0.5	623	0.5	0.3	0.5	624	0.5	0.3	0.4				
VERIFICHE A PUNZONAMENTO															
A	Norm [kN]	beta	sigT [N/mm2]	Pcrit [cm]	Ro [%]	Acrit [cm2]	VRd, c [kN]	VEd [kN]	A staffe [cm2]	VRd, cs [kN]					
A	6 - 2799.448	1.47	0.010	610.4	0.26	108271.4	1620.910	3628.900	73.0	-0.010	Sì				

MACROGUSCIO: Pulvi no7

MACROGUSCIO: Pulvi no7													
INFERIORE ORIZZONTALE								INFERIORE VERTICALE					
GUSCI	spess	Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
701	55	20.52	20.52	11.	0.	0.02	0.05	19.99	34.27	3.	0.	0.00	0.01
702	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
703	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
704	55	20.52	20.52	12.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01
705	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
706	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
707	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
708	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
709	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
710	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
711	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
712	82	20.52	20.52	6.	0.	0.01	0.02	19.99	34.27	0.	0.	0.00	0.00
713	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
714	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
715	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
716	82	20.52	20.52	6.	0.	0.01	0.02	19.99	34.27	0.	0.	0.00	0.00
717	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
718	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
719	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
720	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00

721	55	20.52	20.52	11.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01
722	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
723	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
724	55	20.52	20.52	12.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01
				SUPERIORE ORIZZONTALE				SUPERIORE VERTICALE					
GUSCI	spess	Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
701	55	20.52	20.52	19.	0.	0.03	0.09	34.27	19.99	11.	0.	0.01	0.03
702	55	20.52	20.52	218.	0.	0.36	1.06	34.27	19.99	9.	0.	0.01	0.03
703	55	20.52	20.52	208.	0.	0.34	1.00	34.27	19.99	8.	0.	0.01	0.02
704	55	20.52	20.52	19.	0.	0.03	0.09	34.27	19.99	11.	0.	0.02	0.03
705	55	20.52	20.52	18.	0.	0.03	0.09	34.27	19.99	137.	0.	0.19	0.40
706	55	20.52	20.52	222.	0.	0.37	1.07	34.27	19.99	128.	0.	0.18	0.38
707	55	20.52	20.52	221.	0.	0.36	1.07	34.27	19.99	127.	0.	0.18	0.38
708	55	20.52	20.52	18.	0.	0.03	0.09	34.27	19.99	135.	0.	0.19	0.40
709	82	20.52	20.52	13.	0.	0.01	0.04	34.27	19.99	727.	0.	0.53	1.39
710	82	20.52	20.52	228.	0.	0.20	0.72	34.27	19.99	727.	0.	0.53	1.39
711	82	20.52	20.52	231.	0.	0.20	0.73	34.27	19.99	727.	0.	0.53	1.39
712	82	20.52	20.52	13.	0.	0.01	0.04	34.27	19.99	727.	0.	0.53	1.39
713	82	20.52	20.52	17.	0.	0.01	0.05	34.27	19.99	726.	0.	0.53	1.39
714	82	20.52	20.52	229.	0.	0.20	0.72	34.27	19.99	726.	0.	0.53	1.39
715	82	20.52	20.52	232.	0.	0.20	0.73	34.27	19.99	726.	0.	0.53	1.39
716	82	20.52	20.52	17.	0.	0.01	0.05	34.27	19.99	727.	0.	0.53	1.39
717	55	20.52	20.52	17.	0.	0.03	0.08	34.27	19.99	136.	0.	0.19	0.40
718	55	20.52	20.52	228.	0.	0.38	1.10	34.27	19.99	128.	0.	0.18	0.38
719	55	20.52	20.52	215.	0.	0.35	1.04	34.27	19.99	127.	0.	0.18	0.37
720	55	20.52	20.52	17.	0.	0.03	0.08	34.27	19.99	134.	0.	0.19	0.40
721	55	20.52	20.52	20.	0.	0.03	0.10	34.27	19.99	11.	0.	0.01	0.03
722	55	20.52	20.52	218.	0.	0.36	1.06	34.27	19.99	8.	0.	0.01	0.02
723	55	20.52	20.52	208.	0.	0.34	1.00	34.27	19.99	8.	0.	0.01	0.02
724	55	20.52	20.52	20.	0.	0.03	0.10	34.27	19.99	11.	0.	0.02	0.03
*****				TAGLIO PERPENDI COLARE									
GUSCI	tx	ty	tz	GUSCI	tx	ty	tz	GUSCI	tx	ty	tz		
701	0.5	0.4	0.4	702	0.5	0.4	0.5	703	0.5	0.4	0.5		
704	0.4	0.4	0.4	705	0.5	1.7	1.6	706	0.5	1.5	1.2		
707	0.5	1.5	1.1	708	0.5	1.6	1.6	709	0.4	0.8	0.7		
710	0.8	0.9	0.9	711	0.8	0.9	0.9	712	0.4	0.7	0.7		
713	0.3	0.7	0.7	714	0.8	0.9	0.9	715	0.8	0.9	0.9		
716	0.3	0.7	0.7	717	0.5	1.6	1.5	718	0.5	1.5	1.1		
719	0.5	1.5	1.1	720	0.5	1.6	1.5	721	0.5	0.3	0.4		
722	0.5	0.3	0.5	723	0.5	0.3	0.5	724	0.5	0.3	0.4		
				VERIFICHE A PUNZONAMENTO									
		Norm	beta	sigT	Pcrit	Ro	Acrit	VRd, c	VEd	A staffe	VRd, cs		
		[kN]		[N/mm2]	[cm]	[%]	[cm2]	[kN]	[kN]	[cm2]	[kN]		
A	7	-2817.466	1.47	0.010	610.4	0.26	108271.4	1620.910	3655.610	73.0	-0.010	Sì	

MACROGUSCI 0: Pulvi no8

				INFERIORE ORIZZONTALE				INFERIORE VERTICALE					
GUSCI	spess	Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
801	55	20.52	20.52	12.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01
802	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
803	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
804	55	20.52	20.52	12.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01
805	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
806	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
807	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
808	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
809	82	20.52	20.52	6.	0.	0.01	0.02	19.99	34.27	0.	0.	0.00	0.00
810	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
811	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
812	82	20.52	20.52	6.	0.	0.01	0.02	19.99	34.27	0.	0.	0.00	0.00
813	82	20.52	20.52	6.	0.	0.01	0.02	19.99	34.27	0.	0.	0.00	0.00
814	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
815	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
816	82	20.52	20.52	6.	0.	0.01	0.02	19.99	34.27	0.	0.	0.00	0.00
817	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
818	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
819	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
820	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
821	55	20.52	20.52	12.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01
822	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
823	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
824	55	20.52	20.52	12.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01
				SUPERIORE ORIZZONTALE				SUPERIORE VERTICALE					
GUSCI	spess	Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
801	55	20.52	20.52	19.	0.	0.03	0.09	34.27	19.99	11.	0.	0.02	0.03
802	55	20.52	20.52	222.	0.	0.37	1.07	34.27	19.99	9.	0.	0.01	0.03
803	55	20.52	20.52	210.	0.	0.35	1.01	34.27	19.99	8.	0.	0.01	0.02
804	55	20.52	20.52	19.	0.	0.03	0.09	34.27	19.99	10.	0.	0.01	0.03
805	55	20.52	20.52	18.	0.	0.03	0.09	34.27	19.99	139.	0.	0.19	0.41
806	55	20.52	20.52	226.	0.	0.37	1.09	34.27	19.99	130.	0.	0.18	0.38
807	55	20.52	20.52	222.	0.	0.37	1.07	34.27	19.99	129.	0.	0.18	0.38
808	55	20.52	20.52	18.	0.	0.03	0.09	34.27	19.99	135.	0.	0.19	0.40
809	82	20.52	20.52	13.	0.	0.01	0.04	34.27	19.99	733.	0.	0.53	1.40
810	82	20.52	20.52	231.	0.	0.20	0.72	34.27	19.99	732.	0.	0.53	1.40
811	82	20.52	20.52	231.	0.	0.20	0.73	34.27	19.99	732.	0.	0.53	1.40
812	82	20.52	20.52	13.	0.	0.01	0.04	34.27	19.99	733.	0.	0.53	1.40
813	82	20.52	20.52	17.	0.	0.01	0.05	34.27	19.99	732.	0.	0.53	1.40
814	82	20.52	20.52	232.	0.	0.20	0.73	34.27	19.99	731.	0.	0.53	1.40
815	82	20.52	20.52	232.	0.	0.20	0.73	34.27	19.99	731.	0.	0.53	1.40
816	82	20.52	20.52	17.	0.	0.01	0.05	34.27	19.99	732.	0.	0.53	1.40
817	55	20.52	20.52	17.	0.	0.03	0.08	34.27	19.99	138.	0.	0.19	0.41
818	55	20.52	20.52	232.	0.	0.38	1.12	34.27	19.99	129.	0.	0.18	0.38
819	55	20.52	20.52	216.	0.	0.36	1.04	34.27	19.99	128.	0.	0.18	0.38
820	55	20.52	20.52	17.	0.	0.03	0.08	34.27	19.99	135.	0.	0.19	0.40

821	55	20.52	20.52	20.	0.	0.03	0.10	34.27	19.99	11.	0.	0.02	0.03
822	55	20.52	20.52	222.	0.	0.37	1.07	34.27	19.99	9.	0.	0.01	0.03
823	55	20.52	20.52	210.	0.	0.35	1.01	34.27	19.99	8.	0.	0.01	0.02
824	55	20.52	20.52	20.	0.	0.03	0.10	34.27	19.99	10.	0.	0.01	0.03

***** TAGLIO PERPENDI COLARE

GUSCI	tx	ty	tz	GUSCI	tx	ty	tz	GUSCI	tx	ty	tz
801	0.5	0.4	0.4	802	0.5	0.4	0.5	803	0.5	0.4	0.5
804	0.4	0.4	0.4	805	0.5	1.7	1.6	806	0.5	1.6	1.2
807	0.5	1.5	1.1	808	0.5	1.6	1.6	809	0.4	0.8	0.7
810	0.8	0.9	0.9	811	0.8	0.9	0.9	812	0.4	0.7	0.7
813	0.3	0.7	0.7	814	0.8	0.9	0.9	815	0.8	0.9	0.9
816	0.4	0.7	0.7	817	0.5	1.6	1.5	818	0.5	1.5	1.1
819	0.5	1.5	1.1	820	0.5	1.6	1.5	821	0.5	0.3	0.4
822	0.5	0.4	0.5	823	0.5	0.3	0.5	824	0.5	0.3	0.4

VERIFICHE A PUNZONAMENTO

	Norm	beta	sigT	Pcrit	Ro	Acrit	VRd, c	VEd	A staffe	VRd, cs		
	[kN]		[N/mm ²]	[cm]	[%]	[cm ²]	[kN]	[kN]	[cm ²]	[kN]		
A	8	-2835.448	1.47	0.010	610.4	0.26	108271.4	1620.910	3681.760	73.0	-0.010	Sì

MACROGUSCIO: Pulvino9

GUSCI	spess	INFERIORE ORIZZONTALE						INFERIORE VERTICALE					
		Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
901	55	20.52	20.52	12.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.02
902	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
903	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
904	55	20.52	20.52	11.	0.	0.02	0.05	19.99	34.27	3.	0.	0.00	0.01
905	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
906	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
907	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
908	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
909	82	20.52	20.52	6.	0.	0.01	0.02	19.99	34.27	0.	0.	0.00	0.00
910	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
911	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
912	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
913	82	20.52	20.52	6.	0.	0.01	0.02	19.99	34.27	0.	0.	0.00	0.00
914	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
915	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
916	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
917	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
918	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
919	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
920	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
921	55	20.52	20.52	12.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.02
922	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
923	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
924	55	20.52	20.52	11.	0.	0.02	0.05	19.99	34.27	3.	0.	0.00	0.01

SUPERIORE ORIZZONTALE

SUPERIORE VERTICALE

GUSCI	spess	SUPERIORE ORIZZONTALE						SUPERIORE VERTICALE					
		Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
901	55	20.52	20.52	19.	0.	0.03	0.09	34.27	19.99	11.	0.	0.02	0.03
902	55	20.52	20.52	223.	0.	0.37	1.08	34.27	19.99	9.	0.	0.01	0.03
903	55	20.52	20.52	209.	0.	0.34	1.01	34.27	19.99	7.	0.	0.01	0.02
904	55	20.52	20.52	19.	0.	0.03	0.09	34.27	19.99	10.	0.	0.01	0.03
905	55	20.52	20.52	18.	0.	0.03	0.09	34.27	19.99	138.	0.	0.19	0.41
906	55	20.52	20.52	227.	0.	0.37	1.10	34.27	19.99	129.	0.	0.18	0.38
907	55	20.52	20.52	221.	0.	0.36	1.07	34.27	19.99	128.	0.	0.18	0.38
908	55	20.52	20.52	18.	0.	0.03	0.09	34.27	19.99	134.	0.	0.19	0.39
909	82	20.52	20.52	13.	0.	0.01	0.04	34.27	19.99	728.	0.	0.53	1.39
910	82	20.52	20.52	231.	0.	0.20	0.72	34.27	19.99	728.	0.	0.53	1.39
911	82	20.52	20.52	228.	0.	0.20	0.72	34.27	19.99	728.	0.	0.53	1.39
912	82	20.52	20.52	13.	0.	0.01	0.04	34.27	19.99	729.	0.	0.53	1.39
913	82	20.52	20.52	17.	0.	0.01	0.05	34.27	19.99	727.	0.	0.53	1.39
914	82	20.52	20.52	232.	0.	0.20	0.73	34.27	19.99	727.	0.	0.53	1.39
915	82	20.52	20.52	229.	0.	0.20	0.72	34.27	19.99	727.	0.	0.53	1.39
916	82	20.52	20.52	17.	0.	0.01	0.05	34.27	19.99	727.	0.	0.53	1.39
917	55	20.52	20.52	17.	0.	0.03	0.08	34.27	19.99	138.	0.	0.19	0.41
918	55	20.52	20.52	233.	0.	0.38	1.13	34.27	19.99	129.	0.	0.18	0.38
919	55	20.52	20.52	215.	0.	0.35	1.04	34.27	19.99	128.	0.	0.18	0.38
920	55	20.52	20.52	17.	0.	0.03	0.08	34.27	19.99	133.	0.	0.19	0.39
921	55	20.52	20.52	20.	0.	0.03	0.10	34.27	19.99	11.	0.	0.02	0.03
922	55	20.52	20.52	223.	0.	0.37	1.08	34.27	19.99	9.	0.	0.01	0.03
923	55	20.52	20.52	209.	0.	0.34	1.01	34.27	19.99	7.	0.	0.01	0.02
924	55	20.52	20.52	20.	0.	0.03	0.10	34.27	19.99	10.	0.	0.01	0.03

***** TAGLIO PERPENDI COLARE

GUSCI	tx	ty	tz	GUSCI	tx	ty	tz	GUSCI	tx	ty	tz
901	0.5	0.4	0.4	902	0.5	0.4	0.5	903	0.5	0.4	0.5
904	0.4	0.4	0.4	905	0.5	1.7	1.6	906	0.5	1.6	1.2
907	0.5	1.5	1.1	908	0.5	1.6	1.6	909	0.4	0.8	0.7
910	0.8	0.9	0.9	911	0.8	0.9	0.9	912	0.4	0.7	0.7
913	0.3	0.7	0.7	914	0.8	0.9	0.9	915	0.8	0.9	0.9
916	0.4	0.7	0.7	917	0.5	1.6	1.5	918	0.5	1.5	1.1
919	0.5	1.5	1.1	920	0.5	1.6	1.5	921	0.5	0.3	0.4
922	0.5	0.4	0.5	923	0.5	0.3	0.5	924	0.5	0.3	0.4

VERIFICHE A PUNZONAMENTO

	Norm	beta	sigT	Pcrit	Ro	Acrit	VRd, c	VEd	A staffe	VRd, cs		
	[kN]		[N/mm ²]	[cm]	[%]	[cm ²]	[kN]	[kN]	[cm ²]	[kN]		
A	9	-2817.459	1.47	0.010	610.4	0.26	108271.4	1620.910	3655.610	73.0	-0.010	Sì

MACROGUSCIO: Pulvino10

GUSCI	spess	INFERIORE ORIZZONTALE						INFERIORE VERTICALE					
		Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
1001	55	20.52	20.52	11.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01
1002	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01

1003	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
1004	55	20.52	20.52	11.	0.	0.02	0.05	19.99	34.27	3.	0.	0.00	0.01
1005	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
1006	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1007	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1008	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
1009	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
1010	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1011	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1012	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
1013	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
1014	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1015	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1016	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
1017	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
1018	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1019	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1020	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
1021	55	20.52	20.52	11.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01
1022	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
1023	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
1024	55	20.52	20.52	11.	0.	0.02	0.05	19.99	34.27	3.	0.	0.00	0.01

SUPERIORE ORIZZONTALE

SUPERIORE VERTICALE

GUSCI	spess	Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
1001	55	20.52	20.52	19.	0.	0.03	0.09	34.27	19.99	11.	0.	0.02	0.03
1002	55	20.52	20.52	219.	0.	0.36	1.06	34.27	19.99	9.	0.	0.01	0.03
1003	55	20.52	20.52	207.	0.	0.34	1.00	34.27	19.99	8.	0.	0.01	0.02
1004	55	20.52	20.52	19.	0.	0.03	0.09	34.27	19.99	10.	0.	0.01	0.03
1005	55	20.52	20.52	18.	0.	0.03	0.09	34.27	19.99	137.	0.	0.19	0.40
1006	55	20.52	20.52	223.	0.	0.37	1.08	34.27	19.99	128.	0.	0.18	0.38
1007	55	20.52	20.52	219.	0.	0.36	1.06	34.27	19.99	127.	0.	0.18	0.37
1008	55	20.52	20.52	18.	0.	0.03	0.09	34.27	19.99	133.	0.	0.19	0.39
1009	82	20.52	20.52	13.	0.	0.01	0.04	34.27	19.99	723.	0.	0.53	1.38
1010	82	20.52	20.52	228.	0.	0.20	0.71	34.27	19.99	723.	0.	0.53	1.38
1011	82	20.52	20.52	228.	0.	0.20	0.72	34.27	19.99	723.	0.	0.53	1.38
1012	82	20.52	20.52	13.	0.	0.01	0.04	34.27	19.99	723.	0.	0.53	1.38
1013	82	20.52	20.52	17.	0.	0.01	0.05	34.27	19.99	722.	0.	0.52	1.38
1014	82	20.52	20.52	229.	0.	0.20	0.72	34.27	19.99	722.	0.	0.52	1.38
1015	82	20.52	20.52	229.	0.	0.20	0.72	34.27	19.99	722.	0.	0.52	1.38
1016	82	20.52	20.52	17.	0.	0.01	0.05	34.27	19.99	722.	0.	0.52	1.38
1017	55	20.52	20.52	17.	0.	0.03	0.08	34.27	19.99	136.	0.	0.19	0.40
1018	55	20.52	20.52	229.	0.	0.38	1.11	34.27	19.99	128.	0.	0.18	0.38
1019	55	20.52	20.52	213.	0.	0.35	1.03	34.27	19.99	126.	0.	0.18	0.37
1020	55	20.52	20.52	17.	0.	0.03	0.08	34.27	19.99	133.	0.	0.19	0.39
1021	55	20.52	20.52	20.	0.	0.03	0.10	34.27	19.99	11.	0.	0.02	0.03
1022	55	20.52	20.52	219.	0.	0.36	1.06	34.27	19.99	9.	0.	0.01	0.03
1023	55	20.52	20.52	207.	0.	0.34	1.00	34.27	19.99	8.	0.	0.01	0.02
1024	55	20.52	20.52	20.	0.	0.03	0.10	34.27	19.99	10.	0.	0.01	0.03

***** TAGLIO PERPENDI COLARE

GUSCI	tx	ty	tz	GUSCI	tx	ty	tz	GUSCI	tx	ty	tz
1001	0.5	0.4	0.4	1002	0.5	0.4	0.5	1003	0.5	0.4	0.5
1004	0.4	0.4	0.4	1005	0.5	1.7	1.6	1006	0.5	1.5	1.2
1007	0.5	1.5	1.1	1008	0.5	1.6	1.6	1009	0.4	0.8	0.7
1010	0.8	0.9	0.9	1011	0.8	0.9	0.9	1012	0.4	0.7	0.7
1013	0.3	0.7	0.7	1014	0.8	0.9	0.9	1015	0.8	0.9	0.9
1016	0.3	0.7	0.7	1017	0.5	1.6	1.5	1018	0.5	1.5	1.1
1019	0.5	1.5	1.1	1020	0.5	1.6	1.5	1021	0.5	0.3	0.4
1022	0.5	0.3	0.5	1023	0.5	0.3	0.5	1024	0.5	0.3	0.4

VERIFICHE A PUNZONAMENTO

A	Norm [kN]	beta	sigT [N/mm2]	Pcrit [cm]	Ro [%]	Acrit [cm2]	VRd,c [kN]	VEd [kN]	A staffe [cm2]	VRd,cs [kN]		
A	10	-2799.449	1.47	0.010	610.4	0.26	108271.4	1620.910	3628.840	73.0	-0.010	Sì

MACROGUSCIO: Pulvino11

INFERIORE ORIZZONTALE

INFERIORE VERTICALE

GUSCI	spess	Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
1101	55	20.52	20.52	11.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01
1102	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
1103	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
1104	55	20.52	20.52	11.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01
1105	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
1106	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1107	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1108	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
1109	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
1110	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1111	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1112	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
1113	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
1114	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1115	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1116	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
1117	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
1118	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1119	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1120	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
1121	55	20.52	20.52	11.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01
1122	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
1123	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
1124	55	20.52	20.52	11.	0.	0.02	0.06	19.99	34.27	3.	0.	0.00	0.01

SUPERIORE ORIZZONTALE

SUPERIORE VERTICALE

GUSCI	spess	Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
1101	55	20.52	20.52	19.	0.	0.03	0.09	34.27	19.99	11.	0.	0.02	0.03
1102	55	20.52	20.52	219.	0.	0.36	1.06	34.27	19.99	9.	0.	0.01	0.03

1103	55	20.52	20.52	207.	0.	0.34	1.00	34.27	19.99	8.	0.	0.01	0.02
1104	55	20.52	20.52	19.	0.	0.03	0.09	34.27	19.99	10.	0.	0.01	0.03
1105	55	20.52	20.52	18.	0.	0.03	0.09	34.27	19.99	137.	0.	0.19	0.40
1106	55	20.52	20.52	224.	0.	0.37	1.08	34.27	19.99	128.	0.	0.18	0.38
1107	55	20.52	20.52	219.	0.	0.36	1.06	34.27	19.99	127.	0.	0.18	0.38
1108	55	20.52	20.52	18.	0.	0.03	0.09	34.27	19.99	133.	0.	0.19	0.39
1109	82	20.52	20.52	13.	0.	0.01	0.04	34.27	19.99	723.	0.	0.53	1.38
1110	82	20.52	20.52	228.	0.	0.20	0.71	34.27	19.99	723.	0.	0.53	1.38
1111	82	20.52	20.52	228.	0.	0.20	0.72	34.27	19.99	723.	0.	0.53	1.38
1112	82	20.52	20.52	13.	0.	0.01	0.04	34.27	19.99	724.	0.	0.53	1.38
1113	82	20.52	20.52	17.	0.	0.01	0.05	34.27	19.99	722.	0.	0.52	1.38
1114	82	20.52	20.52	229.	0.	0.20	0.72	34.27	19.99	722.	0.	0.52	1.38
1115	82	20.52	20.52	229.	0.	0.20	0.72	34.27	19.99	722.	0.	0.52	1.38
1116	82	20.52	20.52	17.	0.	0.01	0.05	34.27	19.99	722.	0.	0.52	1.38
1117	55	20.52	20.52	17.	0.	0.03	0.08	34.27	19.99	136.	0.	0.19	0.40
1118	55	20.52	20.52	229.	0.	0.38	1.11	34.27	19.99	128.	0.	0.18	0.38
1119	55	20.52	20.52	213.	0.	0.35	1.03	34.27	19.99	127.	0.	0.18	0.37
1120	55	20.52	20.52	17.	0.	0.03	0.08	34.27	19.99	133.	0.	0.19	0.39
1121	55	20.52	20.52	20.	0.	0.03	0.10	34.27	19.99	11.	0.	0.02	0.03
1122	55	20.52	20.52	219.	0.	0.36	1.06	34.27	19.99	9.	0.	0.01	0.03
1123	55	20.52	20.52	207.	0.	0.34	1.00	34.27	19.99	8.	0.	0.01	0.02
1124	55	20.52	20.52	20.	0.	0.03	0.10	34.27	19.99	10.	0.	0.01	0.03

***** TAGLIO PERPENDI COLARE

GUSCI	τx	τy	τt	GUSCI	τx	τy	τt	GUSCI	τx	τy	τt
1101	0.5	0.4	0.4	1102	0.5	0.4	0.5	1103	0.5	0.4	0.5
1104	0.4	0.4	0.4	1105	0.5	1.7	1.6	1106	0.5	1.5	1.2
1107	0.5	1.5	1.1	1108	0.5	1.6	1.6	1109	0.4	0.8	0.7
1110	0.8	0.9	0.9	1111	0.8	0.9	0.9	1112	0.4	0.7	0.7
1113	0.3	0.7	0.7	1114	0.8	0.9	0.9	1115	0.8	0.9	0.9
1116	0.3	0.7	0.7	1117	0.5	1.6	1.5	1118	0.5	1.5	1.1
1119	0.5	1.5	1.1	1120	0.5	1.6	1.5	1121	0.5	0.3	0.4
1122	0.5	0.4	0.5	1123	0.5	0.3	0.5	1124	0.5	0.3	0.4

VERIFICHE A PUNZONAMENTO

A	11	Norm [kN]	beta	sigT [N/mm2]	Pcrit [cm]	Ro [%]	Acrit [cm2]	VRd, c [kN]	VED [kN]	A staffe [cm2]	VRd, cs [kN]	Sì
		-2799.466	1.47	0.010	610.4	0.26	108271.4	1620.910	3628.940	73.0	-0.010	

MACROGUSCI 0: Pulvi no12

GUSCI	spess	INFERIORE ORIZZONTALE						INFERIORE VERTICALE					
		Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
1201	55	20.52	20.52	11.	0.	0.02	0.05	19.99	34.27	3.	0.	0.00	0.01
1202	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
1203	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
1204	55	20.52	20.52	11.	0.	0.02	0.05	19.99	34.27	3.	0.	0.00	0.01
1205	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
1206	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1207	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1208	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
1209	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
1210	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1211	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1212	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
1213	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
1214	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1215	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1216	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
1217	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
1218	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1219	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1220	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
1221	55	20.52	20.52	11.	0.	0.02	0.05	19.99	34.27	3.	0.	0.00	0.01
1222	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
1223	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
1224	55	20.52	20.52	11.	0.	0.02	0.05	19.99	34.27	3.	0.	0.00	0.01

SUPERIORE ORIZZONTALE

SUPERIORE VERTICALE

GUSCI	spess	SUPERIORE ORIZZONTALE						SUPERIORE VERTICALE					
		Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
1201	55	20.52	20.52	19.	0.	0.03	0.09	34.27	19.99	10.	0.	0.01	0.03
1202	55	20.52	20.52	219.	0.	0.36	1.06	34.27	19.99	9.	0.	0.01	0.03
1203	55	20.52	20.52	207.	0.	0.34	1.00	34.27	19.99	8.	0.	0.01	0.02
1204	55	20.52	20.52	19.	0.	0.03	0.09	34.27	19.99	10.	0.	0.01	0.03
1205	55	20.52	20.52	18.	0.	0.03	0.09	34.27	19.99	137.	0.	0.19	0.40
1206	55	20.52	20.52	223.	0.	0.37	1.08	34.27	19.99	128.	0.	0.18	0.38
1207	55	20.52	20.52	219.	0.	0.36	1.06	34.27	19.99	127.	0.	0.18	0.37
1208	55	20.52	20.52	18.	0.	0.03	0.09	34.27	19.99	133.	0.	0.19	0.39
1209	82	20.52	20.52	13.	0.	0.01	0.04	34.27	19.99	723.	0.	0.53	1.38
1210	82	20.52	20.52	227.	0.	0.20	0.71	34.27	19.99	723.	0.	0.52	1.38
1211	82	20.52	20.52	228.	0.	0.20	0.71	34.27	19.99	723.	0.	0.52	1.38
1212	82	20.52	20.52	13.	0.	0.01	0.04	34.27	19.99	723.	0.	0.53	1.38
1213	82	20.52	20.52	17.	0.	0.01	0.05	34.27	19.99	722.	0.	0.52	1.38
1214	82	20.52	20.52	229.	0.	0.20	0.72	34.27	19.99	722.	0.	0.52	1.38
1215	82	20.52	20.52	228.	0.	0.20	0.72	34.27	19.99	722.	0.	0.52	1.38
1216	82	20.52	20.52	17.	0.	0.01	0.05	34.27	19.99	722.	0.	0.52	1.38
1217	55	20.52	20.52	17.	0.	0.03	0.08	34.27	19.99	136.	0.	0.19	0.40
1218	55	20.52	20.52	229.	0.	0.38	1.11	34.27	19.99	128.	0.	0.18	0.38
1219	55	20.52	20.52	213.	0.	0.35	1.03	34.27	19.99	126.	0.	0.18	0.37
1220	55	20.52	20.52	17.	0.	0.03	0.08	34.27	19.99	133.	0.	0.19	0.39
1221	55	20.52	20.52	20.	0.	0.03	0.10	34.27	19.99	11.	0.	0.02	0.03
1222	55	20.52	20.52	219.	0.	0.36	1.06	34.27	19.99	9.	0.	0.01	0.03
1223	55	20.52	20.52	207.	0.	0.34	1.00	34.27	19.99	8.	0.	0.01	0.02
1224	55	20.52	20.52	20.	0.	0.03	0.10	34.27	19.99	10.	0.	0.01	0.03

***** TAGLIO PERPENDI COLARE

GUSCI	τx	τy	τt	GUSCI	τx	τy	τt	GUSCI	τx	τy	τt
1201	0.5	0.4	0.4	1202	0.5	0.4	0.5	1203	0.5	0.4	0.5
1204	0.4	0.4	0.4	1205	0.5	1.7	1.6	1206	0.5	1.5	1.2

1207	0.5	1.5	1.1	1208	0.5	1.6	1.5	1209	0.4	0.8	0.7
1210	0.8	0.9	0.9	1211	0.8	0.9	0.9	1212	0.4	0.7	0.7
1213	0.3	0.7	0.7	1214	0.8	0.9	0.9	1215	0.8	0.9	0.9
1216	0.3	0.7	0.7	1217	0.5	1.6	1.5	1218	0.5	1.5	1.1
1219	0.5	1.5	1.1	1220	0.5	1.6	1.5	1221	0.5	0.3	0.4
1222	0.5	0.3	0.5	1223	0.5	0.3	0.5	1224	0.5	0.3	0.4

VERIFICHE A PUNZONAMENTO

	Norm	beta	sigT	Pcrit	Ro	Acrit	VRd, c	Ved	A staffe	VRd, cs		
A	12	-2799.450	1.47	0.010	610.4	0.26	108271.4	1620.910	3628.820	73.0	-0.010	Sì
	[kN]		[N/mm2]	[cm]	[%]	[cm2]	[kN]	[kN]	[cm2]	[kN]		

MACROGUSCI0: Pulvi no13

GUSCI	spess	INFERIORE ORIZZONTALE						INFERIORE VERTICALE					
		Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
1301	55	20.52	20.52	11.	0.	0.02	0.05	19.99	34.27	3.	0.	0.00	0.01
1302	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
1303	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
1304	55	20.52	20.52	11.	0.	0.02	0.05	19.99	34.27	3.	0.	0.00	0.01
1305	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
1306	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1307	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1308	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
1309	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
1310	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1311	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1312	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
1313	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
1314	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1315	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1316	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
1317	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
1318	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1319	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1320	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
1321	55	20.52	20.52	11.	0.	0.02	0.05	19.99	34.27	3.	0.	0.00	0.01
1322	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
1323	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
1324	55	20.52	20.52	11.	0.	0.02	0.05	19.99	34.27	3.	0.	0.00	0.01

GUSCI	spess	SUPERIORE ORIZZONTALE						SUPERIORE VERTICALE					
		Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
1301	55	20.52	20.52	19.	0.	0.03	0.09	34.27	19.99	11.	0.	0.01	0.03
1302	55	20.52	20.52	219.	0.	0.36	1.06	34.27	19.99	9.	0.	0.01	0.03
1303	55	20.52	20.52	207.	0.	0.34	1.00	34.27	19.99	8.	0.	0.01	0.02
1304	55	20.52	20.52	19.	0.	0.03	0.09	34.27	19.99	10.	0.	0.01	0.03
1305	55	20.52	20.52	18.	0.	0.03	0.09	34.27	19.99	137.	0.	0.19	0.40
1306	55	20.52	20.52	223.	0.	0.37	1.08	34.27	19.99	128.	0.	0.18	0.38
1307	55	20.52	20.52	219.	0.	0.36	1.06	34.27	19.99	127.	0.	0.18	0.37
1308	55	20.52	20.52	18.	0.	0.03	0.09	34.27	19.99	133.	0.	0.19	0.39
1309	82	20.52	20.52	13.	0.	0.01	0.04	34.27	19.99	723.	0.	0.53	1.38
1310	82	20.52	20.52	228.	0.	0.20	0.71	34.27	19.99	723.	0.	0.53	1.38
1311	82	20.52	20.52	228.	0.	0.20	0.71	34.27	19.99	723.	0.	0.53	1.38
1312	82	20.52	20.52	13.	0.	0.01	0.04	34.27	19.99	723.	0.	0.53	1.38
1313	82	20.52	20.52	17.	0.	0.01	0.05	34.27	19.99	722.	0.	0.52	1.38
1314	82	20.52	20.52	229.	0.	0.20	0.72	34.27	19.99	722.	0.	0.52	1.38
1315	82	20.52	20.52	228.	0.	0.20	0.72	34.27	19.99	722.	0.	0.52	1.38
1316	82	20.52	20.52	17.	0.	0.01	0.05	34.27	19.99	722.	0.	0.52	1.38
1317	55	20.52	20.52	17.	0.	0.03	0.08	34.27	19.99	136.	0.	0.19	0.40
1318	55	20.52	20.52	229.	0.	0.38	1.11	34.27	19.99	128.	0.	0.18	0.38
1319	55	20.52	20.52	213.	0.	0.35	1.03	34.27	19.99	126.	0.	0.18	0.37
1320	55	20.52	20.52	17.	0.	0.03	0.08	34.27	19.99	133.	0.	0.19	0.39
1321	55	20.52	20.52	20.	0.	0.03	0.10	34.27	19.99	11.	0.	0.01	0.03
1322	55	20.52	20.52	219.	0.	0.36	1.06	34.27	19.99	9.	0.	0.01	0.03
1323	55	20.52	20.52	207.	0.	0.34	1.00	34.27	19.99	8.	0.	0.01	0.02
1324	55	20.52	20.52	20.	0.	0.03	0.10	34.27	19.99	10.	0.	0.01	0.03

***** TAGLIO PERPENDI COLARE

GUSCI	tx	ty	tz	GUSCI	tx	ty	tz	GUSCI	tx	ty	tz
1301	0.5	0.4	0.4	1302	0.5	0.4	0.5	1303	0.5	0.4	0.5
1304	0.4	0.4	0.4	1305	0.5	1.7	1.6	1306	0.5	1.5	1.2
1307	0.5	1.5	1.1	1308	0.5	1.6	1.5	1309	0.4	0.8	0.7
1310	0.8	0.9	0.9	1311	0.8	0.9	0.9	1312	0.4	0.7	0.7
1313	0.3	0.7	0.7	1314	0.8	0.9	0.9	1315	0.8	0.9	0.9
1316	0.3	0.7	0.7	1317	0.5	1.6	1.5	1318	0.5	1.5	1.1
1319	0.5	1.5	1.1	1320	0.5	1.6	1.5	1321	0.5	0.3	0.4
1322	0.5	0.3	0.5	1323	0.5	0.3	0.5	1324	0.5	0.3	0.4

VERIFICHE A PUNZONAMENTO

A	13	-2799.466	1.47	0.010	610.4	0.26	108271.4	1620.910	3628.900	73.0	-0.010	Sì
		[kN]		[N/mm2]	[cm]	[%]	[cm2]	[kN]	[kN]	[cm2]	[kN]	

MACROGUSCI0: Pulvi no14

GUSCI	spess	INFERIORE ORIZZONTALE						INFERIORE VERTICALE					
		Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
1401	55	20.52	20.52	11.	0.	0.02	0.05	19.99	34.27	3.	0.	0.00	0.01
1402	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
1403	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
1404	55	20.52	20.52	11.	0.	0.02	0.05	19.99	34.27	3.	0.	0.00	0.01
1405	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
1406	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1407	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1408	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
1409	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
1410	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00

1411	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1412	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
1413	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
1414	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1415	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1416	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
1417	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
1418	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1419	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1420	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
1421	55	20.52	20.52	11.	0.	0.02	0.05	19.99	34.27	3.	0.	0.00	0.01
1422	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
1423	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
1424	55	20.52	20.52	11.	0.	0.02	0.05	19.99	34.27	3.	0.	0.00	0.01
				SUPERIORE ORIZZONTALE				SUPERIORE VERTICALE					
GUSCI	spess	Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
1401	55	20.52	20.52	19.	0.	0.03	0.09	34.27	19.99	11.	0.	0.02	0.03
1402	55	20.52	20.52	219.	0.	0.36	1.06	34.27	19.99	9.	0.	0.01	0.03
1403	55	20.52	20.52	206.	0.	0.34	1.00	34.27	19.99	8.	0.	0.01	0.02
1404	55	20.52	20.52	19.	0.	0.03	0.09	34.27	19.99	10.	0.	0.01	0.03
1405	55	20.52	20.52	18.	0.	0.03	0.09	34.27	19.99	137.	0.	0.19	0.40
1406	55	20.52	20.52	223.	0.	0.37	1.08	34.27	19.99	128.	0.	0.18	0.38
1407	55	20.52	20.52	219.	0.	0.36	1.06	34.27	19.99	127.	0.	0.18	0.38
1408	55	20.52	20.52	18.	0.	0.03	0.09	34.27	19.99	133.	0.	0.19	0.39
1409	82	20.52	20.52	13.	0.	0.01	0.04	34.27	19.99	723.	0.	0.53	1.38
1410	82	20.52	20.52	227.	0.	0.20	0.71	34.27	19.99	723.	0.	0.53	1.38
1411	82	20.52	20.52	227.	0.	0.20	0.71	34.27	19.99	723.	0.	0.53	1.38
1412	82	20.52	20.52	13.	0.	0.01	0.04	34.27	19.99	723.	0.	0.53	1.38
1413	82	20.52	20.52	17.	0.	0.01	0.05	34.27	19.99	722.	0.	0.52	1.38
1414	82	20.52	20.52	229.	0.	0.20	0.72	34.27	19.99	722.	0.	0.52	1.38
1415	82	20.52	20.52	228.	0.	0.20	0.72	34.27	19.99	722.	0.	0.52	1.38
1416	82	20.52	20.52	17.	0.	0.01	0.05	34.27	19.99	722.	0.	0.52	1.38
1417	55	20.52	20.52	17.	0.	0.03	0.08	34.27	19.99	137.	0.	0.19	0.40
1418	55	20.52	20.52	229.	0.	0.38	1.11	34.27	19.99	128.	0.	0.18	0.38
1419	55	20.52	20.52	213.	0.	0.35	1.03	34.27	19.99	127.	0.	0.18	0.37
1420	55	20.52	20.52	17.	0.	0.03	0.08	34.27	19.99	133.	0.	0.19	0.39
1421	55	20.52	20.52	20.	0.	0.03	0.10	34.27	19.99	11.	0.	0.02	0.03
1422	55	20.52	20.52	219.	0.	0.36	1.06	34.27	19.99	9.	0.	0.01	0.03
1423	55	20.52	20.52	206.	0.	0.34	1.00	34.27	19.99	8.	0.	0.01	0.02
1424	55	20.52	20.52	20.	0.	0.03	0.10	34.27	19.99	10.	0.	0.01	0.03

***** TAGLIO PERPENDI COLARE

GUSCI	tx	ty	tz	GUSCI	tx	ty	tz	GUSCI	tx	ty	tz
1401	0.5	0.4	0.4	1402	0.5	0.4	0.5	1403	0.5	0.4	0.5
1404	0.4	0.4	0.4	1405	0.5	1.7	1.6	1406	0.5	1.5	1.2
1407	0.5	1.5	1.1	1408	0.5	1.6	1.5	1409	0.4	0.8	0.7
1410	0.8	0.9	0.9	1411	0.8	0.9	0.9	1412	0.4	0.7	0.7
1413	0.3	0.7	0.7	1414	0.8	0.9	0.9	1415	0.8	0.9	0.9
1416	0.4	0.7	0.7	1417	0.5	1.6	1.5	1418	0.5	1.5	1.1
1419	0.5	1.5	1.1	1420	0.5	1.6	1.5	1421	0.5	0.3	0.4
1422	0.5	0.4	0.5	1423	0.5	0.3	0.5	1424	0.5	0.3	0.4

VERIFICHE A PUNZONAMENTO

A	Norm [kN]	beta	sigT [N/mm2]	Pcrit [cm]	Ro [%]	Acrit [cm2]	VRd,c [kN]	VEd [kN]	A staffe [cm2]	VRd,cs [kN]		
A	14	-2799.454	1.47	0.010	610.4	0.26	108271.4	1620.910	3628.860	73.0	-0.010	Sì

MACROGUSCIO: Pulvino15

INFERIORE ORIZZONTALE								INFERIORE VERTICALE					
GUSCI	spess	Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
1501	55	20.52	20.52	11.	0.	0.02	0.05	19.99	34.27	3.	0.	0.00	0.01
1502	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
1503	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
1504	55	20.52	20.52	11.	0.	0.02	0.05	19.99	34.27	3.	0.	0.00	0.01
1505	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
1506	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1507	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1508	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
1509	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
1510	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1511	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1512	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
1513	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
1514	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1515	82	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1516	82	20.52	20.52	6.	0.	0.00	0.02	19.99	34.27	0.	0.	0.00	0.00
1517	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
1518	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1519	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	0.	0.	0.00	0.00
1520	55	20.52	20.52	10.	0.	0.02	0.05	19.99	34.27	0.	0.	0.00	0.00
1521	55	20.52	20.52	11.	0.	0.02	0.05	19.99	34.27	3.	0.	0.00	0.01
1522	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
1523	55	20.52	20.52	0.	0.	0.00	0.00	19.99	34.27	2.	0.	0.00	0.01
1524	55	20.52	20.52	11.	0.	0.02	0.05	19.99	34.27	3.	0.	0.00	0.01
SUPERIORE ORIZZONTALE								SUPERIORE VERTICALE					
GUSCI	spess	Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF
1501	55	20.52	20.52	19.	0.	0.03	0.09	34.27	19.99	11.	0.	0.01	0.03
1502	55	20.52	20.52	218.	0.	0.36	1.06	34.27	19.99	9.	0.	0.01	0.03
1503	55	20.52	20.52	206.	0.	0.34	1.00	34.27	19.99	8.	0.	0.01	0.02
1504	55	20.52	20.52	19.	0.	0.03	0.09	34.27	19.99	10.	0.	0.01	0.03
1505	55	20.52	20.52	18.	0.	0.03	0.09	34.27	19.99	137.	0.	0.19	0.40
1506	55	20.52	20.52	223.	0.	0.37	1.08	34.27	19.99	128.	0.	0.18	0.38
1507	55	20.52	20.52	218.	0.	0.36	1.06	34.27	19.99	127.	0.	0.18	0.38
1508	55	20.52	20.52	18.	0.	0.03	0.09	34.27	19.99	133.	0.	0.19	0.39
1509	82	20.52	20.52	13.	0.	0.01	0.04	34.27	19.99	723.	0.	0.53	1.38
1510	82	20.52	20.52	227.	0.	0.20	0.71	34.27	19.99	723.	0.	0.53	1.38

1511	82	20.52	20.52	227.	0.	0.20	0.71	34.27	19.99	723.	0.	0.53	1.38
1512	82	20.52	20.52	13.	0.	0.01	0.04	34.27	19.99	723.	0.	0.53	1.38
1513	82	20.52	20.52	17.	0.	0.01	0.05	34.27	19.99	721.	0.	0.52	1.38
1514	82	20.52	20.52	229.	0.	0.20	0.72	34.27	19.99	721.	0.	0.52	1.38
1515	82	20.52	20.52	228.	0.	0.20	0.71	34.27	19.99	721.	0.	0.52	1.38
1516	82	20.52	20.52	17.	0.	0.01	0.05	34.27	19.99	722.	0.	0.52	1.38
1517	55	20.52	20.52	17.	0.	0.03	0.08	34.27	19.99	137.	0.	0.19	0.40
1518	55	20.52	20.52	229.	0.	0.38	1.11	34.27	19.99	128.	0.	0.18	0.38
1519	55	20.52	20.52	212.	0.	0.35	1.03	34.27	19.99	127.	0.	0.18	0.37
1520	55	20.52	20.52	17.	0.	0.03	0.08	34.27	19.99	133.	0.	0.19	0.39
1521	55	20.52	20.52	20.	0.	0.03	0.10	34.27	19.99	11.	0.	0.01	0.03
1522	55	20.52	20.52	218.	0.	0.36	1.06	34.27	19.99	9.	0.	0.01	0.03
1523	55	20.52	20.52	206.	0.	0.34	1.00	34.27	19.99	8.	0.	0.01	0.02
1524	55	20.52	20.52	20.	0.	0.03	0.10	34.27	19.99	10.	0.	0.01	0.03

***** TAGLIO PERPENDI COLARE

GUSCI	τ_x	τ_y	τ_t	GUSCI	τ_x	τ_y	τ_t	GUSCI	τ_x	τ_y	τ_t
1501	0.5	0.4	0.4	1502	0.5	0.4	0.5	1503	0.5	0.4	0.5
1504	0.4	0.4	0.4	1505	0.5	1.7	1.6	1506	0.5	1.5	1.2
1507	0.5	1.5	1.1	1508	0.5	1.6	1.5	1509	0.4	0.8	0.7
1510	0.8	0.9	0.9	1511	0.8	0.9	0.9	1512	0.4	0.7	0.7
1513	0.3	0.7	0.7	1514	0.8	0.9	0.9	1515	0.8	0.9	0.9
1516	0.4	0.7	0.7	1517	0.5	1.6	1.5	1518	0.5	1.5	1.1
1519	0.5	1.5	1.1	1520	0.5	1.6	1.5	1521	0.5	0.3	0.4
1522	0.5	0.4	0.5	1523	0.5	0.3	0.5	1524	0.5	0.3	0.4

VERIFICHE A PUNZONAMENTO

	Norm	beta	sigT	Pcrit	Ro	Acrit	VRd, c	VED	A staffe	VRd, cs		
	[kN]		[N/mm ²]	[cm]	[%]	[cm ²]	[kN]	[kN]	[cm ²]	[kN]		
A	15	-2799.478	1.47	0.010	610.4	0.26	108271.4	1620.910	3628.900	73.0	-0.010	SÌ

VERIFICA PULVINI (fessurazione effetto piastra):

PARAMETRI GENERALI

CASI DI CARICO:

Nome	Descrizione
16	Rara (RARA)
17	Rara VentoY (RARA)
18	Frequente (FREQUENTE)
19	Frequente VentoY (FREQUENTE)
20	Quasi Perm (QUASI PERMANENTE)

DATI:

copriferro inferiore (asse armatura):	3	cm
copriferro superiore (asse armatura):	3	cm
Af	= area effettiva tesa (cm ² al metro)	
Afc	= area effettiva compressa (cm ² al metro)	
Mom	= momento flettente [kNm/m]	
Nor	= sforzo normale [kN]	
σc	= tensione calcestruzzo [N/mm ²]	
	valore max per combinazione rara	= 14.9 N/mm ²
	quasi permanente	= 11.2 N/mm ²
σf	= tensione acciai o [N/mm ²]	
	valore max per combinazione rara	= 360 N/mm ²
wkF	= apertura caratteristica per combinazione frequente (mm)	- valore max = 0.4 mm
wkP	= apertura caratteristica per combinazione quasi permanente (mm)	- valore max = 0.3 mm

MACROGUSCI 0: Pulvi no1

GUSCI	ARMATURA INFERIORE ORIZZONTALE		COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE			
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	WkF	Mom	Nor	σc	WkP
101	20.52	20.52	11.18	0.00	0.26	11.	10.57	0.00	0.004	0.00	0.00	0.00	0.000
102	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
103	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
104	20.52	20.52	11.17	0.00	0.26	11.	10.55	0.00	0.004	0.00	0.00	0.00	0.000
105	20.52	20.52	10.74	0.00	0.25	11.	10.17	0.00	0.004	0.00	0.00	0.00	0.000
106	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
107	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
108	20.52	20.52	10.72	0.00	0.25	11.	10.14	0.00	0.004	0.00	0.00	0.00	0.000
109	20.52	20.52	11.39	0.00	0.14	8.	10.73	0.00	0.003	0.00	0.00	0.00	0.000
110	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
111	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
112	20.52	20.52	11.36	0.00	0.14	7.	10.70	0.00	0.003	0.00	0.00	0.00	0.000
113	20.52	20.52	11.79	0.00	0.14	8.	11.15	0.00	0.003	0.00	0.00	0.00	0.000
114	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
115	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
116	20.52	20.52	11.76	0.00	0.14	8.	11.12	0.00	0.003	0.00	0.00	0.00	0.000
117	20.52	20.52	16.42	0.00	0.38	17.	15.54	0.00	0.006	0.00	0.00	0.00	0.000
118	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
119	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
120	20.52	20.52	16.44	0.00	0.38	17.	15.53	0.00	0.006	0.00	0.00	0.00	0.000
121	20.52	20.52	17.90	0.00	0.41	18.	16.93	0.00	0.007	0.00	0.00	0.00	0.000
122	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
123	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
124	20.52	20.52	17.94	0.00	0.42	18.	16.94	0.00	0.007	0.00	0.00	0.00	0.000

GUSCI	ARMATURA INFERIORE VERTICALE		COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE			
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	WkF	Mom	Nor	σc	WkP
101	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
102	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
103	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
104	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
105	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
106	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
107	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
108	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
109	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
110	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
111	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
112	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
113	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
114	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
115	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
116	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
117	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
118	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
119	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
120	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
121	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
122	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
123	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
124	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000

GUSCI	ARMATURA SUPERIORE ORIZZONTALE		COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE			
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	WkF	Mom	Nor	σc	WkP
101	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	8.84	0.00	0.20	0.003
102	20.52	20.52	137.58	0.00	3.19	140.	130.36	0.00	0.061	112.83	0.00	2.61	0.049
103	20.52	20.52	149.24	0.00	3.46	152.	141.18	0.00	0.068	113.10	0.00	2.62	0.050
104	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	8.80	0.00	0.20	0.003
105	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.79	0.00	0.16	0.003
106	20.52	20.52	145.71	0.00	3.37	148.	138.00	0.00	0.066	122.18	0.00	2.83	0.055
107	20.52	20.52	155.44	0.00	3.60	158.	147.05	0.00	0.072	122.49	0.00	2.84	0.056
108	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.76	0.00	0.16	0.003
109	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.70	0.00	0.09	0.002
110	20.52	20.52	152.48	0.00	1.86	101.	144.46	0.00	0.037	122.91	0.00	1.50	0.031

111	20.52	20.52	157.76	0.00	1.92	104.	149.41	0.00	0.039	123.17	0.00	1.50	0.031
112	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.72	0.00	0.09	0.002
113	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.11	0.00	0.06	0.001
114	20.52	20.52	152.09	0.00	1.85	100.	144.10	0.00	0.037	121.56	0.00	1.48	0.031
115	20.52	20.52	157.14	0.00	1.91	104.	148.85	0.00	0.039	121.81	0.00	1.48	0.031
116	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.11	0.00	0.06	0.001
117	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	3.32	0.00	0.08	0.001
118	20.52	20.52	139.97	0.00	3.24	142.	132.66	0.00	0.062	110.82	0.00	2.57	0.048
119	20.52	20.52	139.15	0.00	3.22	141.	131.96	0.00	0.062	111.15	0.00	2.57	0.048
120	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	3.32	0.00	0.08	0.001
121	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.81	0.00	0.16	0.003
122	20.52	20.52	130.76	0.00	3.03	133.	123.95	0.00	0.057	106.16	0.00	2.46	0.045
123	20.52	20.52	129.66	0.00	3.00	132.	123.01	0.00	0.056	106.44	0.00	2.46	0.045
124	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.78	0.00	0.16	0.003

ARMATURA SUPERIORE VERTICALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE						
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	WkF	Mom	Nor	σc	WkP
101	34.27	19.99	6.98	0.00	0.14	4.	6.59	0.00	0.001	5.59	0.00	0.11	0.001
102	34.27	19.99	3.55	0.00	0.07	2.	3.51	0.00	0.001	2.57	0.00	0.05	0.000
103	34.27	19.99	4.49	0.00	0.09	3.	4.41	0.00	0.001	2.12	0.00	0.04	0.000
104	34.27	19.99	7.74	0.00	0.15	5.	7.30	0.00	0.001	4.97	0.00	0.10	0.001
105	34.27	19.99	84.52	0.00	1.66	52.	78.73	0.00	0.012	63.75	0.00	1.25	0.010
106	34.27	19.99	86.06	0.00	1.69	53.	79.55	0.00	0.012	60.56	0.00	1.19	0.009
107	34.27	19.99	90.97	0.00	1.79	56.	84.40	0.00	0.013	62.35	0.00	1.22	0.009
108	34.27	19.99	91.44	0.00	1.80	57.	84.65	0.00	0.013	70.45	0.00	1.38	0.011
109	34.27	19.99	485.82	0.00	4.97	195.	461.14	0.00	0.066	368.57	0.00	3.77	0.051
110	34.27	19.99	486.03	0.00	4.97	195.	461.33	0.00	0.066	368.46	0.00	3.77	0.051
111	34.27	19.99	486.03	0.00	4.97	195.	461.33	0.00	0.066	368.46	0.00	3.77	0.051
112	34.27	19.99	486.22	0.00	4.97	196.	461.52	0.00	0.066	368.38	0.00	3.76	0.051
113	34.27	19.99	490.36	0.00	5.01	197.	462.09	0.00	0.066	368.57	0.00	3.77	0.051
114	34.27	19.99	490.52	0.00	5.01	197.	462.24	0.00	0.066	368.46	0.00	3.77	0.051
115	34.27	19.99	490.52	0.00	5.01	197.	462.24	0.00	0.066	368.46	0.00	3.77	0.051
116	34.27	19.99	490.71	0.00	5.02	197.	462.43	0.00	0.066	368.38	0.00	3.76	0.051
117	34.27	19.99	78.54	0.00	1.54	49.	74.86	0.00	0.011	63.75	0.00	1.25	0.010
118	34.27	19.99	83.48	0.00	1.64	52.	79.77	0.00	0.012	60.56	0.00	1.19	0.009
119	34.27	19.99	88.96	0.00	1.75	55.	84.73	0.00	0.013	62.35	0.00	1.22	0.009
120	34.27	19.99	89.62	0.00	1.76	56.	85.28	0.00	0.013	70.45	0.00	1.38	0.011
121	34.27	19.99	6.96	0.00	0.14	4.	6.59	0.00	0.001	5.59	0.00	0.11	0.001
122	34.27	19.99	3.54	0.00	0.07	2.	3.51	0.00	0.001	2.57	0.00	0.05	0.000
123	34.27	19.99	4.49	0.00	0.09	3.	4.41	0.00	0.001	2.12	0.00	0.04	0.000
124	34.27	19.99	7.72	0.00	0.15	5.	7.29	0.00	0.001	4.97	0.00	0.10	0.001

MACROGUSCI0: Pulvi no2

ARMATURA INFERIORE ORIZZONTALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE						
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	WkF	Mom	Nor	σc	WkP
201	20.52	20.52	11.16	0.00	0.26	11.	10.54	0.00	0.004	0.00	0.00	0.00	0.000
202	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
203	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
204	20.52	20.52	11.21	0.00	0.26	11.	10.67	0.00	0.004	0.00	0.00	0.00	0.000
205	20.52	20.52	10.71	0.00	0.25	11.	10.13	0.00	0.004	0.00	0.00	0.00	0.000
206	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
207	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
208	20.52	20.52	10.69	0.00	0.25	11.	10.28	0.00	0.004	0.00	0.00	0.00	0.000
209	20.52	20.52	11.33	0.00	0.14	7.	10.67	0.00	0.003	0.00	0.00	0.00	0.000
210	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
211	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
212	20.52	20.52	11.41	0.00	0.14	8.	10.83	0.00	0.003	0.00	0.00	0.00	0.000
213	20.52	20.52	11.74	0.00	0.14	8.	11.10	0.00	0.003	0.00	0.00	0.00	0.000
214	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
215	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
216	20.52	20.52	11.90	0.00	0.14	8.	11.32	0.00	0.003	0.00	0.00	0.00	0.000
217	20.52	20.52	16.45	0.00	0.38	17.	15.53	0.00	0.006	0.00	0.00	0.00	0.000
218	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
219	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
220	20.52	20.52	16.66	0.00	0.39	17.	15.67	0.00	0.006	0.00	0.00	0.00	0.000
221	20.52	20.52	17.96	0.00	0.42	18.	16.94	0.00	0.007	0.00	0.00	0.00	0.000
222	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
223	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
224	20.52	20.52	18.21	0.00	0.42	18.	17.09	0.00	0.007	0.00	0.00	0.00	0.000

ARMATURA INFERIORE VERTICALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE						
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	WkF	Mom	Nor	σc	WkP
201	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
202	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
203	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
204	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
205	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
206	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
207	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
208	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
209	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
210	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
211	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
212	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
213	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
214	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
215	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
216	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
217	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
218	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
219	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
220	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
221	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000

		COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE				
GUSCI	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	WkF	Mom	Nor	σc	WkP
222	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
223	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
224	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000

ARMATURA SUPERIORE ORIZZONTALE

		COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE				
GUSCI	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	WkF	Mom	Nor	σc	WkP
201	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	8.78	0.00	0.20	0.003
202	20.52	20.52	141.96	0.00	3.29	144.	134.40	0.00	0.063	106.56	0.00	2.47	0.045
203	20.52	20.52	139.21	0.00	3.22	141.	131.83	0.00	0.062	106.40	0.00	2.46	0.045
204	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.78	0.00	0.16	0.003
205	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.74	0.00	0.16	0.003
206	20.52	20.52	143.00	0.00	3.31	145.	135.34	0.00	0.064	111.22	0.00	2.58	0.048
207	20.52	20.52	147.03	0.00	3.40	149.	139.25	0.00	0.067	111.08	0.00	2.57	0.048
208	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	3.32	0.00	0.08	0.001
209	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.72	0.00	0.09	0.002
210	20.52	20.52	150.25	0.00	1.83	99.	142.19	0.00	0.036	121.84	0.00	1.48	0.031
211	20.52	20.52	154.83	0.00	1.89	102.	146.76	0.00	0.038	121.80	0.00	1.48	0.031
212	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.11	0.00	0.06	0.001
213	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.11	0.00	0.06	0.001
214	20.52	20.52	152.57	0.00	1.86	101.	144.39	0.00	0.037	123.22	0.00	1.50	0.031
215	20.52	20.52	156.73	0.00	1.91	103.	148.54	0.00	0.039	123.14	0.00	1.50	0.031
216	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.71	0.00	0.09	0.002
217	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	3.31	0.00	0.08	0.001
218	20.52	20.52	145.27	0.00	3.36	148.	137.69	0.00	0.066	122.57	0.00	2.84	0.056
219	20.52	20.52	143.83	0.00	3.33	146.	136.38	0.00	0.065	122.43	0.00	2.83	0.056
220	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.76	0.00	0.16	0.003
221	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.76	0.00	0.16	0.003
222	20.52	20.52	137.07	0.00	3.17	139.	129.94	0.00	0.060	113.22	0.00	2.62	0.050
223	20.52	20.52	135.35	0.00	3.13	138.	128.38	0.00	0.059	113.07	0.00	2.62	0.050
224	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	8.81	0.00	0.20	0.003

ARMATURA SUPERIORE VERTI CALE

MACROGUSCIO: Pul vi no3

		COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE				
GUSCI	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	WkF	Mom	Nor	σc	WkP
301	20.52	20.52	10.90	0.00	0.25	11.	10.38	0.00	0.004	0.00	0.00	0.00	0.000
302	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
303	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
304	20.52	20.52	10.90	0.00	0.25	11.	10.38	0.00	0.004	0.00	0.00	0.00	0.000
305	20.52	20.52	10.32	0.00	0.24	10.	9.89	0.00	0.004	0.00	0.00	0.00	0.000
306	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
307	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
308	20.52	20.52	10.30	0.00	0.24	10.	9.89	0.00	0.004	0.00	0.00	0.00	0.000
309	20.52	20.52	10.86	0.00	0.13	7.	10.32	0.00	0.003	0.00	0.00	0.00	0.000
310	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
311	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
312	20.52	20.52	10.88	0.00	0.13	7.	10.33	0.00	0.003	0.00	0.00	0.00	0.000
313	20.52	20.52	11.41	0.00	0.14	8.	10.87	0.00	0.003	0.00	0.00	0.00	0.000
314	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
315	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
316	20.52	20.52	11.43	0.00	0.14	8.	10.88	0.00	0.003	0.00	0.00	0.00	0.000
317	20.52	20.52	16.38	0.00	0.38	17.	15.52	0.00	0.006	0.00	0.00	0.00	0.000
318	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
319	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
320	20.52	20.52	16.46	0.00	0.38	17.	15.55	0.00	0.006	0.00	0.00	0.00	0.000
321	20.52	20.52	18.07	0.00	0.42	18.	17.11	0.00	0.007	0.00	0.00	0.00	0.000
322	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
323	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
324	20.52	20.52	18.16	0.00	0.42	18.	17.14	0.00	0.007	0.00	0.00	0.00	0.000

ARMATURA INFERIORE VERTI CALE

		COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE				
GUSCI	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	WkF	Mom	Nor	σc	WkP
301	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
302	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
303	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
304	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
305	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000

306	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
307	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
308	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
309	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
310	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
311	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
312	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
313	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
314	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
315	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
316	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
317	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
318	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
319	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
320	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
321	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
322	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
323	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
324	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000

ARMATURA SUPERIORE ORIZZONTALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE						
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	WkF	Mom	Nor	σc	WkP
301	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.92	0.00	0.16	0.003
302	20.52	20.52	153.82	0.00	3.56	156.	145.72	0.00	0.071	116.54	0.00	2.70	0.052
303	20.52	20.52	147.83	0.00	3.42	150.	140.03	0.00	0.067	109.87	0.00	2.54	0.047
304	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.92	0.00	0.16	0.003
305	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	3.64	0.00	0.08	0.001
306	20.52	20.52	159.62	0.00	3.70	162.	151.15	0.00	0.074	125.66	0.00	2.91	0.058
307	20.52	20.52	154.61	0.00	3.58	157.	146.42	0.00	0.071	114.34	0.00	2.65	0.050
308	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	3.64	0.00	0.08	0.001
309	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.05	0.00	0.06	0.001
310	20.52	20.52	161.02	0.00	1.96	106.	152.52	0.00	0.040	126.03	0.00	1.53	0.032
311	20.52	20.52	160.08	0.00	1.95	106.	151.67	0.00	0.040	124.56	0.00	1.52	0.032
312	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.05	0.00	0.06	0.001
313	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.85	0.00	0.10	0.002
314	20.52	20.52	160.23	0.00	1.95	106.	151.78	0.00	0.040	124.56	0.00	1.52	0.032
315	20.52	20.52	162.00	0.00	1.97	107.	153.48	0.00	0.041	126.01	0.00	1.53	0.032
316	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.85	0.00	0.10	0.002
317	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.84	0.00	0.16	0.003
318	20.52	20.52	141.09	0.00	3.27	143.	133.70	0.00	0.063	114.39	0.00	2.65	0.050
319	20.52	20.52	146.02	0.00	3.38	148.	138.41	0.00	0.066	125.61	0.00	2.91	0.058
320	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.84	0.00	0.16	0.003
321	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	8.80	0.00	0.20	0.003
322	20.52	20.52	131.59	0.00	3.05	134.	124.70	0.00	0.057	109.92	0.00	2.55	0.047
323	20.52	20.52	137.53	0.00	3.18	140.	130.38	0.00	0.061	116.49	0.00	2.70	0.052
324	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	8.80	0.00	0.20	0.003

ARMATURA SUPERIORE VERTI CALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE						
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	WkF	Mom	Nor	σc	WkP
301	34.27	19.99	7.65	0.00	0.15	5.	7.22	0.00	0.001	5.97	0.00	0.12	0.001
302	34.27	19.99	3.67	0.00	0.07	2.	3.60	0.00	0.001	2.86	0.00	0.06	0.000
303	34.27	19.99	4.54	0.00	0.09	3.	4.51	0.00	0.001	2.16	0.00	0.04	0.000
304	34.27	19.99	8.08	0.00	0.16	5.	7.67	0.00	0.001	5.05	0.00	0.10	0.001
305	34.27	19.99	91.57	0.00	1.80	57.	77.00	0.00	0.012	71.17	0.00	1.40	0.011
306	34.27	19.99	85.07	0.00	1.67	53.	72.72	0.00	0.011	62.36	0.00	1.22	0.009
307	34.27	19.99	89.02	0.00	1.75	55.	77.85	0.00	0.012	60.42	0.00	1.19	0.009
308	34.27	19.99	88.34	0.00	1.74	55.	78.84	0.00	0.012	64.68	0.00	1.27	0.010
309	34.27	19.99	492.79	0.00	5.04	198.	467.59	0.00	0.067	368.46	0.00	3.77	0.051
310	34.27	19.99	492.98	0.00	5.04	198.	467.77	0.00	0.067	368.54	0.00	3.77	0.051
311	34.27	19.99	492.98	0.00	5.04	198.	467.77	0.00	0.067	368.54	0.00	3.77	0.051
312	34.27	19.99	493.39	0.00	5.04	198.	468.16	0.00	0.067	368.65	0.00	3.77	0.051
313	34.27	19.99	486.37	0.00	4.97	196.	458.50	0.00	0.065	368.46	0.00	3.77	0.051
314	34.27	19.99	486.58	0.00	4.97	196.	458.70	0.00	0.065	368.54	0.00	3.77	0.051
315	34.27	19.99	486.58	0.00	4.97	196.	458.70	0.00	0.065	368.54	0.00	3.77	0.051
316	34.27	19.99	486.76	0.00	4.97	196.	458.88	0.00	0.065	368.65	0.00	3.77	0.051
317	34.27	19.99	81.02	0.00	1.59	50.	76.83	0.00	0.012	71.17	0.00	1.40	0.011
318	34.27	19.99	75.86	0.00	1.49	47.	72.30	0.00	0.011	62.36	0.00	1.22	0.009
319	34.27	19.99	81.08	0.00	1.59	50.	77.38	0.00	0.012	60.42	0.00	1.19	0.009
320	34.27	19.99	82.05	0.00	1.61	51.	78.34	0.00	0.012	64.68	0.00	1.27	0.010
321	34.27	19.99	7.68	0.00	0.15	5.	7.22	0.00	0.001	5.97	0.00	0.12	0.001
322	34.27	19.99	3.67	0.00	0.07	2.	3.61	0.00	0.001	2.86	0.00	0.06	0.000
323	34.27	19.99	4.59	0.00	0.09	3.	4.52	0.00	0.001	2.16	0.00	0.04	0.000
324	34.27	19.99	8.13	0.00	0.16	5.	7.68	0.00	0.001	5.05	0.00	0.10	0.001

MACROGUSCI 0: Pul vi no4

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE						
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	WkF	Mom	Nor	σc	WkP
401	20.52	20.52	10.89	0.00	0.25	11.	10.37	0.00	0.004	0.00	0.00	0.00	0.000
402	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
403	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
404	20.52	20.52	10.90	0.00	0.25	11.	10.38	0.00	0.004	0.00	0.00	0.00	0.000
405	20.52	20.52	10.29	0.00	0.24	10.	9.88	0.00	0.004	0.00	0.00	0.00	0.000
406	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
407	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
408	20.52	20.52	10.31	0.00	0.24	10.	9.90	0.00	0.004	0.00	0.00	0.00	0.000
409	20.52	20.52	10.86	0.00	0.13	7.	10.31	0.00	0.003	0.00	0.00	0.00	0.000
410	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
411	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
412	20.52	20.52	10.88	0.00	0.13	7.	10.34	0.00	0.003	0.00	0.00	0.00	0.000
413	20.52	20.52	11.41	0.00	0.14	8.	10.86	0.00	0.003	0.00	0.00	0.00	0.000
414	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
415	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
416	20.52	20.52	11.43	0.00	0.14	8.	10.89	0.00	0.003	0.00	0.00	0.00	0.000

417	20.52	20.52	16.46	0.00	0.38	17.	15.54	0.00	0.006	0.00	0.00	0.00	0.000
418	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
419	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
420	20.52	20.52	16.46	0.00	0.38	17.	15.55	0.00	0.006	0.00	0.00	0.00	0.000
421	20.52	20.52	18.16	0.00	0.42	18.	17.13	0.00	0.007	0.00	0.00	0.00	0.000
422	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
423	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
424	20.52	20.52	18.15	0.00	0.42	18.	17.14	0.00	0.007	0.00	0.00	0.00	0.000

ARMATURA INFERIORE VERTI CALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE						
	Af	Afc	Mom	Nor	σ_c	σ_f	Mom	Nor	WkF	Mom	Nor	σ_c	WkP
401	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
402	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
403	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
404	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
405	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
406	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
407	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
408	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
409	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
410	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
411	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
412	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
413	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
414	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
415	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
416	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
417	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
418	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
419	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
420	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
421	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
422	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
423	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
424	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000

ARMATURA SUPERIORE ORIZZONTALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE						
	Af	Afc	Mom	Nor	σ_c	σ_f	Mom	Nor	WkF	Mom	Nor	σ_c	WkP
401	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.92	0.00	0.16	0.003
402	20.52	20.52	146.65	0.00	3.40	149.	138.84	0.00	0.066	109.95	0.00	2.55	0.047
403	20.52	20.52	147.87	0.00	3.42	150.	140.03	0.00	0.067	109.84	0.00	2.54	0.047
404	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.92	0.00	0.16	0.003
405	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	3.64	0.00	0.08	0.001
406	20.52	20.52	147.30	0.00	3.41	150.	139.42	0.00	0.067	114.41	0.00	2.65	0.050
407	20.52	20.52	154.64	0.00	3.58	157.	146.42	0.00	0.071	114.31	0.00	2.65	0.050
408	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	3.63	0.00	0.08	0.001
409	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.05	0.00	0.06	0.001
410	20.52	20.52	154.67	0.00	1.88	102.	146.44	0.00	0.038	124.55	0.00	1.52	0.032
411	20.52	20.52	160.08	0.00	1.95	106.	151.66	0.00	0.040	124.54	0.00	1.52	0.032
412	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.05	0.00	0.06	0.001
413	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.86	0.00	0.10	0.002
414	20.52	20.52	157.07	0.00	1.91	104.	148.72	0.00	0.039	126.04	0.00	1.54	0.032
415	20.52	20.52	161.99	0.00	1.97	107.	153.47	0.00	0.041	125.99	0.00	1.53	0.032
416	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.85	0.00	0.10	0.002
417	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.84	0.00	0.16	0.003
418	20.52	20.52	147.30	0.00	3.41	150.	139.65	0.00	0.067	125.68	0.00	2.91	0.058
419	20.52	20.52	146.01	0.00	3.38	148.	138.39	0.00	0.066	125.58	0.00	2.91	0.058
420	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.84	0.00	0.16	0.003
421	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	8.80	0.00	0.20	0.003
422	20.52	20.52	139.07	0.00	3.22	141.	131.88	0.00	0.062	116.56	0.00	2.70	0.052
423	20.52	20.52	137.52	0.00	3.18	140.	130.37	0.00	0.061	116.46	0.00	2.70	0.052
424	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	8.80	0.00	0.20	0.003

ARMATURA SUPERIORE VERTI CALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE						
	Af	Afc	Mom	Nor	σ_c	σ_f	Mom	Nor	WkF	Mom	Nor	σ_c	WkP
401	34.27	19.99	7.65	0.00	0.15	5.	7.23	0.00	0.001	5.98	0.00	0.12	0.001
402	34.27	19.99	3.67	0.00	0.07	2.	3.62	0.00	0.001	2.87	0.00	0.06	0.000
403	34.27	19.99	4.62	0.00	0.09	3.	4.52	0.00	0.001	2.14	0.00	0.04	0.000
404	34.27	19.99	8.15	0.00	0.16	5.	7.69	0.00	0.001	5.06	0.00	0.10	0.001
405	34.27	19.99	91.97	0.00	1.81	57.	77.14	0.00	0.012	71.29	0.00	1.40	0.011
406	34.27	19.99	85.37	0.00	1.68	53.	72.83	0.00	0.011	62.46	0.00	1.23	0.009
407	34.27	19.99	89.25	0.00	1.75	55.	77.91	0.00	0.012	60.51	0.00	1.19	0.009
408	34.27	19.99	88.50	0.00	1.74	55.	78.87	0.00	0.012	64.70	0.00	1.27	0.010
409	34.27	19.99	485.88	0.00	4.97	195.	461.10	0.00	0.066	368.55	0.00	3.77	0.051
410	34.27	19.99	486.09	0.00	4.97	195.	461.30	0.00	0.066	368.62	0.00	3.77	0.051
411	34.27	19.99	486.09	0.00	4.97	195.	461.30	0.00	0.066	368.62	0.00	3.77	0.051
412	34.27	19.99	486.48	0.00	4.97	196.	461.67	0.00	0.066	368.73	0.00	3.77	0.051
413	34.27	19.99	489.82	0.00	5.01	197.	461.91	0.00	0.066	368.55	0.00	3.77	0.051
414	34.27	19.99	489.99	0.00	5.01	197.	462.07	0.00	0.066	368.62	0.00	3.77	0.051
415	34.27	19.99	489.99	0.00	5.01	197.	462.07	0.00	0.066	368.62	0.00	3.77	0.051
416	34.27	19.99	490.39	0.00	5.01	197.	462.45	0.00	0.066	368.73	0.00	3.77	0.051
417	34.27	19.99	81.04	0.00	1.59	50.	76.90	0.00	0.012	71.29	0.00	1.40	0.011
418	34.27	19.99	75.89	0.00	1.49	47.	72.37	0.00	0.011	62.46	0.00	1.23	0.009
419	34.27	19.99	81.25	0.00	1.60	50.	77.44	0.00	0.012	60.51	0.00	1.19	0.009
420	34.27	19.99	82.39	0.00	1.62	51.	78.43	0.00	0.012	64.70	0.00	1.27	0.010
421	34.27	19.99	7.66	0.00	0.15	5.	7.24	0.00	0.001	5.98	0.00	0.12	0.001
422	34.27	19.99	3.70	0.00	0.07	2.	3.62	0.00	0.001	2.87	0.00	0.06	0.000
423	34.27	19.99	4.65	0.00	0.09	3.	4.53	0.00	0.001	2.14	0.00	0.04	0.000
424	34.27	19.99	8.17	0.00	0.16	5.	7.70	0.00	0.001	5.06	0.00	0.10	0.001

MACROGUSCIO: Pul vi no5

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE					
	Af	Afc	Mom	Nor	σ_c	σ_f	Mom	Nor	WkF	Mom	Nor	σ_c

501	20.52	20.52	10.90	0.00	0.25	11.	10.38	0.00	0.004	0.00	0.00	0.00	0.000
502	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
503	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
504	20.52	20.52	10.90	0.00	0.25	11.	10.38	0.00	0.004	0.00	0.00	0.00	0.000
505	20.52	20.52	10.30	0.00	0.24	10.	9.89	0.00	0.004	0.00	0.00	0.00	0.000
506	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
507	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
508	20.52	20.52	10.31	0.00	0.24	10.	9.90	0.00	0.004	0.00	0.00	0.00	0.000
509	20.52	20.52	10.87	0.00	0.13	7.	10.32	0.00	0.003	0.00	0.00	0.00	0.000
510	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
511	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
512	20.52	20.52	10.88	0.00	0.13	7.	10.33	0.00	0.003	0.00	0.00	0.00	0.000
513	20.52	20.52	11.41	0.00	0.14	8.	10.87	0.00	0.003	0.00	0.00	0.00	0.000
514	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
515	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
516	20.52	20.52	11.43	0.00	0.14	8.	10.88	0.00	0.003	0.00	0.00	0.00	0.000
517	20.52	20.52	16.45	0.00	0.38	17.	15.54	0.00	0.006	0.00	0.00	0.00	0.000
518	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
519	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
520	20.52	20.52	16.45	0.00	0.38	17.	15.54	0.00	0.006	0.00	0.00	0.00	0.000
521	20.52	20.52	18.15	0.00	0.42	18.	17.13	0.00	0.007	0.00	0.00	0.00	0.000
522	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
523	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
524	20.52	20.52	18.15	0.00	0.42	18.	17.13	0.00	0.007	0.00	0.00	0.00	0.000

ARMATURA INFERIORE VERTICALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE						
	Af	Afc	Mom	Nor	σ_c	σ_f	Mom	Nor	WkF	Mom	Nor	σ_c	WkP
501	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
502	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
503	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
504	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
505	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
506	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
507	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
508	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
509	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
510	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
511	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
512	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
513	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
514	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
515	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
516	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
517	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
518	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
519	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
520	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
521	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
522	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
523	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
524	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000

ARMATURA SUPERIORE ORIZZONTALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE						
	Af	Afc	Mom	Nor	σ_c	σ_f	Mom	Nor	WkF	Mom	Nor	σ_c	WkP
501	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.92	0.00	0.16	0.003
502	20.52	20.52	146.90	0.00	3.40	149.	138.87	0.00	0.066	109.89	0.00	2.54	0.047
503	20.52	20.52	148.11	0.00	3.43	150.	140.06	0.00	0.067	109.83	0.00	2.54	0.047
504	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.92	0.00	0.16	0.003
505	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	3.64	0.00	0.08	0.001
506	20.52	20.52	147.49	0.00	3.42	150.	139.44	0.00	0.067	114.36	0.00	2.65	0.050
507	20.52	20.52	154.83	0.00	3.59	157.	146.44	0.00	0.071	114.30	0.00	2.65	0.050
508	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	3.63	0.00	0.08	0.001
509	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.05	0.00	0.06	0.001
510	20.52	20.52	154.55	0.00	1.88	102.	146.40	0.00	0.038	124.53	0.00	1.52	0.032
511	20.52	20.52	160.18	0.00	1.95	106.	151.67	0.00	0.040	124.52	0.00	1.52	0.032
512	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.05	0.00	0.06	0.001
513	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.85	0.00	0.10	0.002
514	20.52	20.52	156.95	0.00	1.91	103.	148.68	0.00	0.039	126.00	0.00	1.53	0.032
515	20.52	20.52	162.08	0.00	1.97	107.	153.48	0.00	0.041	125.97	0.00	1.53	0.032
516	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.85	0.00	0.10	0.002
517	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.84	0.00	0.16	0.003
518	20.52	20.52	147.33	0.00	3.41	150.	139.63	0.00	0.067	125.63	0.00	2.91	0.058
519	20.52	20.52	145.96	0.00	3.38	148.	138.37	0.00	0.066	125.57	0.00	2.91	0.058
520	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.84	0.00	0.16	0.003
521	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	8.80	0.00	0.20	0.003
522	20.52	20.52	139.11	0.00	3.22	141.	131.85	0.00	0.062	116.51	0.00	2.70	0.052
523	20.52	20.52	137.47	0.00	3.18	140.	130.34	0.00	0.061	116.45	0.00	2.70	0.052
524	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	8.80	0.00	0.20	0.003

ARMATURA SUPERIORE VERTICALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE						
	Af	Afc	Mom	Nor	σ_c	σ_f	Mom	Nor	WkF	Mom	Nor	σ_c	WkP
501	34.27	19.99	7.61	0.00	0.15	5.	7.20	0.00	0.001	5.97	0.00	0.12	0.001
502	34.27	19.99	3.70	0.00	0.07	2.	3.62	0.00	0.001	2.86	0.00	0.06	0.000
503	34.27	19.99	4.63	0.00	0.09	3.	4.52	0.00	0.001	2.16	0.00	0.04	0.000
504	34.27	19.99	8.13	0.00	0.16	5.	7.68	0.00	0.001	5.05	0.00	0.10	0.001
505	34.27	19.99	92.12	0.00	1.81	57.	77.11	0.00	0.012	71.17	0.00	1.40	0.011
506	34.27	19.99	85.43	0.00	1.68	53.	72.80	0.00	0.011	62.37	0.00	1.23	0.009
507	34.27	19.99	89.32	0.00	1.75	55.	77.83	0.00	0.012	60.42	0.00	1.19	0.009
508	34.27	19.99	88.51	0.00	1.74	55.	78.81	0.00	0.012	64.67	0.00	1.27	0.010
509	34.27	19.99	485.72	0.00	4.96	195.	461.00	0.00	0.066	368.47	0.00	3.77	0.051
510	34.27	19.99	485.93	0.00	4.97	195.	461.20	0.00	0.066	368.54	0.00	3.77	0.051
511	34.27	19.99	485.93	0.00	4.97	195.	461.20	0.00	0.066	368.54	0.00	3.77	0.051
512	34.27	19.99	486.31	0.00	4.97	196.	461.57	0.00	0.066	368.65	0.00	3.77	0.051
513	34.27	19.99	489.95	0.00	5.01	197.	461.87	0.00	0.066	368.47	0.00	3.77	0.051
514	34.27	19.99	490.12	0.00	5.01	197.	462.04	0.00	0.066	368.54	0.00	3.77	0.051
515	34.27	19.99	49										

516	34.27	19.99	490.52	0.00	5.01	197.	462.41	0.00	0.066	368.65	0.00	3.77	0.051
517	34.27	19.99	80.81	0.00	1.59	50.	76.79	0.00	0.012	71.17	0.00	1.40	0.011
518	34.27	19.99	75.75	0.00	1.49	47.	72.29	0.00	0.011	62.37	0.00	1.23	0.009
519	34.27	19.99	81.31	0.00	1.60	50.	77.43	0.00	0.012	60.42	0.00	1.19	0.009
520	34.27	19.99	82.39	0.00	1.62	51.	78.41	0.00	0.012	64.67	0.00	1.27	0.010
521	34.27	19.99	7.61	0.00	0.15	5.	7.20	0.00	0.001	5.97	0.00	0.12	0.001
522	34.27	19.99	3.73	0.00	0.07	2.	3.63	0.00	0.001	2.86	0.00	0.06	0.000
523	34.27	19.99	4.67	0.00	0.09	3.	4.53	0.00	0.001	2.16	0.00	0.04	0.000
524	34.27	19.99	8.15	0.00	0.16	5.	7.68	0.00	0.001	5.05	0.00	0.10	0.001

MACROGUSCI: Pulvi no6

GUSCI	ARMATURA INFERIORE ORIZZONTALE												
	COMBINAZIONE RARA				COMB. FREQUENTE				COMB. QUASI PERMANENTE				
	Af	Afc	Mom	Nor	σ_c	σ_f	Mom	Nor	WkF	Mom	Nor	σ_c	WkP
601	20.52	20.52	10.88	0.00	0.25	11.	10.38	0.00	0.004	0.00	0.00	0.00	0.000
602	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
603	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
604	20.52	20.52	10.90	0.00	0.25	11.	10.39	0.00	0.004	0.00	0.00	0.00	0.000
605	20.52	20.52	10.29	0.00	0.24	10.	9.89	0.00	0.004	0.00	0.00	0.00	0.000
606	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
607	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
608	20.52	20.52	10.30	0.00	0.24	10.	9.90	0.00	0.004	0.00	0.00	0.00	0.000
609	20.52	20.52	10.86	0.00	0.13	7.	10.32	0.00	0.003	0.00	0.00	0.00	0.000
610	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
611	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
612	20.52	20.52	10.89	0.00	0.13	7.	10.35	0.00	0.003	0.00	0.00	0.00	0.000
613	20.52	20.52	11.41	0.00	0.14	8.	10.87	0.00	0.003	0.00	0.00	0.00	0.000
614	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
615	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
616	20.52	20.52	11.44	0.00	0.14	8.	10.89	0.00	0.003	0.00	0.00	0.00	0.000
617	20.52	20.52	16.43	0.00	0.38	17.	15.53	0.00	0.006	0.00	0.00	0.00	0.000
618	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
619	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
620	20.52	20.52	16.44	0.00	0.38	17.	15.55	0.00	0.006	0.00	0.00	0.00	0.000
621	20.52	20.52	18.13	0.00	0.42	18.	17.13	0.00	0.007	0.00	0.00	0.00	0.000
622	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
623	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
624	20.52	20.52	18.13	0.00	0.42	18.	17.13	0.00	0.007	0.00	0.00	0.00	0.000

GUSCI	ARMATURA INFERIORE VERTICALE												
	COMBINAZIONE RARA				COMB. FREQUENTE				COMB. QUASI PERMANENTE				
	Af	Afc	Mom	Nor	σ_c	σ_f	Mom	Nor	WkF	Mom	Nor	σ_c	WkP
601	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
602	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
603	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
604	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
605	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
606	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
607	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
608	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
609	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
610	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
611	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
612	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
613	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
614	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
615	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
616	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
617	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
618	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
619	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
620	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
621	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
622	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
623	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
624	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000

GUSCI	ARMATURA SUPERIORE ORIZZONTALE												
	COMBINAZIONE RARA				COMB. FREQUENTE				COMB. QUASI PERMANENTE				
	Af	Afc	Mom	Nor	σ_c	σ_f	Mom	Nor	WkF	Mom	Nor	σ_c	WkP
601	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.92	0.00	0.16	0.003
602	20.52	20.52	146.90	0.00	3.40	149.	138.87	0.00	0.066	109.91	0.00	2.54	0.047
603	20.52	20.52	148.05	0.00	3.43	150.	140.04	0.00	0.067	109.77	0.00	2.54	0.047
604	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.91	0.00	0.16	0.003
605	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	3.64	0.00	0.08	0.001
606	20.52	20.52	147.51	0.00	3.42	150.	139.44	0.00	0.067	114.37	0.00	2.65	0.050
607	20.52	20.52	154.77	0.00	3.58	157.	146.41	0.00	0.071	114.25	0.00	2.65	0.050
608	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	3.63	0.00	0.08	0.001
609	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.05	0.00	0.06	0.001
610	20.52	20.52	154.47	0.00	1.88	102.	146.38	0.00	0.038	124.52	0.00	1.52	0.032
611	20.52	20.52	160.09	0.00	1.95	106.	151.63	0.00	0.040	124.49	0.00	1.52	0.032
612	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.05	0.00	0.06	0.001
613	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.85	0.00	0.10	0.002
614	20.52	20.52	156.88	0.00	1.91	103.	148.67	0.00	0.039	126.00	0.00	1.53	0.032
615	20.52	20.52	161.99	0.00	1.97	107.	153.44	0.00	0.041	125.94	0.00	1.53	0.032
616	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.85	0.00	0.10	0.002
617	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.84	0.00	0.16	0.003
618	20.52	20.52	147.27	0.00	3.41	150.	139.63	0.00	0.067	125.64	0.00	2.91	0.058
619	20.52	20.52	145.86	0.00	3.38	148.	138.33	0.00	0.066	125.52	0.00	2.91	0.058
620	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.84	0.00	0.16	0.003
621	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	8.80	0.00	0.20	0.003
622	20.52	20.52	139.04	0.00	3.22	141.	131.85	0.00	0.062	116.52	0.00	2.70	0.052
623	20.52	20.52	137.35	0.00	3.18	140.	130.30	0.00	0.061	116.39	0.00	2.70	0.052
624	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	8.80	0.00	0.20	0.003

ARMATURA SUPERIORE VERTICALE COMB. QUASI PERMANENTE

GUSCI	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	WkF	Mom	Nor	σc	WkP
601	34.27	19.99	7.65	0.00	0.15	5.	7.23	0.00	0.001	5.98	0.00	0.12	0.001
602	34.27	19.99	3.69	0.00	0.07	2.	3.61	0.00	0.001	2.87	0.00	0.06	0.000
603	34.27	19.99	4.63	0.00	0.09	3.	4.52	0.00	0.001	2.14	0.00	0.04	0.000
604	34.27	19.99	8.18	0.00	0.16	5.	7.69	0.00	0.001	5.06	0.00	0.10	0.001
605	34.27	19.99	92.31	0.00	1.81	57.	77.19	0.00	0.012	71.29	0.00	1.40	0.011
606	34.27	19.99	85.70	0.00	1.68	53.	72.89	0.00	0.011	62.47	0.00	1.23	0.009
607	34.27	19.99	89.58	0.00	1.76	56.	77.86	0.00	0.012	60.51	0.00	1.19	0.009
608	34.27	19.99	88.84	0.00	1.75	55.	78.84	0.00	0.012	64.69	0.00	1.27	0.010
609	34.27	19.99	485.57	0.00	4.96	195.	461.04	0.00	0.066	368.54	0.00	3.77	0.051
610	34.27	19.99	485.78	0.00	4.96	195.	461.24	0.00	0.066	368.62	0.00	3.77	0.051
611	34.27	19.99	485.78	0.00	4.96	195.	461.24	0.00	0.066	368.62	0.00	3.77	0.051
612	34.27	19.99	486.16	0.00	4.97	196.	461.61	0.00	0.066	368.73	0.00	3.77	0.051
613	34.27	19.99	490.32	0.00	5.01	197.	462.01	0.00	0.066	368.54	0.00	3.77	0.051
614	34.27	19.99	490.50	0.00	5.01	197.	462.18	0.00	0.066	368.62	0.00	3.77	0.051
615	34.27	19.99	490.50	0.00	5.01	197.	462.18	0.00	0.066	368.62	0.00	3.77	0.051
616	34.27	19.99	490.90	0.00	5.02	197.	462.55	0.00	0.066	368.73	0.00	3.77	0.051
617	34.27	19.99	80.94	0.00	1.59	50.	76.88	0.00	0.012	71.29	0.00	1.40	0.011
618	34.27	19.99	75.47	0.00	1.48	47.	72.29	0.00	0.011	62.47	0.00	1.23	0.009
619	34.27	19.99	81.19	0.00	1.59	50.	77.42	0.00	0.012	60.51	0.00	1.19	0.009
620	34.27	19.99	82.18	0.00	1.61	51.	78.38	0.00	0.012	64.69	0.00	1.27	0.010
621	34.27	19.99	7.65	0.00	0.15	5.	7.23	0.00	0.001	5.98	0.00	0.12	0.001
622	34.27	19.99	3.69	0.00	0.07	2.	3.62	0.00	0.001	2.87	0.00	0.06	0.000
623	34.27	19.99	4.63	0.00	0.09	3.	4.52	0.00	0.001	2.14	0.00	0.04	0.000
624	34.27	19.99	8.17	0.00	0.16	5.	7.69	0.00	0.001	5.06	0.00	0.10	0.001

MACROGUSCI0: Pul vi no7

GUSCI	Af		ARMATURA INFERIORE ORIZZONTALE				COMB. FREQUENTE			COMB. QUASI PERMANENTE			
			Mom	Nor	σc	σf	Mom	Nor	WkF	Mom	Nor	σc	WkP
701	20.52	20.52	11.02	0.00	0.26	11.	10.38	0.00	0.004	0.00	0.00	0.00	0.000
702	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
703	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
704	20.52	20.52	10.92	0.00	0.25	11.	10.39	0.00	0.004	0.00	0.00	0.00	0.000
705	20.52	20.52	10.47	0.00	0.24	11.	9.90	0.00	0.004	0.00	0.00	0.00	0.000
706	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
707	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
708	20.52	20.52	10.28	0.00	0.24	10.	9.91	0.00	0.004	0.00	0.00	0.00	0.000
709	20.52	20.52	11.10	0.00	0.14	7.	10.33	0.00	0.003	0.00	0.00	0.00	0.000
710	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
711	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
712	20.52	20.52	10.82	0.00	0.13	7.	10.35	0.00	0.003	0.00	0.00	0.00	0.000
713	20.52	20.52	11.64	0.00	0.14	8.	10.88	0.00	0.003	0.00	0.00	0.00	0.000
714	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
715	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
716	20.52	20.52	11.37	0.00	0.14	7.	10.90	0.00	0.003	0.00	0.00	0.00	0.000
717	20.52	20.52	16.64	0.00	0.39	17.	15.54	0.00	0.006	0.00	0.00	0.00	0.000
718	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
719	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
720	20.52	20.52	16.46	0.00	0.38	17.	15.55	0.00	0.006	0.00	0.00	0.00	0.000
721	20.52	20.52	18.30	0.00	0.42	19.	17.13	0.00	0.007	0.00	0.00	0.00	0.000
722	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
723	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
724	20.52	20.52	18.21	0.00	0.42	18.	17.13	0.00	0.007	0.00	0.00	0.00	0.000

GUSCI	Af		ARMATURA INFERIORE VERTICALE				COMB. FREQUENTE			COMB. QUASI PERMANENTE			
			Mom	Nor	σc	σf	Mom	Nor	WkF	Mom	Nor	σc	WkP
701	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
702	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
703	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
704	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
705	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
706	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
707	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
708	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
709	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
710	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
711	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
712	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
713	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
714	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
715	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
716	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
717	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
718	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
719	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
720	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
721	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
722	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
723	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
724	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000

GUSCI	Af		ARMATURA SUPERIORE ORIZZONTALE				COMB. FREQUENTE			COMB. QUASI PERMANENTE			
			Mom	Nor	σc	σf	Mom	Nor	WkF	Mom	Nor	σc	WkP
701	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.92	0.00	0.16	0.003
702	20.52	20.52	145.42	0.00	3.37	148.	138.76	0.00	0.066	109.83	0.00	2.54	0.047
703	20.52	20.52	148.76	0.00	3.44	151.	139.95	0.00	0.067	109.75	0.00	2.54	0.047
704	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.91	0.00	0.16	0.003
705	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	3.63	0.00	0.08	0.001
706	20.52	20.52	145.98	0.00	3.38	148.	139.35	0.00	0.067	114.30	0.00	2.65	0.050
707	20.52	20.52	155.93	0.00	3.61	158.	146.34	0.00	0.071	114.22	0.00	2.64	0.050
708	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	3.62	0.00	0.08	0.001
709	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.05	0.00	0.06	0.001
710	20.52	20.52	154.42	0.00	1.88	102.	146.38	0.00	0.038	124.48	0.00	1.52	0.032

711	20.52	20.52	162.06	0.00	1.97	107.	151.59	0.00	0.040	124.46	0.00	1.52	0.032
712	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.05	0.00	0.06	0.001
713	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.85	0.00	0.10	0.002
714	20.52	20.52	156.72	0.00	1.91	103.	148.65	0.00	0.039	125.95	0.00	1.53	0.032
715	20.52	20.52	164.09	0.00	2.00	108.	153.39	0.00	0.041	125.90	0.00	1.53	0.032
716	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.84	0.00	0.10	0.002
717	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.84	0.00	0.16	0.003
718	20.52	20.52	146.44	0.00	3.39	149.	139.57	0.00	0.067	125.57	0.00	2.91	0.058
719	20.52	20.52	148.42	0.00	3.44	151.	138.32	0.00	0.066	125.49	0.00	2.91	0.058
720	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.84	0.00	0.16	0.003
721	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	8.80	0.00	0.20	0.003
722	20.52	20.52	138.28	0.00	3.20	140.	131.79	0.00	0.062	116.44	0.00	2.70	0.052
723	20.52	20.52	139.75	0.00	3.24	142.	130.29	0.00	0.061	116.36	0.00	2.69	0.052
724	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	8.80	0.00	0.20	0.003

ARMATURA SUPERIORE VERTICALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE						
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	WkF	Mom	Nor	σc	WkP
701	34.27	19.99	7.36	0.00	0.14	5.	7.20	0.00	0.001	5.96	0.00	0.12	0.001
702	34.27	19.99	4.09	0.00	0.08	3.	3.62	0.00	0.001	2.85	0.00	0.06	0.000
703	34.27	19.99	4.99	0.00	0.10	3.	4.52	0.00	0.001	2.16	0.00	0.04	0.000
704	34.27	19.99	8.48	0.00	0.17	5.	7.68	0.00	0.001	5.05	0.00	0.10	0.001
705	34.27	19.99	91.91	0.00	1.81	57.	77.04	0.00	0.012	71.16	0.00	1.40	0.011
706	34.27	19.99	85.39	0.00	1.68	53.	72.77	0.00	0.011	62.37	0.00	1.23	0.009
707	34.27	19.99	89.34	0.00	1.75	55.	77.86	0.00	0.012	60.43	0.00	1.19	0.009
708	34.27	19.99	88.65	0.00	1.74	55.	78.84	0.00	0.012	64.65	0.00	1.27	0.010
709	34.27	19.99	488.01	0.00	4.99	196.	461.02	0.00	0.066	368.47	0.00	3.77	0.051
710	34.27	19.99	488.22	0.00	4.99	196.	461.22	0.00	0.066	368.54	0.00	3.77	0.051
711	34.27	19.99	488.22	0.00	4.99	196.	461.22	0.00	0.066	368.54	0.00	3.77	0.051
712	34.27	19.99	488.62	0.00	4.99	197.	461.59	0.00	0.066	368.65	0.00	3.77	0.051
713	34.27	19.99	492.14	0.00	5.03	198.	461.84	0.00	0.066	368.47	0.00	3.77	0.051
714	34.27	19.99	492.33	0.00	5.03	198.	462.00	0.00	0.066	368.54	0.00	3.77	0.051
715	34.27	19.99	492.33	0.00	5.03	198.	462.00	0.00	0.066	368.54	0.00	3.77	0.051
716	34.27	19.99	492.73	0.00	5.04	198.	462.38	0.00	0.066	368.65	0.00	3.77	0.051
717	34.27	19.99	81.02	0.00	1.59	50.	76.82	0.00	0.012	71.16	0.00	1.40	0.011
718	34.27	19.99	76.13	0.00	1.50	47.	72.25	0.00	0.011	62.37	0.00	1.23	0.009
719	34.27	19.99	82.05	0.00	1.61	51.	77.37	0.00	0.012	60.43	0.00	1.19	0.009
720	34.27	19.99	83.22	0.00	1.63	52.	78.36	0.00	0.012	64.65	0.00	1.27	0.010
721	34.27	19.99	7.35	0.00	0.14	5.	7.19	0.00	0.001	5.96	0.00	0.12	0.001
722	34.27	19.99	4.09	0.00	0.08	3.	3.62	0.00	0.001	2.85	0.00	0.06	0.000
723	34.27	19.99	5.00	0.00	0.10	3.	4.52	0.00	0.001	2.16	0.00	0.04	0.000
724	34.27	19.99	8.48	0.00	0.17	5.	7.68	0.00	0.001	5.05	0.00	0.10	0.001

MACROGUSCI0: Pulvi no8

ARMATURA INFERIORE ORIZZONTALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE						
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	WkF	Mom	Nor	σc	WkP
801	20.52	20.52	11.04	0.00	0.26	11.	10.38	0.00	0.004	0.00	0.00	0.00	0.000
802	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
803	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
804	20.52	20.52	11.05	0.00	0.26	11.	10.40	0.00	0.004	0.00	0.00	0.00	0.000
805	20.52	20.52	10.44	0.00	0.24	11.	9.90	0.00	0.004	0.00	0.00	0.00	0.000
806	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
807	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
808	20.52	20.52	10.45	0.00	0.24	11.	9.91	0.00	0.004	0.00	0.00	0.00	0.000
809	20.52	20.52	11.02	0.00	0.13	7.	10.33	0.00	0.003	0.00	0.00	0.00	0.000
810	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
811	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
812	20.52	20.52	11.05	0.00	0.13	7.	10.36	0.00	0.003	0.00	0.00	0.00	0.000
813	20.52	20.52	11.57	0.00	0.14	8.	10.88	0.00	0.003	0.00	0.00	0.00	0.000
814	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
815	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
816	20.52	20.52	11.60	0.00	0.14	8.	10.91	0.00	0.003	0.00	0.00	0.00	0.000
817	20.52	20.52	16.65	0.00	0.39	17.	15.54	0.00	0.006	0.00	0.00	0.00	0.000
818	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
819	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
820	20.52	20.52	16.67	0.00	0.39	17.	15.55	0.00	0.006	0.00	0.00	0.00	0.000
821	20.52	20.52	18.36	0.00	0.43	19.	17.13	0.00	0.007	0.00	0.00	0.00	0.000
822	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
823	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
824	20.52	20.52	18.37	0.00	0.43	19.	17.13	0.00	0.007	0.00	0.00	0.00	0.000

ARMATURA INFERIORE VERTICALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE						
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	WkF	Mom	Nor	σc	WkP
801	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
802	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
803	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
804	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
805	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
806	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
807	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
808	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
809	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
810	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
811	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
812	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
813	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
814	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
815	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
816	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
817	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
818	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
819	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
820	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
821	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000

		COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE			
GUSCI	Af AfC	Mom	Nor	σc	σf	Mom	Nor	WkF	Mom	Nor	σc	WkP
822	19.99 34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
823	19.99 34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
824	19.99 34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000

ARMATURA SUPERIORE ORIZZONTALE

		COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE			
GUSCI	Af AfC	Mom	Nor	σc	σf	Mom	Nor	WkF	Mom	Nor	σc	WkP
801	20.52 20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.91	0.00	0.16	0.003
802	20.52 20.52	148.28	0.00	3.43	151.	138.75	0.00	0.066	109.82	0.00	2.54	0.047
803	20.52 20.52	149.47	0.00	3.46	152.	139.92	0.00	0.067	109.69	0.00	2.54	0.047
804	20.52 20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.91	0.00	0.16	0.003
805	20.52 20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	3.63	0.00	0.08	0.001
806	20.52 20.52	148.95	0.00	3.45	151.	139.33	0.00	0.067	114.30	0.00	2.65	0.050
807	20.52 20.52	156.32	0.00	3.62	159.	146.31	0.00	0.071	114.16	0.00	2.64	0.050
808	20.52 20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	3.62	0.00	0.08	0.001
809	20.52 20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.06	0.00	0.06	0.001
810	20.52 20.52	156.40	0.00	1.90	103.	146.36	0.00	0.038	124.45	0.00	1.52	0.032
811	20.52 20.52	161.84	0.00	1.97	107.	151.56	0.00	0.040	124.42	0.00	1.52	0.032
812	20.52 20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.05	0.00	0.06	0.001
813	20.52 20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.85	0.00	0.10	0.002
814	20.52 20.52	158.83	0.00	1.93	105.	148.64	0.00	0.039	125.93	0.00	1.53	0.032
815	20.52 20.52	163.77	0.00	1.99	108.	153.36	0.00	0.041	125.86	0.00	1.53	0.032
816	20.52 20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.84	0.00	0.10	0.002
817	20.52 20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.84	0.00	0.16	0.003
818	20.52 20.52	148.96	0.00	3.45	151.	139.58	0.00	0.067	125.57	0.00	2.91	0.058
819	20.52 20.52	147.62	0.00	3.42	150.	138.29	0.00	0.066	125.44	0.00	2.90	0.058
820	20.52 20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.84	0.00	0.16	0.003
821	20.52 20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	8.79	0.00	0.20	0.003
822	20.52 20.52	140.62	0.00	3.26	143.	131.80	0.00	0.062	116.44	0.00	2.70	0.052
823	20.52 20.52	139.03	0.00	3.22	141.	130.27	0.00	0.061	116.30	0.00	2.69	0.052
824	20.52 20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	8.80	0.00	0.20	0.003

ARMATURA SUPERIORE VERTI CALE

		COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE			
GUSCI	Af AfC	Mom	Nor	σc	σf	Mom	Nor	WkF	Mom	Nor	σc	WkP
801	34.27 19.99	7.72	0.00	0.15	5.	7.21	0.00	0.001	5.97	0.00	0.12	0.001
802	34.27 19.99	3.72	0.00	0.07	2.	3.61	0.00	0.001	2.86	0.00	0.06	0.000
803	34.27 19.99	4.67	0.00	0.09	3.	4.51	0.00	0.001	2.14	0.00	0.04	0.000
804	34.27 19.99	8.24	0.00	0.16	5.	7.68	0.00	0.001	5.05	0.00	0.10	0.001
805	34.27 19.99	93.12	0.00	1.83	58.	77.13	0.00	0.012	71.27	0.00	1.40	0.011
806	34.27 19.99	86.49	0.00	1.70	54.	72.85	0.00	0.011	62.47	0.00	1.23	0.009
807	34.27 19.99	90.41	0.00	1.78	56.	77.89	0.00	0.012	60.52	0.00	1.19	0.009
808	34.27 19.99	89.71	0.00	1.76	56.	78.86	0.00	0.012	64.66	0.00	1.27	0.010
809	34.27 19.99	491.87	0.00	5.03	198.	461.10	0.00	0.066	368.54	0.00	3.77	0.051
810	34.27 19.99	492.08	0.00	5.03	198.	461.30	0.00	0.066	368.62	0.00	3.77	0.051
811	34.27 19.99	492.08	0.00	5.03	198.	461.30	0.00	0.066	368.62	0.00	3.77	0.051
812	34.27 19.99	492.47	0.00	5.03	198.	461.67	0.00	0.066	368.72	0.00	3.77	0.051
813	34.27 19.99	495.88	0.00	5.07	199.	461.92	0.00	0.066	368.54	0.00	3.77	0.051
814	34.27 19.99	496.06	0.00	5.07	199.	462.09	0.00	0.066	368.62	0.00	3.77	0.051
815	34.27 19.99	496.06	0.00	5.07	199.	462.09	0.00	0.066	368.62	0.00	3.77	0.051
816	34.27 19.99	496.46	0.00	5.07	200.	462.46	0.00	0.066	368.72	0.00	3.77	0.051
817	34.27 19.99	82.08	0.00	1.61	51.	76.90	0.00	0.012	71.27	0.00	1.40	0.011
818	34.27 19.99	76.88	0.00	1.51	48.	72.38	0.00	0.011	62.47	0.00	1.23	0.009
819	34.27 19.99	82.25	0.00	1.62	51.	77.42	0.00	0.012	60.52	0.00	1.19	0.009
820	34.27 19.99	83.40	0.00	1.64	52.	78.42	0.00	0.012	64.66	0.00	1.27	0.010
821	34.27 19.99	7.70	0.00	0.15	5.	7.21	0.00	0.001	5.97	0.00	0.12	0.001
822	34.27 19.99	3.71	0.00	0.07	2.	3.61	0.00	0.001	2.86	0.00	0.06	0.000
823	34.27 19.99	4.66	0.00	0.09	3.	4.51	0.00	0.001	2.14	0.00	0.04	0.000
824	34.27 19.99	8.21	0.00	0.16	5.	7.67	0.00	0.001	5.05	0.00	0.10	0.001

MACROGUSCIO: Pul vi no9

		COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE			
GUSCI	Af AfC	Mom	Nor	σc	σf	Mom	Nor	WkF	Mom	Nor	σc	WkP
901	20.52 20.52	10.92	0.00	0.25	11.	10.39	0.00	0.004	0.00	0.00	0.00	0.000
902	20.52 20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
903	20.52 20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
904	20.52 20.52	11.04	0.00	0.26	11.	10.40	0.00	0.004	0.00	0.00	0.00	0.000
905	20.52 20.52	10.29	0.00	0.24	10.	9.91	0.00	0.004	0.00	0.00	0.00	0.000
906	20.52 20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
907	20.52 20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
908	20.52 20.52	10.49	0.00	0.24	11.	9.92	0.00	0.004	0.00	0.00	0.00	0.000
909	20.52 20.52	10.82	0.00	0.13	7.	10.34	0.00	0.003	0.00	0.00	0.00	0.000
910	20.52 20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
911	20.52 20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
912	20.52 20.52	11.14	0.00	0.14	7.	10.36	0.00	0.003	0.00	0.00	0.00	0.000
913	20.52 20.52	11.37	0.00	0.14	7.	10.89	0.00	0.003	0.00	0.00	0.00	0.000
914	20.52 20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
915	20.52 20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
916	20.52 20.52	11.68	0.00	0.14	8.	10.91	0.00	0.003	0.00	0.00	0.00	0.000
917	20.52 20.52	16.46	0.00	0.38	17.	15.54	0.00	0.006	0.00	0.00	0.00	0.000
918	20.52 20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
919	20.52 20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
920	20.52 20.52	16.67	0.00	0.39	17.	15.55	0.00	0.006	0.00	0.00	0.00	0.000
921	20.52 20.52	18.21	0.00	0.42	19.	17.13	0.00	0.007	0.00	0.00	0.00	0.000
922	20.52 20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
923	20.52 20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
924	20.52 20.52	18.32	0.00	0.42	19.	17.13	0.00	0.007	0.00	0.00	0.00	0.000

ARMATURA INFERIORE VERTI CALE

		COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE			
GUSCI	Af AfC	Mom	Nor	σc	σf	Mom	Nor	WkF	Mom	Nor	σc	WkP
901	19.99 34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
902	19.99 34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
903	19.99 34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
904	19.99 34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
905	19.99 34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000

906	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
907	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
908	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
909	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
910	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
911	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
912	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
913	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
914	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
915	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
916	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
917	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
918	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
919	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
920	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
921	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
922	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
923	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
924	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000

ARMATURA SUPERIORE ORIZZONTALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE						
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	WkF	Mom	Nor	σc	WkP
901	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.91	0.00	0.16	0.003
902	20.52	20.52	148.96	0.00	3.45	151.	138.71	0.00	0.066	109.74	0.00	2.54	0.047
903	20.52	20.52	148.34	0.00	3.44	151.	139.89	0.00	0.067	109.64	0.00	2.54	0.047
904	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.91	0.00	0.16	0.003
905	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	3.62	0.00	0.08	0.001
906	20.52	20.52	149.80	0.00	3.47	152.	139.29	0.00	0.067	114.22	0.00	2.64	0.050
907	20.52	20.52	154.81	0.00	3.58	157.	146.28	0.00	0.071	114.13	0.00	2.64	0.050
908	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	3.61	0.00	0.08	0.001
909	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.05	0.00	0.06	0.001
910	20.52	20.52	156.71	0.00	1.91	103.	146.33	0.00	0.038	124.41	0.00	1.52	0.032
911	20.52	20.52	159.70	0.00	1.95	105.	151.53	0.00	0.040	124.37	0.00	1.51	0.032
912	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.05	0.00	0.06	0.001
913	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.85	0.00	0.10	0.002
914	20.52	20.52	159.20	0.00	1.94	105.	148.60	0.00	0.039	125.88	0.00	1.53	0.032
915	20.52	20.52	161.53	0.00	1.97	106.	153.33	0.00	0.041	125.82	0.00	1.53	0.032
916	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.84	0.00	0.10	0.002
917	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.84	0.00	0.16	0.003
918	20.52	20.52	149.65	0.00	3.47	152.	139.53	0.00	0.067	125.49	0.00	2.91	0.058
919	20.52	20.52	145.13	0.00	3.36	147.	138.26	0.00	0.066	125.40	0.00	2.90	0.058
920	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.84	0.00	0.16	0.003
921	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	8.80	0.00	0.20	0.003
922	20.52	20.52	141.23	0.00	3.27	143.	131.75	0.00	0.062	116.36	0.00	2.69	0.052
923	20.52	20.52	136.73	0.00	3.17	139.	130.24	0.00	0.061	116.26	0.00	2.69	0.052
924	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	8.80	0.00	0.20	0.003

ARMATURA SUPERIORE VERTI CALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE						
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	WkF	Mom	Nor	σc	WkP
901	34.27	19.99	7.91	0.00	0.16	5.	7.18	0.00	0.001	5.95	0.00	0.12	0.001
902	34.27	19.99	3.95	0.00	0.08	2.	3.61	0.00	0.001	2.84	0.00	0.06	0.000
903	34.27	19.99	4.31	0.00	0.08	3.	4.51	0.00	0.001	2.15	0.00	0.04	0.000
904	34.27	19.99	7.90	0.00	0.16	5.	7.66	0.00	0.001	5.05	0.00	0.10	0.001
905	34.27	19.99	92.85	0.00	1.82	58.	77.04	0.00	0.012	71.14	0.00	1.40	0.011
906	34.27	19.99	86.25	0.00	1.69	54.	72.78	0.00	0.011	62.37	0.00	1.23	0.009
907	34.27	19.99	90.14	0.00	1.77	56.	77.85	0.00	0.012	60.43	0.00	1.19	0.009
908	34.27	19.99	89.42	0.00	1.76	56.	78.83	0.00	0.012	64.62	0.00	1.27	0.010
909	34.27	19.99	489.38	0.00	5.00	197.	461.02	0.00	0.066	368.47	0.00	3.77	0.051
910	34.27	19.99	489.58	0.00	5.00	197.	461.22	0.00	0.066	368.54	0.00	3.77	0.051
911	34.27	19.99	489.58	0.00	5.00	197.	461.22	0.00	0.066	368.54	0.00	3.77	0.051
912	34.27	19.99	489.96	0.00	5.01	197.	461.59	0.00	0.066	368.65	0.00	3.77	0.051
913	34.27	19.99	493.22	0.00	5.04	198.	461.85	0.00	0.066	368.47	0.00	3.77	0.051
914	34.27	19.99	493.39	0.00	5.04	198.	462.01	0.00	0.066	368.54	0.00	3.77	0.051
915	34.27	19.99	493.39	0.00	5.04	198.	462.01	0.00	0.066	368.54	0.00	3.77	0.051
916	34.27	19.99	493.79	0.00	5.05	199.	462.38	0.00	0.066	368.65	0.00	3.77	0.051
917	34.27	19.99	81.81	0.00	1.61	51.	76.81	0.00	0.012	71.14	0.00	1.40	0.011
918	34.27	19.99	76.66	0.00	1.51	48.	72.32	0.00	0.011	62.37	0.00	1.23	0.009
919	34.27	19.99	81.33	0.00	1.60	50.	77.38	0.00	0.012	60.43	0.00	1.19	0.009
920	34.27	19.99	82.46	0.00	1.62	51.	78.39	0.00	0.012	64.62	0.00	1.27	0.010
921	34.27	19.99	7.92	0.00	0.16	5.	7.18	0.00	0.001	5.95	0.00	0.12	0.001
922	34.27	19.99	3.94	0.00	0.08	2.	3.62	0.00	0.001	2.84	0.00	0.06	0.000
923	34.27	19.99	4.34	0.00	0.09	3.	4.52	0.00	0.001	2.15	0.00	0.04	0.000
924	34.27	19.99	7.93	0.00	0.16	5.	7.67	0.00	0.001	5.05	0.00	0.10	0.001

MACROGUSCIO: Pulvi no10

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE						
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	WkF	Mom	Nor	σc	WkP
1001	20.52	20.52	10.91	0.00	0.25	11.	10.39	0.00	0.004	0.00	0.00	0.00	0.000
1002	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1003	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1004	20.52	20.52	10.92	0.00	0.25	11.	10.41	0.00	0.004	0.00	0.00	0.00	0.000
1005	20.52	20.52	10.32	0.00	0.24	10.	9.91	0.00	0.004	0.00	0.00	0.00	0.000
1006	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1007	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1008	20.52	20.52	10.34	0.00	0.24	11.	9.93	0.00	0.004	0.00	0.00	0.00	0.000
1009	20.52	20.52	10.90	0.00	0.13	7.	10.34	0.00	0.003	0.00	0.00	0.00	0.000
1010	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1011	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1012	20.52	20.52	10.93	0.00	0.13	7.	10.38	0.00	0.003	0.00	0.00	0.00	0.000
1013	20.52	20.52	11.44	0.00	0.14	8.	10.89	0.00	0.003	0.00	0.00	0.00	0.000
1014	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1015	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1016	20.52	20.52	11.47	0.00	0.14	8.	10.92	0.00	0.003	0.00	0.00	0.00	0.000

1017	20.52	20.52	16.46	0.00	0.38	17.	15.54	0.00	0.006	0.00	0.00	0.00	0.000
1018	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1019	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1020	20.52	20.52	16.47	0.00	0.38	17.	15.56	0.00	0.006	0.00	0.00	0.00	0.000
1021	20.52	20.52	18.15	0.00	0.42	18.	17.13	0.00	0.007	0.00	0.00	0.00	0.000
1022	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1023	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1024	20.52	20.52	18.15	0.00	0.42	18.	17.13	0.00	0.007	0.00	0.00	0.00	0.000

ARMATURA INFERIORE VERTI CALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE						
	Af	Afc	Mom	Nor	σ_c	σ_f	Mom	Nor	WkF	Mom	Nor	σ_c	WkP
1001	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1002	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1003	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1004	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1005	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1006	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1007	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1008	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1009	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1010	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1011	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1012	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1013	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1014	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1015	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1016	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1017	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1018	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1019	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1020	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1021	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1022	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1023	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1024	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000

ARMATURA SUPERIORE ORIZZONTALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE						
	Af	Afc	Mom	Nor	σ_c	σ_f	Mom	Nor	WkF	Mom	Nor	σ_c	WkP
1001	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.91	0.00	0.16	0.003
1002	20.52	20.52	146.74	0.00	3.40	149.	138.74	0.00	0.066	109.72	0.00	2.54	0.047
1003	20.52	20.52	147.91	0.00	3.42	150.	139.91	0.00	0.067	109.57	0.00	2.54	0.047
1004	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.90	0.00	0.16	0.003
1005	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	3.62	0.00	0.08	0.001
1006	20.52	20.52	147.35	0.00	3.41	150.	139.31	0.00	0.067	114.20	0.00	2.64	0.050
1007	20.52	20.52	154.62	0.00	3.58	157.	146.28	0.00	0.071	114.05	0.00	2.64	0.050
1008	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	3.61	0.00	0.08	0.001
1009	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.06	0.00	0.06	0.001
1010	20.52	20.52	154.39	0.00	1.88	102.	146.28	0.00	0.038	124.37	0.00	1.51	0.032
1011	20.52	20.52	159.97	0.00	1.95	105.	151.50	0.00	0.040	124.33	0.00	1.51	0.031
1012	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.05	0.00	0.06	0.001
1013	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.85	0.00	0.10	0.002
1014	20.52	20.52	156.79	0.00	1.91	103.	148.56	0.00	0.039	125.85	0.00	1.53	0.032
1015	20.52	20.52	161.86	0.00	1.97	107.	153.31	0.00	0.041	125.76	0.00	1.53	0.032
1016	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.84	0.00	0.10	0.002
1017	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.83	0.00	0.16	0.003
1018	20.52	20.52	147.20	0.00	3.41	150.	139.54	0.00	0.067	125.48	0.00	2.91	0.058
1019	20.52	20.52	145.76	0.00	3.38	148.	138.21	0.00	0.066	125.33	0.00	2.90	0.057
1020	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.83	0.00	0.16	0.003
1021	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	8.79	0.00	0.20	0.003
1022	20.52	20.52	138.97	0.00	3.22	141.	131.76	0.00	0.062	116.34	0.00	2.69	0.052
1023	20.52	20.52	137.26	0.00	3.18	139.	130.19	0.00	0.061	116.19	0.00	2.69	0.052
1024	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	8.80	0.00	0.20	0.003

ARMATURA SUPERIORE VERTI CALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE						
	Af	Afc	Mom	Nor	σ_c	σ_f	Mom	Nor	WkF	Mom	Nor	σ_c	WkP
1001	34.27	19.99	7.60	0.00	0.15	5.	7.19	0.00	0.001	5.96	0.00	0.12	0.001
1002	34.27	19.99	3.68	0.00	0.07	2.	3.60	0.00	0.001	2.85	0.00	0.06	0.000
1003	34.27	19.99	4.62	0.00	0.09	3.	4.51	0.00	0.001	2.14	0.00	0.04	0.000
1004	34.27	19.99	8.13	0.00	0.16	5.	7.67	0.00	0.001	5.05	0.00	0.10	0.001
1005	34.27	19.99	92.24	0.00	1.81	57.	77.17	0.00	0.012	71.25	0.00	1.40	0.011
1006	34.27	19.99	85.62	0.00	1.68	53.	72.90	0.00	0.011	62.47	0.00	1.23	0.009
1007	34.27	19.99	89.49	0.00	1.76	56.	77.83	0.00	0.012	60.52	0.00	1.19	0.009
1008	34.27	19.99	88.73	0.00	1.74	55.	78.82	0.00	0.012	64.63	0.00	1.27	0.010
1009	34.27	19.99	485.76	0.00	4.96	195.	461.08	0.00	0.066	368.54	0.00	3.77	0.051
1010	34.27	19.99	485.97	0.00	4.97	195.	461.28	0.00	0.066	368.61	0.00	3.77	0.051
1011	34.27	19.99	485.97	0.00	4.97	195.	461.28	0.00	0.066	368.61	0.00	3.77	0.051
1012	34.27	19.99	486.36	0.00	4.97	196.	461.66	0.00	0.066	368.72	0.00	3.77	0.051
1013	34.27	19.99	490.11	0.00	5.01	197.	461.98	0.00	0.066	368.54	0.00	3.77	0.051
1014	34.27	19.99	490.28	0.00	5.01	197.	462.14	0.00	0.066	368.61	0.00	3.77	0.051
1015	34.27	19.99	490.28	0.00	5.01	197.	462.14	0.00	0.066	368.61	0.00	3.77	0.051
1016	34.27	19.99	490.68	0.00	5.01	197.	462.51	0.00	0.066	368.72	0.00	3.77	0.051
1017	34.27	19.99	80.92	0.00	1.59	50.	76.87	0.00	0.012	71.25	0.00	1.40	0.011
1018	34.27	19.99	75.84	0.00	1.49	47.	72.38	0.00	0.011	62.47	0.00	1.23	0.009
1019	34.27	19.99	81.32	0.00	1.60	50.	77.43	0.00	0.012	60.52	0.00	1.19	0.009
1020	34.27	19.99	82.37	0.00	1.62	51.	78.41	0.00	0.012	64.63	0.00	1.27	0.010
1021	34.27	19.99	7.59	0.00	0.15	5.	7.19	0.00	0.001	5.96	0.00	0.12	0.001
1022	34.27	19.99	3.66	0.00	0.07	2.	3.60	0.00	0.001	2.85	0.00	0.06	0.000
1023	34.27	19.99	4.61	0.00	0.09	3.	4.51	0.00	0.001	2.14	0.00	0.04	0.000
1024	34.27	19.99	8.09	0.00	0.16	5.	7.66	0.00	0.001	5.05	0.00	0.10	0.001

MACROGUSCIO: Pulvi no11

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE					
	Af	Afc	Mom	Nor	σ_c	σ_f	Mom	Nor	WkF	Mom	Nor	σ_c

1101	20.52	20.52	10.91	0.00	0.25	11.	10.40	0.00	0.004	0.00	0.00	0.00	0.000
1102	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1103	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1104	20.52	20.52	10.92	0.00	0.25	11.	10.41	0.00	0.004	0.00	0.00	0.00	0.000
1105	20.52	20.52	10.32	0.00	0.24	10.	9.92	0.00	0.004	0.00	0.00	0.00	0.000
1106	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1107	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1108	20.52	20.52	10.34	0.00	0.24	11.	9.93	0.00	0.004	0.00	0.00	0.00	0.000
1109	20.52	20.52	10.91	0.00	0.13	7.	10.36	0.00	0.003	0.00	0.00	0.00	0.000
1110	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1111	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1112	20.52	20.52	10.94	0.00	0.13	7.	10.39	0.00	0.003	0.00	0.00	0.00	0.000
1113	20.52	20.52	11.45	0.00	0.14	8.	10.90	0.00	0.003	0.00	0.00	0.00	0.000
1114	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1115	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1116	20.52	20.52	11.47	0.00	0.14	8.	10.93	0.00	0.003	0.00	0.00	0.00	0.000
1117	20.52	20.52	16.44	0.00	0.38	17.	15.54	0.00	0.006	0.00	0.00	0.00	0.000
1118	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1119	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1120	20.52	20.52	16.45	0.00	0.38	17.	15.55	0.00	0.006	0.00	0.00	0.00	0.000
1121	20.52	20.52	18.12	0.00	0.42	18.	17.12	0.00	0.007	0.00	0.00	0.00	0.000
1122	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1123	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1124	20.52	20.52	18.13	0.00	0.42	18.	17.12	0.00	0.007	0.00	0.00	0.00	0.000

ARMATURA INFERIORE VERTICALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE						
	Af	Afc	Mom	Nor	σ_c	σ_f	Mom	Nor	WkF	Mom	Nor	σ_c	WkP
1101	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1102	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1103	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1104	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1105	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1106	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1107	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1108	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1109	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1110	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1111	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1112	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1113	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1114	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1115	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1116	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1117	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1118	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1119	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1120	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1121	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1122	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1123	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1124	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000

ARMATURA SUPERIORE ORIZZONTALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE						
	Af	Afc	Mom	Nor	σ_c	σ_f	Mom	Nor	WkF	Mom	Nor	σ_c	WkP
1101	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.91	0.00	0.16	0.003
1102	20.52	20.52	146.37	0.00	3.39	149.	138.62	0.00	0.066	109.62	0.00	2.54	0.047
1103	20.52	20.52	147.53	0.00	3.42	150.	139.78	0.00	0.067	109.47	0.00	2.53	0.047
1104	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.90	0.00	0.16	0.003
1105	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	3.61	0.00	0.08	0.001
1106	20.52	20.52	147.05	0.00	3.41	149.	139.21	0.00	0.067	114.11	0.00	2.64	0.050
1107	20.52	20.52	154.30	0.00	3.57	157.	146.16	0.00	0.071	113.96	0.00	2.64	0.050
1108	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	3.60	0.00	0.08	0.001
1109	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.05	0.00	0.06	0.001
1110	20.52	20.52	154.45	0.00	1.88	102.	146.27	0.00	0.038	124.32	0.00	1.51	0.031
1111	20.52	20.52	159.76	0.00	1.95	105.	151.41	0.00	0.040	124.24	0.00	1.51	0.031
1112	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.05	0.00	0.06	0.001
1113	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.84	0.00	0.10	0.002
1114	20.52	20.52	156.82	0.00	1.91	103.	148.53	0.00	0.039	125.78	0.00	1.53	0.032
1115	20.52	20.52	161.66	0.00	1.97	107.	153.21	0.00	0.041	125.68	0.00	1.53	0.032
1116	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.83	0.00	0.10	0.002
1117	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.83	0.00	0.16	0.003
1118	20.52	20.52	147.04	0.00	3.40	149.	139.47	0.00	0.067	125.39	0.00	2.90	0.058
1119	20.52	20.52	145.70	0.00	3.37	148.	138.14	0.00	0.066	125.24	0.00	2.90	0.057
1120	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.83	0.00	0.16	0.003
1121	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	8.80	0.00	0.20	0.003
1122	20.52	20.52	138.79	0.00	3.21	141.	131.68	0.00	0.062	116.24	0.00	2.69	0.052
1123	20.52	20.52	137.20	0.00	3.18	139.	130.12	0.00	0.061	116.10	0.00	2.69	0.051
1124	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	8.80	0.00	0.20	0.003

ARMATURA SUPERIORE VERTICALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE						
	Af	Afc	Mom	Nor	σ_c	σ_f	Mom	Nor	WkF	Mom	Nor	σ_c	WkP
1101	34.27	19.99	7.58	0.00	0.15	5.	7.16	0.00	0.001	5.93	0.00	0.12	0.001
1102	34.27	19.99	3.67	0.00	0.07	2.	3.60	0.00	0.001	2.83	0.00	0.06	0.000
1103	34.27	19.99	4.60	0.00	0.09	3.	4.50	0.00	0.001	2.15	0.00	0.04	0.000
1104	34.27	19.99	8.14	0.00	0.16	5.	7.65	0.00	0.001	5.04	0.00	0.10	0.001
1105	34.27	19.99	91.93	0.00	1.81	57.	77.03	0.00	0.012	71.12	0.00	1.40	0.011
1106	34.27	19.99	85.48	0.00	1.68	53.	72.81	0.00	0.011	62.38	0.00	1.23	0.009
1107	34.27	19.99	89.37	0.00	1.76	55.	77.84	0.00	0.012	60.44	0.00	1.19	0.009
1108	34.27	19.99	88.76	0.00	1.74	55.	78.83	0.00	0.012	64.57	0.00	1.27	0.010
1109	34.27	19.99	485.64	0.00	4.96	195.	461.00	0.00	0.066	368.46	0.00	3.77	0.051
1110	34.27	19.99	485.85	0.00	4.97	195.	461.20	0.00	0.066	368.54	0.00	3.77	0.051
1111	34.27	19.99	485.85	0.00	4.97	195.	461.20	0.00	0.066	368.54	0.00	3.77	0.051
1112	34.27	19.99	486.24	0.00	4.97	196.	461.57	0.00	0.066	368.65	0.00	3.77	0.051
1113	34.27	19.99	489.94	0.00	5.01	197.	461.89	0.00	0.066	368.46	0.00	3.77	0.051
1114	34.27	19.99	490.12	0.00	5.01	197.	462.05	0.00					

1116	34.27	19.99	490.52	0.00	5.01	197.	462.42	0.00	0.066	368.65	0.00	3.77	0.051
1117	34.27	19.99	80.99	0.00	1.59	50.	76.81	0.00	0.012	71.12	0.00	1.40	0.011
1118	34.27	19.99	75.52	0.00	1.48	47.	72.27	0.00	0.011	62.38	0.00	1.23	0.009
1119	34.27	19.99	81.00	0.00	1.59	50.	77.33	0.00	0.012	60.44	0.00	1.19	0.009
1120	34.27	19.99	82.10	0.00	1.61	51.	78.33	0.00	0.012	64.57	0.00	1.27	0.010
1121	34.27	19.99	7.58	0.00	0.15	5.	7.16	0.00	0.001	5.93	0.00	0.12	0.001
1122	34.27	19.99	3.67	0.00	0.07	2.	3.60	0.00	0.001	2.83	0.00	0.06	0.000
1123	34.27	19.99	4.61	0.00	0.09	3.	4.50	0.00	0.001	2.15	0.00	0.04	0.000
1124	34.27	19.99	8.13	0.00	0.16	5.	7.65	0.00	0.001	5.04	0.00	0.10	0.001

MACROGUSCI: Pul vi no12

GUSCI	ARMATURA INFERIORE ORIZZONTALE												
	COMBINAZIONE RARA				COMB. FREQUENTE				COMB. QUASI PERMANENTE				
	Af	Afc	Mom	Nor	σ_c	σ_f	Mom	Nor	WkF	Mom	Nor	σ_c	WkP
1201	20.52	20.52	10.93	0.00	0.25	11.	10.41	0.00	0.004	0.00	0.00	0.00	0.000
1202	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1203	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1204	20.52	20.52	10.94	0.00	0.25	11.	10.42	0.00	0.004	0.00	0.00	0.00	0.000
1205	20.52	20.52	10.34	0.00	0.24	11.	9.93	0.00	0.004	0.00	0.00	0.00	0.000
1206	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1207	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1208	20.52	20.52	10.37	0.00	0.24	11.	9.95	0.00	0.004	0.00	0.00	0.00	0.000
1209	20.52	20.52	10.92	0.00	0.13	7.	10.37	0.00	0.003	0.00	0.00	0.00	0.000
1210	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1211	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1212	20.52	20.52	10.95	0.00	0.13	7.	10.40	0.00	0.003	0.00	0.00	0.00	0.000
1213	20.52	20.52	11.47	0.00	0.14	8.	10.91	0.00	0.003	0.00	0.00	0.00	0.000
1214	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1215	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1216	20.52	20.52	11.49	0.00	0.14	8.	10.94	0.00	0.003	0.00	0.00	0.00	0.000
1217	20.52	20.52	16.47	0.00	0.38	17.	15.55	0.00	0.006	0.00	0.00	0.00	0.000
1218	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1219	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1220	20.52	20.52	16.47	0.00	0.38	17.	15.56	0.00	0.006	0.00	0.00	0.00	0.000
1221	20.52	20.52	18.15	0.00	0.42	18.	17.13	0.00	0.007	0.00	0.00	0.00	0.000
1222	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1223	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1224	20.52	20.52	18.14	0.00	0.42	18.	17.13	0.00	0.007	0.00	0.00	0.00	0.000

GUSCI	ARMATURA INFERIORE VERTICALE												
	COMBINAZIONE RARA				COMB. FREQUENTE				COMB. QUASI PERMANENTE				
	Af	Afc	Mom	Nor	σ_c	σ_f	Mom	Nor	WkF	Mom	Nor	σ_c	WkP
1201	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1202	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1203	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1204	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1205	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1206	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1207	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1208	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1209	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1210	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1211	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1212	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1213	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1214	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1215	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1216	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1217	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1218	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1219	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1220	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1221	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1222	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1223	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1224	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000

GUSCI	ARMATURA SUPERIORE ORIZZONTALE												
	COMBINAZIONE RARA				COMB. FREQUENTE				COMB. QUASI PERMANENTE				
	Af	Afc	Mom	Nor	σ_c	σ_f	Mom	Nor	WkF	Mom	Nor	σ_c	WkP
1201	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.90	0.00	0.16	0.003
1202	20.52	20.52	146.35	0.00	3.39	149.	138.57	0.00	0.066	109.56	0.00	2.54	0.047
1203	20.52	20.52	147.54	0.00	3.42	150.	139.74	0.00	0.067	109.38	0.00	2.53	0.047
1204	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.90	0.00	0.16	0.003
1205	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	3.60	0.00	0.08	0.001
1206	20.52	20.52	147.01	0.00	3.40	149.	139.15	0.00	0.066	114.05	0.00	2.64	0.050
1207	20.52	20.52	154.31	0.00	3.57	157.	146.12	0.00	0.071	113.87	0.00	2.64	0.050
1208	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	3.59	0.00	0.08	0.001
1209	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.06	0.00	0.06	0.001
1210	20.52	20.52	154.42	0.00	1.88	102.	146.21	0.00	0.038	124.24	0.00	1.51	0.031
1211	20.52	20.52	159.77	0.00	1.95	105.	151.37	0.00	0.040	124.18	0.00	1.51	0.031
1212	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.06	0.00	0.06	0.001
1213	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.84	0.00	0.10	0.002
1214	20.52	20.52	156.81	0.00	1.91	103.	148.49	0.00	0.039	125.71	0.00	1.53	0.032
1215	20.52	20.52	161.68	0.00	1.97	107.	153.18	0.00	0.041	125.61	0.00	1.53	0.032
1216	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.83	0.00	0.10	0.002
1217	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.83	0.00	0.16	0.003
1218	20.52	20.52	147.08	0.00	3.41	149.	139.44	0.00	0.067	125.32	0.00	2.90	0.057
1219	20.52	20.52	145.71	0.00	3.37	148.	138.11	0.00	0.066	125.16	0.00	2.90	0.057
1220	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.83	0.00	0.16	0.003
1221	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	8.79	0.00	0.20	0.003
1222	20.52	20.52	138.85	0.00	3.22	141.	131.66	0.00	0.062	116.18	0.00	2.69	0.052
1223	20.52	20.52	137.24	0.00	3.18	139.	130.09	0.00	0.061	116.00	0.00	2.69	0.051
1224	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	8.80	0.00	0.20	0.003

GUSCI	ARMATURA SUPERIORE VERTICALE												
	COMBINAZIONE RARA				COMB. FREQUENTE				COMB. QUASI PERMANENTE				

GUSCI	Af	AfC	Mom	Nor	σc	σf	Mom	Nor	WkF	Mom	Nor	σc	WkP
1201	34.27	19.99	7.57	0.00	0.15	5.	7.16	0.00	0.001	5.94	0.00	0.12	0.001
1202	34.27	19.99	3.65	0.00	0.07	2.	3.59	0.00	0.001	2.84	0.00	0.06	0.000
1203	34.27	19.99	4.60	0.00	0.09	3.	4.50	0.00	0.001	2.14	0.00	0.04	0.000
1204	34.27	19.99	8.09	0.00	0.16	5.	7.64	0.00	0.001	5.05	0.00	0.10	0.001
1205	34.27	19.99	91.96	0.00	1.81	57.	77.11	0.00	0.012	71.22	0.00	1.40	0.011
1206	34.27	19.99	85.41	0.00	1.68	53.	72.87	0.00	0.011	62.47	0.00	1.23	0.009
1207	34.27	19.99	89.28	0.00	1.75	55.	77.85	0.00	0.012	60.53	0.00	1.19	0.009
1208	34.27	19.99	88.58	0.00	1.74	55.	78.84	0.00	0.012	64.58	0.00	1.27	0.010
1209	34.27	19.99	485.97	0.00	4.97	195.	461.13	0.00	0.066	368.54	0.00	3.77	0.051
1210	34.27	19.99	486.18	0.00	4.97	196.	461.33	0.00	0.066	368.61	0.00	3.77	0.051
1211	34.27	19.99	486.18	0.00	4.97	196.	461.33	0.00	0.066	368.61	0.00	3.77	0.051
1212	34.27	19.99	486.57	0.00	4.97	196.	461.71	0.00	0.066	368.72	0.00	3.77	0.051
1213	34.27	19.99	489.75	0.00	5.01	197.	461.91	0.00	0.066	368.54	0.00	3.77	0.051
1214	34.27	19.99	489.92	0.00	5.01	197.	462.07	0.00	0.066	368.61	0.00	3.77	0.051
1215	34.27	19.99	489.92	0.00	5.01	197.	462.07	0.00	0.066	368.61	0.00	3.77	0.051
1216	34.27	19.99	490.33	0.00	5.01	197.	462.45	0.00	0.066	368.72	0.00	3.77	0.051
1217	34.27	19.99	81.02	0.00	1.59	50.	76.88	0.00	0.012	71.22	0.00	1.40	0.011
1218	34.27	19.99	75.96	0.00	1.49	47.	72.42	0.00	0.011	62.47	0.00	1.23	0.009
1219	34.27	19.99	81.22	0.00	1.60	50.	77.40	0.00	0.012	60.53	0.00	1.19	0.009
1220	34.27	19.99	82.37	0.00	1.62	51.	78.40	0.00	0.012	64.58	0.00	1.27	0.010
1221	34.27	19.99	7.59	0.00	0.15	5.	7.17	0.00	0.001	5.94	0.00	0.12	0.001
1222	34.27	19.99	3.68	0.00	0.07	2.	3.60	0.00	0.001	2.84	0.00	0.06	0.000
1223	34.27	19.99	4.63	0.00	0.09	3.	4.51	0.00	0.001	2.14	0.00	0.04	0.000
1224	34.27	19.99	8.11	0.00	0.16	5.	7.65	0.00	0.001	5.05	0.00	0.10	0.001

MACROGUSCI 0: Pul vi no13

GUSCI	ARMATURA INFERIORE ORIZZONTALE												
	Af	AfC	COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE			
			Mom	Nor	σc	σf	Mom	Nor	WkF	Mom	Nor	σc	WkP
1301	20.52	20.52	10.93	0.00	0.25	11.	10.42	0.00	0.004	0.00	0.00	0.00	0.000
1302	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1303	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1304	20.52	20.52	10.95	0.00	0.25	11.	10.43	0.00	0.004	0.00	0.00	0.00	0.000
1305	20.52	20.52	10.35	0.00	0.24	11.	9.94	0.00	0.004	0.00	0.00	0.00	0.000
1306	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1307	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1308	20.52	20.52	10.37	0.00	0.24	11.	9.96	0.00	0.004	0.00	0.00	0.00	0.000
1309	20.52	20.52	10.94	0.00	0.13	7.	10.39	0.00	0.003	0.00	0.00	0.00	0.000
1310	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1311	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1312	20.52	20.52	10.97	0.00	0.13	7.	10.42	0.00	0.003	0.00	0.00	0.00	0.000
1313	20.52	20.52	11.48	0.00	0.14	8.	10.93	0.00	0.003	0.00	0.00	0.00	0.000
1314	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1315	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1316	20.52	20.52	11.51	0.00	0.14	8.	10.96	0.00	0.003	0.00	0.00	0.00	0.000
1317	20.52	20.52	16.48	0.00	0.38	17.	15.56	0.00	0.006	0.00	0.00	0.00	0.000
1318	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1319	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1320	20.52	20.52	16.48	0.00	0.38	17.	15.56	0.00	0.006	0.00	0.00	0.00	0.000
1321	20.52	20.52	18.16	0.00	0.42	18.	17.13	0.00	0.007	0.00	0.00	0.00	0.000
1322	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1323	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1324	20.52	20.52	18.15	0.00	0.42	18.	17.13	0.00	0.007	0.00	0.00	0.00	0.000

GUSCI	ARMATURA INFERIORE VERTICALE												
	Af	AfC	COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE			
			Mom	Nor	σc	σf	Mom	Nor	WkF	Mom	Nor	σc	WkP
1301	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1302	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1303	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1304	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1305	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1306	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1307	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1308	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1309	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1310	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1311	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1312	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1313	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1314	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1315	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1316	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1317	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1318	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1319	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1320	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1321	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1322	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1323	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1324	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000

GUSCI	ARMATURA SUPERIORE ORIZZONTALE												
	Af	AfC	COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE			
			Mom	Nor	σc	σf	Mom	Nor	WkF	Mom	Nor	σc	WkP
1301	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.90	0.00	0.16	0.003
1302	20.52	20.52	146.56	0.00	3.39	149.	138.56	0.00	0.066	109.44	0.00	2.53	0.047
1303	20.52	20.52	147.74	0.00	3.42	150.	139.72	0.00	0.067	109.28	0.00	2.53	0.047
1304	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.89	0.00	0.16	0.003
1305	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	3.60	0.00	0.08	0.001
1306	20.52	20.52	147.17	0.00	3.41	150.	139.13	0.00	0.066	113.94	0.00	2.64	0.050
1307	20.52	20.52	154.46	0.00	3.58	157.	146.09	0.00	0.071	113.77	0.00	2.63	0.050
1308	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	3.58	0.00	0.08	0.001
1309	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.06	0.00	0.06	0.001
1310	20.52	20.52	154.25	0.00	1.88	102.	146.14	0.00	0.038	124.17	0.00	1.51	0.031

1311	20.52	20.52	159.80	0.00	1.95	105.	151.32	0.00	0.040	124.08	0.00	1.51	0.031
1312	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.06	0.00	0.06	0.001
1313	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.83	0.00	0.10	0.002
1314	20.52	20.52	156.64	0.00	1.91	103.	148.40	0.00	0.039	125.63	0.00	1.53	0.032
1315	20.52	20.52	161.69	0.00	1.97	107.	153.12	0.00	0.041	125.51	0.00	1.53	0.032
1316	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.83	0.00	0.10	0.002
1317	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.83	0.00	0.16	0.003
1318	20.52	20.52	147.05	0.00	3.40	149.	139.38	0.00	0.067	125.22	0.00	2.90	0.057
1319	20.52	20.52	145.58	0.00	3.37	148.	138.03	0.00	0.066	125.06	0.00	2.90	0.057
1320	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.83	0.00	0.16	0.003
1321	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	8.80	0.00	0.20	0.003
1322	20.52	20.52	138.82	0.00	3.21	141.	131.60	0.00	0.062	116.06	0.00	2.69	0.051
1323	20.52	20.52	137.08	0.00	3.17	139.	130.01	0.00	0.061	115.90	0.00	2.68	0.051
1324	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	8.80	0.00	0.20	0.003

ARMATURA SUPERIORE VERTI CALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE						
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	WkF	Mom	Nor	σc	WkP
1301	34.27	19.99	7.53	0.00	0.15	5.	7.12	0.00	0.001	5.91	0.00	0.12	0.001
1302	34.27	19.99	3.66	0.00	0.07	2.	3.59	0.00	0.001	2.82	0.00	0.06	0.000
1303	34.27	19.99	4.60	0.00	0.09	3.	4.50	0.00	0.001	2.15	0.00	0.04	0.000
1304	34.27	19.99	8.08	0.00	0.16	5.	7.62	0.00	0.001	5.04	0.00	0.10	0.001
1305	34.27	19.99	92.19	0.00	1.81	57.	77.08	0.00	0.012	71.09	0.00	1.40	0.011
1306	34.27	19.99	85.62	0.00	1.68	53.	72.86	0.00	0.011	62.38	0.00	1.23	0.009
1307	34.27	19.99	89.50	0.00	1.76	56.	77.77	0.00	0.012	60.45	0.00	1.19	0.009
1308	34.27	19.99	88.78	0.00	1.74	55.	78.78	0.00	0.012	64.52	0.00	1.27	0.010
1309	34.27	19.99	485.63	0.00	4.96	195.	461.01	0.00	0.066	368.46	0.00	3.77	0.051
1310	34.27	19.99	485.83	0.00	4.97	195.	461.20	0.00	0.066	368.53	0.00	3.77	0.051
1311	34.27	19.99	485.83	0.00	4.97	195.	461.20	0.00	0.066	368.53	0.00	3.77	0.051
1312	34.27	19.99	486.22	0.00	4.97	196.	461.58	0.00	0.066	368.64	0.00	3.77	0.051
1313	34.27	19.99	490.12	0.00	5.01	197.	461.93	0.00	0.066	368.46	0.00	3.77	0.051
1314	34.27	19.99	490.30	0.00	5.01	197.	462.09	0.00	0.066	368.53	0.00	3.77	0.051
1315	34.27	19.99	490.30	0.00	5.01	197.	462.09	0.00	0.066	368.53	0.00	3.77	0.051
1316	34.27	19.99	490.70	0.00	5.01	197.	462.47	0.00	0.066	368.64	0.00	3.77	0.051
1317	34.27	19.99	80.79	0.00	1.59	50.	76.76	0.00	0.012	71.09	0.00	1.40	0.011
1318	34.27	19.99	75.78	0.00	1.49	47.	72.34	0.00	0.011	62.38	0.00	1.23	0.009
1319	34.27	19.99	81.23	0.00	1.60	50.	77.36	0.00	0.012	60.45	0.00	1.19	0.009
1320	34.27	19.99	82.31	0.00	1.62	51.	78.36	0.00	0.012	64.52	0.00	1.27	0.010
1321	34.27	19.99	7.54	0.00	0.15	5.	7.13	0.00	0.001	5.91	0.00	0.12	0.001
1322	34.27	19.99	3.69	0.00	0.07	2.	3.60	0.00	0.001	2.82	0.00	0.06	0.000
1323	34.27	19.99	4.63	0.00	0.09	3.	4.50	0.00	0.001	2.15	0.00	0.04	0.000
1324	34.27	19.99	8.10	0.00	0.16	5.	7.63	0.00	0.001	5.04	0.00	0.10	0.001

MACROGUSCI0: Pulvi no14

ARMATURA INFERIORE ORIZZONTALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE						
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	WkF	Mom	Nor	σc	WkP
1401	20.52	20.52	10.94	0.00	0.25	11.	10.42	0.00	0.004	0.00	0.00	0.00	0.000
1402	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1403	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1404	20.52	20.52	10.96	0.00	0.25	11.	10.45	0.00	0.004	0.00	0.00	0.00	0.000
1405	20.52	20.52	10.36	0.00	0.24	11.	9.95	0.00	0.004	0.00	0.00	0.00	0.000
1406	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1407	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1408	20.52	20.52	10.40	0.00	0.24	11.	9.98	0.00	0.004	0.00	0.00	0.00	0.000
1409	20.52	20.52	10.95	0.00	0.13	7.	10.39	0.00	0.003	0.00	0.00	0.00	0.000
1410	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1411	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1412	20.52	20.52	11.00	0.00	0.13	7.	10.44	0.00	0.003	0.00	0.00	0.00	0.000
1413	20.52	20.52	11.49	0.00	0.14	8.	10.93	0.00	0.003	0.00	0.00	0.00	0.000
1414	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1415	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1416	20.52	20.52	11.54	0.00	0.14	8.	10.98	0.00	0.003	0.00	0.00	0.00	0.000
1417	20.52	20.52	16.47	0.00	0.38	17.	15.55	0.00	0.006	0.00	0.00	0.00	0.000
1418	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1419	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1420	20.52	20.52	16.48	0.00	0.38	17.	15.57	0.00	0.006	0.00	0.00	0.00	0.000
1421	20.52	20.52	18.14	0.00	0.42	18.	17.12	0.00	0.007	0.00	0.00	0.00	0.000
1422	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1423	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1424	20.52	20.52	18.14	0.00	0.42	18.	17.12	0.00	0.007	0.00	0.00	0.00	0.000

ARMATURA INFERIORE VERTI CALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE						
	Af	Afc	Mom	Nor	σc	σf	Mom	Nor	WkF	Mom	Nor	σc	WkP
1401	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1402	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1403	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1404	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1405	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1406	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1407	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1408	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1409	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1410	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1411	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1412	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1413	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1414	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1415	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1416	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1417	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1418	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1419	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1420	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1421	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000

		COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE			
GUSCI	Af AfC	Mom	Nor	σc	σf	Mom	Nor	WkF	Mom	Nor	σc	WkP
1422	19.99 34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1423	19.99 34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1424	19.99 34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000

ARMATURA SUPERIORE ORIZZONTALE

		COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE			
GUSCI	Af AfC	Mom	Nor	σc	σf	Mom	Nor	WkF	Mom	Nor	σc	WkP
1401	20.52 20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.89	0.00	0.16	0.003
1402	20.52 20.52	146.47	0.00	3.39	149.	138.48	0.00	0.066	109.36	0.00	2.53	0.047
1403	20.52 20.52	147.62	0.00	3.42	150.	139.62	0.00	0.067	109.11	0.00	2.53	0.047
1404	20.52 20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.88	0.00	0.16	0.003
1405	20.52 20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	3.59	0.00	0.08	0.001
1406	20.52 20.52	147.08	0.00	3.41	149.	139.06	0.00	0.066	113.87	0.00	2.64	0.050
1407	20.52 20.52	154.32	0.00	3.57	157.	145.99	0.00	0.071	113.61	0.00	2.63	0.050
1408	20.52 20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	3.56	0.00	0.08	0.001
1409	20.52 20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.06	0.00	0.06	0.001
1410	20.52 20.52	154.18	0.00	1.88	102.	146.09	0.00	0.038	124.08	0.00	1.51	0.031
1411	20.52 20.52	159.66	0.00	1.94	105.	151.21	0.00	0.040	123.96	0.00	1.51	0.031
1412	20.52 20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.06	0.00	0.06	0.001
1413	20.52 20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.83	0.00	0.10	0.002
1414	20.52 20.52	156.59	0.00	1.91	103.	148.36	0.00	0.039	125.55	0.00	1.53	0.032
1415	20.52 20.52	161.54	0.00	1.97	107.	153.01	0.00	0.041	125.38	0.00	1.53	0.032
1416	20.52 20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.82	0.00	0.10	0.002
1417	20.52 20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.82	0.00	0.16	0.003
1418	20.52 20.52	147.02	0.00	3.40	149.	139.36	0.00	0.067	125.15	0.00	2.90	0.057
1419	20.52 20.52	145.44	0.00	3.37	148.	137.92	0.00	0.066	124.90	0.00	2.89	0.057
1420	20.52 20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.82	0.00	0.16	0.003
1421	20.52 20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	8.79	0.00	0.20	0.003
1422	20.52 20.52	138.79	0.00	3.21	141.	131.58	0.00	0.062	115.98	0.00	2.69	0.051
1423	20.52 20.52	136.94	0.00	3.17	139.	129.90	0.00	0.060	115.73	0.00	2.68	0.051
1424	20.52 20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	8.80	0.00	0.20	0.003

ARMATURA SUPERIORE VERTICALE

		COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE			
GUSCI	Af AfC	Mom	Nor	σc	σf	Mom	Nor	WkF	Mom	Nor	σc	WkP
1401	34.27 19.99	7.52	0.00	0.15	5.	7.12	0.00	0.001	5.91	0.00	0.12	0.001
1402	34.27 19.99	3.66	0.00	0.07	2.	3.58	0.00	0.001	2.82	0.00	0.06	0.000
1403	34.27 19.99	4.61	0.00	0.09	3.	4.49	0.00	0.001	2.13	0.00	0.04	0.000
1404	34.27 19.99	8.08	0.00	0.16	5.	7.62	0.00	0.001	5.04	0.00	0.10	0.001
1405	34.27 19.99	92.26	0.00	1.81	57.	77.15	0.00	0.012	71.19	0.00	1.40	0.011
1406	34.27 19.99	85.70	0.00	1.68	53.	72.95	0.00	0.011	62.48	0.00	1.23	0.009
1407	34.27 19.99	89.56	0.00	1.76	56.	77.79	0.00	0.012	60.55	0.00	1.19	0.009
1408	34.27 19.99	88.85	0.00	1.75	55.	78.79	0.00	0.012	64.50	0.00	1.27	0.010
1409	34.27 19.99	485.78	0.00	4.96	195.	461.11	0.00	0.066	368.53	0.00	3.77	0.051
1410	34.27 19.99	485.99	0.00	4.97	195.	461.30	0.00	0.066	368.60	0.00	3.77	0.051
1411	34.27 19.99	485.99	0.00	4.97	195.	461.30	0.00	0.066	368.60	0.00	3.77	0.051
1412	34.27 19.99	486.38	0.00	4.97	196.	461.68	0.00	0.066	368.71	0.00	3.77	0.051
1413	34.27 19.99	490.13	0.00	5.01	197.	462.00	0.00	0.066	368.53	0.00	3.77	0.051
1414	34.27 19.99	490.31	0.00	5.01	197.	462.16	0.00	0.066	368.60	0.00	3.77	0.051
1415	34.27 19.99	490.31	0.00	5.01	197.	462.16	0.00	0.066	368.60	0.00	3.77	0.051
1416	34.27 19.99	490.71	0.00	5.01	197.	462.54	0.00	0.066	368.71	0.00	3.77	0.051
1417	34.27 19.99	80.89	0.00	1.59	50.	76.84	0.00	0.012	71.19	0.00	1.40	0.011
1418	34.27 19.99	75.89	0.00	1.49	47.	72.43	0.00	0.011	62.48	0.00	1.23	0.009
1419	34.27 19.99	81.26	0.00	1.60	50.	77.38	0.00	0.012	60.55	0.00	1.19	0.009
1420	34.27 19.99	82.33	0.00	1.62	51.	78.38	0.00	0.012	64.50	0.00	1.27	0.010
1421	34.27 19.99	7.52	0.00	0.15	5.	7.13	0.00	0.001	5.91	0.00	0.12	0.001
1422	34.27 19.99	3.70	0.00	0.07	2.	3.59	0.00	0.001	2.82	0.00	0.06	0.000
1423	34.27 19.99	4.65	0.00	0.09	3.	4.50	0.00	0.001	2.13	0.00	0.04	0.000
1424	34.27 19.99	8.10	0.00	0.16	5.	7.62	0.00	0.001	5.04	0.00	0.10	0.001

MACROGUSCIO: Pulvi no15

ARMATURA INFERIORE ORIZZONTALE

		COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE			
GUSCI	Af AfC	Mom	Nor	σc	σf	Mom	Nor	WkF	Mom	Nor	σc	WkP
1501	20.52 20.52	10.95	0.00	0.25	11.	10.44	0.00	0.004	0.00	0.00	0.00	0.000
1502	20.52 20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1503	20.52 20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1504	20.52 20.52	10.99	0.00	0.25	11.	10.47	0.00	0.004	0.00	0.00	0.00	0.000
1505	20.52 20.52	10.38	0.00	0.24	11.	9.97	0.00	0.004	0.00	0.00	0.00	0.000
1506	20.52 20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1507	20.52 20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1508	20.52 20.52	10.43	0.00	0.24	11.	10.01	0.00	0.004	0.00	0.00	0.00	0.000
1509	20.52 20.52	10.98	0.00	0.13	7.	10.42	0.00	0.003	0.00	0.00	0.00	0.000
1510	20.52 20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1511	20.52 20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1512	20.52 20.52	11.04	0.00	0.13	7.	10.49	0.00	0.003	0.00	0.00	0.00	0.000
1513	20.52 20.52	11.51	0.00	0.14	8.	10.96	0.00	0.003	0.00	0.00	0.00	0.000
1514	20.52 20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1515	20.52 20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1516	20.52 20.52	11.57	0.00	0.14	8.	11.02	0.00	0.003	0.00	0.00	0.00	0.000
1517	20.52 20.52	16.45	0.00	0.38	17.	15.56	0.00	0.006	0.00	0.00	0.00	0.000
1518	20.52 20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1519	20.52 20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1520	20.52 20.52	16.45	0.00	0.38	17.	15.57	0.00	0.006	0.00	0.00	0.00	0.000
1521	20.52 20.52	18.12	0.00	0.42	18.	17.11	0.00	0.007	0.00	0.00	0.00	0.000
1522	20.52 20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1523	20.52 20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1524	20.52 20.52	18.09	0.00	0.42	18.	17.11	0.00	0.007	0.00	0.00	0.00	0.000

ARMATURA INFERIORE VERTICALE

		COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE			
GUSCI	Af AfC	Mom	Nor	σc	σf	Mom	Nor	WkF	Mom	Nor	σc	WkP
1501	19.99 34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1502	19.99 34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1503	19.99 34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1504	19.99 34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1505	19.99 34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000

1506	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1507	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1508	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1509	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1510	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1511	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1512	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1513	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1514	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1515	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1516	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1517	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1518	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1519	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1520	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1521	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1522	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1523	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000
1524	19.99	34.27	0.00	0.00	0.00	0.	0.00	0.00	0.000	0.00	0.00	0.00	0.000

ARMATURA SUPERIORE ORIZZONTALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE						
	Af	Afc	Mom	Nor	σ_c	σ_f	Mom	Nor	WkF	Mom	Nor	σ_c	WkP
1501	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.89	0.00	0.16	0.003
1502	20.52	20.52	146.26	0.00	3.39	149.	138.34	0.00	0.066	109.17	0.00	2.53	0.047
1503	20.52	20.52	147.36	0.00	3.41	150.	139.42	0.00	0.067	108.79	0.00	2.52	0.047
1504	20.52	20.52	0.13	0.00	0.00	0.	0.00	0.00	0.000	6.87	0.00	0.16	0.003
1505	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	3.57	0.00	0.08	0.001
1506	20.52	20.52	146.92	0.00	3.40	149.	138.94	0.00	0.066	113.70	0.00	2.63	0.050
1507	20.52	20.52	154.03	0.00	3.57	156.	145.77	0.00	0.071	113.30	0.00	2.62	0.050
1508	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	3.53	0.00	0.08	0.001
1509	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.06	0.00	0.06	0.001
1510	20.52	20.52	154.06	0.00	1.88	102.	146.01	0.00	0.038	123.95	0.00	1.51	0.031
1511	20.52	20.52	159.35	0.00	1.94	105.	150.98	0.00	0.040	123.69	0.00	1.51	0.031
1512	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	5.06	0.00	0.06	0.001
1513	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.82	0.00	0.10	0.002
1514	20.52	20.52	156.45	0.00	1.91	103.	148.28	0.00	0.039	125.41	0.00	1.53	0.032
1515	20.52	20.52	161.22	0.00	1.96	106.	152.77	0.00	0.040	125.10	0.00	1.52	0.032
1516	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	7.81	0.00	0.10	0.002
1517	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.82	0.00	0.16	0.003
1518	20.52	20.52	146.89	0.00	3.40	149.	139.27	0.00	0.067	124.98	0.00	2.89	0.057
1519	20.52	20.52	145.11	0.00	3.36	147.	137.68	0.00	0.066	124.60	0.00	2.89	0.057
1520	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	6.81	0.00	0.16	0.003
1521	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	8.79	0.00	0.20	0.003
1522	20.52	20.52	138.65	0.00	3.21	141.	131.48	0.00	0.061	115.79	0.00	2.68	0.051
1523	20.52	20.52	136.61	0.00	3.16	139.	129.66	0.00	0.060	115.42	0.00	2.67	0.051
1524	20.52	20.52	0.00	0.00	0.00	0.	0.00	0.00	0.000	8.79	0.00	0.20	0.003

ARMATURA SUPERIORE VERTI CALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE				COMB. QUASI PERMANENTE						
	Af	Afc	Mom	Nor	σ_c	σ_f	Mom	Nor	WkF	Mom	Nor	σ_c	WkP
1501	34.27	19.99	7.46	0.00	0.15	5.	7.06	0.00	0.001	5.87	0.00	0.12	0.001
1502	34.27	19.99	3.68	0.00	0.07	2.	3.57	0.00	0.001	2.80	0.00	0.05	0.000
1503	34.27	19.99	4.62	0.00	0.09	3.	4.48	0.00	0.001	2.14	0.00	0.04	0.000
1504	34.27	19.99	8.09	0.00	0.16	5.	7.58	0.00	0.001	5.03	0.00	0.10	0.001
1505	34.27	19.99	92.22	0.00	1.81	57.	77.07	0.00	0.012	71.06	0.00	1.40	0.011
1506	34.27	19.99	85.75	0.00	1.68	53.	72.93	0.00	0.011	62.41	0.00	1.23	0.009
1507	34.27	19.99	89.60	0.00	1.76	56.	77.71	0.00	0.012	60.50	0.00	1.19	0.009
1508	34.27	19.99	88.97	0.00	1.75	55.	78.73	0.00	0.012	64.38	0.00	1.26	0.010
1509	34.27	19.99	485.71	0.00	4.96	195.	461.05	0.00	0.066	368.45	0.00	3.77	0.051
1510	34.27	19.99	485.92	0.00	4.97	195.	461.24	0.00	0.066	368.52	0.00	3.77	0.051
1511	34.27	19.99	485.92	0.00	4.97	195.	461.24	0.00	0.066	368.52	0.00	3.77	0.051
1512	34.27	19.99	486.31	0.00	4.97	196.	461.62	0.00	0.066	368.63	0.00	3.77	0.051
1513	34.27	19.99	490.08	0.00	5.01	197.	461.93	0.00	0.066	368.45	0.00	3.77	0.051
1514	34.27	19.99	490.25	0.00	5.01	197.	462.10	0.00	0.066	368.52	0.00	3.77	0.051
1515	34.27	19.99	490.25	0.00	5.01	197.	462.10	0.00	0.066	368.52	0.00	3.77	0.051
1516	34.27	19.99	490.65	0.00	5.01	197.	462.47	0.00	0.066	368.63	0.00	3.77	0.051
1517	34.27	19.99	80.83	0.00	1.59	50.	76.77	0.00	0.012	71.06	0.00	1.40	0.011
1518	34.27	19.99	75.54	0.00	1.48	47.	72.34	0.00	0.011	62.41	0.00	1.23	0.009
1519	34.27	19.99	81.09	0.00	1.59	50.	77.29	0.00	0.012	60.50	0.00	1.19	0.009
1520	34.27	19.99	82.11	0.00	1.61	51.	78.29	0.00	0.012	64.38	0.00	1.26	0.010
1521	34.27	19.99	7.40	0.00	0.15	5.	7.05	0.00	0.001	5.87	0.00	0.12	0.001
1522	34.27	19.99	3.71	0.00	0.07	2.	3.57	0.00	0.001	2.80	0.00	0.05	0.000
1523	34.27	19.99	4.65	0.00	0.09	3.	4.48	0.00	0.001	2.14	0.00	0.04	0.000
1524	34.27	19.99	8.11	0.00	0.16	5.	7.59	0.00	0.001	5.03	0.00	0.10	0.001

VERIFICA SEZIONI PULVINI (sezione x-z):

PARAMETRI GENERALI

Tipo verifica : stati limite - pressoflessione retta.
 Unità di misura generiche: kN; cm; kNm; N/mm²; d in mm; deformazioni *1000.
 ferri : diametri in mm; aree in cm².

Simboli :

Vert. = contorno_vertice del CLS; d = diametro;
 S = Sigma (tensioni sui materiali);
 D = Deformazioni x 1000 (epsilon);
 Ve = colonna che indica se la verifica e' soddisfatta;

CARATTERISTICHE MATERIALI

Calcestruzzo: Rck = 30. ; fck = 24.9 ; fcd = 14.11 (.35%)
 Acciaio : Tipo= B450C ; ftk = 540. ; fyk = 450. ; ftd = 469.565 (6.75%)

CARATTERISTICHE SEZIONE

L'asse Z e' rivolto verso destra, l'asse Y e' rivolto verso l'alto.

Tipo sezione: RETTANGOLARE

Cl s:

Acciaio lento:

vert.	Z	Y	ferro	Z	Y	d[mm]	Af[cm ²]
1- 1	-2673.	70.6	1	-2456.	40.6	20.	3.1416
1- 2	-2453.	70.6	2	-2466.	40.6	20.	3.1416
1- 3	-2453.	-11.4	3	-2476.	40.6	20.	3.1416
1- 4	-2673.	-11.4	4	-2487.	40.6	20.	3.1416
			5	-2497.	40.6	20.	3.1416
			6	-2507.	40.6	20.	3.1416
			7	-2517.	40.6	20.	3.1416
			8	-2527.	40.6	20.	3.1416
			9	-2538.	40.6	20.	3.1416
			10	-2548.	40.6	20.	3.1416
			11	-2558.	40.6	20.	3.1416
			12	-2568.	40.6	20.	3.1416
			13	-2578.	40.6	20.	3.1416
			14	-2589.	40.6	20.	3.1416
			15	-2599.	40.6	20.	3.1416
			16	-2609.	40.6	20.	3.1416
			17	-2619.	40.6	20.	3.1416
			18	-2629.	40.6	20.	3.1416
			19	-2639.	40.6	20.	3.1416
			20	-2650.	40.6	20.	3.1416
			21	-2660.	40.6	20.	3.1416
			22	-2670.	40.6	20.	3.1416
			23	-2456.	67.6	20.	3.1416
			24	-2466.	67.6	20.	3.1416
			25	-2476.	67.6	20.	3.1416
			26	-2487.	67.6	20.	3.1416
			27	-2497.	67.6	20.	3.1416
			28	-2507.	67.6	20.	3.1416
			29	-2517.	67.6	20.	3.1416
			30	-2527.	67.6	20.	3.1416
			31	-2538.	67.6	20.	3.1416
			32	-2548.	67.6	20.	3.1416
			33	-2558.	67.6	20.	3.1416
			34	-2568.	67.6	20.	3.1416
			35	-2578.	67.6	20.	3.1416
			36	-2589.	67.6	20.	3.1416
			37	-2599.	67.6	20.	3.1416
			38	-2609.	67.6	20.	3.1416
			39	-2619.	67.6	20.	3.1416
			40	-2629.	67.6	20.	3.1416
			41	-2639.	67.6	20.	3.1416
			42	-2650.	67.6	20.	3.1416
			43	-2660.	67.6	20.	3.1416
			44	-2670.	67.6	20.	3.1416
			45	-2456.	-8.4	20.	3.1416
			46	-2473.	-8.4	20.	3.1416
			47	-2489.	-8.4	20.	3.1416
			48	-2505.	-8.4	20.	3.1416
			49	-2522.	-8.4	20.	3.1416
			50	-2538.	-8.4	20.	3.1416
			51	-2555.	-8.4	20.	3.1416
			52	-2571.	-8.4	20.	3.1416
			53	-2588.	-8.4	20.	3.1416
			54	-2604.	-8.4	20.	3.1416
			55	-2621.	-8.4	20.	3.1416
			56	-2637.	-8.4	20.	3.1416
			57	-2654.	-8.4	20.	3.1416
			58	-2670.	-8.4	20.	3.1416

Descrizione : Pulvino 1

SOLLECITAZIONI AGENTI

Sforzi normali applicati in y= 29.55 (baricentro CLS)
 Convenzioni: N + trazione; Mz + fib. inferiori tese; My + fib. sinistra tese.

N.	N	Mz	My	Descrizione
1	-224.81	-1755.7968	-24.7291	Caso 2.1
2	-161.44	-956.5021	-17.7584	Caso 13.1
3	-156.76	-1125.6675	-17.2436	Caso 7.28
4	-228.28	-1144.1172	25.1108	Caso 7.5
5	-369.21	-1740.9165	-40.6131	Caso 2.2
6	-146.78	-1151.3955	16.1458	Caso 7.9

RISULTATI

Piani di equilibrio (eps= muz * y + muy * z + lam):

Sol.	muz	muy	lambda
1.	.00002504377	0.	-.00037496283
2.	.00001334947	0.	-.00019690799
3.	.00001583308	0.	-.00023203836

4.	.0000159452	0.	- .00024018417
5.	.00002450911	0.	- .00038047374
6.	.00001623269	0.	- .00023688849

Deformazioni sui materiali:

Cls					Acciaio lento			
sol	vert.	D cls	S cls	Ve	ferro	D ferri	S ferri	Ve
1	1- 1	1.3919	0.	si	1	.6406	128.11	si
1	1- 2	1.3919	0.	si	2	.6406	128.11	si
1	1- 3	-.6617	-7.79	si	3	.6406	128.11	si
1	1- 4	-.6617	-7.79	si	4	.6406	128.11	si
1					5	.6406	128.11	si
1					6	.6406	128.11	si
1					7	.6406	128.11	si
1					8	.6406	128.11	si
1					9	.6406	128.11	si
1					10	.6406	128.11	si
1					11	.6406	128.11	si
1					12	.6406	128.11	si
1					13	.6406	128.11	si
1					14	.6406	128.11	si
1					15	.6406	128.11	si
1					16	.6406	128.11	si
1					17	.6406	128.11	si
1					18	.6406	128.11	si
1					19	.6406	128.11	si
1					20	.6406	128.11	si
1					21	.6406	128.11	si
1					22	.6406	128.11	si
1					23	1.3167	263.35	si
1					24	1.3167	263.35	si
1					25	1.3167	263.35	si
1					26	1.3167	263.35	si
1					27	1.3167	263.35	si
1					28	1.3167	263.35	si
1					29	1.3167	263.35	si
1					30	1.3167	263.35	si
1					31	1.3167	263.35	si
1					32	1.3167	263.35	si
1					33	1.3167	263.35	si
1					34	1.3167	263.35	si
1					35	1.3167	263.35	si
1					36	1.3167	263.35	si
1					37	1.3167	263.35	si
1					38	1.3167	263.35	si
1					39	1.3167	263.35	si
1					40	1.3167	263.35	si
1					41	1.3167	263.35	si
1					42	1.3167	263.35	si
1					43	1.3167	263.35	si
1					44	1.3167	263.35	si
1					45	-.5866	-117.32	si
1					46	-.5866	-117.32	si
1					47	-.5866	-117.32	si
1					48	-.5866	-117.32	si
1					49	-.5866	-117.32	si
1					50	-.5866	-117.32	si
1					51	-.5866	-117.32	si
1					52	-.5866	-117.32	si
1					53	-.5866	-117.32	si
1					54	-.5866	-117.32	si
1					55	-.5866	-117.32	si
1					56	-.5866	-117.32	si
1					57	-.5866	-117.32	si
1					58	-.5866	-117.32	si
2	1- 1	.7449	0.	si	1	.3444	68.88	si
2	1- 2	.7449	0.	si	2	.3444	68.88	si
2	1- 3	-.3498	-4.5	si	3	.3444	68.88	si
2	1- 4	-.3498	-4.5	si	4	.3444	68.88	si
2					5	.3444	68.88	si
2					6	.3444	68.88	si
2					7	.3444	68.88	si
2					8	.3444	68.88	si
2					9	.3444	68.88	si
2					10	.3444	68.88	si
2					11	.3444	68.88	si
2					12	.3444	68.88	si
2					13	.3444	68.88	si
2					14	.3444	68.88	si
2					15	.3444	68.88	si
2					16	.3444	68.88	si
2					17	.3444	68.88	si
2					18	.3444	68.88	si
2					19	.3444	68.88	si
2					20	.3444	68.88	si
2					21	.3444	68.88	si
2					22	.3444	68.88	si
2					23	.7048	140.97	si
2					24	.7048	140.97	si
2					25	.7048	140.97	si
2					26	.7048	140.97	si
2					27	.7048	140.97	si
2					28	.7048	140.97	si
2					29	.7048	140.97	si
2					30	.7048	140.97	si
2					31	.7048	140.97	si
2					32	.7048	140.97	si
2					33	.7048	140.97	si

2					34	.7048	140.97	si
2					35	.7048	140.97	si
2					36	.7048	140.97	si
2					37	.7048	140.97	si
2					38	.7048	140.97	si
2					39	.7048	140.97	si
2					40	.7048	140.97	si
2					41	.7048	140.97	si
2					42	.7048	140.97	si
2					43	.7048	140.97	si
2					44	.7048	140.97	si
2					45	-.3097	-61.94	si
2					46	-.3097	-61.94	si
2					47	-.3097	-61.94	si
2					48	-.3097	-61.94	si
2					49	-.3097	-61.94	si
2					50	-.3097	-61.94	si
2					51	-.3097	-61.94	si
2					52	-.3097	-61.94	si
2					53	-.3097	-61.94	si
2					54	-.3097	-61.94	si
2					55	-.3097	-61.94	si
2					56	-.3097	-61.94	si
2					57	-.3097	-61.94	si
2					58	-.3097	-61.94	si
3	1- 1	.885	0.	si	1	.41	82.	si
3	1- 2	.885	0.	si	2	.41	82.	si
3	1- 3	-.4133	-5.23	si	3	.41	82.	si
3	1- 4	-.4133	-5.23	si	4	.41	82.	si
3					5	.41	82.	si
3					6	.41	82.	si
3					7	.41	82.	si
3					8	.41	82.	si
3					9	.41	82.	si
3					10	.41	82.	si
3					11	.41	82.	si
3					12	.41	82.	si
3					13	.41	82.	si
3					14	.41	82.	si
3					15	.41	82.	si
3					16	.41	82.	si
3					17	.41	82.	si
3					18	.41	82.	si
3					19	.41	82.	si
3					20	.41	82.	si
3					21	.41	82.	si
3					22	.41	82.	si
3					23	.8375	167.5	si
3					24	.8375	167.5	si
3					25	.8375	167.5	si
3					26	.8375	167.5	si
3					27	.8375	167.5	si
3					28	.8375	167.5	si
3					29	.8375	167.5	si
3					30	.8375	167.5	si
3					31	.8375	167.5	si
3					32	.8375	167.5	si
3					33	.8375	167.5	si
3					34	.8375	167.5	si
3					35	.8375	167.5	si
3					36	.8375	167.5	si
3					37	.8375	167.5	si
3					38	.8375	167.5	si
3					39	.8375	167.5	si
3					40	.8375	167.5	si
3					41	.8375	167.5	si
3					42	.8375	167.5	si
3					43	.8375	167.5	si
3					44	.8375	167.5	si
3					45	-.3658	-73.17	si
3					46	-.3658	-73.17	si
3					47	-.3658	-73.17	si
3					48	-.3658	-73.17	si
3					49	-.3658	-73.17	si
3					50	-.3658	-73.17	si
3					51	-.3658	-73.17	si
3					52	-.3658	-73.17	si
3					53	-.3658	-73.17	si
3					54	-.3658	-73.17	si
3					55	-.3658	-73.17	si
3					56	-.3658	-73.17	si
3					57	-.3658	-73.17	si
3					58	-.3658	-73.17	si
4	1- 1	.8848	0.	si	1	.4064	81.28	si
4	1- 2	.8848	0.	si	2	.4064	81.28	si
4	1- 3	-.4228	-5.33	si	3	.4064	81.28	si
4	1- 4	-.4228	-5.33	si	4	.4064	81.28	si
4					5	.4064	81.28	si
4					6	.4064	81.28	si
4					7	.4064	81.28	si
4					8	.4064	81.28	si
4					9	.4064	81.28	si
4					10	.4064	81.28	si
4					11	.4064	81.28	si
4					12	.4064	81.28	si
4					13	.4064	81.28	si
4					14	.4064	81.28	si

4				15	.4064	81.28	si
4				16	.4064	81.28	si
4				17	.4064	81.28	si
4				18	.4064	81.28	si
4				19	.4064	81.28	si
4				20	.4064	81.28	si
4				21	.4064	81.28	si
4				22	.4064	81.28	si
4				23	.8369	167.38	si
4				24	.8369	167.38	si
4				25	.8369	167.38	si
4				26	.8369	167.38	si
4				27	.8369	167.38	si
4				28	.8369	167.38	si
4				29	.8369	167.38	si
4				30	.8369	167.38	si
4				31	.8369	167.38	si
4				32	.8369	167.38	si
4				33	.8369	167.38	si
4				34	.8369	167.38	si
4				35	.8369	167.38	si
4				36	.8369	167.38	si
4				37	.8369	167.38	si
4				38	.8369	167.38	si
4				39	.8369	167.38	si
4				40	.8369	167.38	si
4				41	.8369	167.38	si
4				42	.8369	167.38	si
4				43	.8369	167.38	si
4				44	.8369	167.38	si
4				45	-.3749	-74.98	si
4				46	-.3749	-74.98	si
4				47	-.3749	-74.98	si
4				48	-.3749	-74.98	si
4				49	-.3749	-74.98	si
4				50	-.3749	-74.98	si
4				51	-.3749	-74.98	si
4				52	-.3749	-74.98	si
4				53	-.3749	-74.98	si
4				54	-.3749	-74.98	si
4				55	-.3749	-74.98	si
4				56	-.3749	-74.98	si
4				57	-.3749	-74.98	si
4				58	-.3749	-74.98	si
5	1- 1	1.3486	0.	1	.6134	122.67	si
5	1- 2	1.3486	0.	2	.6134	122.67	si
5	1- 3	-.6611	-7.79	3	.6134	122.67	si
5	1- 4	-.6611	-7.79	4	.6134	122.67	si
5				5	.6134	122.67	si
5				6	.6134	122.67	si
5				7	.6134	122.67	si
5				8	.6134	122.67	si
5				9	.6134	122.67	si
5				10	.6134	122.67	si
5				11	.6134	122.67	si
5				12	.6134	122.67	si
5				13	.6134	122.67	si
5				14	.6134	122.67	si
5				15	.6134	122.67	si
5				16	.6134	122.67	si
5				17	.6134	122.67	si
5				18	.6134	122.67	si
5				19	.6134	122.67	si
5				20	.6134	122.67	si
5				21	.6134	122.67	si
5				22	.6134	122.67	si
5				23	1.2751	255.02	si
5				24	1.2751	255.02	si
5				25	1.2751	255.02	si
5				26	1.2751	255.02	si
5				27	1.2751	255.02	si
5				28	1.2751	255.02	si
5				29	1.2751	255.02	si
5				30	1.2751	255.02	si
5				31	1.2751	255.02	si
5				32	1.2751	255.02	si
5				33	1.2751	255.02	si
5				34	1.2751	255.02	si
5				35	1.2751	255.02	si
5				36	1.2751	255.02	si
5				37	1.2751	255.02	si
5				38	1.2751	255.02	si
5				39	1.2751	255.02	si
5				40	1.2751	255.02	si
5				41	1.2751	255.02	si
5				42	1.2751	255.02	si
5				43	1.2751	255.02	si
5				44	1.2751	255.02	si
5				45	-.5876	-117.52	si
5				46	-.5876	-117.52	si
5				47	-.5876	-117.52	si
5				48	-.5876	-117.52	si
5				49	-.5876	-117.52	si
5				50	-.5876	-117.52	si
5				51	-.5876	-117.52	si
5				52	-.5876	-117.52	si
5				53	-.5876	-117.52	si

5				54	-. 5876	- 117. 52	si
5				55	-. 5876	- 117. 52	si
5				56	-. 5876	- 117. 52	si
5				57	-. 5876	- 117. 52	si
5				58	-. 5876	- 117. 52	si
6	1- 1	. 9083	0.	1	. 4213	84. 27	si
6	1- 2	. 9083	0.	2	. 4213	84. 27	si
6	1- 3	-. 4228	- 5. 33	3	. 4213	84. 27	si
6	1- 4	-. 4228	- 5. 33	4	. 4213	84. 27	si
6				5	. 4213	84. 27	si
6				6	. 4213	84. 27	si
6				7	. 4213	84. 27	si
6				8	. 4213	84. 27	si
6				9	. 4213	84. 27	si
6				10	. 4213	84. 27	si
6				11	. 4213	84. 27	si
6				12	. 4213	84. 27	si
6				13	. 4213	84. 27	si
6				14	. 4213	84. 27	si
6				15	. 4213	84. 27	si
6				16	. 4213	84. 27	si
6				17	. 4213	84. 27	si
6				18	. 4213	84. 27	si
6				19	. 4213	84. 27	si
6				20	. 4213	84. 27	si
6				21	. 4213	84. 27	si
6				22	. 4213	84. 27	si
6				23	. 8596	171. 93	si
6				24	. 8596	171. 93	si
6				25	. 8596	171. 93	si
6				26	. 8596	171. 93	si
6				27	. 8596	171. 93	si
6				28	. 8596	171. 93	si
6				29	. 8596	171. 93	si
6				30	. 8596	171. 93	si
6				31	. 8596	171. 93	si
6				32	. 8596	171. 93	si
6				33	. 8596	171. 93	si
6				34	. 8596	171. 93	si
6				35	. 8596	171. 93	si
6				36	. 8596	171. 93	si
6				37	. 8596	171. 93	si
6				38	. 8596	171. 93	si
6				39	. 8596	171. 93	si
6				40	. 8596	171. 93	si
6				41	. 8596	171. 93	si
6				42	. 8596	171. 93	si
6				43	. 8596	171. 93	si
6				44	. 8596	171. 93	si
6				45	-. 3741	- 74. 81	si
6				46	-. 3741	- 74. 81	si
6				47	-. 3741	- 74. 81	si
6				48	-. 3741	- 74. 81	si
6				49	-. 3741	- 74. 81	si
6				50	-. 3741	- 74. 81	si
6				51	-. 3741	- 74. 81	si
6				52	-. 3741	- 74. 81	si
6				53	-. 3741	- 74. 81	si
6				54	-. 3741	- 74. 81	si
6				55	-. 3741	- 74. 81	si
6				56	-. 3741	- 74. 81	si
6				57	-. 3741	- 74. 81	si
6				58	-. 3741	- 74. 81	si

Descrizione : Pulvino 2

SOLLECITAZIONI AGENTI

Sforzi normali applicati in y= 29.55 (baricentro CLS)

Convenzioni: N + trazione; Mz + fib.inferiori tese; My + fib.sinistra tese.

N.	N	Mz	My	Descrizione
1	- 212. 74	- 1750. 2965	- 10904. 2591	Caso 2. 1
2	- 479. 52	- 791. 688	- 24684. 2509	Caso 8. 23
3	- 1351. 02	- 1116. 3046	- 69530. 9574	Caso 7. 22
4	968. 01	- 1143. 8678	49895. 4715	Caso 7. 11

RISULTATI

Piani di equilibrio (eps= muz * y + muy * z + lam):

Sol.	muz	muy	lambda
1.	. 00002498696	0.	-. 00037294538
2.	. 00001024304	0.	-. 00018043368
3.	. 00001310474	0.	-. 00029229563
4.	. 00001858533	0.	-. 00015993159

Deformazioni sui materiali:

sol	Cls			Acciaio lento				
	vert.	D cls	S cls	Ve	ferro D ferri	S ferri	Ve	
1	1- 1	1. 3899	0.	si	1	. 6403	128. 06	si
1	1- 2	1. 3899	0.	si	2	. 6403	128. 06	si
1	1- 3	-. 659	- 7. 77	si	3	. 6403	128. 06	si
1	1- 4	-. 659	- 7. 77	si	4	. 6403	128. 06	si
1					5	. 6403	128. 06	si
1					6	. 6403	128. 06	si
1					7	. 6403	128. 06	si
1					8	. 6403	128. 06	si
1					9	. 6403	128. 06	si
1					10	. 6403	128. 06	si
1					11	. 6403	128. 06	si

4	32	1.0955	219.1	si
4	33	1.0955	219.1	si
4	34	1.0955	219.1	si
4	35	1.0955	219.1	si
4	36	1.0955	219.1	si
4	37	1.0955	219.1	si
4	38	1.0955	219.1	si
4	39	1.0955	219.1	si
4	40	1.0955	219.1	si
4	41	1.0955	219.1	si
4	42	1.0955	219.1	si
4	43	1.0955	219.1	si
4	44	1.0955	219.1	si
4	45	-.317	-63.4	si
4	46	-.317	-63.4	si
4	47	-.317	-63.4	si
4	48	-.317	-63.4	si
4	49	-.317	-63.4	si
4	50	-.317	-63.4	si
4	51	-.317	-63.4	si
4	52	-.317	-63.4	si
4	53	-.317	-63.4	si
4	54	-.317	-63.4	si
4	55	-.317	-63.4	si
4	56	-.317	-63.4	si
4	57	-.317	-63.4	si
4	58	-.317	-63.4	si

Descrizi one : Pul vi no 3

SOLLECITAZIONI AGENTI

Sforzi normali applicati in $y=29.55$ (baricentro CLS)
 Convenzioni: N + trazione; Mz + fib.inferiori tese; My + fib.sinistra tese.
 Convenzioni: N + trazione; Mz + fib.inferiori tese; My + fib.sinistra tese.

N.	N	Mz	My	Descrizione
1	-223.31	-1743.3458	-17167.547	Caso 2.1
2	-154.14	-948.5098	-11852.2262	Caso 13.1
3	-343.1	-1723.9846	-26384.4116	Caso 2.2
4	-80.39	-1117.0283	-6196.5342	Caso 7.13

RISULTATI

Pi ani di equilibrio ($\epsilon = \mu z * y + \mu y * z + \lambda$):

Sol.	muz	muy	lambda
1.	.00002485961	0.	-.00037201195
2.	.00001324932	0.	-.00019482465
3.	.00002431038	0.	-.0003749843
4.	.00001587604	0.	-.00022562132

Deformazioni sui materiali:

sol	Cls			Ve	Acciaio lento			
	vert.	D cls	S cls		ferro	D ferri	S ferri	
1	1-1	1.3818	0.	si	1	.636	127.21	si
1	1-2	1.3818	0.	si	2	.636	127.21	si
1	1-3	-.6567	-7.74	si	3	.636	127.21	si
1	1-4	-.6567	-7.74	si	4	.636	127.21	si
1					5	.636	127.21	si
1					6	.636	127.21	si
1					7	.636	127.21	si
1					8	.636	127.21	si
1					9	.636	127.21	si
1					10	.636	127.21	si
1					11	.636	127.21	si
1					12	.636	127.21	si
1					13	.636	127.21	si
1					14	.636	127.21	si
1					15	.636	127.21	si
1					16	.636	127.21	si
1					17	.636	127.21	si
1					18	.636	127.21	si
1					19	.636	127.21	si
1					20	.636	127.21	si
1					21	.636	127.21	si
1					22	.636	127.21	si
1					23	1.3073	261.45	si
1					24	1.3073	261.45	si
1					25	1.3073	261.45	si
1					26	1.3073	261.45	si
1					27	1.3073	261.45	si
1					28	1.3073	261.45	si
1					29	1.3073	261.45	si
1					30	1.3073	261.45	si
1					31	1.3073	261.45	si
1					32	1.3073	261.45	si
1					33	1.3073	261.45	si
1					34	1.3073	261.45	si
1					35	1.3073	261.45	si
1					36	1.3073	261.45	si
1					37	1.3073	261.45	si
1					38	1.3073	261.45	si
1					39	1.3073	261.45	si
1					40	1.3073	261.45	si
1					41	1.3073	261.45	si
1					42	1.3073	261.45	si
1					43	1.3073	261.45	si
1					44	1.3073	261.45	si
1					45	-.5821	-116.42	si
1					46	-.5821	-116.42	si

3				28	1. 2672	253. 44	si
3				29	1. 2672	253. 44	si
3				30	1. 2672	253. 44	si
3				31	1. 2672	253. 44	si
3				32	1. 2672	253. 44	si
3				33	1. 2672	253. 44	si
3				34	1. 2672	253. 44	si
3				35	1. 2672	253. 44	si
3				36	1. 2672	253. 44	si
3				37	1. 2672	253. 44	si
3				38	1. 2672	253. 44	si
3				39	1. 2672	253. 44	si
3				40	1. 2672	253. 44	si
3				41	1. 2672	253. 44	si
3				42	1. 2672	253. 44	si
3				43	1. 2672	253. 44	si
3				44	1. 2672	253. 44	si
3				45	-. 5804	- 116. 08	si
3				46	-. 5804	- 116. 08	si
3				47	-. 5804	- 116. 08	si
3				48	-. 5804	- 116. 08	si
3				49	-. 5804	- 116. 08	si
3				50	-. 5804	- 116. 08	si
3				51	-. 5804	- 116. 08	si
3				52	-. 5804	- 116. 08	si
3				53	-. 5804	- 116. 08	si
3				54	-. 5804	- 116. 08	si
3				55	-. 5804	- 116. 08	si
3				56	-. 5804	- 116. 08	si
3				57	-. 5804	- 116. 08	si
3				58	-. 5804	- 116. 08	si
4	1- 1	. 8944	0.	1	. 4182	83. 63	si
4	1- 2	. 8944	0.	2	. 4182	83. 63	si
4	1- 3	-. 4074	- 5. 16	3	. 4182	83. 63	si
4	1- 4	-. 4074	- 5. 16	4	. 4182	83. 63	si
4				5	. 4182	83. 63	si
4				6	. 4182	83. 63	si
4				7	. 4182	83. 63	si
4				8	. 4182	83. 63	si
4				9	. 4182	83. 63	si
4				10	. 4182	83. 63	si
4				11	. 4182	83. 63	si
4				12	. 4182	83. 63	si
4				13	. 4182	83. 63	si
4				14	. 4182	83. 63	si
4				15	. 4182	83. 63	si
4				16	. 4182	83. 63	si
4				17	. 4182	83. 63	si
4				18	. 4182	83. 63	si
4				19	. 4182	83. 63	si
4				20	. 4182	83. 63	si
4				21	. 4182	83. 63	si
4				22	. 4182	83. 63	si
4				23	. 8468	169. 36	si
4				24	. 8468	169. 36	si
4				25	. 8468	169. 36	si
4				26	. 8468	169. 36	si
4				27	. 8468	169. 36	si
4				28	. 8468	169. 36	si
4				29	. 8468	169. 36	si
4				30	. 8468	169. 36	si
4				31	. 8468	169. 36	si
4				32	. 8468	169. 36	si
4				33	. 8468	169. 36	si
4				34	. 8468	169. 36	si
4				35	. 8468	169. 36	si
4				36	. 8468	169. 36	si
4				37	. 8468	169. 36	si
4				38	. 8468	169. 36	si
4				39	. 8468	169. 36	si
4				40	. 8468	169. 36	si
4				41	. 8468	169. 36	si
4				42	. 8468	169. 36	si
4				43	. 8468	169. 36	si
4				44	. 8468	169. 36	si
4				45	-. 3598	- 71. 95	si
4				46	-. 3598	- 71. 95	si
4				47	-. 3598	- 71. 95	si
4				48	-. 3598	- 71. 95	si
4				49	-. 3598	- 71. 95	si
4				50	-. 3598	- 71. 95	si
4				51	-. 3598	- 71. 95	si
4				52	-. 3598	- 71. 95	si
4				53	-. 3598	- 71. 95	si
4				54	-. 3598	- 71. 95	si
4				55	-. 3598	- 71. 95	si
4				56	-. 3598	- 71. 95	si
4				57	-. 3598	- 71. 95	si
4				58	-. 3598	- 71. 95	si

Descrizione : Pulvino 4

SOLLECITAZIONI AGENTI

Sforzi normali applicati in $y= 29.55$ (baricentro CLS)

Convenzioni: N + trazione; Mz + fib.inferiori tese; My + fib.sinistra tese.

N.	N	Mz	My	Descrizione
1	-209.74	-1739.3329	-21503.6359	Caso 2. 1
2	-353.79	-1714.356	-36272.1675	Caso 2. 2
3	-153.36	-944.7927	-15722.9486	Caso 13. 1

RISULTATI

Piani di equilibrio (eps= muz * y + muy * z + lam):

Sol.	muz	muy	lambda
1.	.00002482847	0.	-.00037024432
2.	.00002414251	0.	-.00037343123
3.	.00001319691	0.	-.00019400962

Deformazioni sui materiali:

sol	Cls				Acciaio lento			
	vert.	D cls	S cls	Ve	ferro	D ferri	S ferri	Ve
1	1- 1	1.3814	0.	si	1	.6365	127.31	si
1	1- 2	1.3814	0.	si	2	.6365	127.31	si
1	1- 3	-.6545	-7.72	si	3	.6365	127.31	si
1	1- 4	-.6545	-7.72	si	4	.6365	127.31	si
1					5	.6365	127.31	si
1					6	.6365	127.31	si
1					7	.6365	127.31	si
1					8	.6365	127.31	si
1					9	.6365	127.31	si
1					10	.6365	127.31	si
1					11	.6365	127.31	si
1					12	.6365	127.31	si
1					13	.6365	127.31	si
1					14	.6365	127.31	si
1					15	.6365	127.31	si
1					16	.6365	127.31	si
1					17	.6365	127.31	si
1					18	.6365	127.31	si
1					19	.6365	127.31	si
1					20	.6365	127.31	si
1					21	.6365	127.31	si
1					22	.6365	127.31	si
1					23	1.3069	261.38	si
1					24	1.3069	261.38	si
1					25	1.3069	261.38	si
1					26	1.3069	261.38	si
1					27	1.3069	261.38	si
1					28	1.3069	261.38	si
1					29	1.3069	261.38	si
1					30	1.3069	261.38	si
1					31	1.3069	261.38	si
1					32	1.3069	261.38	si
1					33	1.3069	261.38	si
1					34	1.3069	261.38	si
1					35	1.3069	261.38	si
1					36	1.3069	261.38	si
1					37	1.3069	261.38	si
1					38	1.3069	261.38	si
1					39	1.3069	261.38	si
1					40	1.3069	261.38	si
1					41	1.3069	261.38	si
1					42	1.3069	261.38	si
1					43	1.3069	261.38	si
1					44	1.3069	261.38	si
1					45	-.58	-116.01	si
1					46	-.58	-116.01	si
1					47	-.58	-116.01	si
1					48	-.58	-116.01	si
1					49	-.58	-116.01	si
1					50	-.58	-116.01	si
1					51	-.58	-116.01	si
1					52	-.58	-116.01	si
1					53	-.58	-116.01	si
1					54	-.58	-116.01	si
1					55	-.58	-116.01	si
1					56	-.58	-116.01	si
1					57	-.58	-116.01	si
1					58	-.58	-116.01	si
2	1- 1	1.3298	0.	si	1	.6055	121.11	si
2	1- 2	1.3298	0.	si	2	.6055	121.11	si
2	1- 3	-.6499	-7.68	si	3	.6055	121.11	si
2	1- 4	-.6499	-7.68	si	4	.6055	121.11	si
2					5	.6055	121.11	si
2					6	.6055	121.11	si
2					7	.6055	121.11	si
2					8	.6055	121.11	si
2					9	.6055	121.11	si
2					10	.6055	121.11	si
2					11	.6055	121.11	si
2					12	.6055	121.11	si
2					13	.6055	121.11	si
2					14	.6055	121.11	si
2					15	.6055	121.11	si
2					16	.6055	121.11	si
2					17	.6055	121.11	si
2					18	.6055	121.11	si
2					19	.6055	121.11	si
2					20	.6055	121.11	si
2					21	.6055	121.11	si
2					22	.6055	121.11	si
2					23	1.2574	251.48	si
2					24	1.2574	251.48	si
2					25	1.2574	251.48	si
2					26	1.2574	251.48	si

Convenzioni: N + trazione; Mz + fib. inferiori tese; My + fib. sinistra tese.

N.	N	Mz	My	Descrizione
1	-212.27	-1733.1624	-27203.6782	Caso 2.1
2	-354.44	-1705.3377	-45421.9841	Caso 2.2
3	-154.22	-940.6635	-19764.1616	Caso 13.1

RISULTATI

Piani di equilibrio (eps= muz * y + muy * z + lam):

Sol.	muz	muy	lambda
1.	.00002473021	0.	-.00036898955
2.	.00002400548	0.	-.0003714055
3.	.00001313483	0.	-.00019320587

Deformazioni sui materiali:

Cls					Acciaio lento			
sol	vert.	D cls	S cls	Ve	ferro	D ferri	S ferri	Ve
1	1- 1	1.3757	0.	si	1	.6338	126.76	si
1	1- 2	1.3757	0.	si	2	.6338	126.76	si
1	1- 3	-.6522	-7.7	si	3	.6338	126.76	si
1	1- 4	-.6522	-7.7	si	4	.6338	126.76	si
1					5	.6338	126.76	si
1					6	.6338	126.76	si
1					7	.6338	126.76	si
1					8	.6338	126.76	si
1					9	.6338	126.76	si
1					10	.6338	126.76	si
1					11	.6338	126.76	si
1					12	.6338	126.76	si
1					13	.6338	126.76	si
1					14	.6338	126.76	si
1					15	.6338	126.76	si
1					16	.6338	126.76	si
1					17	.6338	126.76	si
1					18	.6338	126.76	si
1					19	.6338	126.76	si
1					20	.6338	126.76	si
1					21	.6338	126.76	si
1					22	.6338	126.76	si
1					23	1.3015	260.31	si
1					24	1.3015	260.31	si
1					25	1.3015	260.31	si
1					26	1.3015	260.31	si
1					27	1.3015	260.31	si
1					28	1.3015	260.31	si
1					29	1.3015	260.31	si
1					30	1.3015	260.31	si
1					31	1.3015	260.31	si
1					32	1.3015	260.31	si
1					33	1.3015	260.31	si
1					34	1.3015	260.31	si
1					35	1.3015	260.31	si
1					36	1.3015	260.31	si
1					37	1.3015	260.31	si
1					38	1.3015	260.31	si
1					39	1.3015	260.31	si
1					40	1.3015	260.31	si
1					41	1.3015	260.31	si
1					42	1.3015	260.31	si
1					43	1.3015	260.31	si
1					44	1.3015	260.31	si
1					45	-.578	-115.59	si
1					46	-.578	-115.59	si
1					47	-.578	-115.59	si
1					48	-.578	-115.59	si
1					49	-.578	-115.59	si
1					50	-.578	-115.59	si
1					51	-.578	-115.59	si
1					52	-.578	-115.59	si
1					53	-.578	-115.59	si
1					54	-.578	-115.59	si
1					55	-.578	-115.59	si
1					56	-.578	-115.59	si
1					57	-.578	-115.59	si
1					58	-.578	-115.59	si
2	1- 1	1.3222	0.	si	1	.602	120.4	si
2	1- 2	1.3222	0.	si	2	.602	120.4	si
2	1- 3	-.6463	-7.65	si	3	.602	120.4	si
2	1- 4	-.6463	-7.65	si	4	.602	120.4	si
2					5	.602	120.4	si
2					6	.602	120.4	si
2					7	.602	120.4	si
2					8	.602	120.4	si
2					9	.602	120.4	si
2					10	.602	120.4	si
2					11	.602	120.4	si
2					12	.602	120.4	si
2					13	.602	120.4	si
2					14	.602	120.4	si
2					15	.602	120.4	si
2					16	.602	120.4	si
2					17	.602	120.4	si
2					18	.602	120.4	si
2					19	.602	120.4	si
2					20	.602	120.4	si
2					21	.602	120.4	si
2					22	.602	120.4	si
2					23	1.2502	250.03	si
2					24	1.2502	250.03	si
2					25	1.2502	250.03	si

Sforzi normali applicati in y= 29.55 (baricentro CLS)

Convenzioni: N + trazione; Mz + fib.inferiori tese; My + fib.sinistra tese.

N.	N	Mz	My	Descrizione
1	-209.7	-1729.2697	-32249.4779	Caso 2.1
2	-354.22	-1695.6387	-54473.6533	Caso 2.2
3	-153.46	-936.9606	-23600.4543	Caso 13.1

RISULTATI

Piani di equilibrio (eps= muz * y +muy * z + lam):

Sol.	muz	muy	lambda
1.	.00002467722	0.	-.00036793825
2.	.00002386016	0.	-.00036917351
3.	.0000130826	0.	-.00019239569

Deformazioni sui materiali:

sol	Cls				Acciaio lento			
	vert.	D cls	S cls	Ve	ferro	D ferri	S ferri	Ve
1	1- 1	1.373	0.	si	1	.6327	126.54	si
1	1- 2	1.373	0.	si	2	.6327	126.54	si
1	1- 3	-.6505	-7.69	si	3	.6327	126.54	si
1	1- 4	-.6505	-7.69	si	4	.6327	126.54	si
1					5	.6327	126.54	si
1					6	.6327	126.54	si
1					7	.6327	126.54	si
1					8	.6327	126.54	si
1					9	.6327	126.54	si
1					10	.6327	126.54	si
1					11	.6327	126.54	si
1					12	.6327	126.54	si
1					13	.6327	126.54	si
1					14	.6327	126.54	si
1					15	.6327	126.54	si
1					16	.6327	126.54	si
1					17	.6327	126.54	si
1					18	.6327	126.54	si
1					19	.6327	126.54	si
1					20	.6327	126.54	si
1					21	.6327	126.54	si
1					22	.6327	126.54	si
1					23	1.299	259.8	si
1					24	1.299	259.8	si
1					25	1.299	259.8	si
1					26	1.299	259.8	si
1					27	1.299	259.8	si
1					28	1.299	259.8	si
1					29	1.299	259.8	si
1					30	1.299	259.8	si
1					31	1.299	259.8	si
1					32	1.299	259.8	si
1					33	1.299	259.8	si
1					34	1.299	259.8	si
1					35	1.299	259.8	si
1					36	1.299	259.8	si
1					37	1.299	259.8	si
1					38	1.299	259.8	si
1					39	1.299	259.8	si
1					40	1.299	259.8	si
1					41	1.299	259.8	si
1					42	1.299	259.8	si
1					43	1.299	259.8	si
1					44	1.299	259.8	si
1					45	-.5765	-115.29	si
1					46	-.5765	-115.29	si
1					47	-.5765	-115.29	si
1					48	-.5765	-115.29	si
1					49	-.5765	-115.29	si
1					50	-.5765	-115.29	si
1					51	-.5765	-115.29	si
1					52	-.5765	-115.29	si
1					53	-.5765	-115.29	si
1					54	-.5765	-115.29	si
1					55	-.5765	-115.29	si
1					56	-.5765	-115.29	si
1					57	-.5765	-115.29	si
1					58	-.5765	-115.29	si
2	1- 1	1.3142	0.	si	1	.5984	119.67	si
2	1- 2	1.3142	0.	si	2	.5984	119.67	si
2	1- 3	-.6424	-7.61	si	3	.5984	119.67	si
2	1- 4	-.6424	-7.61	si	4	.5984	119.67	si
2					5	.5984	119.67	si
2					6	.5984	119.67	si
2					7	.5984	119.67	si
2					8	.5984	119.67	si
2					9	.5984	119.67	si
2					10	.5984	119.67	si
2					11	.5984	119.67	si
2					12	.5984	119.67	si
2					13	.5984	119.67	si
2					14	.5984	119.67	si
2					15	.5984	119.67	si
2					16	.5984	119.67	si
2					17	.5984	119.67	si
2					18	.5984	119.67	si
2					19	.5984	119.67	si
2					20	.5984	119.67	si
2					21	.5984	119.67	si
2					22	.5984	119.67	si
2					23	1.2426	248.52	si
2					24	1.2426	248.52	si

SOLLECITAZIONI AGENTI

Sforzi normali applicati in y= 29.55

Convenzioni: N + trazione; Mz + fib. inferiori tese; My + fib. sinistra tese.

N.	N	Mz	My	Descrizione
1	-214.58	-1734.0062	-38497.7849	Caso 2. 1
2	-356.69	-1698.1147	-63993.4083	Caso 2. 2
3	-154.37	-932.7779	-27696.5152	Caso 13. 1

RISULTATI

Piani di equilibrio (eps= muz * y +muy * z + lam):

Sol.	muz	muy	lambda
1.	.00002473792	0.	-.00036932701
2.	.00002389205	0.	-.00036989036
3.	.00001301965	0.	-.00019158454

Deformazioni sui materiali:

sol	Cls				Acciaio lento			
	vert.	D cls	S cls	Ve	ferro	D ferri	S ferri	Ve
1	1- 1	1.3759	0.	si	1	.6338	126.76	si
1	1- 2	1.3759	0.	si	2	.6338	126.76	si
1	1- 3	-.6526	-7.71	si	3	.6338	126.76	si
1	1- 4	-.6526	-7.71	si	4	.6338	126.76	si
1					5	.6338	126.76	si
1					6	.6338	126.76	si
1					7	.6338	126.76	si
1					8	.6338	126.76	si
1					9	.6338	126.76	si
1					10	.6338	126.76	si
1					11	.6338	126.76	si
1					12	.6338	126.76	si
1					13	.6338	126.76	si
1					14	.6338	126.76	si
1					15	.6338	126.76	si
1					16	.6338	126.76	si
1					17	.6338	126.76	si
1					18	.6338	126.76	si
1					19	.6338	126.76	si
1					20	.6338	126.76	si
1					21	.6338	126.76	si
1					22	.6338	126.76	si
1					23	1.3017	260.34	si
1					24	1.3017	260.34	si
1					25	1.3017	260.34	si
1					26	1.3017	260.34	si
1					27	1.3017	260.34	si
1					28	1.3017	260.34	si
1					29	1.3017	260.34	si
1					30	1.3017	260.34	si
1					31	1.3017	260.34	si
1					32	1.3017	260.34	si
1					33	1.3017	260.34	si
1					34	1.3017	260.34	si
1					35	1.3017	260.34	si
1					36	1.3017	260.34	si
1					37	1.3017	260.34	si
1					38	1.3017	260.34	si
1					39	1.3017	260.34	si
1					40	1.3017	260.34	si
1					41	1.3017	260.34	si
1					42	1.3017	260.34	si
1					43	1.3017	260.34	si
1					44	1.3017	260.34	si
1					45	-.5784	-115.67	si
1					46	-.5784	-115.67	si
1					47	-.5784	-115.67	si
1					48	-.5784	-115.67	si
1					49	-.5784	-115.67	si
1					50	-.5784	-115.67	si
1					51	-.5784	-115.67	si
1					52	-.5784	-115.67	si
1					53	-.5784	-115.67	si
1					54	-.5784	-115.67	si
1					55	-.5784	-115.67	si
1					56	-.5784	-115.67	si
1					57	-.5784	-115.67	si
1					58	-.5784	-115.67	si
2	1- 1	1.3157	0.	si	1	.5989	119.79	si
2	1- 2	1.3157	0.	si	2	.5989	119.79	si
2	1- 3	-.6435	-7.62	si	3	.5989	119.79	si
2	1- 4	-.6435	-7.62	si	4	.5989	119.79	si
2					5	.5989	119.79	si
2					6	.5989	119.79	si
2					7	.5989	119.79	si
2					8	.5989	119.79	si
2					9	.5989	119.79	si
2					10	.5989	119.79	si
2					11	.5989	119.79	si
2					12	.5989	119.79	si
2					13	.5989	119.79	si
2					14	.5989	119.79	si
2					15	.5989	119.79	si
2					16	.5989	119.79	si
2					17	.5989	119.79	si
2					18	.5989	119.79	si
2					19	.5989	119.79	si
2					20	.5989	119.79	si
2					21	.5989	119.79	si
2					22	.5989	119.79	si
2					23	1.244	248.8	si

Descrizione : Pulvi no 8

SOLLECITAZIONI AGENTI

Sforzi normali applicati in y= 29.55 (baricentro CLS)

Convenzioni: N + trazione; Mz + fib. inferiori tese; My + fib. sinistra tese.

N.	N	Mz	My	Descrizione
1	-214.72	-1740.4278	-44027.7599	Caso 2.1
2	-357.8	-1700.6188	-73365.033	Caso 2.2
3	-153.64	-929.1061	-31502.9884	Caso 13.1

RISULTATI

Piani di equilibrio (eps= muz * y + muy * z + lam):

Sol.	muz	muy	lambda
1.	.00002483421	0.	-.0003708065
2.	.0000239273	0.	-.00037053086
3.	.00001296781	0.	-.00019078327

Deformazioni sui materiali:

Cls					Acciaio lento			
sol	vert.	D cls	S cls	Ve	ferro	D ferri	S ferri	Ve
1	1- 1	1.3812	0.	si	1	.6362	127.24	si
1	1- 2	1.3812	0.	si	2	.6362	127.24	si
1	1- 3	-.6552	-7.73	si	3	.6362	127.24	si
1	1- 4	-.6552	-7.73	si	4	.6362	127.24	si
1					5	.6362	127.24	si
1					6	.6362	127.24	si
1					7	.6362	127.24	si
1					8	.6362	127.24	si
1					9	.6362	127.24	si
1					10	.6362	127.24	si
1					11	.6362	127.24	si
1					12	.6362	127.24	si
1					13	.6362	127.24	si
1					14	.6362	127.24	si
1					15	.6362	127.24	si
1					16	.6362	127.24	si
1					17	.6362	127.24	si
1					18	.6362	127.24	si
1					19	.6362	127.24	si
1					20	.6362	127.24	si
1					21	.6362	127.24	si
1					22	.6362	127.24	si
1					23	1.3067	261.35	si
1					24	1.3067	261.35	si
1					25	1.3067	261.35	si
1					26	1.3067	261.35	si
1					27	1.3067	261.35	si
1					28	1.3067	261.35	si
1					29	1.3067	261.35	si
1					30	1.3067	261.35	si
1					31	1.3067	261.35	si
1					32	1.3067	261.35	si
1					33	1.3067	261.35	si
1					34	1.3067	261.35	si
1					35	1.3067	261.35	si
1					36	1.3067	261.35	si
1					37	1.3067	261.35	si
1					38	1.3067	261.35	si
1					39	1.3067	261.35	si
1					40	1.3067	261.35	si
1					41	1.3067	261.35	si
1					42	1.3067	261.35	si
1					43	1.3067	261.35	si
1					44	1.3067	261.35	si
1					45	-.5807	-116.13	si
1					46	-.5807	-116.13	si
1					47	-.5807	-116.13	si
1					48	-.5807	-116.13	si
1					49	-.5807	-116.13	si
1					50	-.5807	-116.13	si
1					51	-.5807	-116.13	si
1					52	-.5807	-116.13	si
1					53	-.5807	-116.13	si
1					54	-.5807	-116.13	si
1					55	-.5807	-116.13	si
1					56	-.5807	-116.13	si
1					57	-.5807	-116.13	si
1					58	-.5807	-116.13	si
2	1- 1	1.3175	0.	si	1	.5997	119.94	si
2	1- 2	1.3175	0.	si	2	.5997	119.94	si
2	1- 3	-.6445	-7.63	si	3	.5997	119.94	si
2	1- 4	-.6445	-7.63	si	4	.5997	119.94	si
2					5	.5997	119.94	si
2					6	.5997	119.94	si
2					7	.5997	119.94	si
2					8	.5997	119.94	si
2					9	.5997	119.94	si
2					10	.5997	119.94	si
2					11	.5997	119.94	si
2					12	.5997	119.94	si
2					13	.5997	119.94	si
2					14	.5997	119.94	si
2					15	.5997	119.94	si
2					16	.5997	119.94	si
2					17	.5997	119.94	si
2					18	.5997	119.94	si
2					19	.5997	119.94	si
2					20	.5997	119.94	si
2					21	.5997	119.94	si

Descrizione : Pulvi no 9

SOLLECITAZIONI AGENTI

Sforzi normali applicati in y= 29.55 (baricentro CLS)

Convenzioni: N + trazione; Mz + fib. inferiori tese; My + fib. sinistra tese.

N.	N	Mz	My	Descrizione
1	-214.47	-1723.1011	-49471.5335	Caso 2.1
2	-357.53	-1679.7489	-82471.7633	Caso 2.2
3	-154.57	-924.87	-35654.204	Caso 13.1

RISULTATI

Piani di equilibrio (eps= muz * y + muy * z + lam):

Sol.	muz	muy	lambda
1.	.0000245742	0.	-.00036682551
2.	.00002361429	0.	-.00036574678
3.	.00001290406	0.	-.000189963

Deformazioni sui materiali:

Cls					Acciaio lento			
sol	vert.	D cls	S cls	Ve	ferro	D ferri	S ferri	Ve
1	1- 1	1.3669	0.	si	1	.6297	125.93	si
1	1- 2	1.3669	0.	si	2	.6297	125.93	si
1	1- 3	-.6482	-7.66	si	3	.6297	125.93	si
1	1- 4	-.6482	-7.66	si	4	.6297	125.93	si
1					5	.6297	125.93	si
1					6	.6297	125.93	si
1					7	.6297	125.93	si
1					8	.6297	125.93	si
1					9	.6297	125.93	si
1					10	.6297	125.93	si
1					11	.6297	125.93	si
1					12	.6297	125.93	si
1					13	.6297	125.93	si
1					14	.6297	125.93	si
1					15	.6297	125.93	si
1					16	.6297	125.93	si
1					17	.6297	125.93	si
1					18	.6297	125.93	si
1					19	.6297	125.93	si
1					20	.6297	125.93	si
1					21	.6297	125.93	si
1					22	.6297	125.93	si
1					23	1.2932	258.63	si
1					24	1.2932	258.63	si
1					25	1.2932	258.63	si
1					26	1.2932	258.63	si
1					27	1.2932	258.63	si
1					28	1.2932	258.63	si
1					29	1.2932	258.63	si
1					30	1.2932	258.63	si
1					31	1.2932	258.63	si
1					32	1.2932	258.63	si
1					33	1.2932	258.63	si
1					34	1.2932	258.63	si
1					35	1.2932	258.63	si
1					36	1.2932	258.63	si
1					37	1.2932	258.63	si
1					38	1.2932	258.63	si
1					39	1.2932	258.63	si
1					40	1.2932	258.63	si
1					41	1.2932	258.63	si
1					42	1.2932	258.63	si
1					43	1.2932	258.63	si
1					44	1.2932	258.63	si
1					45	-.5745	-114.9	si
1					46	-.5745	-114.9	si
1					47	-.5745	-114.9	si
1					48	-.5745	-114.9	si
1					49	-.5745	-114.9	si
1					50	-.5745	-114.9	si
1					51	-.5745	-114.9	si
1					52	-.5745	-114.9	si
1					53	-.5745	-114.9	si
1					54	-.5745	-114.9	si
1					55	-.5745	-114.9	si
1					56	-.5745	-114.9	si
1					57	-.5745	-114.9	si
1					58	-.5745	-114.9	si
2	1- 1	1.3002	0.	si	1	.5918	118.36	si
2	1- 2	1.3002	0.	si	2	.5918	118.36	si
2	1- 3	-.6361	-7.55	si	3	.5918	118.36	si
2	1- 4	-.6361	-7.55	si	4	.5918	118.36	si
2					5	.5918	118.36	si
2					6	.5918	118.36	si
2					7	.5918	118.36	si
2					8	.5918	118.36	si
2					9	.5918	118.36	si
2					10	.5918	118.36	si
2					11	.5918	118.36	si
2					12	.5918	118.36	si
2					13	.5918	118.36	si
2					14	.5918	118.36	si
2					15	.5918	118.36	si
2					16	.5918	118.36	si
2					17	.5918	118.36	si
2					18	.5918	118.36	si
2					19	.5918	118.36	si

Descrizione : Pulvino 10

SOLLECITAZIONI AGENTI

Sforzi normali applicati in y= 29.55 (baricentro CLS)

Convenzioni: N + trazione; Mz + fib.inferiori tese; My + fib.sinistra tese.

N.	N	Mz	My	Descrizione
1	-211.74	-1706.7052	-54268.9738	Caso 2.1
2	-353.71	-1660.3653	-90656.1378	Caso 2.2
3	-153.86	-921.2243	-39435.1344	Caso 13.1

RISULTATI

Piani di equilibrio (eps= muz * y + muy * z + lam):

Sol.	muz	muy	lambda
1.	.00002433372	0.	-.00036291166
2.	.00002333153	0.	-.00036109847
3.	.00001285258	0.	-.00018916901

Deformazioni sui materiali:

Cls					Acciaio lento			
sol	vert.	D cls	S cls	Ve	ferro	D ferri	S ferri	Ve
1	1- 1	1.3538	0.	si	1	.6238	124.76	si
1	1- 2	1.3538	0.	si	2	.6238	124.76	si
1	1- 3	-.6415	-7.6	si	3	.6238	124.76	si
1	1- 4	-.6415	-7.6	si	4	.6238	124.76	si
1					5	.6238	124.76	si
1					6	.6238	124.76	si
1					7	.6238	124.76	si
1					8	.6238	124.76	si
1					9	.6238	124.76	si
1					10	.6238	124.76	si
1					11	.6238	124.76	si
1					12	.6238	124.76	si
1					13	.6238	124.76	si
1					14	.6238	124.76	si
1					15	.6238	124.76	si
1					16	.6238	124.76	si
1					17	.6238	124.76	si
1					18	.6238	124.76	si
1					19	.6238	124.76	si
1					20	.6238	124.76	si
1					21	.6238	124.76	si
1					22	.6238	124.76	si
1					23	1.2808	256.17	si
1					24	1.2808	256.17	si
1					25	1.2808	256.17	si
1					26	1.2808	256.17	si
1					27	1.2808	256.17	si
1					28	1.2808	256.17	si
1					29	1.2808	256.17	si
1					30	1.2808	256.17	si
1					31	1.2808	256.17	si
1					32	1.2808	256.17	si
1					33	1.2808	256.17	si
1					34	1.2808	256.17	si
1					35	1.2808	256.17	si
1					36	1.2808	256.17	si
1					37	1.2808	256.17	si
1					38	1.2808	256.17	si
1					39	1.2808	256.17	si
1					40	1.2808	256.17	si
1					41	1.2808	256.17	si
1					42	1.2808	256.17	si
1					43	1.2808	256.17	si
1					44	1.2808	256.17	si
1					45	-.5685	-113.71	si
1					46	-.5685	-113.71	si
1					47	-.5685	-113.71	si
1					48	-.5685	-113.71	si
1					49	-.5685	-113.71	si
1					50	-.5685	-113.71	si
1					51	-.5685	-113.71	si
1					52	-.5685	-113.71	si
1					53	-.5685	-113.71	si
1					54	-.5685	-113.71	si
1					55	-.5685	-113.71	si
1					56	-.5685	-113.71	si
1					57	-.5685	-113.71	si
1					58	-.5685	-113.71	si
2	1- 1	1.2849	0.	si	1	.585	117.	si
2	1- 2	1.2849	0.	si	2	.585	117.	si
2	1- 3	-.6282	-7.47	si	3	.585	117.	si
2	1- 4	-.6282	-7.47	si	4	.585	117.	si
2					5	.585	117.	si
2					6	.585	117.	si
2					7	.585	117.	si
2					8	.585	117.	si
2					9	.585	117.	si
2					10	.585	117.	si
2					11	.585	117.	si
2					12	.585	117.	si
2					13	.585	117.	si
2					14	.585	117.	si
2					15	.585	117.	si
2					16	.585	117.	si
2					17	.585	117.	si
2					18	.585	117.	si

2				19	.585	117.	si
2				20	.585	117.	si
2				21	.585	117.	si
2				22	.585	117.	si
2				23	1.2149	242.99	si
2				24	1.2149	242.99	si
2				25	1.2149	242.99	si
2				26	1.2149	242.99	si
2				27	1.2149	242.99	si
2				28	1.2149	242.99	si
2				29	1.2149	242.99	si
2				30	1.2149	242.99	si
2				31	1.2149	242.99	si
2				32	1.2149	242.99	si
2				33	1.2149	242.99	si
2				34	1.2149	242.99	si
2				35	1.2149	242.99	si
2				36	1.2149	242.99	si
2				37	1.2149	242.99	si
2				38	1.2149	242.99	si
2				39	1.2149	242.99	si
2				40	1.2149	242.99	si
2				41	1.2149	242.99	si
2				42	1.2149	242.99	si
2				43	1.2149	242.99	si
2				44	1.2149	242.99	si
2				45	-.5582	-111.65	si
2				46	-.5582	-111.65	si
2				47	-.5582	-111.65	si
2				48	-.5582	-111.65	si
2				49	-.5582	-111.65	si
2				50	-.5582	-111.65	si
2				51	-.5582	-111.65	si
2				52	-.5582	-111.65	si
2				53	-.5582	-111.65	si
2				54	-.5582	-111.65	si
2				55	-.5582	-111.65	si
2				56	-.5582	-111.65	si
2				57	-.5582	-111.65	si
2				58	-.5582	-111.65	si
3	1- 1	.7176	0.	1	.332	66.4	si
3	1- 2	.7176	0.	2	.332	66.4	si
3	1- 3	-.3363	-4.35	3	.332	66.4	si
3	1- 4	-.3363	-4.35	4	.332	66.4	si
3				5	.332	66.4	si
3				6	.332	66.4	si
3				7	.332	66.4	si
3				8	.332	66.4	si
3				9	.332	66.4	si
3				10	.332	66.4	si
3				11	.332	66.4	si
3				12	.332	66.4	si
3				13	.332	66.4	si
3				14	.332	66.4	si
3				15	.332	66.4	si
3				16	.332	66.4	si
3				17	.332	66.4	si
3				18	.332	66.4	si
3				19	.332	66.4	si
3				20	.332	66.4	si
3				21	.332	66.4	si
3				22	.332	66.4	si
3				23	.679	135.8	si
3				24	.679	135.8	si
3				25	.679	135.8	si
3				26	.679	135.8	si
3				27	.679	135.8	si
3				28	.679	135.8	si
3				29	.679	135.8	si
3				30	.679	135.8	si
3				31	.679	135.8	si
3				32	.679	135.8	si
3				33	.679	135.8	si
3				34	.679	135.8	si
3				35	.679	135.8	si
3				36	.679	135.8	si
3				37	.679	135.8	si
3				38	.679	135.8	si
3				39	.679	135.8	si
3				40	.679	135.8	si
3				41	.679	135.8	si
3				42	.679	135.8	si
3				43	.679	135.8	si
3				44	.679	135.8	si
3				45	-.2978	-59.55	si
3				46	-.2978	-59.55	si
3				47	-.2978	-59.55	si
3				48	-.2978	-59.55	si
3				49	-.2978	-59.55	si
3				50	-.2978	-59.55	si
3				51	-.2978	-59.55	si
3				52	-.2978	-59.55	si
3				53	-.2978	-59.55	si
3				54	-.2978	-59.55	si
3				55	-.2978	-59.55	si
3				56	-.2978	-59.55	si
3				57	-.2978	-59.55	si

Descrizione : Pulvino 11**SOLLECITAZIONI AGENTI**Sforzi normali applicati in $y = 29.55$

Convenzioni: N + trazione; Mz + fib.inferiori tese; My + fib.sinistra tese.

N.	N	Mz	My	Descrizione
1	-212.15	-1701.8069	-59811.4451	Caso 2.1
2	-356.97	-1649.3916	-100639.3376	Caso 2.2
3	-154.86	-916.9108	-43658.1926	Caso 13.1

RISULTATIPiani di equilibrio ($\epsilon = \mu z * y + \mu y * z + \lambda$):

Sol.	μz	μy	λ
1.	.00002425927	0.	-.00036182046
2.	.00002315986	0.	-.0003588017
3.	.00001278755	0.	-.00018833761

Deformazioni sui materiali:

sol	Cls				Acciaio lento			
	vert.	D cls	S cls	Ve	ferro	D ferri	S ferri	Ve
1	1- 1	1.3497	0.	si	1	.6219	124.38	si
1	1- 2	1.3497	0.	si	2	.6219	124.38	si
1	1- 3	-.6396	-7.58	si	3	.6219	124.38	si
1	1- 4	-.6396	-7.58	si	4	.6219	124.38	si
1					5	.6219	124.38	si
1					6	.6219	124.38	si
1					7	.6219	124.38	si
1					8	.6219	124.38	si
1					9	.6219	124.38	si
1					10	.6219	124.38	si
1					11	.6219	124.38	si
1					12	.6219	124.38	si
1					13	.6219	124.38	si
1					14	.6219	124.38	si
1					15	.6219	124.38	si
1					16	.6219	124.38	si
1					17	.6219	124.38	si
1					18	.6219	124.38	si
1					19	.6219	124.38	si
1					20	.6219	124.38	si
1					21	.6219	124.38	si
1					22	.6219	124.38	si
1					23	1.2769	255.38	si
1					24	1.2769	255.38	si
1					25	1.2769	255.38	si
1					26	1.2769	255.38	si
1					27	1.2769	255.38	si
1					28	1.2769	255.38	si
1					29	1.2769	255.38	si
1					30	1.2769	255.38	si
1					31	1.2769	255.38	si
1					32	1.2769	255.38	si
1					33	1.2769	255.38	si
1					34	1.2769	255.38	si
1					35	1.2769	255.38	si
1					36	1.2769	255.38	si
1					37	1.2769	255.38	si
1					38	1.2769	255.38	si
1					39	1.2769	255.38	si
1					40	1.2769	255.38	si
1					41	1.2769	255.38	si
1					42	1.2769	255.38	si
1					43	1.2769	255.38	si
1					44	1.2769	255.38	si
1					45	-.5668	-113.36	si
1					46	-.5668	-113.36	si
1					47	-.5668	-113.36	si
1					48	-.5668	-113.36	si
1					49	-.5668	-113.36	si
1					50	-.5668	-113.36	si
1					51	-.5668	-113.36	si
1					52	-.5668	-113.36	si
1					53	-.5668	-113.36	si
1					54	-.5668	-113.36	si
1					55	-.5668	-113.36	si
1					56	-.5668	-113.36	si
1					57	-.5668	-113.36	si
1					58	-.5668	-113.36	si
2	1- 1	1.2751	0.	si	1	.5803	116.07	si
2	1- 2	1.2751	0.	si	2	.5803	116.07	si
2	1- 3	-.624	-7.43	si	3	.5803	116.07	si
2	1- 4	-.624	-7.43	si	4	.5803	116.07	si
2					5	.5803	116.07	si
2					6	.5803	116.07	si
2					7	.5803	116.07	si
2					8	.5803	116.07	si
2					9	.5803	116.07	si
2					10	.5803	116.07	si
2					11	.5803	116.07	si
2					12	.5803	116.07	si
2					13	.5803	116.07	si
2					14	.5803	116.07	si
2					15	.5803	116.07	si
2					16	.5803	116.07	si
2					17	.5803	116.07	si

2				18	. 5803	116. 07	si
2				19	. 5803	116. 07	si
2				20	. 5803	116. 07	si
2				21	. 5803	116. 07	si
2				22	. 5803	116. 07	si
2				23	1. 2056	241. 13	si
2				24	1. 2056	241. 13	si
2				25	1. 2056	241. 13	si
2				26	1. 2056	241. 13	si
2				27	1. 2056	241. 13	si
2				28	1. 2056	241. 13	si
2				29	1. 2056	241. 13	si
2				30	1. 2056	241. 13	si
2				31	1. 2056	241. 13	si
2				32	1. 2056	241. 13	si
2				33	1. 2056	241. 13	si
2				34	1. 2056	241. 13	si
2				35	1. 2056	241. 13	si
2				36	1. 2056	241. 13	si
2				37	1. 2056	241. 13	si
2				38	1. 2056	241. 13	si
2				39	1. 2056	241. 13	si
2				40	1. 2056	241. 13	si
2				41	1. 2056	241. 13	si
2				42	1. 2056	241. 13	si
2				43	1. 2056	241. 13	si
2				44	1. 2056	241. 13	si
2				45	-. 5545	-110. 9	si
2				46	-. 5545	-110. 9	si
2				47	-. 5545	-110. 9	si
2				48	-. 5545	-110. 9	si
2				49	-. 5545	-110. 9	si
2				50	-. 5545	-110. 9	si
2				51	-. 5545	-110. 9	si
2				52	-. 5545	-110. 9	si
2				53	-. 5545	-110. 9	si
2				54	-. 5545	-110. 9	si
2				55	-. 5545	-110. 9	si
2				56	-. 5545	-110. 9	si
2				57	-. 5545	-110. 9	si
2				58	-. 5545	-110. 9	si
3	1- 1	. 7138	0.	1	. 3302	66. 04	si
3	1- 2	. 7138	0.	2	. 3302	66. 04	si
3	1- 3	-. 3348	-4. 33	3	. 3302	66. 04	si
3	1- 4	-. 3348	-4. 33	4	. 3302	66. 04	si
3				5	. 3302	66. 04	si
3				6	. 3302	66. 04	si
3				7	. 3302	66. 04	si
3				8	. 3302	66. 04	si
3				9	. 3302	66. 04	si
3				10	. 3302	66. 04	si
3				11	. 3302	66. 04	si
3				12	. 3302	66. 04	si
3				13	. 3302	66. 04	si
3				14	. 3302	66. 04	si
3				15	. 3302	66. 04	si
3				16	. 3302	66. 04	si
3				17	. 3302	66. 04	si
3				18	. 3302	66. 04	si
3				19	. 3302	66. 04	si
3				20	. 3302	66. 04	si
3				21	. 3302	66. 04	si
3				22	. 3302	66. 04	si
3				23	. 6755	135. 09	si
3				24	. 6755	135. 09	si
3				25	. 6755	135. 09	si
3				26	. 6755	135. 09	si
3				27	. 6755	135. 09	si
3				28	. 6755	135. 09	si
3				29	. 6755	135. 09	si
3				30	. 6755	135. 09	si
3				31	. 6755	135. 09	si
3				32	. 6755	135. 09	si
3				33	. 6755	135. 09	si
3				34	. 6755	135. 09	si
3				35	. 6755	135. 09	si
3				36	. 6755	135. 09	si
3				37	. 6755	135. 09	si
3				38	. 6755	135. 09	si
3				39	. 6755	135. 09	si
3				40	. 6755	135. 09	si
3				41	. 6755	135. 09	si
3				42	. 6755	135. 09	si
3				43	. 6755	135. 09	si
3				44	. 6755	135. 09	si
3				45	-. 2964	-59. 28	si
3				46	-. 2964	-59. 28	si
3				47	-. 2964	-59. 28	si
3				48	-. 2964	-59. 28	si
3				49	-. 2964	-59. 28	si
3				50	-. 2964	-59. 28	si
3				51	-. 2964	-59. 28	si
3				52	-. 2964	-59. 28	si
3				53	-. 2964	-59. 28	si
3				54	-. 2964	-59. 28	si
3				55	-. 2964	-59. 28	si
3				56	-. 2964	-59. 28	si

3	57	-.2964	-59.28	si
3	58	-.2964	-59.28	si

Descrizi one : Pul vi no 12

SOLLECITAZIONI AGENTI

Sforzi normali applicati in y= 29.55

Convenzioni: N + trazione; Mz + fib.inferiori tese; My + fib.sinistra tese.

N.	N	Mz	My	Descrizione
1	-212.53	-1695.4582	-65366.5842	Caso 2.1
2	-354.29	-1642.4146	-108965.6667	Caso 2.2
3	-154.22	-913.2828	-47433.0661	Caso 13.1

RISULTATI

Piani di equilibrio (eps= muz * y +muy * z + lam):

Sol.	muz	muy	lambda
1.	.00002416312	0.	-.00036039779
2.	.00002306102	0.	-.0003570547
3.	.00001273619	0.	-.00018755209

Deformazioni sui materiali:

Cls					Acciaio lento			
sol	vert.	D cls	S cls	Ve	ferro	D ferri	S ferri	Ve
1	1- 1	1.3443	0.	si	1	.6194	123.88	si
1	1- 2	1.3443	0.	si	2	.6194	123.88	si
1	1- 3	-.6371	-7.56	si	3	.6194	123.88	si
1	1- 4	-.6371	-7.56	si	4	.6194	123.88	si
1					5	.6194	123.88	si
1					6	.6194	123.88	si
1					7	.6194	123.88	si
1					8	.6194	123.88	si
1					9	.6194	123.88	si
1					10	.6194	123.88	si
1					11	.6194	123.88	si
1					12	.6194	123.88	si
1					13	.6194	123.88	si
1					14	.6194	123.88	si
1					15	.6194	123.88	si
1					16	.6194	123.88	si
1					17	.6194	123.88	si
1					18	.6194	123.88	si
1					19	.6194	123.88	si
1					20	.6194	123.88	si
1					21	.6194	123.88	si
1					22	.6194	123.88	si
1					23	1.2718	254.36	si
1					24	1.2718	254.36	si
1					25	1.2718	254.36	si
1					26	1.2718	254.36	si
1					27	1.2718	254.36	si
1					28	1.2718	254.36	si
1					29	1.2718	254.36	si
1					30	1.2718	254.36	si
1					31	1.2718	254.36	si
1					32	1.2718	254.36	si
1					33	1.2718	254.36	si
1					34	1.2718	254.36	si
1					35	1.2718	254.36	si
1					36	1.2718	254.36	si
1					37	1.2718	254.36	si
1					38	1.2718	254.36	si
1					39	1.2718	254.36	si
1					40	1.2718	254.36	si
1					41	1.2718	254.36	si
1					42	1.2718	254.36	si
1					43	1.2718	254.36	si
1					44	1.2718	254.36	si
1					45	-.5646	-112.92	si
1					46	-.5646	-112.92	si
1					47	-.5646	-112.92	si
1					48	-.5646	-112.92	si
1					49	-.5646	-112.92	si
1					50	-.5646	-112.92	si
1					51	-.5646	-112.92	si
1					52	-.5646	-112.92	si
1					53	-.5646	-112.92	si
1					54	-.5646	-112.92	si
1					55	-.5646	-112.92	si
1					56	-.5646	-112.92	si
1					57	-.5646	-112.92	si
1					58	-.5646	-112.92	si
2	1- 1	1.2699	0.	si	1	.5781	115.61	si
2	1- 2	1.2699	0.	si	2	.5781	115.61	si
2	1- 3	-.6211	-7.4	si	3	.5781	115.61	si
2	1- 4	-.6211	-7.4	si	4	.5781	115.61	si
2					5	.5781	115.61	si
2					6	.5781	115.61	si
2					7	.5781	115.61	si
2					8	.5781	115.61	si
2					9	.5781	115.61	si
2					10	.5781	115.61	si
2					11	.5781	115.61	si
2					12	.5781	115.61	si
2					13	.5781	115.61	si
2					14	.5781	115.61	si
2					15	.5781	115.61	si
2					16	.5781	115.61	si

2				17	. 5781	115. 61	si
2				18	. 5781	115. 61	si
2				19	. 5781	115. 61	si
2				20	. 5781	115. 61	si
2				21	. 5781	115. 61	si
2				22	. 5781	115. 61	si
2				23	1. 2007	240. 14	si
2				24	1. 2007	240. 14	si
2				25	1. 2007	240. 14	si
2				26	1. 2007	240. 14	si
2				27	1. 2007	240. 14	si
2				28	1. 2007	240. 14	si
2				29	1. 2007	240. 14	si
2				30	1. 2007	240. 14	si
2				31	1. 2007	240. 14	si
2				32	1. 2007	240. 14	si
2				33	1. 2007	240. 14	si
2				34	1. 2007	240. 14	si
2				35	1. 2007	240. 14	si
2				36	1. 2007	240. 14	si
2				37	1. 2007	240. 14	si
2				38	1. 2007	240. 14	si
2				39	1. 2007	240. 14	si
2				40	1. 2007	240. 14	si
2				41	1. 2007	240. 14	si
2				42	1. 2007	240. 14	si
2				43	1. 2007	240. 14	si
2				44	1. 2007	240. 14	si
2				45	-. 5519	-110. 38	si
2				46	-. 5519	-110. 38	si
2				47	-. 5519	-110. 38	si
2				48	-. 5519	-110. 38	si
2				49	-. 5519	-110. 38	si
2				50	-. 5519	-110. 38	si
2				51	-. 5519	-110. 38	si
2				52	-. 5519	-110. 38	si
2				53	-. 5519	-110. 38	si
2				54	-. 5519	-110. 38	si
2				55	-. 5519	-110. 38	si
2				56	-. 5519	-110. 38	si
2				57	-. 5519	-110. 38	si
2				58	-. 5519	-110. 38	si
3	1- 1	. 711	0.	1	. 3289	65. 78	si
3	1- 2	. 711	0.	2	. 3289	65. 78	si
3	1- 3	-. 3334	-4. 31	3	. 3289	65. 78	si
3	1- 4	-. 3334	-4. 31	4	. 3289	65. 78	si
3				5	. 3289	65. 78	si
3				6	. 3289	65. 78	si
3				7	. 3289	65. 78	si
3				8	. 3289	65. 78	si
3				9	. 3289	65. 78	si
3				10	. 3289	65. 78	si
3				11	. 3289	65. 78	si
3				12	. 3289	65. 78	si
3				13	. 3289	65. 78	si
3				14	. 3289	65. 78	si
3				15	. 3289	65. 78	si
3				16	. 3289	65. 78	si
3				17	. 3289	65. 78	si
3				18	. 3289	65. 78	si
3				19	. 3289	65. 78	si
3				20	. 3289	65. 78	si
3				21	. 3289	65. 78	si
3				22	. 3289	65. 78	si
3				23	. 6728	134. 56	si
3				24	. 6728	134. 56	si
3				25	. 6728	134. 56	si
3				26	. 6728	134. 56	si
3				27	. 6728	134. 56	si
3				28	. 6728	134. 56	si
3				29	. 6728	134. 56	si
3				30	. 6728	134. 56	si
3				31	. 6728	134. 56	si
3				32	. 6728	134. 56	si
3				33	. 6728	134. 56	si
3				34	. 6728	134. 56	si
3				35	. 6728	134. 56	si
3				36	. 6728	134. 56	si
3				37	. 6728	134. 56	si
3				38	. 6728	134. 56	si
3				39	. 6728	134. 56	si
3				40	. 6728	134. 56	si
3				41	. 6728	134. 56	si
3				42	. 6728	134. 56	si
3				43	. 6728	134. 56	si
3				44	. 6728	134. 56	si
3				45	-. 2952	-59. 03	si
3				46	-. 2952	-59. 03	si
3				47	-. 2952	-59. 03	si
3				48	-. 2952	-59. 03	si
3				49	-. 2952	-59. 03	si
3				50	-. 2952	-59. 03	si
3				51	-. 2952	-59. 03	si
3				52	-. 2952	-59. 03	si
3				53	-. 2952	-59. 03	si
3				54	-. 2952	-59. 03	si
3				55	-. 2952	-59. 03	si

3	56	-. 2952	-59.03	si
3	57	-. 2952	-59.03	si
3	58	-. 2952	-59.03	si

Descrizione : Pulvino 13

SOLLECITAZIONI AGENTI

Sforzi normali applicati in y= 29.55

Convenzioni: N + trazione; Mz + fib.inferiori tese; My + fib.sinistra tese.

N.	N	Mz	My	Descrizione
1	-213.31	-1690.073	-71072.0971	Caso 2.1
2	-155.25	-908.9094	-51726.7084	Caso 13.1
3	-357.3	-1631.7052	-119047.3802	Caso 2.2
4	-154.87	-1089.8584	-51602.4011	Caso 7.23

RISULTATI

Piani di equilibrio (eps= muz * y + muy * z + lam):

Sol.	muz	muy	lambda
1.	.00002408059	0.	-.00035922046
2.	.00001267024	0.	-.00018671084
3.	.00002289397	0.	-.00035480822
4.	.00001531248	0.	-.00022437188

Deformazioni sui materiali:

Cls					Acciaio lento			
sol	vert.	D cls	S cls	Ve	ferro	D ferri	S ferri	Ve
1	1- 1	1.3397	0.	si	1	.6172	123.45	si
1	1- 2	1.3397	0.	si	2	.6172	123.45	si
1	1- 3	-.6349	-7.54	si	3	.6172	123.45	si
1	1- 4	-.6349	-7.54	si	4	.6172	123.45	si
1					5	.6172	123.45	si
1					6	.6172	123.45	si
1					7	.6172	123.45	si
1					8	.6172	123.45	si
1					9	.6172	123.45	si
1					10	.6172	123.45	si
1					11	.6172	123.45	si
1					12	.6172	123.45	si
1					13	.6172	123.45	si
1					14	.6172	123.45	si
1					15	.6172	123.45	si
1					16	.6172	123.45	si
1					17	.6172	123.45	si
1					18	.6172	123.45	si
1					19	.6172	123.45	si
1					20	.6172	123.45	si
1					21	.6172	123.45	si
1					22	.6172	123.45	si
1					23	1.2674	253.48	si
1					24	1.2674	253.48	si
1					25	1.2674	253.48	si
1					26	1.2674	253.48	si
1					27	1.2674	253.48	si
1					28	1.2674	253.48	si
1					29	1.2674	253.48	si
1					30	1.2674	253.48	si
1					31	1.2674	253.48	si
1					32	1.2674	253.48	si
1					33	1.2674	253.48	si
1					34	1.2674	253.48	si
1					35	1.2674	253.48	si
1					36	1.2674	253.48	si
1					37	1.2674	253.48	si
1					38	1.2674	253.48	si
1					39	1.2674	253.48	si
1					40	1.2674	253.48	si
1					41	1.2674	253.48	si
1					42	1.2674	253.48	si
1					43	1.2674	253.48	si
1					44	1.2674	253.48	si
1					45	-.5627	-112.54	si
1					46	-.5627	-112.54	si
1					47	-.5627	-112.54	si
1					48	-.5627	-112.54	si
1					49	-.5627	-112.54	si
1					50	-.5627	-112.54	si
1					51	-.5627	-112.54	si
1					52	-.5627	-112.54	si
1					53	-.5627	-112.54	si
1					54	-.5627	-112.54	si
1					55	-.5627	-112.54	si
1					56	-.5627	-112.54	si
1					57	-.5627	-112.54	si
1					58	-.5627	-112.54	si
2	1- 1	.7072	0.	si	1	.3271	65.41	si
2	1- 2	.7072	0.	si	2	.3271	65.41	si
2	1- 3	-.3318	-4.29	si	3	.3271	65.41	si
2	1- 4	-.3318	-4.29	si	4	.3271	65.41	si
2					5	.3271	65.41	si
2					6	.3271	65.41	si
2					7	.3271	65.41	si
2					8	.3271	65.41	si
2					9	.3271	65.41	si
2					10	.3271	65.41	si
2					11	.3271	65.41	si
2					12	.3271	65.41	si
2					13	.3271	65.41	si

3				53	-.5483	-109.65	si
3				54	-.5483	-109.65	si
3				55	-.5483	-109.65	si
3				56	-.5483	-109.65	si
3				57	-.5483	-109.65	si
3				58	-.5483	-109.65	si
4	1- 1	.8559	0.	1	.3965	79.31	si
4	1- 2	.8559	0.	2	.3965	79.31	si
4	1- 3	-.3997	-5.08	3	.3965	79.31	si
4	1- 4	-.3997	-5.08	4	.3965	79.31	si
4				5	.3965	79.31	si
4				6	.3965	79.31	si
4				7	.3965	79.31	si
4				8	.3965	79.31	si
4				9	.3965	79.31	si
4				10	.3965	79.31	si
4				11	.3965	79.31	si
4				12	.3965	79.31	si
4				13	.3965	79.31	si
4				14	.3965	79.31	si
4				15	.3965	79.31	si
4				16	.3965	79.31	si
4				17	.3965	79.31	si
4				18	.3965	79.31	si
4				19	.3965	79.31	si
4				20	.3965	79.31	si
4				21	.3965	79.31	si
4				22	.3965	79.31	si
4				23	.81	162.	si
4				24	.81	162.	si
4				25	.81	162.	si
4				26	.81	162.	si
4				27	.81	162.	si
4				28	.81	162.	si
4				29	.81	162.	si
4				30	.81	162.	si
4				31	.81	162.	si
4				32	.81	162.	si
4				33	.81	162.	si
4				34	.81	162.	si
4				35	.81	162.	si
4				36	.81	162.	si
4				37	.81	162.	si
4				38	.81	162.	si
4				39	.81	162.	si
4				40	.81	162.	si
4				41	.81	162.	si
4				42	.81	162.	si
4				43	.81	162.	si
4				44	.81	162.	si
4				45	-.3538	-70.75	si
4				46	-.3538	-70.75	si
4				47	-.3538	-70.75	si
4				48	-.3538	-70.75	si
4				49	-.3538	-70.75	si
4				50	-.3538	-70.75	si
4				51	-.3538	-70.75	si
4				52	-.3538	-70.75	si
4				53	-.3538	-70.75	si
4				54	-.3538	-70.75	si
4				55	-.3538	-70.75	si
4				56	-.3538	-70.75	si
4				57	-.3538	-70.75	si
4				58	-.3538	-70.75	si

Descrizione : Pulvino 14

SOLLECITAZIONI AGENTI

Sforzi normali applicati in $y=29.55$

Convenzioni: N + trazione; Mz + fib.inferiori tese; My + fib.sinistra tese.

N.	N	Mz	My	Descrizione
1	-213.13	-1684.7059	-76474.0491	Caso 2.1
2	-154.7	-905.2687	-55509.3045	Caso 13.1
3	-355.5	-1623.6959	-127559.9041	Caso 2.2
4	-148.47	-1088.5556	-53276.0186	Caso 7.23

RISULTATI

Piani di equilibrio ($\epsilon = \mu z * y + \mu y * z + \lambda m$):

Sol.	μz	μy	λ
1.	.00002400043	0.	-.00035798838
2.	.00001261851	0.	-.00018592868
3.	.00002277784	0.	-.00035288482
4.	.00001530763	0.	-.00022371676

Deformazioni sui materiali:

sol	Cls				Acciaio lento			
	vert.	D cls	S cls	Ve	ferro	D ferri	S ferri	Ve
1	1- 1	1.3352	0.	si	1	.6152	123.05	si
1	1- 2	1.3352	0.	si	2	.6152	123.05	si
1	1- 3	-.6328	-7.52	si	3	.6152	123.05	si
1	1- 4	-.6328	-7.52	si	4	.6152	123.05	si
1					5	.6152	123.05	si
1					6	.6152	123.05	si
1					7	.6152	123.05	si
1					8	.6152	123.05	si
1					9	.6152	123.05	si
1					10	.6152	123.05	si

4	31	. 8103	162. 06	si
4	32	. 8103	162. 06	si
4	33	. 8103	162. 06	si
4	34	. 8103	162. 06	si
4	35	. 8103	162. 06	si
4	36	. 8103	162. 06	si
4	37	. 8103	162. 06	si
4	38	. 8103	162. 06	si
4	39	. 8103	162. 06	si
4	40	. 8103	162. 06	si
4	41	. 8103	162. 06	si
4	42	. 8103	162. 06	si
4	43	. 8103	162. 06	si
4	44	. 8103	162. 06	si
4	45	-. 3531	- 70. 61	si
4	46	-. 3531	- 70. 61	si
4	47	-. 3531	- 70. 61	si
4	48	-. 3531	- 70. 61	si
4	49	-. 3531	- 70. 61	si
4	50	-. 3531	- 70. 61	si
4	51	-. 3531	- 70. 61	si
4	52	-. 3531	- 70. 61	si
4	53	-. 3531	- 70. 61	si
4	54	-. 3531	- 70. 61	si
4	55	-. 3531	- 70. 61	si
4	56	-. 3531	- 70. 61	si
4	57	-. 3531	- 70. 61	si
4	58	-. 3531	- 70. 61	si

Descrizione : Pulvino 15

SOLLECITAZIONI AGENTI

Sforzi normali applicati in $y = 29.55$

Convenzioni: N + trazione; Mz + fib.inferiori tese; My + fib.sinistra tese.

N.	N	Mz	My	Descrizione
1	- 216. 16	- 1678. 002	- 83097. 0846	Caso 2. 1
2	- 156. 02	- 900. 7344	- 59978. 2861	Caso 13. 1
3	- 357. 36	- 1613. 7023	- 137381. 2557	Caso 2. 2
4	- 143. 96	- 1086. 6702	- 55345. 4929	Caso 7. 23

RISULTATI

Piani di equilibrio ($\epsilon = \mu z * y + \mu y * z + \lambda$):

Sol.	muz	muy	lambda
1.	. 0000238933	0.	-. 00035665296
2.	. 00001254959	0.	-. 00018507198
3.	. 00002262412	0.	-. 00035073619
4.	. 00001529004	0.	-. 00022305136

Deformazioni sui materiali:

sol	Cls				Acciaio lento			
	vert.	D cls	S cls	Ve	ferro	D ferri	S ferri	Ve
1	1- 1	1. 329	0.	si	1	. 6122	122. 44	si
1	1- 2	1. 329	0.	si	2	. 6122	122. 44	si
1	1- 3	-. 6302	- 7. 49	si	3	. 6122	122. 44	si
1	1- 4	-. 6302	- 7. 49	si	4	. 6122	122. 44	si
1					5	. 6122	122. 44	si
1					6	. 6122	122. 44	si
1					7	. 6122	122. 44	si
1					8	. 6122	122. 44	si
1					9	. 6122	122. 44	si
1					10	. 6122	122. 44	si
1					11	. 6122	122. 44	si
1					12	. 6122	122. 44	si
1					13	. 6122	122. 44	si
1					14	. 6122	122. 44	si
1					15	. 6122	122. 44	si
1					16	. 6122	122. 44	si
1					17	. 6122	122. 44	si
1					18	. 6122	122. 44	si
1					19	. 6122	122. 44	si
1					20	. 6122	122. 44	si
1					21	. 6122	122. 44	si
1					22	. 6122	122. 44	si
1					23	1. 2573	251. 47	si
1					24	1. 2573	251. 47	si
1					25	1. 2573	251. 47	si
1					26	1. 2573	251. 47	si
1					27	1. 2573	251. 47	si
1					28	1. 2573	251. 47	si
1					29	1. 2573	251. 47	si
1					30	1. 2573	251. 47	si
1					31	1. 2573	251. 47	si
1					32	1. 2573	251. 47	si
1					33	1. 2573	251. 47	si
1					34	1. 2573	251. 47	si
1					35	1. 2573	251. 47	si
1					36	1. 2573	251. 47	si
1					37	1. 2573	251. 47	si
1					38	1. 2573	251. 47	si
1					39	1. 2573	251. 47	si
1					40	1. 2573	251. 47	si
1					41	1. 2573	251. 47	si
1					42	1. 2573	251. 47	si
1					43	1. 2573	251. 47	si
1					44	1. 2573	251. 47	si
1					45	-. 5586	- 111. 71	si
1					46	-. 5586	- 111. 71	si

VERIFICA SEZIONI PULVINI (sezione y-z):

PARAMETRI GENERALI

Tipo verifica : stati limite - pressoflessione deviata.
 Unità di misura generiche: kN; cm; kNm; N/mm²; d in mm; deformazioni *1000.
 ferri : diametri in mm; aree in cm².

Simboli :

Vert. = contorno vertice del CLS; d = diametro;
 S = Sigma (tensioni sui materiali);
 D = Deformazioni x 1000 (epsilon);
 Ve = colonna che indica se la verifica e' soddisfatta;

CARATTERISTICHE MATERIALI

Calcestruzzo: Rck = 30. ; fck = 24.9 ; fcd = 14.11 (.35%)
 Acciaio : Tipo= B450C ; ftk = 540. ; fyk = 450. ; ftd = 469.565 (6.75%)

CARATTERISTICHE SEZIONE

L'asse Z e' rivolto verso destra, l'asse Y e' rivolto verso l'alto.

Tipo sezione: U_Pul

Cl s:

vert.		Z	Y	Acciaio lento:		d [mm]	Af [cm ²]
1-	2			ferro	Z	Y	
1- 1	0.	55.	1	301.4	79.	20.	3.1416
1- 2	63.	55.	2	285.7	79.	20.	3.1416
1- 3	63.	82.	3	270.	79.	20.	3.1416
1- 4	304.4	82.	4	254.3	79.	20.	3.1416
1- 5	304.4	55.	5	238.6	79.	20.	3.1416
1- 6	367.4	55.	6	222.9	79.	20.	3.1416
1- 7	367.4	0.	7	207.2	79.	20.	3.1416
1- 8	0.	0.	8	191.5	79.	20.	3.1416
			9	175.9	79.	20.	3.1416
			10	160.2	79.	20.	3.1416
			11	144.5	79.	20.	3.1416
			12	128.8	79.	20.	3.1416
			13	113.1	79.	20.	3.1416
			14	97.4	79.	20.	3.1416
			15	81.7	79.	20.	3.1416
			16	66.	79.	20.	3.1416
			17	66.	52.	20.	3.1416
			18	45.	52.	20.	3.1416
			19	24.	52.	20.	3.1416
			20	3.	52.	20.	3.1416
			21	364.4	52.	20.	3.1416
			22	343.4	52.	20.	3.1416
			23	322.4	52.	20.	3.1416
			24	301.4	52.	20.	3.1416
			25	364.4	3.	20.	3.1416
			26	348.7	3.	20.	3.1416
			27	333.	3.	20.	3.1416
			28	317.3	3.	20.	3.1416
			29	301.5	3.	20.	3.1416
			30	285.8	3.	20.	3.1416
			31	270.1	3.	20.	3.1416
			32	254.4	3.	20.	3.1416
			33	238.7	3.	20.	3.1416
			34	223.	3.	20.	3.1416
			35	207.3	3.	20.	3.1416
			36	191.6	3.	20.	3.1416
			37	175.8	3.	20.	3.1416
			38	160.1	3.	20.	3.1416
			39	144.4	3.	20.	3.1416
			40	128.7	3.	20.	3.1416
			41	113.	3.	20.	3.1416
			42	97.3	3.	20.	3.1416
			43	81.6	3.	20.	3.1416
			44	65.9	3.	20.	3.1416
			45	50.1	3.	20.	3.1416
			46	34.4	3.	20.	3.1416
			47	18.7	3.	20.	3.1416
			48	3.	3.	20.	3.1416

Descrizione : Pulvino 1

SOLLECITAZIONI AGENTI

Sforzi normali applicati in z= 183.7 ; y= 37.5 (baricentro CLS)

Convenzioni: N + trazione; Mz + fib.inferiori tese; My + fib.sinistra tese.

N.	N	Mz	My	Descrizione
1	-243.62	-855.8193	-226.9263	Caso 2.1
2	-129.52	-472.6612	-237.9249	Caso 13.1
3	-197.67	-556.7633	-1066.0253	Caso 7.22
4	-115.95	-556.5847	489.9101	Caso 7.11
5	-253.5	-556.8497	-260.6506	Caso 6.20
6	-60.12	-556.4983	-315.4646	Caso 6.13

RISULTATI

Piani di equilibrio (eps= muz * y + muy * z + lam):

Sol.	muz	muy	lambda
1.	.00001442131	.00000017568	-.00028184997
2.	.00000796243	.00000018231	-.00016915003
3.	.00000920734	.00000088509	-.00030445484
4.	.00000952892	-.0000003872	-.00008553115
5.	.00000899799	.00000019208	-.00019802351
6.	.00000973772	.00000025251	-.00020356955

Deformazioni sui materiali:

Cl s				Acciaio lento				
sol	vert.	D cls	S cls	Ve	ferro	D ferri	S ferri	Ve
1	1- 1	.5113	0.	si	1	.9104	182.08	si
1	1- 2	.5224	0.	si	2	.9076	181.53	si
1	1- 3	.9118	0.	si	3	.9049	180.97	si
1	1- 4	.9542	0.	si	4	.9021	180.42	si

1	1- 5	. 5648	0.	si	5	. 8994	179. 87	si
1	1- 6	. 5759	0.	si	6	. 8966	179. 32	si
1	1- 7	- . 2173	-2. 9	si	7	. 8938	178. 77	si
1	1- 8	- . 2818	-3. 7	si	8	. 8911	178. 22	si
1					9	. 8883	177. 67	si
1					10	. 8856	177. 11	si
1					11	. 8828	176. 56	si
1					12	. 8801	176. 01	si
1					13	. 8773	175. 46	si
1					14	. 8745	174. 91	si
1					15	. 8718	174. 36	si
1					16	. 869	173. 81	si
1					17	. 4797	95. 93	si
1					18	. 476	95. 19	si
1					19	. 4723	94. 45	si
1					20	. 4686	93. 72	si
1					21	. 5321	106. 42	si
1					22	. 5284	105. 68	si
1					23	. 5247	104. 94	si
1					24	. 521	104. 2	si
1					25	- . 1746	-34. 91	si
1					26	- . 1773	-35. 47	si
1					27	- . 1801	-36. 02	si
1					28	- . 1828	-36. 57	si
1					29	- . 1856	-37. 12	si
1					30	- . 1884	-37. 67	si
1					31	- . 1911	-38. 23	si
1					32	- . 1939	-38. 78	si
1					33	- . 1967	-39. 33	si
1					34	- . 1994	-39. 88	si
1					35	- . 2022	-40. 43	si
1					36	- . 2049	-40. 99	si
1					37	- . 2077	-41. 54	si
1					38	- . 2105	-42. 09	si
1					39	- . 2132	-42. 64	si
1					40	- . 216	-43. 19	si
1					41	- . 2187	-43. 75	si
1					42	- . 2215	-44. 3	si
1					43	- . 2243	-44. 85	si
1					44	- . 227	-45. 4	si
1					45	- . 2298	-45. 96	si
1					46	- . 2325	-46. 51	si
1					47	- . 2353	-47. 06	si
1					48	- . 2381	-47. 61	si
2	1- 1	. 2688	0.	si	1	. 5148	102. 97	si
2	1- 2	. 2803	0.	si	2	. 512	102. 39	si
2	1- 3	. 4953	0.	si	3	. 5091	101. 82	si
2	1- 4	. 5393	0.	si	4	. 5062	101. 25	si
2	1- 5	. 3243	0.	si	5	. 5034	100. 68	si
2	1- 6	. 3358	0.	si	6	. 5005	100. 1	si
2	1- 7	- . 1022	-1. 4	si	7	. 4977	99. 53	si
2	1- 8	- . 1692	-2. 29	si	8	. 4948	98. 96	si
2					9	. 4919	98. 39	si
2					10	. 4891	97. 82	si
2					11	. 4862	97. 24	si
2					12	. 4834	96. 67	si
2					13	. 4805	96. 1	si
2					14	. 4776	95. 53	si
2					15	. 4748	94. 96	si
2					16	. 4719	94. 38	si
2					17	. 2569	51. 39	si
2					18	. 2531	50. 62	si
2					19	. 2493	49. 85	si
2					20	. 2454	49. 09	si
2					21	. 3113	62. 27	si
2					22	. 3075	61. 5	si
2					23	. 3037	60. 73	si
2					24	. 2998	59. 97	si
2					25	- . 0788	-15. 77	si
2					26	- . 0817	-16. 34	si
2					27	- . 0846	-16. 91	si
2					28	- . 0874	-17. 48	si
2					29	- . 0903	-18. 06	si
2					30	- . 0932	-18. 63	si
2					31	- . 096	-19. 2	si
2					32	- . 0989	-19. 78	si
2					33	- . 1017	-20. 35	si
2					34	- . 1046	-20. 92	si
2					35	- . 1075	-21. 5	si
2					36	- . 1103	-22. 07	si
2					37	- . 1132	-22. 64	si
2					38	- . 1161	-23. 21	si
2					39	- . 1189	-23. 79	si
2					40	- . 1218	-24. 36	si
2					41	- . 1247	-24. 93	si
2					42	- . 1275	-25. 51	si
2					43	- . 1304	-26. 08	si
2					44	- . 1333	-26. 65	si
2					45	- . 1361	-27. 22	si
2					46	- . 139	-27. 8	si
2					47	- . 1419	-28. 37	si
2					48	- . 1447	-28. 94	si
3	1- 1	. 2019	0.	si	1	. 6897	137. 94	si
3	1- 2	. 2577	0.	si	2	. 6758	135. 16	si
3	1- 3	. 5063	0.	si	3	. 6619	132. 38	si
3	1- 4	. 72	0.	si	4	. 648	129. 6	si
3	1- 5	. 4714	0.	si	5	. 6341	126. 83	si

3	1- 6	. 5271	0.	si	6	. 6202	124. 05	si
3	1- 7	. 0207	0.	si	7	. 6064	121. 27	si
3	1- 8	- . 3045	-3. 97	si	8	. 5925	118. 49	si
3					9	. 5786	115. 71	si
3					10	. 5647	112. 94	si
3					11	. 5508	110. 16	si
3					12	. 5369	107. 38	si
3					13	. 523	104. 6	si
3					14	. 5091	101. 82	si
3					15	. 4952	99. 05	si
3					16	. 4813	96. 27	si
3					17	. 2327	46. 55	si
3					18	. 2142	42. 83	si
3					19	. 1956	39. 11	si
3					20	. 177	35. 4	si
3					21	. 4969	99. 37	si
3					22	. 4783	95. 65	si
3					23	. 4597	91. 94	si
3					24	. 4411	88. 22	si
3					25	. 0457	9. 14	si
3					26	. 0318	6. 36	si
3					27	. 0179	3. 58	si
3					28	. 004	. 79	si
3					29	- . 0099	-1. 99	si
3					30	- . 0238	-4. 77	si
3					31	- . 0377	-7. 55	si
3					32	- . 0517	-10. 33	si
3					33	- . 0656	-13. 11	si
3					34	- . 0795	-15. 89	si
3					35	- . 0934	-18. 68	si
3					36	- . 1073	-21. 46	si
3					37	- . 1212	-24. 24	si
3					38	- . 1351	-27. 02	si
3					39	- . 149	-29. 8	si
3					40	- . 1629	-32. 58	si
3					41	- . 1768	-35. 37	si
3					42	- . 1907	-38. 15	si
3					43	- . 2046	-40. 93	si
3					44	- . 2185	-43. 71	si
3					45	- . 2325	-46. 49	si
3					46	- . 2464	-49. 27	si
3					47	- . 2603	-52. 05	si
3					48	- . 2742	-54. 84	si
4	1- 1	. 4386	0.	si	1	. 5506	110. 11	si
4	1- 2	. 4142	0.	si	2	. 5566	111. 33	si
4	1- 3	. 6714	0.	si	3	. 5627	112. 54	si
4	1- 4	. 578	0.	si	4	. 5688	113. 76	si
4	1- 5	. 3207	0.	si	5	. 5749	114. 97	si
4	1- 6	. 2963	0.	si	6	. 5809	116. 19	si
4	1- 7	- . 2278	-3. 03	si	7	. 587	117. 4	si
4	1- 8	- . 0855	-1. 18	si	8	. 5931	118. 62	si
4					9	. 5992	119. 83	si
4					10	. 6052	121. 05	si
4					11	. 6113	122. 26	si
4					12	. 6174	123. 48	si
4					13	. 6235	124. 69	si
4					14	. 6295	125. 91	si
4					15	. 6356	127. 12	si
4					16	. 6417	128. 34	si
4					17	. 3844	76. 88	si
4					18	. 3925	78. 51	si
4					19	. 4007	80. 14	si
4					20	. 4088	81. 76	si
4					21	. 2689	53. 78	si
4					22	. 277	55. 4	si
4					23	. 2851	57. 03	si
4					24	. 2933	58. 65	si
4					25	- . 198	-39. 61	si
4					26	- . 192	-38. 39	si
4					27	- . 1859	-37. 17	si
4					28	- . 1798	-35. 96	si
4					29	- . 1737	-34. 74	si
4					30	- . 1676	-33. 52	si
4					31	- . 1615	-32. 31	si
4					32	- . 1555	-31. 09	si
4					33	- . 1494	-29. 87	si
4					34	- . 1433	-28. 66	si
4					35	- . 1372	-27. 44	si
4					36	- . 1311	-26. 22	si
4					37	- . 125	-25. 01	si
4					38	- . 1189	-23. 79	si
4					39	- . 1129	-22. 57	si
4					40	- . 1068	-21. 36	si
4					41	- . 1007	-20. 14	si
4					42	- . 0946	-18. 92	si
4					43	- . 0885	-17. 71	si
4					44	- . 0824	-16. 49	si
4					45	- . 0764	-15. 27	si
4					46	- . 0703	-14. 05	si
4					47	- . 0642	-12. 84	si
4					48	- . 0581	-11. 62	si
5	1- 1	. 2969	0.	si	1	. 5707	114. 14	si
5	1- 2	. 309	0.	si	2	. 5677	113. 54	si
5	1- 3	. 5519	0.	si	3	. 5647	112. 94	si
5	1- 4	. 5983	0.	si	4	. 5617	112. 33	si
5	1- 5	. 3553	0.	si	5	. 5587	111. 73	si
5	1- 6	. 3674	0.	si	6	. 5556	111. 13	si

5	1- 7	-. 1275	-1. 74	si	7	. 5526	110. 52	si
5	1- 8	-. 198	-2. 66	si	8	. 5496	109. 92	si
5					9	. 5466	109. 32	si
5					10	. 5436	108. 72	si
5					11	. 5406	108. 11	si
5					12	. 5376	107. 51	si
5					13	. 5345	106. 91	si
5					14	. 5315	106. 3	si
5					15	. 5285	105. 7	si
5					16	. 5255	105. 1	si
5					17	. 2825	56. 51	si
5					18	. 2785	55. 7	si
5					19	. 2745	54. 9	si
5					20	. 2704	54. 09	si
5					21	. 3399	67. 97	si
5					22	. 3358	67. 17	si
5					23	. 3318	66. 36	si
5					24	. 3278	65. 55	si
5					25	-. 101	-20. 21	si
5					26	-. 1041	-20. 81	si
5					27	-. 1071	-21. 41	si
5					28	-. 1101	-22. 02	si
5					29	-. 1131	-22. 62	si
5					30	-. 1161	-23. 23	si
5					31	-. 1191	-23. 83	si
5					32	-. 1222	-24. 43	si
5					33	-. 1252	-25. 04	si
5					34	-. 1282	-25. 64	si
5					35	-. 1312	-26. 24	si
5					36	-. 1342	-26. 85	si
5					37	-. 1373	-27. 45	si
5					38	-. 1403	-28. 05	si
5					39	-. 1433	-28. 66	si
5					40	-. 1463	-29. 26	si
5					41	-. 1493	-29. 87	si
5					42	-. 1523	-30. 47	si
5					43	-. 1554	-31. 07	si
5					44	-. 1584	-31. 68	si
5					45	-. 1614	-32. 28	si
5					46	-. 1644	-32. 88	si
5					47	-. 1674	-33. 49	si
5					48	-. 1705	-34. 09	si
6	1- 1	. 332	0.	si	1	. 6418	128. 36	si
6	1- 2	. 3479	0.	si	2	. 6379	127. 57	si
6	1- 3	. 6108	0.	si	3	. 6339	126. 78	si
6	1- 4	. 6718	0.	si	4	. 6299	125. 99	si
6	1- 5	. 4089	0.	si	5	. 626	125. 19	si
6	1- 6	. 4248	0.	si	6	. 622	124. 4	si
6	1- 7	-. 1108	-1. 52	si	7	. 618	123. 61	si
6	1- 8	-. 2036	-2. 73	si	8	. 6141	122. 82	si
6					9	. 6101	122. 02	si
6					10	. 6062	121. 23	si
6					11	. 6022	120. 44	si
6					12	. 5982	119. 65	si
6					13	. 5943	118. 85	si
6					14	. 5903	118. 06	si
6					15	. 5863	117. 27	si
6					16	. 5824	116. 48	si
6					17	. 3195	63. 89	si
6					18	. 3142	62. 83	si
6					19	. 3089	61. 77	si
6					20	. 3035	60. 71	si
6					21	. 3948	78. 96	si
6					22	. 3895	77. 9	si
6					23	. 3842	76. 84	si
6					24	. 3789	75. 78	si
6					25	-. 0823	-16. 47	si
6					26	-. 0863	-17. 26	si
6					27	-. 0903	-18. 06	si
6					28	-. 0942	-18. 85	si
6					29	-. 0982	-19. 64	si
6					30	-. 1022	-20. 44	si
6					31	-. 1061	-21. 23	si
6					32	-. 1101	-22. 02	si
6					33	-. 1141	-22. 82	si
6					34	-. 1181	-23. 61	si
6					35	-. 122	-24. 4	si
6					36	-. 126	-25. 2	si
6					37	-. 13	-25. 99	si
6					38	-. 1339	-26. 78	si
6					39	-. 1379	-27. 58	si
6					40	-. 1419	-28. 37	si
6					41	-. 1458	-29. 16	si
6					42	-. 1498	-29. 96	si
6					43	-. 1538	-30. 75	si
6					44	-. 1577	-31. 55	si
6					45	-. 1617	-32. 34	si
6					46	-. 1657	-33. 13	si
6					47	-. 1696	-33. 93	si
6					48	-. 1736	-34. 72	si

Descrizi one : Pul vi no 2

SOLLECITAZIONI AGENTI

Sforzi normali applicati in z= 183.7 ; y= 37.5 (baricentro CLS)

Convenzioni: N + trazione; Mz + fib. inferiori tese; My + fib. sinistra tese.

N.	N	Mz	My	Descrizione
1	-237.39	-954.1015	-765.574	Caso 8.10
2	-50.27	-149.5459	237.1411	Caso 8.23
3	-206.69	-671.6013	-1714.424	Caso 7.8
4	-80.97	-432.046	1185.9911	Caso 7.25
5	-294.89	-952.6072	-210.7182	Caso 8.24
6	7.23	-151.0401	-317.7147	Caso 8.9

RISULTATI

Piani di equilibrio (eps= muz * y +muy * z + lam):

Sol.	muz	muy	lambda
1.	.00001624014	.00000060793	-.0003854937
2.	.00000247899	-.00000018708	-.00000527813
3.	.00001104893	.00000159426	-.00043050369
4.	.00000717584	-.00000116073	.00013894547
5.	.000015973	.00000016286	-.00030919523
6.	.00000267163	.00000030254	-.0000872711

Deformazioni sui materiali:

Cls					Acciaio lento			
sol	vert.	D cls	S cls	Ve	ferro	D ferri	S ferri	Ve
1	1- 1	.5077	0.	si	1	1.0807	216.14	si
1	1- 2	.546	0.	si	2	1.0712	214.23	si
1	1- 3	.9845	0.	si	3	1.0616	212.33	si
1	1- 4	1.1313	0.	si	4	1.0521	210.42	si
1	1- 5	.6928	0.	si	5	1.0425	208.51	si
1	1- 6	.7311	0.	si	6	1.033	206.6	si
1	1- 7	-.1621	-2.2	si	7	1.0235	204.69	si
1	1- 8	-.3855	-4.92	si	8	1.0139	202.78	si
1					9	1.0044	200.88	si
1					10	.9948	198.97	si
1					11	.9853	197.06	si
1					12	.9758	195.15	si
1					13	.9662	193.24	si
1					14	.9567	191.34	si
1					15	.9471	189.43	si
1					16	.9376	187.52	si
1					17	.4991	99.82	si
1					18	.4864	97.27	si
1					19	.4736	94.72	si
1					20	.4608	92.16	si
1					21	.6805	136.1	si
1					22	.6678	133.55	si
1					23	.655	131.	si
1					24	.6422	128.44	si
1					25	-.1152	-23.05	si
1					26	-.1248	-24.96	si
1					27	-.1343	-26.87	si
1					28	-.1439	-28.78	si
1					29	-.1535	-30.69	si
1					30	-.163	-32.6	si
1					31	-.1726	-34.51	si
1					32	-.1821	-36.42	si
1					33	-.1917	-38.33	si
1					34	-.2012	-40.24	si
1					35	-.2108	-42.15	si
1					36	-.2203	-44.06	si
1					37	-.2299	-45.97	si
1					38	-.2394	-47.89	si
1					39	-.249	-49.8	si
1					40	-.2585	-51.71	si
1					41	-.2681	-53.62	si
1					42	-.2776	-55.53	si
1					43	-.2872	-57.44	si
1					44	-.2967	-59.35	si
1					45	-.3063	-61.26	si
1					46	-.3158	-63.17	si
1					47	-.3254	-65.08	si
1					48	-.3349	-66.99	si
2	1- 1	.1311	0.	si	1	.1342	26.84	si
2	1- 2	.1193	0.	si	2	.1371	27.42	si
2	1- 3	.1862	0.	si	3	.14	28.01	si
2	1- 4	.1411	0.	si	4	.143	28.6	si
2	1- 5	.0741	0.	si	5	.1459	29.18	si
2	1- 6	.0623	0.	si	6	.1489	29.77	si
2	1- 7	-.074	-1.02	si	7	.1518	30.36	si
2	1- 8	-.0053	-.07	si	8	.1547	30.95	si
2					9	.1577	31.53	si
2					10	.1606	32.12	si
2					11	.1635	32.71	si
2					12	.1665	33.29	si
2					13	.1694	33.88	si
2					14	.1723	34.47	si
2					15	.1753	35.06	si
2					16	.1782	35.64	si
2					17	.1113	22.26	si
2					18	.1152	23.04	si
2					19	.1191	23.83	si
2					20	.1231	24.61	si
2					21	.0555	11.09	si
2					22	.0594	11.88	si
2					23	.0633	12.66	si
2					24	.0672	13.45	si
2					25	-.066	-13.2	si
2					26	-.0631	-12.61	si
2					27	-.0601	-12.03	si
2					28	-.0572	-11.44	si
2					29	-.0543	-10.85	si

2					30	-.0513	-10.26	si
2					31	-.0484	-9.68	si
2					32	-.0454	-9.09	si
2					33	-.0425	-8.5	si
2					34	-.0396	-7.91	si
2					35	-.0366	-7.32	si
2					36	-.0337	-6.74	si
2					37	-.0307	-6.15	si
2					38	-.0278	-5.56	si
2					39	-.0249	-4.97	si
2					40	-.0219	-4.38	si
2					41	-.019	-3.8	si
2					42	-.016	-3.21	si
2					43	-.0131	-2.62	si
2					44	-.0102	-2.03	si
2					45	-.0072	-1.44	si
2					46	-.0043	-.86	si
2					47	-.0013	-.27	si
2					48	.0016	.32	si
3	1- 1	.1772	0.	si	1	.9229	184.57	si
3	1- 2	.2776	0.	si	2	.8979	179.57	si
3	1- 3	.5759	0.	si	3	.8728	174.57	si
3	1- 4	.9608	0.	si	4	.8478	169.56	si
3	1- 5	.6625	0.	si	5	.8228	164.56	si
3	1- 6	.7629	0.	si	6	.7978	159.55	si
3	1- 7	.1552	0.	si	7	.7728	154.55	si
3	1- 8	-.4305	-5.42	si	8	.7477	149.55	si
3					9	.7227	144.54	si
3					10	.6977	139.54	si
3					11	.6727	134.54	si
3					12	.6477	129.53	si
3					13	.6226	124.53	si
3					14	.5976	119.52	si
3					15	.5726	114.52	si
3					16	.5476	109.52	si
3					17	.2493	49.85	si
3					18	.2158	43.16	si
3					19	.1823	36.46	si
3					20	.1488	29.76	si
3					21	.725	145.	si
3					22	.6915	138.3	si
3					23	.658	131.61	si
3					24	.6246	124.91	si
3					25	.1836	36.72	si
3					26	.1585	31.71	si
3					27	.1335	26.7	si
3					28	.1084	21.69	si
3					29	.0834	16.68	si
3					30	.0583	11.67	si
3					31	.0333	6.66	si
3					32	.0082	1.65	si
3					33	-.0168	-3.36	si
3					34	-.0419	-8.37	si
3					35	-.0669	-13.38	si
3					36	-.092	-18.39	si
3					37	-.117	-23.4	si
3					38	-.1421	-28.41	si
3					39	-.1671	-33.42	si
3					40	-.1922	-38.43	si
3					41	-.2172	-43.44	si
3					42	-.2423	-48.45	si
3					43	-.2673	-53.46	si
3					44	-.2924	-58.47	si
3					45	-.3174	-63.48	si
3					46	-.3425	-68.49	si
3					47	-.3675	-73.5	si
3					48	-.3926	-78.51	si
4	1- 1	.5336	0.	si	1	.356	71.2	si
4	1- 2	.4605	0.	si	2	.3742	74.84	si
4	1- 3	.6542	0.	si	3	.3924	78.49	si
4	1- 4	.374	0.	si	4	.4106	82.13	si
4	1- 5	.1803	0.	si	5	.4289	85.77	si
4	1- 6	.1072	0.	si	6	.4471	89.41	si
4	1- 7	-.2875	-3.77	si	7	.4653	93.06	si
4	1- 8	.1389	0.	si	8	.4835	96.7	si
4					9	.5017	100.34	si
4					10	.5199	103.99	si
4					11	.5381	107.63	si
4					12	.5564	111.27	si
4					13	.5746	114.92	si
4					14	.5928	118.56	si
4					15	.611	122.2	si
4					16	.6292	125.85	si
4					17	.4355	87.1	si
4					18	.4599	91.97	si
4					19	.4842	96.85	si
4					20	.5086	101.72	si
4					21	.0891	17.82	si
4					22	.1135	22.7	si
4					23	.1379	27.57	si
4					24	.1622	32.45	si
4					25	-.2625	-52.5	si
4					26	-.2443	-48.85	si
4					27	-.226	-45.2	si
4					28	-.2078	-41.56	si
4					29	-.1895	-37.91	si
4					30	-.1713	-34.26	si

6	32	-.0023	-.46	si
6	33	-.007	-1.41	si
6	34	-.0118	-2.36	si
6	35	-.0165	-3.31	si
6	36	-.0213	-4.26	si
6	37	-.0261	-5.21	si
6	38	-.0308	-6.16	si
6	39	-.0356	-7.11	si
6	40	-.0403	-8.06	si
6	41	-.0451	-9.01	si
6	42	-.0498	-9.97	si
6	43	-.0546	-10.92	si
6	44	-.0593	-11.87	si
6	45	-.0641	-12.82	si
6	46	-.0688	-13.77	si
6	47	-.0736	-14.72	si
6	48	-.0783	-15.67	si

Descrizione : Pulvino 3

SOLLECITAZIONI AGENTI

Sforzi normali applicati in z= 183.7 ; y= 37.5 (baricentro CLS)
 Convenzioni: N + trazione; Mz + fib.inferiori tese; My + fib.sinistra tese.

N.	N	Mz	My	Descrizione
1	-34.07	-470.7194	-62.5912	Caso 13. 1
2	-61.72	-852.1424	-314.3492	Caso 2. 2
3	-62.92	-852.2243	85.3986	Caso 2. 1
4	-73.89	-534.0474	-145.4704	Caso 8. 10
5	-7.48	-574.6543	-4.0022	Caso 8. 23

RISULTATI

Piani di equilibrio (eps= muz * y +my * z + lam):

Sol.	muz	my	lambda
1.	.00000829474	.00000004998	-.00014260776
2.	.00001505748	.00000025575	-.00028997775
3.	.00001505215	-.00000006925	-.00023124636
4.	.00000927859	.00000011485	-.00017345347
5.	.00001026562	.00000000325	-.00016298341

Deformazioni sui materiali:

Cls					Acciaio lento			
sol	vert.	D cls	S cls	Ve	ferro	D ferri	S ferri	Ve
1	1- 1	.3136	0.	si	1	.5277	105.55	si
1	1- 2	.3168	0.	si	2	.527	105.39	si
1	1- 3	.5407	0.	si	3	.5262	105.23	si
1	1- 4	.5528	0.	si	4	.5254	105.08	si
1	1- 5	.3288	0.	si	5	.5246	104.92	si
1	1- 6	.332	0.	si	6	.5238	104.76	si
1	1- 7	-.1242	-1.7	si	7	.523	104.61	si
1	1- 8	-.1426	-1.94	si	8	.5222	104.45	si
1					9	.5215	104.29	si
1					10	.5207	104.14	si
1					11	.5199	103.98	si
1					12	.5191	103.82	si
1					13	.5183	103.67	si
1					14	.5175	103.51	si
1					15	.5168	103.35	si
1					16	.516	103.2	si
1					17	.292	58.4	si
1					18	.291	58.19	si
1					19	.2899	57.98	si
1					20	.2889	57.77	si
1					21	.3069	61.39	si
1					22	.3059	61.18	si
1					23	.3048	60.97	si
1					24	.3038	60.76	si
1					25	-.0995	-19.9	si
1					26	-.1003	-20.06	si
1					27	-.1011	-20.22	si
1					28	-.1019	-20.37	si
1					29	-.1027	-20.53	si
1					30	-.1034	-20.69	si
1					31	-.1042	-20.84	si
1					32	-.105	-21.	si
1					33	-.1058	-21.16	si
1					34	-.1066	-21.32	si
1					35	-.1074	-21.47	si
1					36	-.1081	-21.63	si
1					37	-.1089	-21.79	si
1					38	-.1097	-21.94	si
1					39	-.1105	-22.1	si
1					40	-.1113	-22.26	si
1					41	-.1121	-22.42	si
1					42	-.1129	-22.57	si
1					43	-.1136	-22.73	si
1					44	-.1144	-22.89	si
1					45	-.1152	-23.04	si
1					46	-.116	-23.2	si
1					47	-.1168	-23.36	si
1					48	-.1176	-23.51	si
2	1- 1	.5382	0.	si	1	.9766	195.33	si
2	1- 2	.5543	0.	si	2	.9726	194.53	si
2	1- 3	.9608	0.	si	3	.9686	193.72	si
2	1- 4	1.0226	0.	si	4	.9646	192.92	si
2	1- 5	.616	0.	si	5	.9606	192.12	si
2	1- 6	.6321	0.	si	6	.9566	191.32	si
2	1- 7	-.196	-2.63	si	7	.9526	190.51	si

2	1- 8	- .29	-3.79	si	8	.9486	189.71	si
2					9	.9445	188.91	si
2					10	.9405	188.1	si
2					11	.9365	187.3	si
2					12	.9325	186.5	si
2					13	.9285	185.7	si
2					14	.9245	184.89	si
2					15	.9205	184.09	si
2					16	.9164	183.29	si
2					17	.5099	101.98	si
2					18	.5045	100.9	si
2					19	.4991	99.83	si
2					20	.4938	98.76	si
2					21	.5862	117.24	si
2					22	.5808	116.17	si
2					23	.5755	115.09	si
2					24	.5701	114.02	si
2					25	-.1516	-30.32	si
2					26	-.1556	-31.13	si
2					27	-.1596	-31.93	si
2					28	-.1637	-32.73	si
2					29	-.1677	-33.54	si
2					30	-.1717	-34.34	si
2					31	-.1757	-35.14	si
2					32	-.1797	-35.95	si
2					33	-.1838	-36.75	si
2					34	-.1878	-37.56	si
2					35	-.1918	-38.36	si
2					36	-.1958	-39.16	si
2					37	-.1998	-39.97	si
2					38	-.2039	-40.77	si
2					39	-.2079	-41.57	si
2					40	-.2119	-42.38	si
2					41	-.2159	-43.18	si
2					42	-.2199	-43.99	si
2					43	-.2239	-44.79	si
2					44	-.228	-45.59	si
2					45	-.232	-46.4	si
2					46	-.236	-47.2	si
2					47	-.24	-48.	si
2					48	-.244	-48.81	si
3	1- 1	.5966	0.	si	1	.937	187.4	si
3	1- 2	.5923	0.	si	2	.9381	187.62	si
3	1- 3	.9987	0.	si	3	.9392	187.83	si
3	1- 4	.9819	0.	si	4	.9403	188.05	si
3	1- 5	.5755	0.	si	5	.9413	188.27	si
3	1- 6	.5712	0.	si	6	.9424	188.49	si
3	1- 7	-.2567	-3.39	si	7	.9435	188.7	si
3	1- 8	-.2312	-3.07	si	8	.9446	188.92	si
3					9	.9457	189.14	si
3					10	.9468	189.36	si
3					11	.9479	189.57	si
3					12	.949	189.79	si
3					13	.95	190.01	si
3					14	.9511	190.23	si
3					15	.9522	190.44	si
3					16	.9533	190.66	si
3					17	.5469	109.38	si
3					18	.5483	109.67	si
3					19	.5498	109.96	si
3					20	.5513	110.25	si
3					21	.5262	105.25	si
3					22	.5277	105.54	si
3					23	.5291	105.83	si
3					24	.5306	106.12	si
3					25	-.2113	-42.27	si
3					26	-.2102	-42.05	si
3					27	-.2091	-41.83	si
3					28	-.2081	-41.61	si
3					29	-.207	-41.39	si
3					30	-.2059	-41.18	si
3					31	-.2048	-40.96	si
3					32	-.2037	-40.74	si
3					33	-.2026	-40.52	si
3					34	-.2015	-40.31	si
3					35	-.2004	-40.09	si
3					36	-.1994	-39.87	si
3					37	-.1983	-39.65	si
3					38	-.1972	-39.44	si
3					39	-.1961	-39.22	si
3					40	-.195	-39.	si
3					41	-.1939	-38.78	si
3					42	-.1928	-38.57	si
3					43	-.1917	-38.35	si
3					44	-.1907	-38.13	si
3					45	-.1896	-37.91	si
3					46	-.1885	-37.69	si
3					47	-.1874	-37.48	si
3					48	-.1863	-37.26	si
4	1- 1	.3369	0.	si	1	.5942	118.83	si
4	1- 2	.3441	0.	si	2	.5924	118.47	si
4	1- 3	.5946	0.	si	3	.5906	118.11	si
4	1- 4	.6224	0.	si	4	.5888	117.75	si
4	1- 5	.3718	0.	si	5	.587	117.39	si
4	1- 6	.3791	0.	si	6	.5852	117.03	si
4	1- 7	-.1313	-1.79	si	7	.5834	116.67	si
4	1- 8	-.1735	-2.34	si	8	.5816	116.31	si

4				9	.5798	115.95	si
4				10	.578	115.59	si
4				11	.5761	115.23	si
4				12	.5743	114.87	si
4				13	.5725	114.51	si
4				14	.5707	114.15	si
4				15	.5689	113.79	si
4				16	.5671	113.43	si
4				17	.3166	63.32	si
4				18	.3142	62.84	si
4				19	.3118	62.36	si
4				20	.3094	61.88	si
4				21	.3509	70.18	si
4				22	.3485	69.69	si
4				23	.3461	69.21	si
4				24	.3437	68.73	si
4				25	-.1038	-20.75	si
4				26	-.1056	-21.11	si
4				27	-.1074	-21.47	si
4				28	-.1092	-21.84	si
4				29	-.111	-22.2	si
4				30	-.1128	-22.56	si
4				31	-.1146	-22.92	si
4				32	-.1164	-23.28	si
4				33	-.1182	-23.64	si
4				34	-.12	-24.	si
4				35	-.1218	-24.36	si
4				36	-.1236	-24.72	si
4				37	-.1254	-25.08	si
4				38	-.1272	-25.45	si
4				39	-.129	-25.81	si
4				40	-.1308	-26.17	si
4				41	-.1326	-26.53	si
4				42	-.1344	-26.89	si
4				43	-.1362	-27.25	si
4				44	-.1381	-27.61	si
4				45	-.1399	-27.97	si
4				46	-.1417	-28.33	si
4				47	-.1435	-28.69	si
4				48	-.1453	-29.05	si
5	1- 1	.4016	0.	1	.649	129.8	si
5	1- 2	.4018	0.	2	.6489	129.79	si
5	1- 3	.679	0.	3	.6489	129.78	si
5	1- 4	.6798	0.	4	.6488	129.77	si
5	1- 5	.4026	0.	5	.6488	129.76	si
5	1- 6	.4028	0.	6	.6487	129.75	si
5	1- 7	-.1618	-2.19	7	.6487	129.73	si
5	1- 8	-.163	-2.21	8	.6486	129.72	si
5				9	.6486	129.71	si
5				10	.6485	129.7	si
5				11	.6485	129.69	si
5				12	.6484	129.68	si
5				13	.6484	129.67	si
5				14	.6483	129.66	si
5				15	.6483	129.65	si
5				16	.6482	129.64	si
5				17	.371	74.21	si
5				18	.371	74.2	si
5				19	.3709	74.18	si
5				20	.3708	74.17	si
5				21	.372	74.4	si
5				22	.3719	74.39	si
5				23	.3719	74.38	si
5				24	.3718	74.36	si
5				25	-.131	-26.2	si
5				26	-.1311	-26.21	si
5				27	-.1311	-26.22	si
5				28	-.1312	-26.23	si
5				29	-.1312	-26.24	si
5				30	-.1313	-26.25	si
5				31	-.1313	-26.26	si
5				32	-.1314	-26.27	si
5				33	-.1314	-26.28	si
5				34	-.1315	-26.29	si
5				35	-.1315	-26.3	si
5				36	-.1316	-26.31	si
5				37	-.1316	-26.32	si
5				38	-.1317	-26.33	si
5				39	-.1317	-26.34	si
5				40	-.1318	-26.35	si
5				41	-.1318	-26.36	si
5				42	-.1319	-26.37	si
5				43	-.1319	-26.38	si
5				44	-.132	-26.39	si
5				45	-.132	-26.4	si
5				46	-.1321	-26.41	si
5				47	-.1321	-26.43	si
5				48	-.1322	-26.44	si

Descrizi one : Pul vi no 4

SOLLECITAZIONI AGENTI

Sforzi normali applicati in z= 183.7 ; y= 37.5 (baricentro CLS)

Convenzioni: N + trazione; Mz + fib.inferiori tese; My + fib.sinistra tese.

N.	N	Mz	My	Descrizione
----	---	----	----	-------------

1	-34.77	-469.8203	-63.8709	Caso 13. 1
2	-63.01	-850.512	-307.9812	Caso 2. 2
3	-64.21	-850.5638	74.2728	Caso 2. 1
4	-73.68	-550.9001	-126.5501	Caso 8. 10
5	-9.38	-555.6525	-26.0322	Caso 8. 23

RISULTATI

Piani di equilibrio (eps= muz * y +muy * z + lam):

Sol.	muz	muy	lambda
1.	.00000827588	.00000005098	-.00014255269
2.	.00001502298	.00000025043	-.00028860365
3.	.00001501714	-.0000000602	-.00023248264
4.	.00000958216	.00000010004	-.00017563495
5.	.00000991661	.00000002112	-.00016087733

Deformazioni sui materiali:

Cls					Acciaio lento			
sol	vert.	D cls	S cls	Ve	ferro	D ferri	S ferri	Ve
1	1- 1	.3126	0.	si	1	.5266	105.32	si
1	1- 2	.3158	0.	si	2	.5258	105.16	si
1	1- 3	.5393	0.	si	3	.525	105.	si
1	1- 4	.5516	0.	si	4	.5242	104.84	si
1	1- 5	.3281	0.	si	5	.5234	104.68	si
1	1- 6	.3314	0.	si	6	.5226	104.52	si
1	1- 7	-.1238	-1.69	si	7	.5218	104.36	si
1	1- 8	-.1426	-1.94	si	8	.521	104.2	si
1					9	.5202	104.04	si
1					10	.5194	103.88	si
1					11	.5186	103.72	si
1					12	.5178	103.56	si
1					13	.517	103.4	si
1					14	.5162	103.24	si
1					15	.5154	103.08	si
1					16	.5146	102.92	si
1					17	.2912	58.23	si
1					18	.2901	58.02	si
1					19	.289	57.8	si
1					20	.2879	57.59	si
1					21	.3064	61.27	si
1					22	.3053	61.06	si
1					23	.3042	60.85	si
1					24	.3032	60.63	si
1					25	-.0991	-19.83	si
1					26	-.0999	-19.99	si
1					27	-.1007	-20.15	si
1					28	-.1016	-20.31	si
1					29	-.1024	-20.47	si
1					30	-.1032	-20.63	si
1					31	-.104	-20.79	si
1					32	-.1048	-20.95	si
1					33	-.1056	-21.11	si
1					34	-.1064	-21.27	si
1					35	-.1072	-21.43	si
1					36	-.108	-21.59	si
1					37	-.1088	-21.75	si
1					38	-.1096	-21.91	si
1					39	-.1104	-22.07	si
1					40	-.1112	-22.23	si
1					41	-.112	-22.39	si
1					42	-.1128	-22.55	si
1					43	-.1136	-22.71	si
1					44	-.1144	-22.87	si
1					45	-.1152	-23.03	si
1					46	-.116	-23.19	si
1					47	-.1168	-23.35	si
1					48	-.1176	-23.51	si
2	1- 1	.5377	0.	si	1	.9737	194.74	si
2	1- 2	.5534	0.	si	2	.9698	193.95	si
2	1- 3	.9591	0.	si	3	.9658	193.17	si
2	1- 4	1.0195	0.	si	4	.9619	192.38	si
2	1- 5	.6139	0.	si	5	.958	191.59	si
2	1- 6	.6297	0.	si	6	.954	190.81	si
2	1- 7	-.1966	-2.64	si	7	.9501	190.02	si
2	1- 8	-.2886	-3.78	si	8	.9462	189.24	si
2					9	.9423	188.45	si
2					10	.9383	187.66	si
2					11	.9344	186.88	si
2					12	.9305	186.09	si
2					13	.9265	185.31	si
2					14	.9226	184.52	si
2					15	.9187	183.73	si
2					16	.9147	182.95	si
2					17	.5091	101.82	si
2					18	.5039	100.77	si
2					19	.4986	99.72	si
2					20	.4933	98.67	si
2					21	.5838	116.77	si
2					22	.5786	115.72	si
2					23	.5733	114.67	si
2					24	.5681	113.61	si
2					25	-.1523	-30.46	si
2					26	-.1562	-31.24	si
2					27	-.1601	-32.03	si
2					28	-.1641	-32.82	si
2					29	-.168	-33.6	si
2					30	-.172	-34.39	si
2					31	-.1759	-35.18	si
2					32	-.1798	-35.96	si
2					33	-.1838	-36.75	si

4					35	-. 1262	-25. 23	si
4					36	-. 1277	-25. 54	si
4					37	-. 1293	-25. 86	si
4					38	-. 1309	-26. 17	si
4					39	-. 1324	-26. 49	si
4					40	-. 134	-26. 8	si
4					41	-. 1356	-27. 12	si
4					42	-. 1372	-27. 43	si
4					43	-. 1387	-27. 75	si
4					44	-. 1403	-28. 06	si
4					45	-. 1419	-28. 37	si
4					46	-. 1434	-28. 69	si
4					47	-. 145	-29.	si
4					48	-. 1466	-29. 32	si
5	1- 1	. 3845	0.	si	1	. 6289	125. 78	si
5	1- 2	. 3859	0.	si	2	. 6286	125. 71	si
5	1- 3	. 6536	0.	si	3	. 6282	125. 65	si
5	1- 4	. 6587	0.	si	4	. 6279	125. 58	si
5	1- 5	. 391	0.	si	5	. 6276	125. 51	si
5	1- 6	. 3923	0.	si	6	. 6272	125. 45	si
5	1- 7	-. 1531	-2. 08	si	7	. 6269	125. 38	si
5	1- 8	-. 1609	-2. 18	si	8	. 6266	125. 32	si
5					9	. 6262	125. 25	si
5					10	. 6259	125. 18	si
5					11	. 6256	125. 12	si
5					12	. 6253	125. 05	si
5					13	. 6249	124. 98	si
5					14	. 6246	124. 92	si
5					15	. 6243	124. 85	si
5					16	. 6239	124. 79	si
5					17	. 3562	71. 24	si
5					18	. 3557	71. 15	si
5					19	. 3553	71. 06	si
5					20	. 3548	70. 97	si
5					21	. 3625	72. 5	si
5					22	. 362	72. 41	si
5					23	. 3616	72. 32	si
5					24	. 3612	72. 23	si
5					25	-. 1234	-24. 69	si
5					26	-. 1238	-24. 75	si
5					27	-. 1241	-24. 82	si
5					28	-. 1244	-24. 89	si
5					29	-. 1248	-24. 95	si
5					30	-. 1251	-25. 02	si
5					31	-. 1254	-25. 08	si
5					32	-. 1258	-25. 15	si
5					33	-. 1261	-25. 22	si
5					34	-. 1264	-25. 28	si
5					35	-. 1268	-25. 35	si
5					36	-. 1271	-25. 42	si
5					37	-. 1274	-25. 48	si
5					38	-. 1277	-25. 55	si
5					39	-. 1281	-25. 62	si
5					40	-. 1284	-25. 68	si
5					41	-. 1287	-25. 75	si
5					42	-. 1291	-25. 81	si
5					43	-. 1294	-25. 88	si
5					44	-. 1297	-25. 95	si
5					45	-. 1301	-26. 01	si
5					46	-. 1304	-26. 08	si
5					47	-. 1307	-26. 15	si
5					48	-. 1311	-26. 21	si

Descrizione : Pulvino 5

SOLLECITAZIONI AGENTI

Sforzi normali applicati in $z=183.7$; $y=-37.5$ (baricentro CLS)
 Convenzioni: N + trazione; Mz + fib. inferiori tese; My + fib. sinistra tese.

N.	N	Mz	My	Descrizioni
1	-35. 23	-468. 8666	-64. 7124	Caso 13. 1
2	-63. 86	-848. 7808	-299. 8109	Caso 2. 2
3	-65. 06	-848. 8015	62. 9705	Caso 2. 1
4	-74. 59	-548. 8857	-130. 1297	Caso 8. 10
5	-9. 59	-555. 3851	-24. 5226	Caso 8. 23

RISULTATI

Piani di equilibrio ($\epsilon = \mu z + \mu y * z + \lambda$):

Sol.	mu z	mu y	lambda
1.	. 00000825697	. 00000005164	-. 0001424128
2.	. 00001498834	. 00000024366	-. 00028693253
3.	. 000014982	-. 00000005102	-. 0002336977
4.	. 00000954245	. 00000010282	-. 00017557946
5.	. 00000991099	. 00000001989	-. 00016058304

Deformazioni sui materiali:

sol	Cls				Acciaio lento			
	vert.	D cls	S cls	Ve	ferro	D ferri	S ferri	Ve
1	1- 1	. 3117	0.	si	1	. 5255	105. 09	si
1	1- 2	. 315	0.	si	2	. 5246	104. 93	si
1	1- 3	. 5379	0.	si	3	. 5238	104. 77	si
1	1- 4	. 5504	0.	si	4	. 523	104. 6	si
1	1- 5	. 3274	0.	si	5	. 5222	104. 44	si
1	1- 6	. 3307	0.	si	6	. 5214	104. 28	si
1	1- 7	-. 1234	-1. 69	si	7	. 5206	104. 12	si
1	1- 8	-. 1424	-1. 94	si	8	. 5198	103. 96	si
1					9	. 519	103. 79	si
1					10	. 5182	103. 63	si

1					11	.5173	103.47	si
1					12	.5165	103.31	si
1					13	.5157	103.15	si
1					14	.5149	102.98	si
1					15	.5141	102.82	si
1					16	.5133	102.66	si
1					17	.2904	58.07	si
1					18	.2893	57.85	si
1					19	.2882	57.64	si
1					20	.2871	57.42	si
1					21	.3058	61.15	si
1					22	.3047	60.94	si
1					23	.3036	60.72	si
1					24	.3025	60.5	si
1					25	-.0988	-19.77	si
1					26	-.0996	-19.93	si
1					27	-.1004	-20.09	si
1					28	-.1013	-20.25	si
1					29	-.1021	-20.41	si
1					30	-.1029	-20.58	si
1					31	-.1037	-20.74	si
1					32	-.1045	-20.9	si
1					33	-.1053	-21.06	si
1					34	-.1061	-21.23	si
1					35	-.1069	-21.39	si
1					36	-.1078	-21.55	si
1					37	-.1086	-21.71	si
1					38	-.1094	-21.87	si
1					39	-.1102	-22.04	si
1					40	-.111	-22.2	si
1					41	-.1118	-22.36	si
1					42	-.1126	-22.52	si
1					43	-.1134	-22.69	si
1					44	-.1142	-22.85	si
1					45	-.1151	-23.01	si
1					46	-.1159	-23.17	si
1					47	-.1167	-23.34	si
1					48	-.1175	-23.5	si
2	1- 1	.5374	0.	si	1	.9706	194.12	si
2	1- 2	.5528	0.	si	2	.9668	193.35	si
2	1- 3	.9575	0.	si	3	.9629	192.59	si
2	1- 4	1.0163	0.	si	4	.9591	191.82	si
2	1- 5	.6116	0.	si	5	.9553	191.06	si
2	1- 6	.6269	0.	si	6	.9515	190.29	si
2	1- 7	-.1974	-2.65	si	7	.9476	189.53	si
2	1- 8	-.2869	-3.76	si	8	.9438	188.76	si
2					9	.94	188.	si
2					10	.9362	187.23	si
2					11	.9323	186.47	si
2					12	.9285	185.7	si
2					13	.9247	184.94	si
2					14	.9209	184.18	si
2					15	.9171	183.41	si
2					16	.9132	182.65	si
2					17	.5085	101.71	si
2					18	.5034	100.69	si
2					19	.4983	99.66	si
2					20	.4932	98.64	si
2					21	.5813	116.25	si
2					22	.5761	115.23	si
2					23	.571	114.2	si
2					24	.5659	113.18	si
2					25	-.1532	-30.64	si
2					26	-.157	-31.4	si
2					27	-.1608	-32.17	si
2					28	-.1647	-32.93	si
2					29	-.1685	-33.7	si
2					30	-.1723	-34.46	si
2					31	-.1761	-35.23	si
2					32	-.18	-36.	si
2					33	-.1838	-36.76	si
2					34	-.1876	-37.53	si
2					35	-.1915	-38.29	si
2					36	-.1953	-39.06	si
2					37	-.1991	-39.82	si
2					38	-.2029	-40.59	si
2					39	-.2068	-41.36	si
2					40	-.2106	-42.12	si
2					41	-.2144	-42.89	si
2					42	-.2183	-43.65	si
2					43	-.2221	-44.42	si
2					44	-.2259	-45.18	si
2					45	-.2298	-45.95	si
2					46	-.2336	-46.72	si
2					47	-.2374	-47.48	si
2					48	-.2412	-48.25	si
3	1- 1	.5903	0.	si	1	.9345	186.9	si
3	1- 2	.5871	0.	si	2	.9353	187.06	si
3	1- 3	.9916	0.	si	3	.9361	187.22	si
3	1- 4	.9793	0.	si	4	.9369	187.38	si
3	1- 5	.5748	0.	si	5	.9377	187.54	si
3	1- 6	.5716	0.	si	6	.9385	187.7	si
3	1- 7	-.2524	-3.34	si	7	.9393	187.86	si
3	1- 8	-.2337	-3.1	si	8	.9401	188.02	si
3					9	.9409	188.18	si
3					10	.9417	188.34	si
3					11	.9425	188.5	si

3					12	.9433	188.66	si
3					13	.9441	188.82	si
3					14	.9449	188.98	si
3					15	.9457	189.14	si
3					16	.9465	189.3	si
3					17	.542	108.4	si
3					18	.5431	108.61	si
3					19	.5441	108.83	si
3					20	.5452	109.04	si
3					21	.5268	105.35	si
3					22	.5278	105.57	si
3					23	.5289	105.78	si
3					24	.53	106.	si
3					25	-.2073	-41.47	si
3					26	-.2065	-41.31	si
3					27	-.2057	-41.15	si
3					28	-.2049	-40.99	si
3					29	-.2041	-40.83	si
3					30	-.2033	-40.67	si
3					31	-.2025	-40.51	si
3					32	-.2017	-40.35	si
3					33	-.2009	-40.19	si
3					34	-.2001	-40.03	si
3					35	-.1993	-39.87	si
3					36	-.1985	-39.7	si
3					37	-.1977	-39.54	si
3					38	-.1969	-39.38	si
3					39	-.1961	-39.22	si
3					40	-.1953	-39.06	si
3					41	-.1945	-38.9	si
3					42	-.1937	-38.74	si
3					43	-.1929	-38.58	si
3					44	-.1921	-38.42	si
3					45	-.1913	-38.26	si
3					46	-.1905	-38.1	si
3					47	-.1897	-37.94	si
3					48	-.1889	-37.78	si
4	1- 1	.3493	0.	si	1	.6093	121.85	si
4	1- 2	.3557	0.	si	2	.6077	121.53	si
4	1- 3	.6134	0.	si	3	.606	121.21	si
4	1- 4	.6382	0.	si	4	.6044	120.88	si
4	1- 5	.3806	0.	si	5	.6028	120.56	si
4	1- 6	.387	0.	si	6	.6012	120.24	si
4	1- 7	-.1378	-1.88	si	7	.5996	119.92	si
4	1- 8	-.1756	-2.37	si	8	.598	119.59	si
4					9	.5964	119.27	si
4					10	.5947	118.95	si
4					11	.5931	118.63	si
4					12	.5915	118.3	si
4					13	.5899	117.98	si
4					14	.5883	117.66	si
4					15	.5867	117.33	si
4					16	.5851	117.01	si
4					17	.3274	65.48	si
4					18	.3253	65.05	si
4					19	.3231	64.62	si
4					20	.3209	64.19	si
4					21	.3581	71.62	si
4					22	.3559	71.19	si
4					23	.3538	70.76	si
4					24	.3516	70.32	si
4					25	-.1095	-21.9	si
4					26	-.1111	-22.22	si
4					27	-.1127	-22.54	si
4					28	-.1143	-22.87	si
4					29	-.1159	-23.19	si
4					30	-.1176	-23.51	si
4					31	-.1192	-23.84	si
4					32	-.1208	-24.16	si
4					33	-.1224	-24.48	si
4					34	-.124	-24.8	si
4					35	-.1256	-25.13	si
4					36	-.1273	-25.45	si
4					37	-.1289	-25.77	si
4					38	-.1305	-26.1	si
4					39	-.1321	-26.42	si
4					40	-.1337	-26.74	si
4					41	-.1353	-27.07	si
4					42	-.1369	-27.39	si
4					43	-.1386	-27.71	si
4					44	-.1402	-28.04	si
4					45	-.1418	-28.36	si
4					46	-.1434	-28.68	si
4					47	-.145	-29.01	si
4					48	-.1466	-29.33	si
5	1- 1	.3845	0.	si	1	.6284	125.68	si
5	1- 2	.3858	0.	si	2	.6281	125.61	si
5	1- 3	.6534	0.	si	3	.6278	125.55	si
5	1- 4	.6582	0.	si	4	.6274	125.49	si
5	1- 5	.3906	0.	si	5	.6271	125.43	si
5	1- 6	.3918	0.	si	6	.6268	125.36	si
5	1- 7	-.1533	-2.08	si	7	.6265	125.3	si
5	1- 8	-.1606	-2.17	si	8	.6262	125.24	si
5					9	.6259	125.18	si
5					10	.6256	125.11	si
5					11	.6253	125.05	si
5					12	.6249	124.99	si

5	13	. 6246	124. 93	si
5	14	. 6243	124. 86	si
5	15	. 624	124. 8	si
5	16	. 6237	124. 74	si
5	17	. 3561	71. 22	si
5	18	. 3557	71. 14	si
5	19	. 3553	71. 05	si
5	20	. 3548	70. 97	si
5	21	. 362	72. 41	si
5	22	. 3616	72. 32	si
5	23	. 3612	72. 24	si
5	24	. 3608	72. 16	si
5	25	-. 1236	-24. 72	si
5	26	-. 1239	-24. 78	si
5	27	-. 1242	-24. 85	si
5	28	-. 1245	-24. 91	si
5	29	-. 1249	-24. 97	si
5	30	-. 1252	-25. 03	si
5	31	-. 1255	-25. 1	si
5	32	-. 1258	-25. 16	si
5	33	-. 1261	-25. 22	si
5	34	-. 1264	-25. 28	si
5	35	-. 1267	-25. 35	si
5	36	-. 127	-25. 41	si
5	37	-. 1274	-25. 47	si
5	38	-. 1277	-25. 53	si
5	39	-. 128	-25. 6	si
5	40	-. 1283	-25. 66	si
5	41	-. 1286	-25. 72	si
5	42	-. 1289	-25. 78	si
5	43	-. 1292	-25. 85	si
5	44	-. 1295	-25. 91	si
5	45	-. 1299	-25. 97	si
5	46	-. 1302	-26. 03	si
5	47	-. 1305	-26. 1	si
5	48	-. 1308	-26. 16	si

Descrizione : Pulvi no 6

SOLLECITAZIONI AGENTI

Sforzi normali applicati in z= 183.7 ; y= 37.5

Convenzioni: N + trazione; Mz + fib.inferiori tese; My + fib.sinistra tese.

N.	N	Mz	My	Descrizione
1	-36.49	-467.829	-67.0322	Caso 13. 1
2	-66.19	-846.8952	-351.5833	Caso 2. 2
3	-67.39	-846.8857	106.1839	Caso 2. 1
4	-77.78	-546.5976	-135.9257	Caso 8. 10
5	-9.47	-555.1871	-24.3637	Caso 8. 23

RI SULTATI

Piani di equilibrio (eps= muz * y + muy * z + lam):

Sol.	muz	muy	lambda
1.	.00000823345	.00000005345	-.00014248106
2.	.00001494608	.00000028585	-.0002938612
3.	.0000149386	-.00000008599	-.00022671404
4.	.00000948901	.00000010725	-.00017580163
5.	.0000099079	.00000001976	-.00016049943

Deformazioni sui materiali:

sol	Cls				Acciaio lento			
	vert.	D cls	S cls	Ve	ferro	D ferri	S ferri	Ve
1	1- 1	. 3104	0.	si	1	. 5241	104. 81	si
1	1- 2	. 3137	0.	si	2	. 5232	104. 65	si
1	1- 3	. 536	0.	si	3	. 5224	104. 48	si
1	1- 4	. 5489	0.	si	4	. 5216	104. 31	si
1	1- 5	. 3266	0.	si	5	. 5207	104. 14	si
1	1- 6	. 33	0.	si	6	. 5199	103. 98	si
1	1- 7	-. 1228	-1. 68	si	7	. 519	103. 81	si
1	1- 8	-. 1425	-1. 94	si	8	. 5182	103. 64	si
1					9	. 5174	103. 47	si
1					10	. 5165	103. 3	si
1					11	. 5157	103. 14	si
1					12	. 5148	102. 97	si
1					13	. 514	102. 8	si
1					14	. 5132	102. 63	si
1					15	. 5123	102. 47	si
1					16	. 5115	102. 3	si
1					17	. 2892	57. 84	si
1					18	. 2881	57. 61	si
1					19	. 2869	57. 39	si
1					20	. 2858	57. 16	si
1					21	. 3051	61. 03	si
1					22	. 304	60. 8	si
1					23	. 3029	60. 58	si
1					24	. 3018	60. 35	si
1					25	-. 0983	-19. 66	si
1					26	-. 0991	-19. 83	si
1					27	-. 1	-20.	si
1					28	-. 1008	-20. 16	si
1					29	-. 1017	-20. 33	si
1					30	-. 1025	-20. 5	si
1					31	-. 1033	-20. 67	si
1					32	-. 1042	-20. 84	si
1					33	-. 105	-21.	si
1					34	-. 1059	-21. 17	si
1					35	-. 1067	-21. 34	si
1					36	-. 1075	-21. 51	si

1					37	-. 1084	-21. 68	si
1					38	-. 1092	-21. 84	si
1					39	-. 1101	-22. 01	si
1					40	-. 1109	-22. 18	si
1					41	-. 1117	-22. 35	si
1					42	-. 1126	-22. 52	si
1					43	-. 1134	-22. 68	si
1					44	-. 1143	-22. 85	si
1					45	-. 1151	-23. 02	si
1					46	-. 1159	-23. 19	si
1					47	-. 1168	-23. 36	si
1					48	-. 1176	-23. 52	si
2	1- 1	. 5282	0.	si	1	. 973	194. 61	si
2	1- 2	. 5462	0.	si	2	. 9685	193. 71	si
2	1- 3	. 9497	0.	si	3	. 9641	192. 81	si
2	1- 4	1. 0187	0.	si	4	. 9596	191. 92	si
2	1- 5	. 6152	0.	si	5	. 9551	191. 02	si
2	1- 6	. 6332	0.	si	6	. 9506	190. 12	si
2	1- 7	-. 1888	-2. 54	si	7	. 9461	189. 22	si
2	1- 8	-. 2939	-3. 84	si	8	. 9416	188. 33	si
2					9	. 9371	187. 43	si
2					10	. 9327	186. 53	si
2					11	. 9282	185. 64	si
2					12	. 9237	184. 74	si
2					13	. 9192	183. 84	si
2					14	. 9147	182. 94	si
2					15	. 9102	182. 05	si
2					16	. 9057	181. 15	si
2					17	. 5022	100. 44	si
2					18	. 4962	99. 24	si
2					19	. 4902	98. 04	si
2					20	. 4842	96. 84	si
2					21	. 5875	117. 5	si
2					22	. 5815	116. 3	si
2					23	. 5755	115. 1	si
2					24	. 5695	113. 9	si
2					25	-. 1449	-28. 97	si
2					26	-. 1494	-29. 87	si
2					27	-. 1538	-30. 77	si
2					28	-. 1583	-31. 67	si
2					29	-. 1628	-32. 57	si
2					30	-. 1673	-33. 46	si
2					31	-. 1718	-34. 36	si
2					32	-. 1763	-35. 26	si
2					33	-. 1808	-36. 16	si
2					34	-. 1853	-37. 06	si
2					35	-. 1898	-37. 96	si
2					36	-. 1943	-38. 85	si
2					37	-. 1988	-39. 75	si
2					38	-. 2033	-40. 65	si
2					39	-. 2077	-41. 55	si
2					40	-. 2122	-42. 45	si
2					41	-. 2167	-43. 34	si
2					42	-. 2212	-44. 24	si
2					43	-. 2257	-45. 14	si
2					44	-. 2302	-46. 04	si
2					45	-. 2347	-46. 94	si
2					46	-. 2392	-47. 84	si
2					47	-. 2437	-48. 73	si
2					48	-. 2482	-49. 63	si
3	1- 1	. 5949	0.	si	1	. 9275	185. 5	si
3	1- 2	. 5895	0.	si	2	. 9289	185. 77	si
3	1- 3	. 9928	0.	si	3	. 9302	186. 04	si
3	1- 4	. 9721	0.	si	4	. 9316	186. 31	si
3	1- 5	. 5687	0.	si	5	. 9329	186. 58	si
3	1- 6	. 5633	0.	si	6	. 9343	186. 85	si
3	1- 7	-. 2583	-3. 41	si	7	. 9356	187. 12	si
3	1- 8	-. 2267	-3. 02	si	8	. 937	187. 39	si
3					9	. 9383	187. 66	si
3					10	. 9397	187. 93	si
3					11	. 941	188. 2	si
3					12	. 9424	188. 47	si
3					13	. 9437	188. 74	si
3					14	. 9451	189. 01	si
3					15	. 9464	189. 28	si
3					16	. 9478	189. 55	si
3					17	. 5444	108. 88	si
3					18	. 5462	109. 24	si
3					19	. 548	109. 61	si
3					20	. 5498	109. 97	si
3					21	. 5188	103. 75	si
3					22	. 5206	104. 11	si
3					23	. 5224	104. 47	si
3					24	. 5242	104. 84	si
3					25	-. 2132	-42. 65	si
3					26	-. 2119	-42. 38	si
3					27	-. 2105	-42. 11	si
3					28	-. 2092	-41. 84	si
3					29	-. 2078	-41. 57	si
3					30	-. 2065	-41. 3	si
3					31	-. 2051	-41. 03	si
3					32	-. 2038	-40. 75	si
3					33	-. 2024	-40. 48	si
3					34	-. 2011	-40. 21	si
3					35	-. 1997	-39. 94	si
3					36	-. 1984	-39. 67	si
3					37	-. 197	-39. 4	si

5	39	-. 1279	-25. 58	si
5	40	-. 1282	-25. 65	si
5	41	-. 1285	-25. 71	si
5	42	-. 1289	-25. 77	si
5	43	-. 1292	-25. 83	si
5	44	-. 1295	-25. 89	si
5	45	-. 1298	-25. 96	si
5	46	-. 1301	-26. 02	si
5	47	-. 1304	-26. 08	si
5	48	-. 1307	-26. 14	si

Descrizione : Pulvino 7

SOLLECITAZIONI AGENTI

Sforzi normali applicati in z= 183.7 ; y= 37.5 (baricentro CLS)
 Convenzioni: N + trazione; Mz + fib. inferiori tese; My + fib. sinistra tese.

N.	N	Mz	My	Descrizione
1	-37.49	-466.7266	-68.866	Caso 13. 1
2	-71.46	-855.0569	-344.4652	Caso 2. 2
3	-72.67	-855.0164	79.6992	Caso 2. 1
4	-81.21	-544.067	-146.2545	Caso 8. 10
5	-8.49	-555.0735	-18.5172	Caso 8. 23

RISULTATI

Piani di equilibrio (eps= muz * y +muy * z + lam):

Sol.	muz	muy	lambda
1.	.00000820978	.00000005488	-.00014245396
2.	.00001507302	.00000027975	-.00029533186
3.	.00001506485	-.00000006447	-.00023323162
4.	.00000943034	.00000011523	-.00017659259
5.	.00000990965	.00000001503	-.00015957137

Deformazioni sui materiali:

Cls					Acciaio lento			
sol	vert.	D cls	S cls	Ve	ferro	D ferri	S ferri	Ve
1	1- 1	.3091	0.	si	1	.5227	104.53	si
1	1- 2	.3125	0.	si	2	.5218	104.36	si
1	1- 3	.5342	0.	si	3	.5209	104.19	si
1	1- 4	.5475	0.	si	4	.5201	104.02	si
1	1- 5	.3258	0.	si	5	.5192	103.84	si
1	1- 6	.3292	0.	si	6	.5184	103.67	si
1	1- 7	-.1223	-1.67	si	7	.5175	103.5	si
1	1- 8	-.1425	-1.94	si	8	.5166	103.33	si
1					9	.5158	103.15	si
1					10	.5149	102.98	si
1					11	.514	102.81	si
1					12	.5132	102.64	si
1					13	.5123	102.46	si
1					14	.5115	102.29	si
1					15	.5106	102.12	si
1					16	.5097	101.95	si
1					17	.2881	57.62	si
1					18	.2869	57.38	si
1					19	.2858	57.15	si
1					20	.2846	56.92	si
1					21	.3045	60.89	si
1					22	.3033	60.66	si
1					23	.3021	60.43	si
1					24	.301	60.2	si
1					25	-.0978	-19.56	si
1					26	-.0987	-19.74	si
1					27	-.0995	-19.91	si
1					28	-.1004	-20.08	si
1					29	-.1013	-20.25	si
1					30	-.1021	-20.43	si
1					31	-.103	-20.6	si
1					32	-.1039	-20.77	si
1					33	-.1047	-20.94	si
1					34	-.1056	-21.12	si
1					35	-.1064	-21.29	si
1					36	-.1073	-21.46	si
1					37	-.1082	-21.63	si
1					38	-.109	-21.81	si
1					39	-.1099	-21.98	si
1					40	-.1108	-22.15	si
1					41	-.1116	-22.32	si
1					42	-.1125	-22.5	si
1					43	-.1133	-22.67	si
1					44	-.1142	-22.84	si
1					45	-.1151	-23.01	si
1					46	-.1159	-23.19	si
1					47	-.1168	-23.36	si
1					48	-.1177	-23.53	si
2	1- 1	.5337	0.	si	1	.9798	195.95	si
2	1- 2	.5513	0.	si	2	.9754	195.07	si
2	1- 3	.9583	0.	si	3	.971	194.19	si
2	1- 4	1.0258	0.	si	4	.9666	193.32	si
2	1- 5	.6188	0.	si	5	.9622	192.44	si
2	1- 6	.6365	0.	si	6	.9578	191.56	si
2	1- 7	-.1926	-2.59	si	7	.9534	190.68	si
2	1- 8	-.2953	-3.86	si	8	.949	189.8	si
2					9	.9446	188.93	si
2					10	.9402	188.05	si
2					11	.9359	187.17	si
2					12	.9315	186.29	si
2					13	.9271	185.41	si
2					14	.9227	184.54	si

4				16	.576	115.2	si
4				17	.3214	64.28	si
4				18	.319	63.79	si
4				19	.3166	63.31	si
4				20	.3141	62.83	si
4				21	.3558	71.15	si
4				22	.3534	70.67	si
4				23	.3509	70.19	si
4				24	.3485	69.7	si
4				25	-.1063	-21.26	si
4				26	-.1081	-21.62	si
4				27	-.1099	-21.99	si
4				28	-.1117	-22.35	si
4				29	-.1136	-22.71	si
4				30	-.1154	-23.07	si
4				31	-.1172	-23.44	si
4				32	-.119	-23.8	si
4				33	-.1208	-24.16	si
4				34	-.1226	-24.52	si
4				35	-.1244	-24.88	si
4				36	-.1262	-25.25	si
4				37	-.128	-25.61	si
4				38	-.1299	-25.97	si
4				39	-.1317	-26.33	si
4				40	-.1335	-26.69	si
4				41	-.1353	-27.06	si
4				42	-.1371	-27.42	si
4				43	-.1389	-27.78	si
4				44	-.1407	-28.14	si
4				45	-.1425	-28.5	si
4				46	-.1443	-28.87	si
4				47	-.1461	-29.23	si
4				48	-.148	-29.59	si
5	1- 1	.3855	0.	1	.6278	125.56	si
5	1- 2	.3864	0.	2	.6276	125.52	si
5	1- 3	.654	0.	3	.6273	125.47	si
5	1- 4	.6576	0.	4	.6271	125.42	si
5	1- 5	.39	0.	5	.6269	125.38	si
5	1- 6	.391	0.	6	.6266	125.33	si
5	1- 7	-.1541	-2.09	7	.6264	125.28	si
5	1- 8	-.1596	-2.16	8	.6262	125.23	si
5				9	.6259	125.19	si
5				10	.6257	125.14	si
5				11	.6255	125.09	si
5				12	.6252	125.05	si
5				13	.625	125.	si
5				14	.6248	124.95	si
5				15	.6245	124.9	si
5				16	.6243	124.86	si
5				17	.3567	71.34	si
5				18	.3564	71.28	si
5				19	.3561	71.22	si
5				20	.3558	71.16	si
5				21	.3612	72.24	si
5				22	.3609	72.18	si
5				23	.3606	72.12	si
5				24	.3603	72.05	si
5				25	-.1244	-24.87	si
5				26	-.1246	-24.92	si
5				27	-.1248	-24.97	si
5				28	-.1251	-25.01	si
5				29	-.1253	-25.06	si
5				30	-.1255	-25.11	si
5				31	-.1258	-25.16	si
5				32	-.126	-25.2	si
5				33	-.1263	-25.25	si
5				34	-.1265	-25.3	si
5				35	-.1267	-25.35	si
5				36	-.127	-25.39	si
5				37	-.1272	-25.44	si
5				38	-.1274	-25.49	si
5				39	-.1277	-25.53	si
5				40	-.1279	-25.58	si
5				41	-.1281	-25.63	si
5				42	-.1284	-25.68	si
5				43	-.1286	-25.72	si
5				44	-.1289	-25.77	si
5				45	-.1291	-25.82	si
5				46	-.1293	-25.87	si
5				47	-.1296	-25.91	si
5				48	-.1298	-25.96	si

Descrizione : Pulvino 8

SOLLECITAZIONI AGENTI

Sforzi normali applicati in $z=183.7$; $y=37.5$ (baricentro CLS)

Convenzioni: N + trazione; Mz + fib.inferiori tese; My + fib.sinistra tese.

N.	N	Mz	My	Descrizione
1	-38.94	-465.535	-71.5317	Caso 13. 1
2	-74.46	-853.2791	-347.5826	Caso 2. 2
3	-75.66	-853.2085	71.8213	Caso 2. 1
4	-85.87	-541.1966	-158.2049	Caso 8. 10
5	-7.35	-555.0838	-13.0399	Caso 8. 23

RISULTATI

Piani di equilibrio ($\epsilon_{ps} = m_{uz} * y + m_{uy} * z + l_{am}$):

Sol.	muz	muy	lambda
1.	.00000818276	.00000005697	-.00014253104
2.	.00001502942	.00000028204	-.00029530374
3.	.00001502062	-.00000005804	-.00023398635
4.	.00000936083	.00000012439	-.00017752652
5.	.00000991426	.00000001059	-.0001587272

Deformazioni sui materiali:

Cls					Acciaio lento			
sol	vert.	D cls	S cls	Ve	ferro	D ferri	S ferri	Ve
1	1- 1	.3075	0.	si	1	.5211	104.22	si
1	1- 2	.3111	0.	si	2	.5202	104.04	si
1	1- 3	.532	0.	si	3	.5193	103.86	si
1	1- 4	.5458	0.	si	4	.5184	103.68	si
1	1- 5	.3249	0.	si	5	.5175	103.5	si
1	1- 6	.3284	0.	si	6	.5166	103.32	si
1	1- 7	-.1216	-1.66	si	7	.5157	103.14	si
1	1- 8	-.1425	-1.94	si	8	.5148	102.96	si
1					9	.5139	102.78	si
1					10	.513	102.61	si
1					11	.5121	102.43	si
1					12	.5112	102.25	si
1					13	.5103	102.07	si
1					14	.5095	101.89	si
1					15	.5086	101.71	si
1					16	.5077	101.53	si
1					17	.2867	57.35	si
1					18	.2855	57.11	si
1					19	.2843	56.87	si
1					20	.2831	56.63	si
1					21	.3037	60.75	si
1					22	.3025	60.51	si
1					23	.3013	60.27	si
1					24	.3001	60.03	si
1					25	-.0972	-19.44	si
1					26	-.0981	-19.62	si
1					27	-.099	-19.8	si
1					28	-.0999	-19.98	si
1					29	-.1008	-20.16	si
1					30	-.1017	-20.34	si
1					31	-.1026	-20.52	si
1					32	-.1035	-20.7	si
1					33	-.1044	-20.88	si
1					34	-.1053	-21.06	si
1					35	-.1062	-21.24	si
1					36	-.1071	-21.41	si
1					37	-.108	-21.59	si
1					38	-.1089	-21.77	si
1					39	-.1098	-21.95	si
1					40	-.1107	-22.13	si
1					41	-.1115	-22.31	si
1					42	-.1124	-22.49	si
1					43	-.1133	-22.67	si
1					44	-.1142	-22.85	si
1					45	-.1151	-23.03	si
1					46	-.116	-23.2	si
1					47	-.1169	-23.38	si
1					48	-.1178	-23.56	si
2	1- 1	.5313	0.	si	1	.977	195.41	si
2	1- 2	.5491	0.	si	2	.9726	194.52	si
2	1- 3	.9549	0.	si	3	.9682	193.64	si
2	1- 4	1.023	0.	si	4	.9637	192.75	si
2	1- 5	.6172	0.	si	5	.9593	191.86	si
2	1- 6	.6349	0.	si	6	.9549	190.98	si
2	1- 7	-.1917	-2.58	si	7	.9505	190.09	si
2	1- 8	-.2953	-3.86	si	8	.946	189.21	si
2					9	.9416	188.32	si
2					10	.9372	187.44	si
2					11	.9328	186.55	si
2					12	.9283	185.67	si
2					13	.9239	184.78	si
2					14	.9195	183.9	si
2					15	.9151	183.01	si
2					16	.9106	182.13	si
2					17	.5048	100.97	si
2					18	.4989	99.78	si
2					19	.493	98.6	si
2					20	.4871	97.41	si
2					21	.589	117.8	si
2					22	.5831	116.62	si
2					23	.5772	115.43	si
2					24	.5712	114.25	si
2					25	-.1474	-29.49	si
2					26	-.1519	-30.37	si
2					27	-.1563	-31.26	si
2					28	-.1607	-32.15	si
2					29	-.1652	-33.03	si
2					30	-.1696	-33.92	si
2					31	-.174	-34.81	si
2					32	-.1785	-35.69	si
2					33	-.1829	-36.58	si
2					34	-.1873	-37.46	si
2					35	-.1918	-38.35	si
2					36	-.1962	-39.24	si
2					37	-.2006	-40.12	si
2					38	-.2051	-41.01	si
2					39	-.2095	-41.9	si

2					40	-.2139	-42.78	si
2					41	-.2183	-43.67	si
2					42	-.2228	-44.56	si
2					43	-.2272	-45.44	si
2					44	-.2316	-46.33	si
2					45	-.2361	-47.21	si
2					46	-.2405	-48.1	si
2					47	-.2449	-48.99	si
2					48	-.2494	-49.87	si
3	1- 1	.5921	0.	si	1	.9351	187.03	si
3	1- 2	.5885	0.	si	2	.9361	187.21	si
3	1- 3	.994	0.	si	3	.937	187.39	si
3	1- 4	.98	0.	si	4	.9379	187.58	si
3	1- 5	.5745	0.	si	5	.9388	187.76	si
3	1- 6	.5708	0.	si	6	.9397	187.94	si
3	1- 7	-.2553	-3.37	si	7	.9406	188.12	si
3	1- 8	-.234	-3.11	si	8	.9415	188.3	si
3					9	.9424	188.49	si
3					10	.9433	188.67	si
3					11	.9443	188.85	si
3					12	.9452	189.03	si
3					13	.9461	189.22	si
3					14	.947	189.4	si
3					15	.9479	189.58	si
3					16	.9488	189.76	si
3					17	.5433	108.65	si
3					18	.5445	108.89	si
3					19	.5457	109.14	si
3					20	.5469	109.38	si
3					21	.5259	105.19	si
3					22	.5272	105.43	si
3					23	.5284	105.67	si
3					24	.5296	105.92	si
3					25	-.2101	-42.02	si
3					26	-.2092	-41.83	si
3					27	-.2083	-41.65	si
3					28	-.2073	-41.47	si
3					29	-.2064	-41.29	si
3					30	-.2055	-41.1	si
3					31	-.2046	-40.92	si
3					32	-.2037	-40.74	si
3					33	-.2028	-40.56	si
3					34	-.2019	-40.37	si
3					35	-.201	-40.19	si
3					36	-.2	-40.01	si
3					37	-.1991	-39.83	si
3					38	-.1982	-39.64	si
3					39	-.1973	-39.46	si
3					40	-.1964	-39.28	si
3					41	-.1955	-39.1	si
3					42	-.1946	-38.91	si
3					43	-.1937	-38.73	si
3					44	-.1927	-38.55	si
3					45	-.1918	-38.37	si
3					46	-.1909	-38.18	si
3					47	-.19	-38.	si
3					48	-.1891	-37.82	si
4	1- 1	.3373	0.	si	1	.5995	119.89	si
4	1- 2	.3452	0.	si	2	.5975	119.5	si
4	1- 3	.5979	0.	si	3	.5956	119.11	si
4	1- 4	.6279	0.	si	4	.5936	118.72	si
4	1- 5	.3752	0.	si	5	.5917	118.33	si
4	1- 6	.383	0.	si	6	.5897	117.94	si
4	1- 7	-.1318	-1.8	si	7	.5878	117.55	si
4	1- 8	-.1775	-2.39	si	8	.5858	117.16	si
4					9	.5839	116.77	si
4					10	.5819	116.38	si
4					11	.58	115.99	si
4					12	.578	115.6	si
4					13	.576	115.21	si
4					14	.5741	114.82	si
4					15	.5721	114.43	si
4					16	.5702	114.04	si
4					17	.3174	63.49	si
4					18	.3148	62.97	si
4					19	.3122	62.44	si
4					20	.3096	61.92	si
4					21	.3546	70.91	si
4					22	.352	70.39	si
4					23	.3493	69.87	si
4					24	.3467	69.35	si
4					25	-.1041	-20.82	si
4					26	-.1061	-21.21	si
4					27	-.108	-21.6	si
4					28	-.11	-22.	si
4					29	-.1119	-22.39	si
4					30	-.1139	-22.78	si
4					31	-.1158	-23.17	si
4					32	-.1178	-23.56	si
4					33	-.1198	-23.95	si
4					34	-.1217	-24.34	si
4					35	-.1237	-24.73	si
4					36	-.1256	-25.12	si
4					37	-.1276	-25.51	si
4					38	-.1295	-25.9	si
4					39	-.1315	-26.3	si
4					40	-.1334	-26.69	si

4				41	- .1354	-27.08	si
4				42	- .1373	-27.47	si
4				43	- .1393	-27.86	si
4				44	- .1413	-28.25	si
4				45	- .1432	-28.64	si
4				46	- .1452	-29.03	si
4				47	- .1471	-29.42	si
4				48	- .1491	-29.81	si
5	1- 1	.3866	0.	1	.6277	125.54	si
5	1- 2	.3872	0.	2	.6275	125.5	si
5	1- 3	.6549	0.	3	.6274	125.47	si
5	1- 4	.6575	0.	4	.6272	125.44	si
5	1- 5	.3898	0.	5	.627	125.41	si
5	1- 6	.3904	0.	6	.6269	125.37	si
5	1- 7	- .1548	-2.1	7	.6267	125.34	si
5	1- 8	- .1587	-2.15	8	.6265	125.31	si
5				9	.6264	125.27	si
5				10	.6262	125.24	si
5				11	.626	125.21	si
5				12	.6259	125.17	si
5				13	.6257	125.14	si
5				14	.6255	125.11	si
5				15	.6254	125.07	si
5				16	.6252	125.04	si
5				17	.3575	71.5	si
5				18	.3573	71.46	si
5				19	.3571	71.41	si
5				20	.3568	71.37	si
5				21	.3607	72.13	si
5				22	.3604	72.09	si
5				23	.3602	72.05	si
5				24	.36	72.	si
5				25	- .1251	-25.03	si
5				26	- .1253	-25.06	si
5				27	- .1255	-25.09	si
5				28	- .1256	-25.13	si
5				29	- .1258	-25.16	si
5				30	- .126	-25.19	si
5				31	- .1261	-25.22	si
5				32	- .1263	-25.26	si
5				33	- .1265	-25.29	si
5				34	- .1266	-25.32	si
5				35	- .1268	-25.36	si
5				36	- .127	-25.39	si
5				37	- .1271	-25.42	si
5				38	- .1273	-25.46	si
5				39	- .1275	-25.49	si
5				40	- .1276	-25.52	si
5				41	- .1278	-25.56	si
5				42	- .128	-25.59	si
5				43	- .1281	-25.62	si
5				44	- .1283	-25.66	si
5				45	- .1285	-25.69	si
5				46	- .1286	-25.72	si
5				47	- .1288	-25.76	si
5				48	- .129	-25.79	si

Descrizione : Pulvino 9

SOLLECITAZIONI AGENTI

Sforzi normali applicati in z= 183.7 ; y= 37.5 (baricentro CLS)
 Convenzioni: N + trazione; Mz + fib.inferiori tese; My + fib.sinistra tese.

N.	N	Mz	My	Descrizione
1	-40.25	-464.2547	-73.9457	Caso 13.1
2	-73.69	-840.81	-339.3986	Caso 2.2
3	-74.89	-840.7083	66.4679	Caso 2.1
4	-90.99	-537.9418	-170.7772	Caso 8.10
5	-5.43	-555.2615	-6.3572	Caso 8.23

RISULTATI

Piani di equilibrio (eps= muz * y + muy * z + lam):

Sol.	muz	muy	lambda
1.	.00000815469	.00000005885	- .00014254241
2.	.00001480717	.00000027521	- .00029044391
3.	.00001479791	- .00000005368	- .00023114213
4.	.00000928267	.00000013398	- .00017843171
5.	.00000992491	.00000000517	- .00015772634

Deformazioni sui materiali:

Cls					Acciaio lento			
sol	vert.	D cls	S cls	Ve	ferro	D ferri	S ferri	Ve
1	1- 1	.306	0.	si	1	.5194	103.88	si
1	1- 2	.3097	0.	si	2	.5185	103.7	si
1	1- 3	.5298	0.	si	3	.5176	103.51	si
1	1- 4	.5441	0.	si	4	.5166	103.33	si
1	1- 5	.3239	0.	si	5	.5157	103.14	si
1	1- 6	.3276	0.	si	6	.5148	102.96	si
1	1- 7	- .1209	-1.65	si	7	.5139	102.77	si
1	1- 8	- .1425	-1.94	si	8	.5129	102.59	si
1					9	.512	102.41	si
1					10	.5111	102.22	si
1					11	.5102	102.04	si
1					12	.5093	101.85	si
1					13	.5083	101.67	si
1					14	.5074	101.48	si
1					15	.5065	101.3	si
1					16	.5056	101.11	si

1					17	.2854	57.08	si
1					18	.2841	56.83	si
1					19	.2829	56.58	si
1					20	.2817	56.34	si
1					21	.3029	60.59	si
1					22	.3017	60.34	si
1					23	.3005	60.09	si
1					24	.2992	59.85	si
1					25	-.0966	-19.33	si
1					26	-.0976	-19.51	si
1					27	-.0985	-19.7	si
1					28	-.0994	-19.88	si
1					29	-.1003	-20.07	si
1					30	-.1013	-20.25	si
1					31	-.1022	-20.44	si
1					32	-.1031	-20.62	si
1					33	-.104	-20.81	si
1					34	-.105	-20.99	si
1					35	-.1059	-21.18	si
1					36	-.1068	-21.36	si
1					37	-.1077	-21.55	si
1					38	-.1087	-21.73	si
1					39	-.1096	-21.92	si
1					40	-.1105	-22.1	si
1					41	-.1114	-22.29	si
1					42	-.1124	-22.47	si
1					43	-.1133	-22.66	si
1					44	-.1142	-22.84	si
1					45	-.1151	-23.03	si
1					46	-.1161	-23.21	si
1					47	-.117	-23.4	si
1					48	-.1179	-23.58	si
2	1- 1	.524	0.	si	1	.9623	192.45	si
2	1- 2	.5413	0.	si	2	.958	191.59	si
2	1- 3	.9411	0.	si	3	.9536	190.73	si
2	1- 4	1.0075	0.	si	4	.9493	189.86	si
2	1- 5	.6077	0.	si	5	.945	189.	si
2	1- 6	.6251	0.	si	6	.9407	188.14	si
2	1- 7	-.1893	-2.55	si	7	.9364	187.27	si
2	1- 8	-.2904	-3.8	si	8	.932	186.41	si
2					9	.9277	185.54	si
2					10	.9234	184.68	si
2					11	.9191	183.82	si
2					12	.9148	182.95	si
2					13	.9104	182.09	si
2					14	.9061	181.22	si
2					15	.9018	180.36	si
2					16	.8975	179.5	si
2					17	.4977	99.54	si
2					18	.4919	98.38	si
2					19	.4861	97.23	si
2					20	.4804	96.07	si
2					21	.5798	115.96	si
2					22	.574	114.81	si
2					23	.5683	113.65	si
2					24	.5625	112.5	si
2					25	-.1457	-29.15	si
2					26	-.1501	-30.01	si
2					27	-.1544	-30.88	si
2					28	-.1587	-31.74	si
2					29	-.163	-32.61	si
2					30	-.1674	-33.47	si
2					31	-.1717	-34.34	si
2					32	-.176	-35.2	si
2					33	-.1803	-36.07	si
2					34	-.1847	-36.93	si
2					35	-.189	-37.8	si
2					36	-.1933	-38.66	si
2					37	-.1976	-39.53	si
2					38	-.202	-40.39	si
2					39	-.2063	-41.26	si
2					40	-.2106	-42.12	si
2					41	-.2149	-42.99	si
2					42	-.2193	-43.85	si
2					43	-.2236	-44.71	si
2					44	-.2279	-45.58	si
2					45	-.2322	-46.44	si
2					46	-.2365	-47.31	si
2					47	-.2409	-48.17	si
2					48	-.2452	-49.04	si
3	1- 1	.5827	0.	si	1	.9217	184.34	si
3	1- 2	.5794	0.	si	2	.9226	184.51	si
3	1- 3	.9789	0.	si	3	.9234	184.68	si
3	1- 4	.9659	0.	si	4	.9242	184.85	si
3	1- 5	.5664	0.	si	5	.9251	185.02	si
3	1- 6	.563	0.	si	6	.9259	185.19	si
3	1- 7	-.2509	-3.32	si	7	.9268	185.35	si
3	1- 8	-.2311	-3.07	si	8	.9276	185.52	si
3					9	.9285	185.69	si
3					10	.9293	185.86	si
3					11	.9301	186.03	si
3					12	.931	186.2	si
3					13	.9318	186.36	si
3					14	.9327	186.53	si
3					15	.9335	186.7	si
3					16	.9343	186.87	si
3					17	.5348	106.96	si

3				18	.5359	107.19	si
3				19	.5371	107.41	si
3				20	.5382	107.64	si
3				21	.5188	103.76	si
3				22	.5199	103.98	si
3				23	.521	104.21	si
3				24	.5222	104.43	si
3				25	-.2063	-41.26	si
3				26	-.2055	-41.09	si
3				27	-.2046	-40.92	si
3				28	-.2038	-40.76	si
3				29	-.2029	-40.59	si
3				30	-.2021	-40.42	si
3				31	-.2012	-40.25	si
3				32	-.2004	-40.08	si
3				33	-.1996	-39.91	si
3				34	-.1987	-39.74	si
3				35	-.1979	-39.58	si
3				36	-.197	-39.41	si
3				37	-.1962	-39.24	si
3				38	-.1953	-39.07	si
3				39	-.1945	-38.9	si
3				40	-.1937	-38.73	si
3				41	-.1928	-38.56	si
3				42	-.192	-38.39	si
3				43	-.1911	-38.23	si
3				44	-.1903	-38.06	si
3				45	-.1894	-37.89	si
3				46	-.1886	-37.72	si
3				47	-.1878	-37.55	si
3				48	-.1869	-37.38	si
4	1- 1	.3321	0.	1	.5953	119.06	si
4	1- 2	.3406	0.	2	.5932	118.64	si
4	1- 3	.5912	0.	3	.5911	118.22	si
4	1- 4	.6235	0.	4	.589	117.79	si
4	1- 5	.3729	0.	5	.5869	117.37	si
4	1- 6	.3813	0.	6	.5848	116.95	si
4	1- 7	-.1292	-1.76	7	.5827	116.53	si
4	1- 8	-.1784	-2.41	8	.5806	116.11	si
4				9	.5785	115.69	si
4				10	.5764	115.27	si
4				11	.5743	114.85	si
4				12	.5722	114.43	si
4				13	.5701	114.01	si
4				14	.5679	113.59	si
4				15	.5658	113.17	si
4				16	.5637	112.75	si
4				17	.3131	62.62	si
4				18	.3103	62.06	si
4				19	.3075	61.5	si
4				20	.3047	60.93	si
4				21	.3531	70.62	si
4				22	.3503	70.06	si
4				23	.3475	69.49	si
4				24	.3447	68.93	si
4				25	-.1018	-20.35	si
4				26	-.1039	-20.77	si
4				27	-.106	-21.19	si
4				28	-.1081	-21.62	si
4				29	-.1102	-22.04	si
4				30	-.1123	-22.46	si
4				31	-.1144	-22.88	si
4				32	-.1165	-23.3	si
4				33	-.1186	-23.72	si
4				34	-.1207	-24.14	si
4				35	-.1228	-24.56	si
4				36	-.1249	-24.98	si
4				37	-.127	-25.4	si
4				38	-.1291	-25.83	si
4				39	-.1312	-26.25	si
4				40	-.1333	-26.67	si
4				41	-.1354	-27.09	si
4				42	-.1375	-27.51	si
4				43	-.1397	-27.93	si
4				44	-.1418	-28.35	si
4				45	-.1439	-28.77	si
4				46	-.146	-29.19	si
4				47	-.1481	-29.62	si
4				48	-.1502	-30.04	si
5	1- 1	.3881	0.	1	.6279	125.58	si
5	1- 2	.3885	0.	2	.6278	125.56	si
5	1- 3	.6564	0.	3	.6277	125.55	si
5	1- 4	.6577	0.	4	.6277	125.53	si
5	1- 5	.3897	0.	5	.6276	125.51	si
5	1- 6	.39	0.	6	.6275	125.5	si
5	1- 7	-.1558	-2.11	7	.6274	125.48	si
5	1- 8	-.1577	-2.14	8	.6273	125.47	si
5				9	.6272	125.45	si
5				10	.6272	125.43	si
5				11	.6271	125.42	si
5				12	.627	125.4	si
5				13	.6269	125.39	si
5				14	.6268	125.37	si
5				15	.6268	125.35	si
5				16	.6267	125.34	si
5				17	.3587	71.74	si
5				18	.3586	71.72	si

5	19	.3585	71.7	si
5	20	.3584	71.68	si
5	21	.3603	72.05	si
5	22	.3601	72.03	si
5	23	.36	72.01	si
5	24	.3599	71.99	si
5	25	-.1261	-25.21	si
5	26	-.1262	-25.23	si
5	27	-.1262	-25.25	si
5	28	-.1263	-25.26	si
5	29	-.1264	-25.28	si
5	30	-.1265	-25.3	si
5	31	-.1266	-25.31	si
5	32	-.1266	-25.33	si
5	33	-.1267	-25.34	si
5	34	-.1268	-25.36	si
5	35	-.1269	-25.38	si
5	36	-.127	-25.39	si
5	37	-.127	-25.41	si
5	38	-.1271	-25.42	si
5	39	-.1272	-25.44	si
5	40	-.1273	-25.46	si
5	41	-.1274	-25.47	si
5	42	-.1274	-25.49	si
5	43	-.1275	-25.51	si
5	44	-.1276	-25.52	si
5	45	-.1277	-25.54	si
5	46	-.1278	-25.55	si
5	47	-.1279	-25.57	si
5	48	-.1279	-25.59	si

Descrizi one : Pul vi no 10

SOLLECITAZIONI AGENTI

Sforzi normali applicati in z= 183.7 ; y= 37.5 (baricentro CLS)
 Convenzioni: N + trazione; Mz + fib.inferiori tese; My + fib.sinistra tese.

N.	N	Mz	My	Descrizi one
1	-42.12	-462.8234	-77.3771	Caso 13.1
2	-77.	-837.6811	-345.3238	Caso 2.2
3	-78.19	-837.5495	60.2385	Caso 2.1
4	-97.63	-534.132	-186.0345	Caso 8.10
5	-3.33	-555.6287	.6117	Caso 8.23

RISULTATI

Piani di equilibrio (eps= muz * y +muy * z + lam):

Sol.	muz	muy	lambda
1.	.00000812174	.00000006152	-.00014266843
2.	.00001473804	.00000027975	-.00029042335
3.	.00001472811	-.0000000486	-.00023126341
4.	.00000918873	.00000014554	-.00017955884
5.	.00000993966	-.0000000005	-.00015672829

Deformazioni sui materiali:

Cls					Acciaio lento			
sol	vert.	D cls	S cls	Ve	ferro	D ferri	S ferri	Ve
1	1- 1	.304	0.	si	1	.5175	103.5	si
1	1- 2	.3079	0.	si	2	.5165	103.3	si
1	1- 3	.5272	0.	si	3	.5156	103.11	si
1	1- 4	.542	0.	si	4	.5146	102.92	si
1	1- 5	.3228	0.	si	5	.5136	102.73	si
1	1- 6	.3266	0.	si	6	.5127	102.53	si
1	1- 7	-.1201	-1.64	si	7	.5117	102.34	si
1	1- 8	-.1427	-1.94	si	8	.5107	102.15	si
1					9	.5098	101.95	si
1					10	.5088	101.76	si
1					11	.5078	101.57	si
1					12	.5069	101.37	si
1					13	.5059	101.18	si
1					14	.5049	100.99	si
1					15	.504	100.79	si
1					16	.503	100.6	si
1					17	.2837	56.74	si
1					18	.2824	56.49	si
1					19	.2811	56.23	si
1					20	.2798	55.97	si
1					21	.3021	60.42	si
1					22	.3008	60.16	si
1					23	.2995	59.9	si
1					24	.2982	59.64	si
1					25	-.0959	-19.18	si
1					26	-.0969	-19.37	si
1					27	-.0978	-19.56	si
1					28	-.0988	-19.76	si
1					29	-.0998	-19.95	si
1					30	-.1007	-20.14	si
1					31	-.1017	-20.34	si
1					32	-.1027	-20.53	si
1					33	-.1036	-20.72	si
1					34	-.1046	-20.92	si
1					35	-.1056	-21.11	si
1					36	-.1065	-21.3	si
1					37	-.1075	-21.5	si
1					38	-.1085	-21.69	si
1					39	-.1094	-21.88	si
1					40	-.1104	-22.08	si
1					41	-.1114	-22.27	si
1					42	-.1123	-22.46	si

1					43	-.1133	-22.66	si
1					44	-.1143	-22.85	si
1					45	-.1152	-23.04	si
1					46	-.1162	-23.24	si
1					47	-.1172	-23.43	si
1					48	-.1181	-23.62	si
2	1- 1	.5202	0.	si	1	.9582	191.64	si
2	1- 2	.5378	0.	si	2	.9538	190.76	si
2	1- 3	.9357	0.	si	3	.9494	189.88	si
2	1- 4	1.0033	0.	si	4	.945	189.01	si
2	1- 5	.6053	0.	si	5	.9406	188.13	si
2	1- 6	.6229	0.	si	6	.9362	187.25	si
2	1- 7	-.1876	-2.52	si	7	.9319	186.37	si
2	1- 8	-.2904	-3.8	si	8	.9275	185.49	si
2					9	.9231	184.62	si
2					10	.9187	183.74	si
2					11	.9143	182.86	si
2					12	.9099	181.98	si
2					13	.9055	181.1	si
2					14	.9011	180.23	si
2					15	.8967	179.35	si
2					16	.8923	178.47	si
2					17	.4944	98.88	si
2					18	.4885	97.71	si
2					19	.4827	96.53	si
2					20	.4768	95.36	si
2					21	.5779	115.58	si
2					22	.572	114.4	si
2					23	.5661	113.23	si
2					24	.5603	112.05	si
2					25	-.1443	-28.85	si
2					26	-.1487	-29.73	si
2					27	-.1531	-30.61	si
2					28	-.1575	-31.49	si
2					29	-.1619	-32.37	si
2					30	-.1662	-33.25	si
2					31	-.1706	-34.13	si
2					32	-.175	-35.01	si
2					33	-.1794	-35.89	si
2					34	-.1838	-36.77	si
2					35	-.1882	-37.65	si
2					36	-.1926	-38.52	si
2					37	-.197	-39.4	si
2					38	-.2014	-40.28	si
2					39	-.2058	-41.16	si
2					40	-.2102	-42.04	si
2					41	-.2146	-42.92	si
2					42	-.219	-43.8	si
2					43	-.2234	-44.68	si
2					44	-.2278	-45.56	si
2					45	-.2322	-46.44	si
2					46	-.2366	-47.32	si
2					47	-.241	-48.19	si
2					48	-.2454	-49.07	si
3	1- 1	.5788	0.	si	1	.9176	183.52	si
3	1- 2	.5757	0.	si	2	.9184	183.67	si
3	1- 3	.9734	0.	si	3	.9191	183.83	si
3	1- 4	.9616	0.	si	4	.9199	183.98	si
3	1- 5	.564	0.	si	5	.9207	184.13	si
3	1- 6	.5609	0.	si	6	.9214	184.28	si
3	1- 7	-.2491	-3.3	si	7	.9222	184.44	si
3	1- 8	-.2313	-3.07	si	8	.9229	184.59	si
3					9	.9237	184.74	si
3					10	.9245	184.89	si
3					11	.9252	185.05	si
3					12	.926	185.2	si
3					13	.9268	185.35	si
3					14	.9275	185.5	si
3					15	.9283	185.66	si
3					16	.9291	185.81	si
3					17	.5314	106.28	si
3					18	.5324	106.48	si
3					19	.5334	106.69	si
3					20	.5345	106.89	si
3					21	.5169	103.38	si
3					22	.5179	103.58	si
3					23	.5189	103.79	si
3					24	.52	103.99	si
3					25	-.2048	-40.96	si
3					26	-.204	-40.8	si
3					27	-.2033	-40.65	si
3					28	-.2025	-40.5	si
3					29	-.2017	-40.35	si
3					30	-.201	-40.19	si
3					31	-.2002	-40.04	si
3					32	-.1994	-39.89	si
3					33	-.1987	-39.74	si
3					34	-.1979	-39.58	si
3					35	-.1972	-39.43	si
3					36	-.1964	-39.28	si
3					37	-.1956	-39.12	si
3					38	-.1949	-38.97	si
3					39	-.1941	-38.82	si
3					40	-.1933	-38.67	si
3					41	-.1926	-38.51	si
3					42	-.1918	-38.36	si
3					43	-.191	-38.21	si

5	45	- .1269	-25.39	si
5	46	- .1269	-25.39	si
5	47	- .1269	-25.38	si
5	48	- .1269	-25.38	si

Descrizione : Pulvino 11

SOLLECITAZIONI AGENTI

Sforzi normali applicati in z= 183.7 ; y= 37.5 (baricentro CLS)
 Convenzioni: N + trazione; Mz + fib.inferiori tese; My + fib.sinistra tese.

N.	N	Mz	My	Descrizione
1	-44.79	-461.0495	-82.2741	Caso 13. 1
2	-82.08	-834.3843	-384.495	Caso 2. 2
3	-83.28	-834.2217	80.7313	Caso 2. 1
4	-108.3	-528.901	-210.4321	Caso 8. 10
5	.84	-556.5813	13.0374	Caso 8. 23

RISULTATI

Piani di equilibrio (eps= muz * y + muy * z + lam):

Sol.	muz	muy	lambda
1.	.00000807955	.00000006532	-.00014292234
2.	.00001465966	.00000031129	-.00029511581
3.	.00001464845	-.00000006503	-.00022739756
4.	.00000905389	.00000016389	-.00018156819
5.	.00000997298	-.00000001062	-.00015501168

Deformazioni sui materiali:

Cls					Acciaio lento				
sol	vert.	D cls	S cls	Ve	ferro	D ferri	S ferri	Ve	
1	1- 1	.3015	0.	si	1	.515	103.01	si	
1	1- 2	.3056	0.	si	2	.514	102.8	si	
1	1- 3	.5237	0.	si	3	.513	102.6	si	
1	1- 4	.5395	0.	si	4	.512	102.39	si	
1	1- 5	.3213	0.	si	5	.5109	102.19	si	
1	1- 6	.3255	0.	si	6	.5099	101.98	si	
1	1- 7	-.1189	-1.63	si	7	.5089	101.78	si	
1	1- 8	-.1429	-1.94	si	8	.5079	101.57	si	
1					9	.5068	101.37	si	
1					10	.5058	101.16	si	
1					11	.5048	100.96	si	
1					12	.5038	100.75	si	
1					13	.5027	100.55	si	
1					14	.5017	100.34	si	
1					15	.5007	100.14	si	
1					16	.4997	99.93	si	
1					17	.2815	56.31	si	
1					18	.2802	56.03	si	
1					19	.2788	55.76	si	
1					20	.2774	55.48	si	
1					21	.301	60.2	si	
1					22	.2996	59.93	si	
1					23	.2983	59.65	si	
1					24	.2969	59.38	si	
1					25	-.0949	-18.98	si	
1					26	-.0959	-19.18	si	
1					27	-.0969	-19.39	si	
1					28	-.098	-19.59	si	
1					29	-.099	-19.8	si	
1					30	-.1	-20.	si	
1					31	-.101	-20.21	si	
1					32	-.1021	-20.41	si	
1					33	-.1031	-20.62	si	
1					34	-.1041	-20.82	si	
1					35	-.1051	-21.03	si	
1					36	-.1062	-21.23	si	
1					37	-.1072	-21.44	si	
1					38	-.1082	-21.64	si	
1					39	-.1093	-21.85	si	
1					40	-.1103	-22.06	si	
1					41	-.1113	-22.26	si	
1					42	-.1123	-22.47	si	
1					43	-.1134	-22.67	si	
1					44	-.1144	-22.88	si	
1					45	-.1154	-23.08	si	
1					46	-.1164	-23.29	si	
1					47	-.1175	-23.49	si	
1					48	-.1185	-23.7	si	
2	1- 1	.5112	0.	si	1	.9568	191.36	si	
2	1- 2	.5308	0.	si	2	.9519	190.39	si	
2	1- 3	.9266	0.	si	3	.947	189.41	si	
2	1- 4	1.0017	0.	si	4	.9422	188.43	si	
2	1- 5	.6059	0.	si	5	.9373	187.46	si	
2	1- 6	.6255	0.	si	6	.9324	186.48	si	
2	1- 7	-.1807	-2.44	si	7	.9275	185.5	si	
2	1- 8	-.2951	-3.86	si	8	.9226	184.52	si	
2					9	.9177	183.55	si	
2					10	.9129	182.57	si	
2					11	.908	181.59	si	
2					12	.9031	180.62	si	
2					13	.8982	179.64	si	
2					14	.8933	178.66	si	
2					15	.8884	177.69	si	
2					16	.8835	176.71	si	
2					17	.4877	97.55	si	
2					18	.4812	96.24	si	
2					19	.4747	94.93	si	
2					20	.4681	93.62	si	

2					21	.5806	116.12	si
2					22	.5741	114.82	si
2					23	.5675	113.51	si
2					24	.561	112.2	si
2					25	-.1377	-27.54	si
2					26	-.1426	-28.52	si
2					27	-.1475	-29.5	si
2					28	-.1524	-30.48	si
2					29	-.1573	-31.45	si
2					30	-.1622	-32.43	si
2					31	-.1671	-33.41	si
2					32	-.1719	-34.39	si
2					33	-.1768	-35.37	si
2					34	-.1817	-36.34	si
2					35	-.1866	-37.32	si
2					36	-.1915	-38.3	si
2					37	-.1964	-39.28	si
2					38	-.2013	-40.26	si
2					39	-.2062	-41.24	si
2					40	-.2111	-42.21	si
2					41	-.216	-43.19	si
2					42	-.2209	-44.17	si
2					43	-.2257	-45.15	si
2					44	-.2306	-46.13	si
2					45	-.2355	-47.11	si
2					46	-.2404	-48.08	si
2					47	-.2453	-49.06	si
2					48	-.2502	-50.04	si
3	1- 1	.5783	0.	si	1	.9102	182.05	si
3	1- 2	.5742	0.	si	2	.9112	182.25	si
3	1- 3	.9697	0.	si	3	.9123	182.45	si
3	1- 4	.954	0.	si	4	.9133	182.66	si
3	1- 5	.5585	0.	si	5	.9143	182.86	si
3	1- 6	.5544	0.	si	6	.9153	183.07	si
3	1- 7	-.2513	-3.32	si	7	.9164	183.27	si
3	1- 8	-.2274	-3.03	si	8	.9174	183.47	si
3					9	.9184	183.68	si
3					10	.9194	183.88	si
3					11	.9204	184.09	si
3					12	.9215	184.29	si
3					13	.9225	184.5	si
3					14	.9235	184.7	si
3					15	.9245	184.9	si
3					16	.9255	185.11	si
3					17	.53	106.01	si
3					18	.5314	106.28	si
3					19	.5328	106.55	si
3					20	.5341	106.83	si
3					21	.5106	102.12	si
3					22	.512	102.4	si
3					23	.5134	102.67	si
3					24	.5147	102.94	si
3					25	-.2071	-41.43	si
3					26	-.2061	-41.23	si
3					27	-.2051	-41.02	si
3					28	-.2041	-40.82	si
3					29	-.2031	-40.61	si
3					30	-.202	-40.41	si
3					31	-.201	-40.2	si
3					32	-.2	-40.	si
3					33	-.199	-39.79	si
3					34	-.198	-39.59	si
3					35	-.1969	-39.39	si
3					36	-.1959	-39.18	si
3					37	-.1949	-38.98	si
3					38	-.1939	-38.77	si
3					39	-.1928	-38.57	si
3					40	-.1918	-38.36	si
3					41	-.1908	-38.16	si
3					42	-.1898	-37.96	si
3					43	-.1888	-37.75	si
3					44	-.1877	-37.55	si
3					45	-.1867	-37.34	si
3					46	-.1857	-37.14	si
3					47	-.1847	-36.93	si
3					48	-.1836	-36.73	si
4	1- 1	.3164	0.	si	1	.5831	116.62	si
4	1- 2	.3267	0.	si	2	.5805	116.1	si
4	1- 3	.5712	0.	si	3	.5779	115.59	si
4	1- 4	.6107	0.	si	4	.5754	115.07	si
4	1- 5	.3663	0.	si	5	.5728	114.56	si
4	1- 6	.3766	0.	si	6	.5702	114.05	si
4	1- 7	-.1214	-1.66	si	7	.5677	113.53	si
4	1- 8	-.1816	-2.45	si	8	.5651	113.02	si
4					9	.5625	112.5	si
4					10	.5599	111.99	si
4					11	.5574	111.47	si
4					12	.5548	110.96	si
4					13	.5522	110.44	si
4					14	.5496	109.93	si
4					15	.5471	109.42	si
4					16	.5445	108.9	si
4					17	.3001	60.01	si
4					18	.2966	59.32	si
4					19	.2932	58.63	si
4					20	.2897	57.95	si
4					21	.349	69.79	si

4				22	.3455	69.1	si
4				23	.3421	68.41	si
4				24	.3386	67.73	si
4				25	-.0947	-18.94	si
4				26	-.0973	-19.45	si
4				27	-.0998	-19.97	si
4				28	-.1024	-20.48	si
4				29	-.105	-21.	si
4				30	-.1076	-21.51	si
4				31	-.1101	-22.03	si
4				32	-.1127	-22.54	si
4				33	-.1153	-23.06	si
4				34	-.1179	-23.57	si
4				35	-.1204	-24.09	si
4				36	-.123	-24.6	si
4				37	-.1256	-25.12	si
4				38	-.1282	-25.63	si
4				39	-.1307	-26.15	si
4				40	-.1333	-26.66	si
4				41	-.1359	-27.18	si
4				42	-.1385	-27.69	si
4				43	-.141	-28.21	si
4				44	-.1436	-28.72	si
4				45	-.1462	-29.24	si
4				46	-.1488	-29.75	si
4				47	-.1513	-30.27	si
4				48	-.1539	-30.78	si
5	1- 1	.3935	0.	1	.6297	125.93	si
5	1- 2	.3928	0.	2	.6298	125.96	si
5	1- 3	.6621	0.	3	.63	126.	si
5	1- 4	.6595	0.	4	.6302	126.03	si
5	1- 5	.3903	0.	5	.6303	126.06	si
5	1- 6	.3896	0.	6	.6305	126.1	si
5	1- 7	-.1589	-2.15	7	.6307	126.13	si
5	1- 8	-.155	-2.1	8	.6308	126.16	si
5				9	.631	126.2	si
5				10	.6312	126.23	si
5				11	.6313	126.26	si
5				12	.6315	126.3	si
5				13	.6317	126.33	si
5				14	.6318	126.36	si
5				15	.632	126.4	si
5				16	.6322	126.43	si
5				17	.3629	72.58	si
5				18	.3631	72.62	si
5				19	.3633	72.67	si
5				20	.3636	72.71	si
5				21	.3597	71.94	si
5				22	.3599	71.99	si
5				23	.3602	72.03	si
5				24	.3604	72.08	si
5				25	-.129	-25.79	si
5				26	-.1288	-25.76	si
5				27	-.1286	-25.73	si
5				28	-.1285	-25.69	si
5				29	-.1283	-25.66	si
5				30	-.1281	-25.63	si
5				31	-.128	-25.59	si
5				32	-.1278	-25.56	si
5				33	-.1276	-25.53	si
5				34	-.1275	-25.49	si
5				35	-.1273	-25.46	si
5				36	-.1271	-25.43	si
5				37	-.127	-25.39	si
5				38	-.1268	-25.36	si
5				39	-.1266	-25.33	si
5				40	-.1265	-25.29	si
5				41	-.1263	-25.26	si
5				42	-.1261	-25.23	si
5				43	-.126	-25.19	si
5				44	-.1258	-25.16	si
5				45	-.1256	-25.13	si
5				46	-.1255	-25.09	si
5				47	-.1253	-25.06	si
5				48	-.1251	-25.02	si

Descrizi one : Pulvino 12

SOLLECITAZIONI AGENTI

Sforzi normali applicati in z= 183.7 ; y= 37.5 (baricentro CLS)
 Convenzioni: N + trazione; Mz + fib.inferiori tese; My + fib.sinistra tese.

N.	N	Mz	My	Descrizione
1	-47.25	-459.2457	-86.7921	Caso 13. 1
2	-86.74	-831.037	-346.8922	Caso 2. 2
3	-87.94	-830.8446	26.0164	Caso 2. 1
4	-117.53	-523.6015	-226.0659	Caso 8. 10
5	4.11	-557.5328	17.6975	Caso 8. 23

RISULTATI

Piani	di equilibrio (eps= muz * y +muy * z + lam):			
Sol.	muz	muy	lambda	
1.	.00000803763	.00000006881	-.00014310577	
2.	.00001458064	.00000028017	-.00028884256	
3.	.00001456931	-.00000002092	-.00023471273	
4.	.00000892332	.00000017534	-.00018228982	
5.	.00001000278	-.00000001444	-.00015448065	

4					48	-.155	-31.	si
5	1- 1	.3957	0.	si	1	.6314	126.28	si
5	1- 2	.3948	0.	si	2	.6316	126.32	si
5	1- 3	.6648	0.	si	3	.6318	126.37	si
5	1- 4	.6614	0.	si	4	.6321	126.41	si
5	1- 5	.3913	0.	si	5	.6323	126.46	si
5	1- 6	.3904	0.	si	6	.6325	126.5	si
5	1- 7	-.1598	-2.16	si	7	.6327	126.55	si
5	1- 8	-.1545	-2.1	si	8	.633	126.59	si
5					9	.6332	126.64	si
5					10	.6334	126.69	si
5					11	.6337	126.73	si
5					12	.6339	126.78	si
5					13	.6341	126.82	si
5					14	.6343	126.87	si
5					15	.6346	126.91	si
5					16	.6348	126.96	si
5					17	.3647	72.94	si
5					18	.365	73.	si
5					19	.3653	73.06	si
5					20	.3656	73.12	si
5					21	.3604	72.08	si
5					22	.3607	72.14	si
5					23	.361	72.2	si
5					24	.3613	72.26	si
5					25	-.1297	-25.95	si
5					26	-.1295	-25.9	si
5					27	-.1293	-25.86	si
5					28	-.1291	-25.81	si
5					29	-.1288	-25.77	si
5					30	-.1286	-25.72	si
5					31	-.1284	-25.67	si
5					32	-.1281	-25.63	si
5					33	-.1279	-25.58	si
5					34	-.1277	-25.54	si
5					35	-.1275	-25.49	si
5					36	-.1272	-25.45	si
5					37	-.127	-25.4	si
5					38	-.1268	-25.36	si
5					39	-.1266	-25.31	si
5					40	-.1263	-25.27	si
5					41	-.1261	-25.22	si
5					42	-.1259	-25.18	si
5					43	-.1256	-25.13	si
5					44	-.1254	-25.08	si
5					45	-.1252	-25.04	si
5					46	-.125	-24.99	si
5					47	-.1247	-24.95	si
5					48	-.1245	-24.9	si

Descrizione : Pulvino 13

SOLLECITAZIONI AGENTI

Sforzi normali applicati in $z=183.7$; $y=37.5$ (baricentro CLS)
 Convenzioni: N + trazione; Mz + fib.inferiori tese; My + fib.sinistra tese.

N.	N	Mz	My	Descrizione
1	-50.22	-457.113	-92.2493	Caso 13. 1
2	-92.37	-827.0667	-370.1709	Caso 2. 2
3	9.08	-559.1297	43.1604	Caso 8. 5
4	-129.74	-516.8531	-250.985	Caso 8. 10
5	9.08	-559.1303	29.3297	Caso 8. 23

RISULTATI

Piani di equilibrio ($\epsilon = \mu_z * y + \mu_y * z + \lambda$):

Sol.	μ_z	μ_y	λ
1.	.00000798784	.00000007302	-.00014333672
2.	.00001448774	.0000002986	-.00029106738
3.	.00001005081	-.00000003529	-.00015092922
4.	.00000875554	.00000019363	-.00018384849
5.	.00001005081	-.00000002398	-.00015302351

Deformazioni sui materiali:

Cls					Acciaio lento				
sol	vert.	D cls	S cls	Ve	ferro	D ferri	S ferri	Ve	
1	1- 1	.296	0.	si	1	.5097	101.94	si	
1	1- 2	.3006	0.	si	2	.5086	101.71	si	
1	1- 3	.5163	0.	si	3	.5074	101.48	si	
1	1- 4	.5339	0.	si	4	.5063	101.25	si	
1	1- 5	.3182	0.	si	5	.5051	101.03	si	
1	1- 6	.3228	0.	si	6	.504	100.8	si	
1	1- 7	-.1165	-1.6	si	7	.5028	100.57	si	
1	1- 8	-.1433	-1.95	si	8	.5017	100.34	si	
1					9	.5005	100.11	si	
1					10	.4994	99.88	si	
1					11	.4983	99.65	si	
1					12	.4971	99.42	si	
1					13	.496	99.19	si	
1					14	.4948	98.96	si	
1					15	.4937	98.73	si	
1					16	.4925	98.5	si	
1					17	.2769	55.37	si	
1					18	.2753	55.06	si	
1					19	.2738	54.76	si	
1					20	.2723	54.45	si	
1					21	.2986	59.73	si	
1					22	.2971	59.42	si	
1					23	.2956	59.11	si	

1					24	.294	58.81	si
1					25	-.0928	-18.55	si
1					26	-.0939	-18.78	si
1					27	-.0951	-19.01	si
1					28	-.0962	-19.24	si
1					29	-.0974	-19.47	si
1					30	-.0985	-19.7	si
1					31	-.0996	-19.93	si
1					32	-.1008	-20.16	si
1					33	-.1019	-20.39	si
1					34	-.1031	-20.62	si
1					35	-.1042	-20.85	si
1					36	-.1054	-21.08	si
1					37	-.1065	-21.31	si
1					38	-.1077	-21.54	si
1					39	-.1088	-21.77	si
1					40	-.11	-21.99	si
1					41	-.1111	-22.22	si
1					42	-.1123	-22.45	si
1					43	-.1134	-22.68	si
1					44	-.1146	-22.91	si
1					45	-.1157	-23.14	si
1					46	-.1169	-23.37	si
1					47	-.118	-23.6	si
1					48	-.1192	-23.83	si
2	1- 1	.5058	0.	si	1	.9435	188.69	si
2	1- 2	.5246	0.	si	2	.9388	187.76	si
2	1- 3	.9157	0.	si	3	.9341	186.82	si
2	1- 4	.9878	0.	si	4	.9294	185.88	si
2	1- 5	.5967	0.	si	5	.9247	184.94	si
2	1- 6	.6155	0.	si	6	.92	184.01	si
2	1- 7	-.1814	-2.44	si	7	.9153	183.07	si
2	1- 8	-.2911	-3.81	si	8	.9107	182.13	si
2					9	.906	181.19	si
2					10	.9013	180.26	si
2					11	.8966	179.32	si
2					12	.8919	178.38	si
2					13	.8872	177.45	si
2					14	.8825	176.51	si
2					15	.8779	175.57	si
2					16	.8732	174.63	si
2					17	.482	96.4	si
2					18	.4757	95.15	si
2					19	.4695	93.89	si
2					20	.4632	92.64	si
2					21	.5711	114.22	si
2					22	.5648	112.97	si
2					23	.5586	111.71	si
2					24	.5523	110.46	si
2					25	-.1388	-27.76	si
2					26	-.1435	-28.7	si
2					27	-.1482	-29.64	si
2					28	-.1529	-30.57	si
2					29	-.1576	-31.51	si
2					30	-.1623	-32.45	si
2					31	-.1669	-33.39	si
2					32	-.1716	-34.33	si
2					33	-.1763	-35.27	si
2					34	-.181	-36.2	si
2					35	-.1857	-37.14	si
2					36	-.1904	-38.08	si
2					37	-.1951	-39.02	si
2					38	-.1998	-39.96	si
2					39	-.2045	-40.9	si
2					40	-.2092	-41.83	si
2					41	-.2139	-42.77	si
2					42	-.2186	-43.71	si
2					43	-.2232	-44.65	si
2					44	-.2279	-45.59	si
2					45	-.2326	-46.53	si
2					46	-.2373	-47.46	si
2					47	-.242	-48.4	si
2					48	-.2467	-49.34	si
3	1- 1	.4019	0.	si	1	.6324	126.49	si
3	1- 2	.3996	0.	si	2	.633	126.6	si
3	1- 3	.671	0.	si	3	.6336	126.71	si
3	1- 4	.6625	0.	si	4	.6341	126.82	si
3	1- 5	.3911	0.	si	5	.6347	126.93	si
3	1- 6	.3889	0.	si	6	.6352	127.04	si
3	1- 7	-.1639	-2.22	si	7	.6358	127.15	si
3	1- 8	-.1509	-2.05	si	8	.6363	127.26	si
3					9	.6369	127.38	si
3					10	.6374	127.49	si
3					11	.638	127.6	si
3					12	.6385	127.71	si
3					13	.6391	127.82	si
3					14	.6396	127.93	si
3					15	.6402	128.04	si
3					16	.6408	128.15	si
3					17	.3694	73.88	si
3					18	.3701	74.02	si
3					19	.3709	74.17	si
3					20	.3716	74.32	si
3					21	.3589	71.77	si
3					22	.3596	71.92	si
3					23	.3603	72.07	si
3					24	.3611	72.22	si

5	26	- .1312	-26.25	si
5	27	- .1309	-26.17	si
5	28	- .1305	-26.1	si
5	29	- .1301	-26.02	si
5	30	- .1297	-25.95	si
5	31	- .1293	-25.87	si
5	32	- .129	-25.79	si
5	33	- .1286	-25.72	si
5	34	- .1282	-25.64	si
5	35	- .1278	-25.57	si
5	36	- .1275	-25.49	si
5	37	- .1271	-25.42	si
5	38	- .1267	-25.34	si
5	39	- .1263	-25.27	si
5	40	- .126	-25.19	si
5	41	- .1256	-25.12	si
5	42	- .1252	-25.04	si
5	43	- .1248	-24.97	si
5	44	- .1245	-24.89	si
5	45	- .1241	-24.81	si
5	46	- .1237	-24.74	si
5	47	- .1233	-24.66	si
5	48	- .1229	-24.59	si

Descrizione : Pulvi no 14

SOLLECITAZIONI AGENTI

Sforzi normali applicati in z= 183.7 ; y= 37.5 (baricentro CLS)

Convenzioni: N + trazione; Mz + fib.inferiori tese; My + fib.sinistra tese.

N.	N	Mz	My	Descrizione
1	-54.6	-454.4039	-100.3094	Caso 13.1
2	-100.66	-822.0123	-389.0758	Caso 2.2
3	15.6	-561.5376	64.6927	Caso 8.5
4	-146.92	-507.8963	-283.023	Caso 8.10
5	15.6	-561.5382	41.7819	Caso 8.23

RISULTATI

Piani di equilibrio (eps= muz * y + muy * z + lam):

Sol.	muz	muy	lambda
1.	.00000792226	.00000007922	-.00014379642
2.	.000014365	.00000031318	-.00029236953
3.	.00001011943	-.00000005305	-.00014811571
4.	.0000085294	.00000021669	-.00018568782
5.	.00001011942	-.00000003426	-.00015160841

Deformazioni sui materiali:

Cls				Acciaio lento			
sol	vert.	D cls	S cls	ferro	D ferri	S ferri	Ve
1	1- 1	.2919	0.	1	.5059	101.19	si
1	1- 2	.2969	0.	2	.5047	100.94	si
1	1- 3	.5108	0.	3	.5035	100.69	si
1	1- 4	.5299	0.	4	.5022	100.44	si
1	1- 5	.316	0.	5	.501	100.19	si
1	1- 6	.321	0.	6	.4997	99.94	si
1	1- 7	-.1147	-1.57	7	.4985	99.7	si
1	1- 8	-.1438	-1.96	8	.4972	99.45	si
1				9	.496	99.2	si
1				10	.4948	98.95	si
1				11	.4935	98.7	si
1				12	.4923	98.45	si
1				13	.491	98.2	si
1				14	.4898	97.96	si
1				15	.4885	97.71	si
1				16	.4873	97.46	si
1				17	.2734	54.68	si
1				18	.2717	54.35	si
1				19	.2701	54.01	si
1				20	.2684	53.68	si
1				21	.297	59.41	si
1				22	.2954	59.07	si
1				23	.2937	58.74	si
1				24	.292	58.41	si
1				25	-.0912	-18.23	si
1				26	-.0924	-18.48	si
1				27	-.0937	-18.73	si
1				28	-.0949	-18.98	si
1				29	-.0961	-19.23	si
1				30	-.0974	-19.48	si
1				31	-.0986	-19.73	si
1				32	-.0999	-19.97	si
1				33	-.1011	-20.22	si
1				34	-.1024	-20.47	si
1				35	-.1036	-20.72	si
1				36	-.1049	-20.97	si
1				37	-.1061	-21.22	si
1				38	-.1073	-21.47	si
1				39	-.1086	-21.72	si
1				40	-.1098	-21.97	si
1				41	-.1111	-22.22	si
1				42	-.1123	-22.46	si
1				43	-.1136	-22.71	si
1				44	-.1148	-22.96	si
1				45	-.1161	-23.21	si
1				46	-.1173	-23.46	si
1				47	-.1185	-23.71	si
1				48	-.1198	-23.96	si
2	1- 1	.4977	0.	1	.9369	187.37	si

2	1- 2	. 5174	0.	si	2	. 9319	186. 39	si
2	1- 3	. 9053	0.	si	3	. 927	185. 41	si
2	1- 4	. 9809	0.	si	4	. 9221	184. 42	si
2	1- 5	. 593	0.	si	5	. 9172	183. 44	si
2	1- 6	. 6128	0.	si	6	. 9123	182. 46	si
2	1- 7	- . 1773	-2. 39	si	7	. 9074	181. 47	si
2	1- 8	- . 2924	-3. 82	si	8	. 9025	180. 49	si
2					9	. 8975	179. 51	si
2					10	. 8926	178. 52	si
2					11	. 8877	177. 54	si
2					12	. 8828	176. 56	si
2					13	. 8779	175. 58	si
2					14	. 873	174. 59	si
2					15	. 868	173. 61	si
2					16	. 8631	172. 63	si
2					17	. 4753	95. 06	si
2					18	. 4687	93. 74	si
2					19	. 4621	92. 43	si
2					20	. 4555	91. 11	si
2					21	. 5687	113. 75	si
2					22	. 5622	112. 43	si
2					23	. 5556	111. 12	si
2					24	. 549	109. 8	si
2					25	- . 1352	-27. 03	si
2					26	- . 1401	-28. 01	si
2					27	- . 145	-29.	si
2					28	- . 1499	-29. 98	si
2					29	- . 1548	-30. 97	si
2					30	- . 1598	-31. 95	si
2					31	- . 1647	-32. 94	si
2					32	- . 1696	-33. 92	si
2					33	- . 1745	-34. 9	si
2					34	- . 1794	-35. 89	si
2					35	- . 1844	-36. 87	si
2					36	- . 1893	-37. 86	si
2					37	- . 1942	-38. 84	si
2					38	- . 1991	-39. 82	si
2					39	- . 204	-40. 81	si
2					40	- . 209	-41. 79	si
2					41	- . 2139	-42. 78	si
2					42	- . 2188	-43. 76	si
2					43	- . 2237	-44. 75	si
2					44	- . 2287	-45. 73	si
2					45	- . 2336	-46. 71	si
2					46	- . 2385	-47. 7	si
2					47	- . 2434	-48. 68	si
2					48	- . 2483	-49. 67	si
3	1- 1	. 4085	0.	si	1	. 6353	127. 07	si
3	1- 2	. 4051	0.	si	2	. 6362	127. 23	si
3	1- 3	. 6783	0.	si	3	. 637	127. 4	si
3	1- 4	. 6655	0.	si	4	. 6378	127. 57	si
3	1- 5	. 3923	0.	si	5	. 6387	127. 73	si
3	1- 6	. 389	0.	si	6	. 6395	127. 9	si
3	1- 7	- . 1676	-2. 27	si	7	. 6403	128. 07	si
3	1- 8	- . 1481	-2. 01	si	8	. 6412	128. 23	si
3					9	. 642	128. 4	si
3					10	. 6428	128. 56	si
3					11	. 6437	128. 73	si
3					12	. 6445	128. 9	si
3					13	. 6453	129. 06	si
3					14	. 6462	129. 23	si
3					15	. 647	129. 4	si
3					16	. 6478	129. 56	si
3					17	. 3746	74. 92	si
3					18	. 3757	75. 14	si
3					19	. 3768	75. 36	si
3					20	. 3779	75. 59	si
3					21	. 3588	71. 75	si
3					22	. 3599	71. 98	si
3					23	. 361	72. 2	si
3					24	. 3621	72. 42	si
3					25	- . 1371	-27. 42	si
3					26	- . 1363	-27. 25	si
3					27	- . 1354	-27. 08	si
3					28	- . 1346	-26. 92	si
3					29	- . 1338	-26. 75	si
3					30	- . 1329	-26. 58	si
3					31	- . 1321	-26. 42	si
3					32	- . 1313	-26. 25	si
3					33	- . 1304	-26. 08	si
3					34	- . 1296	-25. 92	si
3					35	- . 1288	-25. 75	si
3					36	- . 1279	-25. 58	si
3					37	- . 1271	-25. 42	si
3					38	- . 1263	-25. 25	si
3					39	- . 1254	-25. 08	si
3					40	- . 1246	-24. 92	si
3					41	- . 1238	-24. 75	si
3					42	- . 1229	-24. 58	si
3					43	- . 1221	-24. 42	si
3					44	- . 1213	-24. 25	si
3					45	- . 1204	-24. 08	si
3					46	- . 1196	-23. 92	si
3					47	- . 1188	-23. 75	si
3					48	- . 1179	-23. 58	si
4	1- 1	. 2834	0.	si	1	. 5534	110. 69	si
4	1- 2	. 2971	0.	si	2	. 55	110. 01	si

4	1- 3	. 5274	0.	si	3	. 5466	109. 33	si
4	1- 4	. 5797	0.	si	4	. 5432	108. 65	si
4	1- 5	. 3494	0.	si	5	. 5398	107. 97	si
4	1- 6	. 363	0.	si	6	. 5364	107. 29	si
4	1- 7	-. 1061	-1. 46	si	7	. 533	106. 61	si
4	1- 8	-. 1857	-2. 5	si	8	. 5296	105. 93	si
4					9	. 5262	105. 25	si
4					10	. 5228	104. 57	si
4					11	. 5194	103. 89	si
4					12	. 516	103. 21	si
4					13	. 5126	102. 53	si
4					14	. 5092	101. 85	si
4					15	. 5058	101. 17	si
4					16	. 5024	100. 49	si
4					17	. 2721	54. 43	si
4					18	. 2676	53. 52	si
4					19	. 263	52. 61	si
4					20	. 2585	51. 7	si
4					21	. 3368	67. 36	si
4					22	. 3323	66. 45	si
4					23	. 3277	65. 54	si
4					24	. 3232	64. 63	si
4					25	-. 0811	-16. 23	si
4					26	-. 0845	-16. 91	si
4					27	-. 0879	-17. 59	si
4					28	-. 0914	-18. 27	si
4					29	-. 0948	-18. 95	si
4					30	-. 0982	-19. 63	si
4					31	-. 1016	-20. 31	si
4					32	-. 105	-20. 99	si
4					33	-. 1084	-21. 68	si
4					34	-. 1118	-22. 36	si
4					35	-. 1152	-23. 04	si
4					36	-. 1186	-23. 72	si
4					37	-. 122	-24. 4	si
4					38	-. 1254	-25. 08	si
4					39	-. 1288	-25. 76	si
4					40	-. 1322	-26. 44	si
4					41	-. 1356	-27. 12	si
4					42	-. 139	-27. 8	si
4					43	-. 1424	-28. 49	si
4					44	-. 1458	-29. 17	si
4					45	-. 1492	-29. 85	si
4					46	-. 1526	-30. 53	si
4					47	-. 156	-31. 21	si
4					48	-. 1594	-31. 89	si
5	1- 1	. 405	0.	si	1	. 6375	127. 5	si
5	1- 2	. 4028	0.	si	2	. 638	127. 61	si
5	1- 3	. 676	0.	si	3	. 6386	127. 72	si
5	1- 4	. 6678	0.	si	4	. 6391	127. 82	si
5	1- 5	. 3945	0.	si	5	. 6397	127. 93	si
5	1- 6	. 3924	0.	si	6	. 6402	128. 04	si
5	1- 7	-. 1642	-2. 22	si	7	. 6407	128. 15	si
5	1- 8	-. 1516	-2. 06	si	8	. 6413	128. 25	si
5					9	. 6418	128. 36	si
5					10	. 6423	128. 47	si
5					11	. 6429	128. 58	si
5					12	. 6434	128. 68	si
5					13	. 644	128. 79	si
5					14	. 6445	128. 9	si
5					15	. 645	129. 01	si
5					16	. 6456	129. 11	si
5					17	. 3723	74. 47	si
5					18	. 3731	74. 61	si
5					19	. 3738	74. 76	si
5					20	. 3745	74. 9	si
5					21	. 3621	72. 42	si
5					22	. 3628	72. 57	si
5					23	. 3636	72. 71	si
5					24	. 3643	72. 86	si
5					25	-. 1337	-26. 75	si
5					26	-. 1332	-26. 64	si
5					27	-. 1327	-26. 53	si
5					28	-. 1321	-26. 42	si
5					29	-. 1316	-26. 32	si
5					30	-. 131	-26. 21	si
5					31	-. 1305	-26. 1	si
5					32	-. 13	-25. 99	si
5					33	-. 1294	-25. 89	si
5					34	-. 1289	-25. 78	si
5					35	-. 1284	-25. 67	si
5					36	-. 1278	-25. 56	si
5					37	-. 1273	-25. 45	si
5					38	-. 1267	-25. 35	si
5					39	-. 1262	-25. 24	si
5					40	-. 1257	-25. 13	si
5					41	-. 1251	-25. 02	si
5					42	-. 1246	-24. 92	si
5					43	-. 124	-24. 81	si
5					44	-. 1235	-24. 7	si
5					45	-. 123	-24. 59	si
5					46	-. 1224	-24. 49	si
5					47	-. 1219	-24. 38	si
5					48	-. 1214	-24. 27	si

Descrizione : Pulvino 15

SOLLECITAZIONI AGENTI

Sforzi normali applicati in z= 183.7 ; y= 37.5 (baricentro CLS)

Convenzioni: N + trazione; Mz + fib.inferiori tese; My + fib.sinistra tese.

N.	N	Mz	My	Descrizione
1	-63.07	-449.9687	-115.8567	Caso 13.1
2	-116.65	-813.6984	-444.1513	Caso 2.2
3	29.58	-566.8934	107.1779	Caso 8.5
4	-181.49	-491.7901	-348.523	Caso 8.10
5	29.58	-566.894	69.4585	Caso 8.23

RISULTATI

Piani di equilibrio (eps= muz * y + muy * z + lam):

Sol.	muz	muy	lambda
1.	.00000780989	.0000000911	-.00014488536
2.	.00001415475	.00000035629	-.00029785876
3.	.00001027003	-.00000008846	-.00014258586
4.	.00000811009	.00000026283	-.00018974838
5.	.00001026999	-.0000000573	-.00014842014

Deformazioni sui materiali:

Cls					Acciaio lento			
sol	vert.	D cls	S cls	Ve	ferro	D ferri	S ferri	Ve
1	1- 1	.2847	0.	si	1	.4996	99.91	si
1	1- 2	.2904	0.	si	2	.4981	99.62	si
1	1- 3	.5013	0.	si	3	.4967	99.34	si
1	1- 4	.5233	0.	si	4	.4953	99.05	si
1	1- 5	.3124	0.	si	5	.4938	98.77	si
1	1- 6	.3181	0.	si	6	.4924	98.48	si
1	1- 7	-.1114	-1.53	si	7	.491	98.2	si
1	1- 8	-.1449	-1.97	si	8	.4895	97.91	si
1					9	.4881	97.62	si
1					10	.4867	97.34	si
1					11	.4853	97.05	si
1					12	.4838	96.77	si
1					13	.4824	96.48	si
1					14	.481	96.19	si
1					15	.4795	95.91	si
1					16	.4781	95.62	si
1					17	.2672	53.45	si
1					18	.2653	53.07	si
1					19	.2634	52.68	si
1					20	.2615	52.3	si
1					21	.2944	58.89	si
1					22	.2925	58.5	si
1					23	.2906	58.12	si
1					24	.2887	57.74	si
1					25	-.0883	-17.65	si
1					26	-.0897	-17.94	si
1					27	-.0911	-18.22	si
1					28	-.0926	-18.51	si
1					29	-.094	-18.8	si
1					30	-.0954	-19.08	si
1					31	-.0968	-19.37	si
1					32	-.0983	-19.66	si
1					33	-.0997	-19.94	si
1					34	-.1011	-20.23	si
1					35	-.1026	-20.51	si
1					36	-.104	-20.8	si
1					37	-.1054	-21.09	si
1					38	-.1069	-21.37	si
1					39	-.1083	-21.66	si
1					40	-.1097	-21.95	si
1					41	-.1112	-22.23	si
1					42	-.1126	-22.52	si
1					43	-.114	-22.81	si
1					44	-.1155	-23.09	si
1					45	-.1169	-23.38	si
1					46	-.1183	-23.66	si
1					47	-.1198	-23.95	si
1					48	-.1212	-24.24	si
2	1- 1	.4807	0.	si	1	.9278	185.55	si
2	1- 2	.5031	0.	si	2	.9222	184.43	si
2	1- 3	.8853	0.	si	3	.9166	183.31	si
2	1- 4	.9713	0.	si	4	.911	182.2	si
2	1- 5	.5891	0.	si	5	.9054	181.08	si
2	1- 6	.6116	0.	si	6	.8998	179.96	si
2	1- 7	-.167	-2.26	si	7	.8942	178.84	si
2	1- 8	-.2979	-3.89	si	8	.8886	177.72	si
2					9	.883	176.6	si
2					10	.8774	175.49	si
2					11	.8718	174.37	si
2					12	.8662	173.25	si
2					13	.8607	172.13	si
2					14	.8551	171.01	si
2					15	.8495	169.89	si
2					16	.8439	168.78	si
2					17	.4617	92.34	si
2					18	.4542	90.84	si
2					19	.4467	89.35	si
2					20	.4393	87.85	si
2					21	.568	113.6	si
2					22	.5605	112.11	si
2					23	.5531	110.61	si
2					24	.5456	109.11	si
2					25	-.1256	-25.11	si
2					26	-.1312	-26.23	si
2					27	-.1368	-27.35	si

4					29	-.0862	-17.23	si
4					30	-.0903	-18.06	si
4					31	-.0944	-18.88	si
4					32	-.0986	-19.71	si
4					33	-.1027	-20.54	si
4					34	-.1068	-21.36	si
4					35	-.1109	-22.19	si
4					36	-.1151	-23.01	si
4					37	-.1192	-23.84	si
4					38	-.1233	-24.67	si
4					39	-.1275	-25.49	si
4					40	-.1316	-26.32	si
4					41	-.1357	-27.14	si
4					42	-.1399	-27.97	si
4					43	-.144	-28.8	si
4					44	-.1481	-29.62	si
4					45	-.1522	-30.45	si
4					46	-.1564	-31.27	si
4					47	-.1605	-32.1	si
4					48	-.1646	-32.93	si
5	1- 1	.4164	0.	si	1	.6456	129.13	si
5	1- 2	.4128	0.	si	2	.6465	129.31	si
5	1- 3	.6901	0.	si	3	.6474	129.49	si
5	1- 4	.6763	0.	si	4	.6483	129.67	si
5	1- 5	.399	0.	si	5	.6492	129.85	si
5	1- 6	.3954	0.	si	6	.6501	130.03	si
5	1- 7	-.1695	-2.29	si	7	.651	130.21	si
5	1- 8	-.1484	-2.02	si	8	.6519	130.39	si
5					9	.6528	130.57	si
5					10	.6537	130.75	si
5					11	.6546	130.93	si
5					12	.6555	131.11	si
5					13	.6564	131.29	si
5					14	.6573	131.47	si
5					15	.6582	131.65	si
5					16	.6591	131.83	si
5					17	.3818	76.37	si
5					18	.383	76.61	si
5					19	.3842	76.85	si
5					20	.3854	77.09	si
5					21	.3647	72.95	si
5					22	.3659	73.19	si
5					23	.3671	73.43	si
5					24	.3684	73.67	si
5					25	-.1385	-27.7	si
5					26	-.1376	-27.52	si
5					27	-.1367	-27.34	si
5					28	-.1358	-27.16	si
5					29	-.1349	-26.98	si
5					30	-.134	-26.8	si
5					31	-.1331	-26.62	si
5					32	-.1322	-26.44	si
5					33	-.1313	-26.26	si
5					34	-.1304	-26.08	si
5					35	-.1295	-25.9	si
5					36	-.1286	-25.72	si
5					37	-.1277	-25.54	si
5					38	-.1268	-25.36	si
5					39	-.1259	-25.18	si
5					40	-.125	-25.	si
5					41	-.1241	-24.82	si
5					42	-.1232	-24.64	si
5					43	-.1223	-24.46	si
5					44	-.1214	-24.28	si
5					45	-.1205	-24.1	si
5					46	-.1196	-23.92	si
5					47	-.1187	-23.74	si
5					48	-.1178	-23.56	si

DIAGRAMMI SFORZI-DEFORMAZIONI DELLE SEZIONI:

N.B. Per ogni pulvino (in sezione XZ e in sezione YZ) è rappresentata la sezione soggetta al sestetto del caso di carico che induce la massima combinazione sforzi-deformazioni.

Ripristino Ponte-Tubo
VERIFICA PULVINO XZ 1

DESCRIZIONI
Tipo sezione : RETTANGOLARE
Tipo verifica: stato limite ultimo

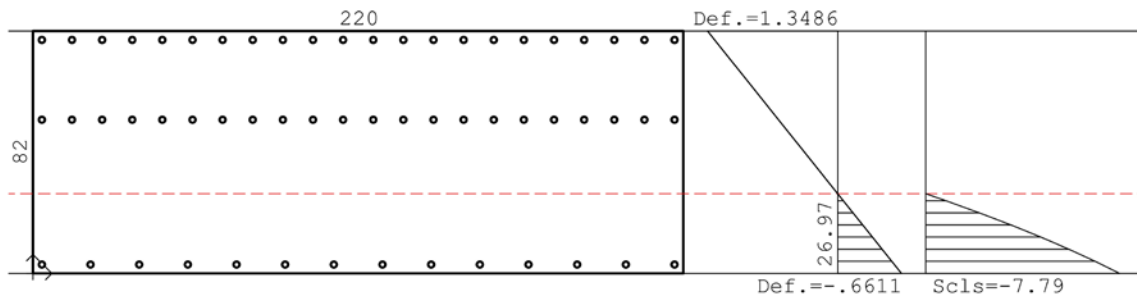
CARATTERISTICHE DEI MATERIALI
Calcestruzzo: Rck= 30.
fck= 24.9
fcd= 14.11 (.35%)
Acciaio lento: Tipo= B450C
fyk= 450.
ftk= 540.
ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
eps= muz * y +muy * z + lam
muz= 2.45091117867728E-05
muy= 0
lam=-3.80473735842816E-04

SOLLECITAZIONI AGENTI:
Nd in y= 29.6 (baricentro CLS)
Nd = -369.21
Mdz=-1740.9165
verifica in pressoflessione retta

UNITA' DI MISURA:
kN; cm; kNm; N/mm2.
Ø in mm; deformazioni*1000.

SIMBOLI:
S=sigma (tensioni sui materiali);
D=deformazioni (epsilon):



TENSIONI NEL CLS:					
ver	Z	Y	Dcls	Scls	Ve
1	-2673.	70.6	1.34864	0.	si
2	-2453.	70.6	1.34864	0.	si
3	-2453.	-11.4	-.6611	-7.79	si
4	-2673.	-11.4	-.6611	-7.79	si

TENSIONI NEI FERRI:										
Fer	Z	Y	Ø (mm)	Af (cm2)	D	ferri	S	ferri	Ve	
1	-2456.	40.6	20	3.14		.61337	122.67	si		
3	-2476.	40.6	20	3.14		.61337	122.67	si		
4	-2487.	40.6	20	3.14		.61337	122.67	si		
5	-2497.	40.6	20	3.14		.61337	122.67	si		
6	-2507.	40.6	20	3.14		.61337	122.67	si		
7	-2517.	40.6	20	3.14		.61337	122.67	si		
8	-2527.	40.6	20	3.14		.61337	122.67	si		
9	-2538.	40.6	20	3.14		.61337	122.67	si		
10	-2548.	40.6	20	3.14		.61337	122.67	si		
11	-2558.	40.6	20	3.14		.61337	122.67	si		
12	-2568.	40.6	20	3.14		.61337	122.67	si		
13	-2578.	40.6	20	3.14		.61337	122.67	si		
14	-2589.	40.6	20	3.14		.61337	122.67	si		
15	-2599.	40.6	20	3.14		.61337	122.67	si		
16	-2609.	40.6	20	3.14		.61337	122.67	si		
17	-2619.	40.6	20	3.14		.61337	122.67	si		
18	-2629.	40.6	20	3.14		.61337	122.67	si		
19	-2639.	40.6	20	3.14		.61337	122.67	si		
20	-2650.	40.6	20	3.14		.61337	122.67	si		
21	-2660.	40.6	20	3.14		.61337	122.67	si		
22	-2670.	40.6	20	3.14		.61337	122.67	si		
23	-2456.	67.6	20	3.14	1.27512	255.02	si			
24	-2466.	67.6	20	3.14	1.27512	255.02	si			
25	-2476.	67.6	20	3.14	1.27512	255.02	si			
26	-2487.	67.6	20	3.14	1.27512	255.02	si			
27	-2497.	67.6	20	3.14	1.27512	255.02	si			
28	-2507.	67.6	20	3.14	1.27512	255.02	si			
29	-2517.	67.6	20	3.14	1.27512	255.02	si			
30	-2527.	67.6	20	3.14	1.27512	255.02	si			
31	-2538.	67.6	20	3.14	1.27512	255.02	si			
32	-2548.	67.6	20	3.14	1.27512	255.02	si			
33	-2558.	67.6	20	3.14	1.27512	255.02	si			
34	-2568.	67.6	20	3.14	1.27512	255.02	si			
35	-2578.	67.6	20	3.14	1.27512	255.02	si			
36	-2589.	67.6	20	3.14	1.27512	255.02	si			
37	-2599.	67.6	20	3.14	1.27512	255.02	si			
38	-2609.	67.6	20	3.14	1.27512	255.02	si			
39	-2619.	67.6	20	3.14	1.27512	255.02	si			
40	-2629.	67.6	20	3.14	1.27512	255.02	si			
41	-2639.	67.6	20	3.14	1.27512	255.02	si			
42	-2650.	67.6	20	3.14	1.27512	255.02	si			
43	-2660.	67.6	20	3.14	1.27512	255.02	si			
44	-2670.	67.6	20	3.14	1.27512	255.02	si			
45	-2456.	-8.4	20	3.14	-.58758	-117.52	si			
46	-2473.	-8.4	20	3.14	-.58758	-117.52	si			
47	-2489.	-8.4	20	3.14	-.58758	-117.52	si			
48	-2505.	-8.4	20	3.14	-.58758	-117.52	si			
49	-2522.	-8.4	20	3.14	-.58758	-117.52	si			
50	-2538.	-8.4	20	3.14	-.58758	-117.52	si			
51	-2555.	-8.4	20	3.14	-.58758	-117.52	si			
52	-2571.	-8.4	20	3.14	-.58758	-117.52	si			
53	-2588.	-8.4	20	3.14	-.58758	-117.52	si			
54	-2604.	-8.4	20	3.14	-.58758	-117.52	si			
55	-2621.	-8.4	20	3.14	-.58758	-117.52	si			
56	-2637.	-8.4	20	3.14	-.58758	-117.52	si			
57	-2654.	-8.4	20	3.14	-.58758	-117.52	si			
58	-2670.	-8.4	20	3.14	-.58758	-117.52	si			

% ARMAT.: tesa = .77; comp. = .24; tot. = 1.01

Ripristino Ponte-Tubo
VERIFICA PULVINO YZ 1

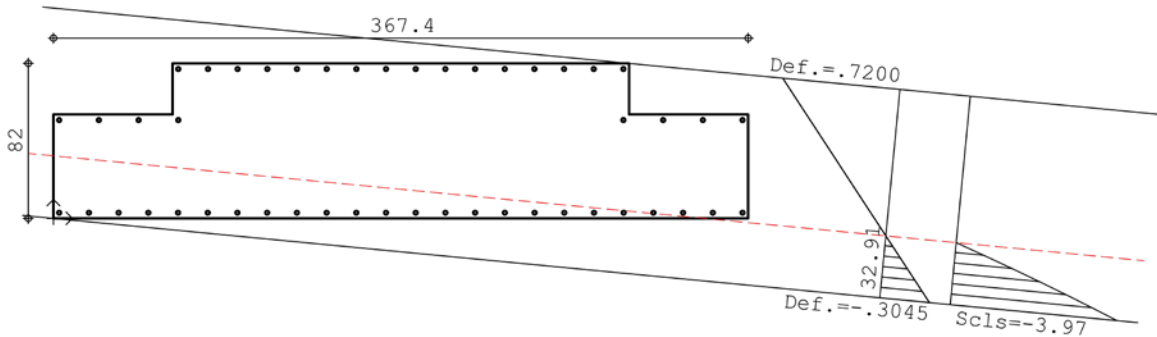
DESCRIZIONI
Tipo sezione : U Pul
Tipo verifica: sEato limite ultimo

CARATTERISTICHE DEI MATERIALI
Calcestruzzo: Rck= 30.
fck= 24.9
fcd= 14.11 (.35%)
Acciaio lento: Tipo= B450C
fyk= 450.
ftk= 540.
ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
eps= muz * y +muy * z + lam
muz= 9.20733842050261E-06
muy= 8.85092773290332E-07
lam=-3.04454836496454E-04

SOLLECITAZIONI AGENTI:
Nd in z= 183.7; y= 37.5 (baricentro CLS)
Nd = -197.67
Mdz= -556.7633
Mdy=-1066.0253

UNITA' DI MISURA:
kN; cm; kNm; N/mm2.
Ø in mm; deformazioni*1000.
SIMBOLI:
S=sigma (tensioni sui materiali);
D=deformazioni (epsilon):



TENSIONI NEL CLS:					
ver	z	y	Dcls	Scls	Vel
1	0.	55.	.20195	0.	si
2	63.	55.	.25771	0.	si
3	63.	82.	.50631	0.	si
4	304.4	82.	.71997	0.	si
5	304.4	55.	.47137	0.	si
6	367.4	55.	.52713	0.	si
7	367.4	0.	.02073	0.	si
8	0.	0.	-.30445	-3.97	si

TENSIONI NEI FERRI:										
fer	z	y	Ø (mm)	Af (cm2)	D ferri	S ferri	Vel ferri			
1	301.4	79.	20	3.14	.68969	137.94	si			
2	285.7	79.	20	3.14	.6758	135.16	si			
3	270.	79.	20	3.14	.66191	132.38	si			
4	254.3	79.	20	3.14	.64802	129.6	si			
5	238.6	79.	20	3.14	.63413	126.83	si			
6	222.9	79.	20	3.14	.62024	124.05	si			
7	207.2	79.	20	3.14	.60635	121.27	si			
8	191.5	79.	20	3.14	.59246	118.49	si			
9	175.9	79.	20	3.14	.57857	115.71	si			
10	160.2	79.	20	3.14	.56468	112.94	si			
11	144.5	79.	20	3.14	.55079	110.16	si			
12	128.8	79.	20	3.14	.5369	107.38	si			
13	113.1	79.	20	3.14	.52301	104.6	si			
14	97.4	79.	20	3.14	.50912	101.82	si			
15	81.7	79.	20	3.14	.49523	99.05	si			
16	66.	79.	20	3.14	.48134	96.27	si			
17	66.	52.	20	3.14	.23274	46.55	si			
18	45.	52.	20	3.14	.21416	42.83	si			
19	24.	52.	20	3.14	.19557	39.11	si			
20	3.	52.	20	3.14	.17698	35.4	si			
21	364.4	52.	20	3.14	.49685	99.37	si			
22	343.4	52.	20	3.14	.47827	95.65	si			
23	322.4	52.	20	3.14	.45968	91.94	si			
24	301.4	52.	20	3.14	.44109	88.22	si			
25	364.4	3.	20	3.14	.04569	9.14	si			
26	348.7	3.	20	3.14	.03179	6.36	si			
27	333.	3.	20	3.14	.01788	3.58	si			
28	317.3	3.	20	3.14	-.00397	-.79	si			
29	301.5	3.	20	3.14	-.00993	-1.99	si			
30	285.8	3.	20	3.14	-.02384	-4.77	si			
31	270.1	3.	20	3.14	-.03775	-7.55	si			
32	254.4	3.	20	3.14	-.05166	-10.33	si			
33	238.7	3.	20	3.14	-.06556	-13.11	si			
34	223.	3.	20	3.14	-.07947	-15.89	si			
35	207.3	3.	20	3.14	-.09338	-18.68	si			
36	191.6	3.	20	3.14	-.10729	-21.46	si			
37	175.8	3.	20	3.14	-.1212	-24.24	si			
38	160.1	3.	20	3.14	-.1351	-27.02	si			
39	144.4	3.	20	3.14	-.14901	-29.8	si			
40	128.7	3.	20	3.14	-.16292	-32.58	si			
41	113.	3.	20	3.14	-.17683	-35.37	si			
42	97.3	3.	20	3.14	-.19073	-38.15	si			
43	81.6	3.	20	3.14	-.20464	-40.93	si			
44	65.9	3.	20	3.14	-.21855	-43.71	si			
45	50.1	3.	20	3.14	-.23246	-46.49	si			
46	34.4	3.	20	3.14	-.24636	-49.27	si			
47	18.7	3.	20	3.14	-.26027	-52.05	si			
48	3.	3.	20	3.14	-.27418	-54.84	si			

% ARMAT.: tesa= .33; comp.= .24; tot.= .56

Ripristino Ponte-Tubo
VERIFICA PULVINO XZ 2

DESCRIZIONI
Tipo sezione : RETTANGOLARE
Tipo verifica: stato limite ultimo

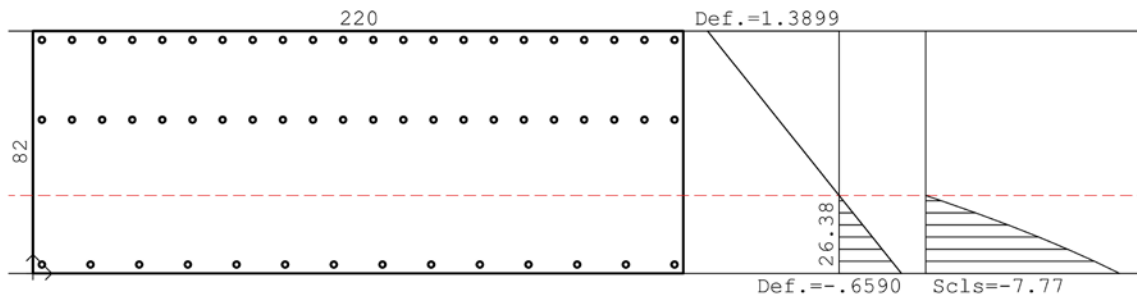
CARATTERISTICHE DEI MATERIALI
Calcestruzzo: Rck= 30.
fck= 24.9
fcd= 14.11 (.35%)
Acciaio lento: Tipo= B450C
fyk= 450.
ftk= 540.
ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
eps= muz * y +muy * z + lam
muz= 2.49869624475728E-05
muy= 0
lam=-3.72945376690354E-04

SOLLECITAZIONI AGENTI:
Nd in y= 29.6 (baricentro CLS)
Nd = -212.74
Mdz=-1750.2965
verifica in pressoflessione retta

UNITA' DI MISURA:
kN; cm; kNm; N/mm2.
Ø in mm; deformazioni*1000.

SIMBOLI:
S=sigma (tensioni sui materiali);
D=deformazioni (epsilon):



TENSIONI NEL CLS:				
ver	Z	Y	Dcls	Scls Ve
1	-2673.	70.6	1.38988	0. si
2	-2453.	70.6	1.38988	0. si
3	-2453.	-11.4	-6.5905	-7.77 si
4	-2673.	-11.4	-6.5905	-7.77 si

TENSIONI NEI FERRI:									
Fer	Z	Y	Ø (mm)	Af (cm2)	D	ferri	S	ferri	Ve
1	-2456.	40.6	20	3.14	.64028	128.06	si		
3	-2476.	40.6	20	3.14	.64028	128.06	si		
4	-2487.	40.6	20	3.14	.64028	128.06	si		
5	-2497.	40.6	20	3.14	.64028	128.06	si		
6	-2507.	40.6	20	3.14	.64028	128.06	si		
7	-2517.	40.6	20	3.14	.64028	128.06	si		
8	-2527.	40.6	20	3.14	.64028	128.06	si		
9	-2538.	40.6	20	3.14	.64028	128.06	si		
10	-2548.	40.6	20	3.14	.64028	128.06	si		
11	-2558.	40.6	20	3.14	.64028	128.06	si		
12	-2568.	40.6	20	3.14	.64028	128.06	si		
13	-2578.	40.6	20	3.14	.64028	128.06	si		
14	-2589.	40.6	20	3.14	.64028	128.06	si		
15	-2599.	40.6	20	3.14	.64028	128.06	si		
16	-2609.	40.6	20	3.14	.64028	128.06	si		
17	-2619.	40.6	20	3.14	.64028	128.06	si		
18	-2629.	40.6	20	3.14	.64028	128.06	si		
19	-2639.	40.6	20	3.14	.64028	128.06	si		
20	-2650.	40.6	20	3.14	.64028	128.06	si		
21	-2660.	40.6	20	3.14	.64028	128.06	si		
22	-2670.	40.6	20	3.14	.64028	128.06	si		
23	-2456.	67.6	20	3.14	1.31492	262.98	si		
24	-2466.	67.6	20	3.14	1.31492	262.98	si		
25	-2476.	67.6	20	3.14	1.31492	262.98	si		
26	-2487.	67.6	20	3.14	1.31492	262.98	si		
27	-2497.	67.6	20	3.14	1.31492	262.98	si		
28	-2507.	67.6	20	3.14	1.31492	262.98	si		
29	-2517.	67.6	20	3.14	1.31492	262.98	si		
30	-2527.	67.6	20	3.14	1.31492	262.98	si		
31	-2538.	67.6	20	3.14	1.31492	262.98	si		
32	-2548.	67.6	20	3.14	1.31492	262.98	si		
33	-2558.	67.6	20	3.14	1.31492	262.98	si		
34	-2568.	67.6	20	3.14	1.31492	262.98	si		
35	-2578.	67.6	20	3.14	1.31492	262.98	si		
36	-2589.	67.6	20	3.14	1.31492	262.98	si		
37	-2599.	67.6	20	3.14	1.31492	262.98	si		
38	-2609.	67.6	20	3.14	1.31492	262.98	si		
39	-2619.	67.6	20	3.14	1.31492	262.98	si		
40	-2629.	67.6	20	3.14	1.31492	262.98	si		
41	-2639.	67.6	20	3.14	1.31492	262.98	si		
42	-2650.	67.6	20	3.14	1.31492	262.98	si		
43	-2660.	67.6	20	3.14	1.31492	262.98	si		
44	-2670.	67.6	20	3.14	1.31492	262.98	si		
45	-2456.	-8.4	20	3.14	-58409	-116.82	si		
46	-2473.	-8.4	20	3.14	-58409	-116.82	si		
47	-2489.	-8.4	20	3.14	-58409	-116.82	si		
48	-2505.	-8.4	20	3.14	-58409	-116.82	si		
49	-2522.	-8.4	20	3.14	-58409	-116.82	si		
50	-2538.	-8.4	20	3.14	-58409	-116.82	si		
51	-2555.	-8.4	20	3.14	-58409	-116.82	si		
52	-2571.	-8.4	20	3.14	-58409	-116.82	si		
53	-2588.	-8.4	20	3.14	-58409	-116.82	si		
54	-2604.	-8.4	20	3.14	-58409	-116.82	si		
55	-2621.	-8.4	20	3.14	-58409	-116.82	si		
56	-2637.	-8.4	20	3.14	-58409	-116.82	si		
57	-2654.	-8.4	20	3.14	-58409	-116.82	si		
58	-2670.	-8.4	20	3.14	-58409	-116.82	si		

% ARMAT.: tesa = .77; comp. = .24; tot. = 1.01

Ripristino Ponte-Tubo
VERIFICA PULVINO YZ 2

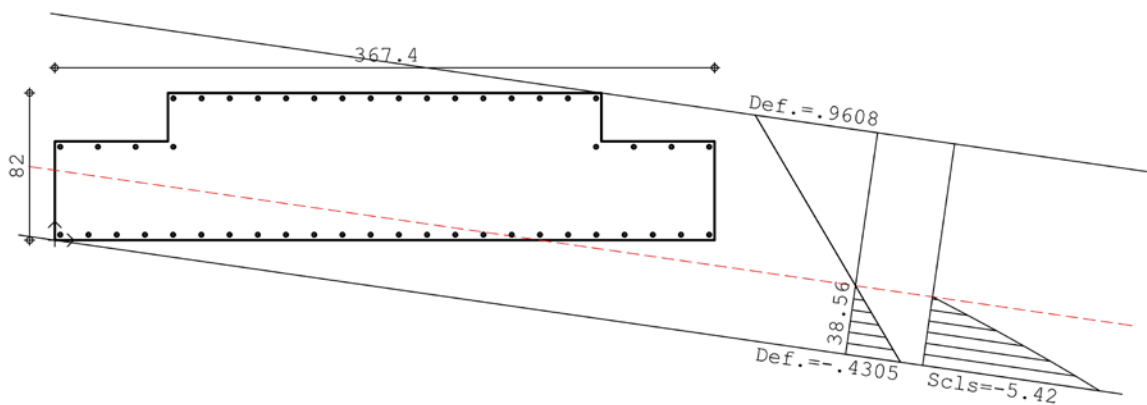
DESCRIZIONI
Tipo sezione : U Pul
Tipo verifica: sEato limite ultimo

CARATTERISTICHE DEI MATERIALI
Calcestruzzo: Rck= 30.
fck= 24.9
fcd= 14.11 (.35%)
Acciaio lento: Tipo= B450C
fyk= 450.
ftk= 540.
ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
eps= muz * y +muy * z + lam
muz= 1.10489328215218E-05
muy= 1.59425866965021E-06
lam=-4.30503694172218E-04

SOLLECITAZIONI AGENTI:
Nd in z= 183.7; y= 37.5 (baricentro CLS)
Nd = -206.69
Mdz= -671.6013
Mdy=-1714.424

UNITA' DI MISURA:
kN; cm; kNm; N/mm2.
Ø in mm; deformazioni*1000.
SIMBOLI:
S=sigma (tensioni sui materiali);
D=deformazioni (epsilon):



TENSIONI NEL CLS:					
ver	Z	Y	Dcls	Scls	Vel
1	0.	55.	.17719	0.	si
2	63.	55.	.27763	0.	si
3	63.	82.	.57595	0.	si
4	304.4	82.	.9608	0.	si
5	304.4	55.	.66248	0.	si
6	367.4	55.	.76292	0.	si
7	367.4	0.	.15523	0.	si
8	0.	0.	-.4305	-5.42	si

TENSIONI NEI FERRI:											
Fer	Z	Y	Ø (mm)	Af (cm2)	D ferri	S ferri	Vel ferri	Vel			
1	301.4	79.	20	3.14	.92287	184.57	si				
2	285.7	79.	20	3.14	.87785	179.57	si				
3	270.	79.	20	3.14	.87283	174.57	si				
4	254.3	79.	20	3.14	.84781	169.56	si				
5	238.6	79.	20	3.14	.8228	164.56	si				
6	222.9	79.	20	3.14	.79777	159.55	si				
7	207.2	79.	20	3.14	.77276	154.55	si				
8	191.5	79.	20	3.14	.74774	149.55	si				
9	175.9	79.	20	3.14	.72272	144.54	si				
10	160.2	79.	20	3.14	.6977	139.54	si				
11	144.5	79.	20	3.14	.67268	134.54	si				
12	128.8	79.	20	3.14	.64766	129.53	si				
13	113.1	79.	20	3.14	.62264	124.53	si				
14	97.4	79.	20	3.14	.59762	119.52	si				
15	81.7	79.	20	3.14	.5726	114.52	si				
16	66.	79.	20	3.14	.54758	109.52	si				
17	66.	52.	20	3.14	.24926	49.85	si				
18	45.	52.	20	3.14	.21578	43.16	si				
19	24.	52.	20	3.14	.1823	36.46	si				
20	3.	52.	20	3.14	.14882	29.76	si				
21	364.4	52.	20	3.14	.72499	145.	si				
22	343.4	52.	20	3.14	.69151	138.3	si				
23	322.4	52.	20	3.14	.65803	131.61	si				
24	301.4	52.	20	3.14	.62455	124.91	si				
25	364.4	3.	20	3.14	.18359	36.72	si				
26	348.7	3.	20	3.14	.15854	31.71	si				
27	333.	3.	20	3.14	.13349	26.7	si				
28	317.3	3.	20	3.14	.10844	21.69	si				
29	301.5	3.	20	3.14	.08339	16.68	si				
30	285.8	3.	20	3.14	.05834	11.67	si				
31	270.1	3.	20	3.14	.03329	6.66	si				
32	254.4	3.	20	3.14	.00824	1.65	si				
33	238.7	3.	20	3.14	-.01681	-3.36	si				
34	223.	3.	20	3.14	-.04186	-8.37	si				
35	207.3	3.	20	3.14	-.06691	-13.38	si				
36	191.6	3.	20	3.14	-.09197	-18.39	si				
37	175.8	3.	20	3.14	-.11702	-23.4	si				
38	160.1	3.	20	3.14	-.14207	-28.41	si				
39	144.4	3.	20	3.14	-.16712	-33.42	si				
40	128.7	3.	20	3.14	-.19217	-38.43	si				
41	113.	3.	20	3.14	-.21722	-43.44	si				
42	97.3	3.	20	3.14	-.24227	-48.45	si				
43	81.6	3.	20	3.14	-.26732	-53.46	si				
44	65.9	3.	20	3.14	-.29237	-58.47	si				
45	50.1	3.	20	3.14	-.31742	-63.48	si				
46	34.4	3.	20	3.14	-.34247	-68.49	si				
47	18.7	3.	20	3.14	-.36752	-73.5	si				
48	3.	3.	20	3.14	-.39257	-78.51	si				

% ARMAT.: tesa= .38; comp.= .19; tot.= .56

Ripristino Ponte-Tubo
VERIFICA PULVINO XZ 3

DESCRIZIONI
Tipo sezione : RETTANGOLARE
Tipo verifica: stato limite ultimo

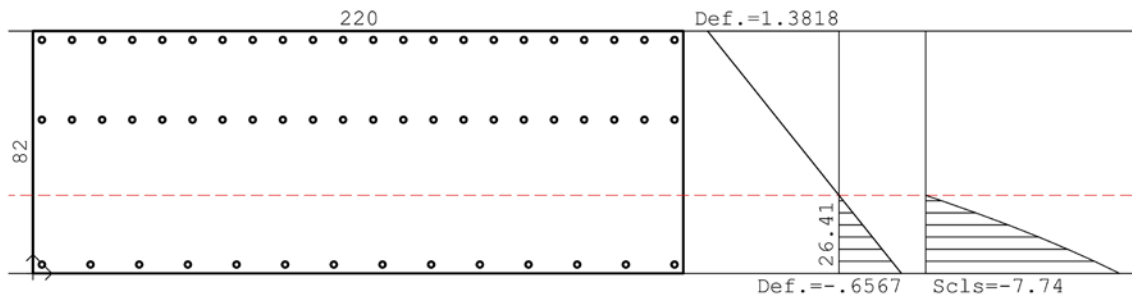
CARATTERISTICHE DEI MATERIALI
Calcestruzzo: Rck= 30.
fck= 24.9
fcd= 14.11 (.35%)
Acciaio lento: Tipo= B450C
fyk= 450.
ftk= 540.
ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
eps= muz * y +muy * z + lam
muz= 2.48596093305834E-05
muy= 0
lam=-3.72011950602552E-04

SOLLECITAZIONI AGENTI:
Nd in y= 29.6 (baricentro CLS)
Nd = -223.31
Mdz=-1743.3458
verifica in pressoflessione retta

UNITA' DI MISURA:
kN; cm; kNm; N/mm2.
Ø in mm; deformazioni*1000.

SIMBOLI:
S=sigma (tensioni sui materiali);
D=deformazioni (epsilon):



TENSIONI NEL CLS:					
ver	Z	Y	Dcls	Scls	Ve
1	-2673.	70.6	1.38183	0.	si
2	-2453.	70.6	1.38183	0.	si
3	-2453.	-11.4	-6.5665	-7.74	si
4	-2673.	-11.4	-6.5665	-7.74	si

TENSIONI NEI FERRI:											
Fer	Z	Y	Ø (mm)	Af (cm2)	D	ferri	S	ferri	Ve		
1	-2456.	40.6	20	3.14		.63605	127.21	si			
37	-2466.	40.6	20	3.14		.63605	127.21	si			
3	-2476.	40.6	20	3.14		.63605	127.21	si			
4	-2487.	40.6	20	3.14		.63605	127.21	si			
5	-2497.	40.6	20	3.14		.63605	127.21	si			
6	-2507.	40.6	20	3.14		.63605	127.21	si			
7	-2517.	40.6	20	3.14		.63605	127.21	si			
8	-2527.	40.6	20	3.14		.63605	127.21	si			
9	-2538.	40.6	20	3.14		.63605	127.21	si			
10	-2548.	40.6	20	3.14		.63605	127.21	si			
11	-2558.	40.6	20	3.14		.63605	127.21	si			
12	-2568.	40.6	20	3.14		.63605	127.21	si			
13	-2578.	40.6	20	3.14		.63605	127.21	si			
14	-2589.	40.6	20	3.14		.63605	127.21	si			
15	-2599.	40.6	20	3.14		.63605	127.21	si			
16	-2609.	40.6	20	3.14		.63605	127.21	si			
17	-2619.	40.6	20	3.14		.63605	127.21	si			
18	-2629.	40.6	20	3.14		.63605	127.21	si			
19	-2639.	40.6	20	3.14		.63605	127.21	si			
20	-2650.	40.6	20	3.14		.63605	127.21	si			
21	-2660.	40.6	20	3.14		.63605	127.21	si			
22	-2670.	40.6	20	3.14		.63605	127.21	si			
23	-2456.	67.6	20	3.14	1.30725	261.45	si				
24	-2466.	67.6	20	3.14	1.30725	261.45	si				
25	-2476.	67.6	20	3.14	1.30725	261.45	si				
26	-2487.	67.6	20	3.14	1.30725	261.45	si				
27	-2497.	67.6	20	3.14	1.30725	261.45	si				
28	-2507.	67.6	20	3.14	1.30725	261.45	si				
29	-2517.	67.6	20	3.14	1.30725	261.45	si				
30	-2527.	67.6	20	3.14	1.30725	261.45	si				
31	-2538.	67.6	20	3.14	1.30725	261.45	si				
32	-2548.	67.6	20	3.14	1.30725	261.45	si				
33	-2558.	67.6	20	3.14	1.30725	261.45	si				
34	-2568.	67.6	20	3.14	1.30725	261.45	si				
35	-2578.	67.6	20	3.14	1.30725	261.45	si				
36	-2589.	67.6	20	3.14	1.30725	261.45	si				
37	-2599.	67.6	20	3.14	1.30725	261.45	si				
38	-2609.	67.6	20	3.14	1.30725	261.45	si				
39	-2619.	67.6	20	3.14	1.30725	261.45	si				
40	-2629.	67.6	20	3.14	1.30725	261.45	si				
41	-2639.	67.6	20	3.14	1.30725	261.45	si				
42	-2650.	67.6	20	3.14	1.30725	261.45	si				
43	-2660.	67.6	20	3.14	1.30725	261.45	si				
44	-2670.	67.6	20	3.14	1.30725	261.45	si				
45	-2456.	-8.4	20	3.14	-.58208	-116.42	si				
46	-2473.	-8.4	20	3.14	-.58208	-116.42	si				
47	-2489.	-8.4	20	3.14	-.58208	-116.42	si				
48	-2505.	-8.4	20	3.14	-.58208	-116.42	si				
49	-2522.	-8.4	20	3.14	-.58208	-116.42	si				
50	-2538.	-8.4	20	3.14	-.58208	-116.42	si				
51	-2555.	-8.4	20	3.14	-.58208	-116.42	si				
52	-2571.	-8.4	20	3.14	-.58208	-116.42	si				
53	-2588.	-8.4	20	3.14	-.58208	-116.42	si				
54	-2604.	-8.4	20	3.14	-.58208	-116.42	si				
55	-2621.	-8.4	20	3.14	-.58208	-116.42	si				
56	-2637.	-8.4	20	3.14	-.58208	-116.42	si				
57	-2654.	-8.4	20	3.14	-.58208	-116.42	si				
58	-2670.	-8.4	20	3.14	-.58208	-116.42	si				

% ARMAT.: tesa = .77; comp. = .24; tot. = 1.01

Ripristino Ponte-Tubo VERIFICA PULVINO YZ 3

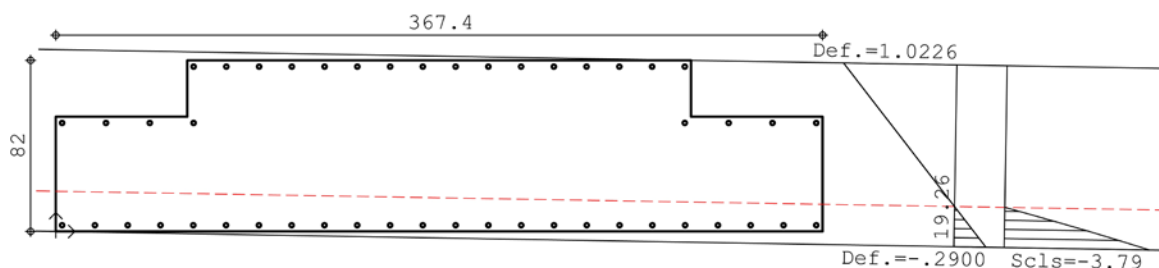
DESCRIZIONI
 Tipo sezione : U Pul
 Tipo verifica: sTato limite ultimo

CARATTERISTICHE DEI MATERIALI
 Calcestruzzo: Rck= 30.
 fck= 24.9
 fcd= 14.11 (.35%)
 Acciaio lento: Tipo= B450C
 fyk= 450.
 ftk= 540.
 ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
 eps= muz * y +muy * z + lam
 muz= 1.50574752418491E-05
 muy= 2.55749069612752E-07
 lam=-2.8997775205942E-04

SOLLECITAZIONI AGENTI:
 Nd in z= 183.7; y= 37.5 (baricentro CLS)
 Nd = -61.72
 Mdz= -852.1424
 Mdy= -314.3492

UNITA' DI MISURA:
 kN; cm; kNm; N/mm2.
 Ø in mm; deformazioni*1000.
 SIMBOLI:
 S=sigma (tensioni sui materiali);
 D=deformazioni (epsilon):



TENSIONI NEL CLS:			Dcls	Scls	Ve
ver	z	y			
1	0.	55.	.53818	0.	si
2	63.	55.	.5543	0.	si
3	63.	82.	.96085	0.	si
4	304.4	82.	1.02259	0.	si
5	304.4	55.	.61603	0.	si
6	367.4	55.	.63215	0.	si
7	367.4	0.	-.19602	-2.63	si
8	0.	0.	-.28998	-3.79	si

TENSIONI NEI FERRI:									
fer	z	y	Ø (mm)	Af (cm2)	D ferri	S ferri	Ve ferri	Ve	
1	301.4	79.	20	3.14	.97665		195.33	si	
2	285.7	79.	20	3.14	.97663		194.53	si	
3	270.	79.	20	3.14	.96862		193.72	si	
4	254.3	79.	20	3.14	.9646		192.92	si	
5	238.6	79.	20	3.14	.96059		192.12	si	
6	222.9	79.	20	3.14	.95658		191.32	si	
7	207.2	79.	20	3.14	.95256		190.51	si	
8	191.5	79.	20	3.14	.94855		189.71	si	
9	175.9	79.	20	3.14	.94454		188.91	si	
10	160.2	79.	20	3.14	.94052		188.1	si	
11	144.5	79.	20	3.14	.93651		187.3	si	
12	128.8	79.	20	3.14	.9325		186.5	si	
13	113.1	79.	20	3.14	.92848		185.7	si	
14	97.4	79.	20	3.14	.92447		184.89	si	
15	81.7	79.	20	3.14	.92046		184.09	si	
16	66.	79.	20	3.14	.91644		183.29	si	
17	66.	52.	20	3.14	.50989		101.98	si	
18	45.	52.	20	3.14	.50452		100.9	si	
19	24.	52.	20	3.14	.49915		99.83	si	
20	3.	52.	20	3.14	.49378		98.76	si	
21	364.4	52.	20	3.14	.58621		117.24	si	
22	343.4	52.	20	3.14	.58084		116.17	si	
23	322.4	52.	20	3.14	.57546		115.09	si	
24	301.4	52.	20	3.14	.57009		114.02	si	
25	364.4	3.	20	3.14	-.15161		-30.32	si	
26	348.7	3.	20	3.14	-.15563		-31.13	si	
27	333.	3.	20	3.14	-.15965		-31.93	si	
28	317.3	3.	20	3.14	-.16367		-32.73	si	
29	301.5	3.	20	3.14	-.16768		-33.54	si	
30	285.8	3.	20	3.14	-.1717		-34.34	si	
31	270.1	3.	20	3.14	-.17572		-35.14	si	
32	254.4	3.	20	3.14	-.17974		-35.95	si	
33	238.7	3.	20	3.14	-.18376		-36.75	si	
34	223.	3.	20	3.14	-.18778		-37.56	si	
35	207.3	3.	20	3.14	-.1918		-38.36	si	
36	191.6	3.	20	3.14	-.19581		-39.16	si	
37	175.8	3.	20	3.14	-.19983		-39.97	si	
38	160.1	3.	20	3.14	-.20385		-40.77	si	
39	144.4	3.	20	3.14	-.20787		-41.57	si	
40	128.7	3.	20	3.14	-.21189		-42.38	si	
41	113.	3.	20	3.14	-.21591		-43.18	si	
42	97.3	3.	20	3.14	-.21993		-43.99	si	
43	81.6	3.	20	3.14	-.22395		-44.79	si	
44	65.9	3.	20	3.14	-.22796		-45.59	si	
45	50.1	3.	20	3.14	-.23198		-46.4	si	
46	34.4	3.	20	3.14	-.236		-47.2	si	
47	18.7	3.	20	3.14	-.24002		-48.	si	
48	3.	3.	20	3.14	-.24404		-48.81	si	

% ARMAT.: tesa= .28; comp.= .28; tot.= .56

Ripristino Ponte-Tubo
VERIFICA PULVINO XZ 4

DESCRIZIONI
Tipo sezione : RETTANGOLARE
Tipo verifica: stato limite ultimo

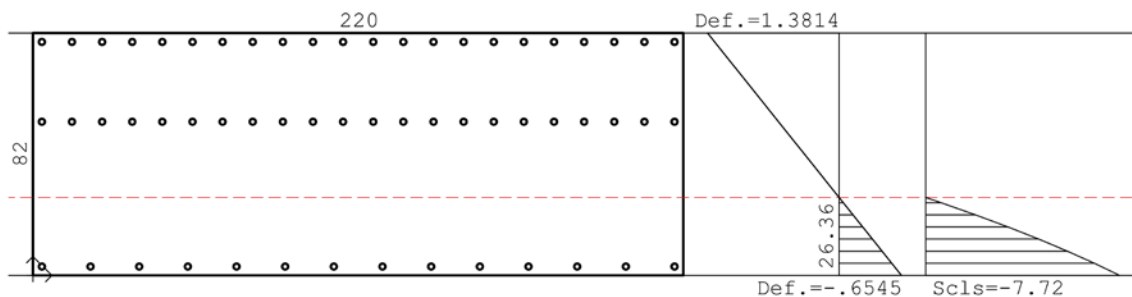
CARATTERISTICHE DEI MATERIALI
Calcestruzzo: Rck= 30.
fck= 24.9
fcd= 14.11 (.35%)
Acciaio lento: Tipo= B450C
fyk= 450.
ftk= 540.
ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
eps= muz * y +muy * z + lam
muz= 2.48284663287668E-05
muy= 0
lam=-3.70244317972872E-04

SOLLECITAZIONI AGENTI:
Nd in y= 29.6 (baricentro CLS)
Nd = -209.74
Mdz=-1739.3329
verifica in pressoflessione retta

UNITA' DI MISURA:
kN; cm; kNm; N/mm2.
Ø in mm; deformazioni*1000.

SIMBOLI:
S=sigma (tensioni sui materiali);
D=deformazioni (epsilon):



TENSIONI NEL CLS:		Z	Y	Dcls	Scls	Ve
1	-2673.	70.6	1.3814	0.	si	
2	-2453.	70.6	1.3814	0.	si	
3	-2453.	-11.4	-65453	-7.72	si	
4	-2673.	-11.4	-65453	-7.72	si	

TENSIONI NEI FERRI:		Z	Y	Ø (mm)	Af (cm2)	D	ferri	S	ferri	Ve
1	-2456.	40.6	20	3.14	.63655	127.31	si			
3	-2476.	40.6	20	3.14	.63655	127.31	si			
4	-2487.	40.6	20	3.14	.63655	127.31	si			
5	-2497.	40.6	20	3.14	.63655	127.31	si			
6	-2507.	40.6	20	3.14	.63655	127.31	si			
7	-2517.	40.6	20	3.14	.63655	127.31	si			
8	-2527.	40.6	20	3.14	.63655	127.31	si			
9	-2538.	40.6	20	3.14	.63655	127.31	si			
10	-2548.	40.6	20	3.14	.63655	127.31	si			
11	-2558.	40.6	20	3.14	.63655	127.31	si			
12	-2568.	40.6	20	3.14	.63655	127.31	si			
13	-2578.	40.6	20	3.14	.63655	127.31	si			
14	-2589.	40.6	20	3.14	.63655	127.31	si			
15	-2599.	40.6	20	3.14	.63655	127.31	si			
16	-2609.	40.6	20	3.14	.63655	127.31	si			
17	-2619.	40.6	20	3.14	.63655	127.31	si			
18	-2629.	40.6	20	3.14	.63655	127.31	si			
19	-2639.	40.6	20	3.14	.63655	127.31	si			
20	-2650.	40.6	20	3.14	.63655	127.31	si			
21	-2660.	40.6	20	3.14	.63655	127.31	si			
22	-2670.	40.6	20	3.14	.63655	127.31	si			
23	-2456.	67.6	20	3.14	1.30692	261.38	si			
24	-2466.	67.6	20	3.14	1.30692	261.38	si			
25	-2476.	67.6	20	3.14	1.30692	261.38	si			
26	-2487.	67.6	20	3.14	1.30692	261.38	si			
27	-2497.	67.6	20	3.14	1.30692	261.38	si			
28	-2507.	67.6	20	3.14	1.30692	261.38	si			
29	-2517.	67.6	20	3.14	1.30692	261.38	si			
30	-2527.	67.6	20	3.14	1.30692	261.38	si			
31	-2538.	67.6	20	3.14	1.30692	261.38	si			
32	-2548.	67.6	20	3.14	1.30692	261.38	si			
33	-2558.	67.6	20	3.14	1.30692	261.38	si			
34	-2568.	67.6	20	3.14	1.30692	261.38	si			
35	-2578.	67.6	20	3.14	1.30692	261.38	si			
36	-2589.	67.6	20	3.14	1.30692	261.38	si			
37	-2599.	67.6	20	3.14	1.30692	261.38	si			
38	-2609.	67.6	20	3.14	1.30692	261.38	si			
39	-2619.	67.6	20	3.14	1.30692	261.38	si			
40	-2629.	67.6	20	3.14	1.30692	261.38	si			
41	-2639.	67.6	20	3.14	1.30692	261.38	si			
42	-2650.	67.6	20	3.14	1.30692	261.38	si			
43	-2660.	67.6	20	3.14	1.30692	261.38	si			
44	-2670.	67.6	20	3.14	1.30692	261.38	si			
45	-2456.	-8.4	20	3.14	-58004	-116.01	si			
46	-2473.	-8.4	20	3.14	-58004	-116.01	si			
47	-2489.	-8.4	20	3.14	-58004	-116.01	si			
48	-2505.	-8.4	20	3.14	-58004	-116.01	si			
49	-2522.	-8.4	20	3.14	-58004	-116.01	si			
50	-2538.	-8.4	20	3.14	-58004	-116.01	si			
51	-2555.	-8.4	20	3.14	-58004	-116.01	si			
52	-2571.	-8.4	20	3.14	-58004	-116.01	si			
53	-2588.	-8.4	20	3.14	-58004	-116.01	si			
54	-2604.	-8.4	20	3.14	-58004	-116.01	si			
55	-2621.	-8.4	20	3.14	-58004	-116.01	si			
56	-2637.	-8.4	20	3.14	-58004	-116.01	si			
57	-2654.	-8.4	20	3.14	-58004	-116.01	si			
58	-2670.	-8.4	20	3.14	-58004	-116.01	si			

% ARMAT.: tesa = .77; comp. = .24; tot. = 1.01

Ripristino Ponte-Tubo

VERIFICA PULVINO YZ 4

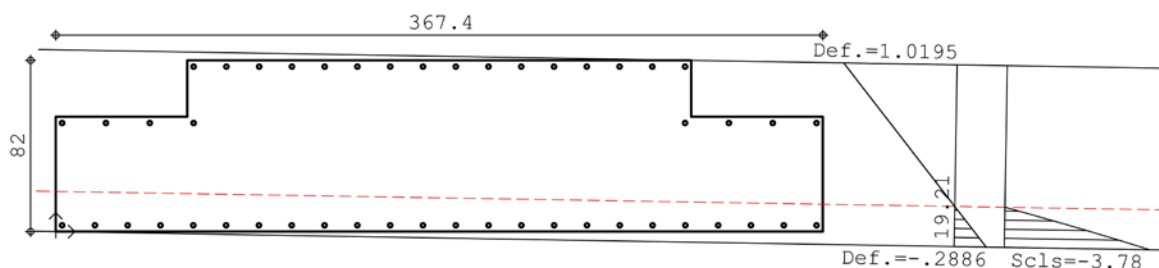
DESCRIZIONI
 Tipo sezione : U Pul
 Tipo verifica: sTato limite ultimo

CARATTERISTICHE DEI MATERIALI
 Calcestruzzo: Rck= 30.
 fck= 24.9
 fcd= 14.11 (.35%)
 Acciaio lento: Tipo= B450C
 fyk= 450.
 ftk= 540.
 ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
 eps= muz * y +muy * z + lam
 muz= 1.50229819347792E-05
 muy= 2.50426726509754E-07
 lam=-2.88603646591644E-04

SOLLECITAZIONI AGENTI:
 Nd in z= 183.7; y= 37.5 (baricentro CLS)
 Nd = -63.01
 Mdz= -850.512
 Mdy= -307.9812

UNITA' DI MISURA:
 kN; cm; kNm; N/mm2.
 Ø in mm; deformazioni*1000.
 SIMBOLI:
 S=sigma (tensioni sui materiali);
 D=deformazioni (epsilon):



TENSIONI NEL CLS:			Dcls	Scls	Vel
ver	z	y			
1	0.	55.	.53766	0.	si
2	63.	55.	.55344	0.	si
3	63.	82.	.95906	0.	si
4	304.4	82.	1.01951	0.	si
5	304.4	55.	.61389	0.	si
6	367.4	55.	.62967	0.	si
7	367.4	0.	-.1966	-2.64	si
8	0.	0.	-.2886	-3.78	si

TENSIONI NEI FERRI:									
Fer	z	y	Ø (mm)	Af (cm2)	D ferri	S ferri	Vel		
1	301.4	79.	20	3.14	.97369	194.74	si		
2	285.7	79.	20	3.14	.96976	193.95	si		
3	270.	79.	20	3.14	.96583	193.17	si		
4	254.3	79.	20	3.14	.9619	192.38	si		
5	238.6	79.	20	3.14	.95797	191.59	si		
6	222.9	79.	20	3.14	.95404	190.81	si		
7	207.2	79.	20	3.14	.95011	190.02	si		
8	191.5	79.	20	3.14	.94618	189.24	si		
9	175.9	79.	20	3.14	.94225	188.45	si		
10	160.2	79.	20	3.14	.93832	187.66	si		
11	144.5	79.	20	3.14	.93439	186.88	si		
12	128.8	79.	20	3.14	.93046	186.09	si		
13	113.1	79.	20	3.14	.92653	185.31	si		
14	97.4	79.	20	3.14	.9226	184.52	si		
15	81.7	79.	20	3.14	.91867	183.73	si		
16	66.	79.	20	3.14	.91474	182.95	si		
17	66.	52.	20	3.14	.50912	101.82	si		
18	45.	52.	20	3.14	.50386	100.77	si		
19	24.	52.	20	3.14	.4986	99.72	si		
20	3.	52.	20	3.14	.49334	98.67	si		
21	364.4	52.	20	3.14	.58385	116.77	si		
22	343.4	52.	20	3.14	.57859	115.72	si		
23	322.4	52.	20	3.14	.57333	114.67	si		
24	301.4	52.	20	3.14	.56807	113.61	si		
25	364.4	3.	20	3.14	-.15228	-30.46	si		
26	348.7	3.	20	3.14	-.15621	-31.24	si		
27	333.	3.	20	3.14	-.16015	-32.03	si		
28	317.3	3.	20	3.14	-.16408	-32.82	si		
29	301.5	3.	20	3.14	-.16802	-33.6	si		
30	285.8	3.	20	3.14	-.17195	-34.39	si		
31	270.1	3.	20	3.14	-.17589	-35.18	si		
32	254.4	3.	20	3.14	-.17982	-35.96	si		
33	238.7	3.	20	3.14	-.18376	-36.75	si		
34	223.	3.	20	3.14	-.18769	-37.54	si		
35	207.3	3.	20	3.14	-.19163	-38.33	si		
36	191.6	3.	20	3.14	-.19556	-39.11	si		
37	175.8	3.	20	3.14	-.1995	-39.9	si		
38	160.1	3.	20	3.14	-.20343	-40.69	si		
39	144.4	3.	20	3.14	-.20737	-41.47	si		
40	128.7	3.	20	3.14	-.2113	-42.26	si		
41	113.	3.	20	3.14	-.21524	-43.05	si		
42	97.3	3.	20	3.14	-.21917	-43.83	si		
43	81.6	3.	20	3.14	-.22311	-44.62	si		
44	65.9	3.	20	3.14	-.22704	-45.41	si		
45	50.1	3.	20	3.14	-.23098	-46.2	si		
46	34.4	3.	20	3.14	-.23491	-46.98	si		
47	18.7	3.	20	3.14	-.23885	-47.77	si		
48	3.	3.	20	3.14	-.24278	-48.56	si		

% ARMAT.: tesa= .28; comp.= .28; tot.= .56

Ripristino Ponte-Tubo
VERIFICA PULVINO XZ 5

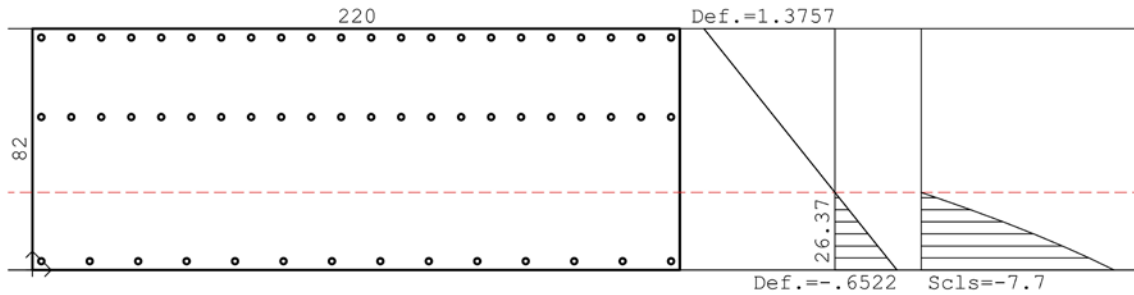
DESCRIZIONI
Tipo sezione : RETTANGOLARE
Tipo verifica: stato limite ultimo

CARATTERISTICHE DEI MATERIALI
Calcestruzzo: Rck= 30.
fck= 24.9
fcd= 14.11 (.35%)
Acciaio lento: Tipo= B450C
fyk= 450.
ftk= 540.
ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
eps= muz * y +muy * z + lam
muz= 2.47302103532955E-05
muy= 0
lam=-3.68989550074321E-04

SOLLECITAZIONI AGENTI:
Nd in y= 29.6 (baricentro CLS)
Nd = -212.27
Mdz=-1733.1624
verifica in pressoflessione retta

UNITA' DI MISURA:
kN; cm; kNm; N/mm2.
Ø in mm; deformazioni*1000.
SIMBOLI:
S=sigma (tensioni sui materiali);
D=deformazioni (epsilon):



TENSIONI NEL CLS:

ver	Z	Y	Dcls	Scls	Ve
1	-2673.	70.6	1.37573	0.	si
2	-2453.	70.6	1.37573	0.	si
3	-2453.	-11.4	-.65215	-7.7	si
4	-2673.	-11.4	-.65215	-7.7	si

TENSIONI NEI FERRI:

Fer	Z	Y	Ø (mm)	Af (cm2)	D ferri	S ferri	Ve
1	-2456.	40.6	20	3.14	.63382	126.76	si
2	-2466.	40.6	20	3.14	.63382	126.76	si
3	-2476.	40.6	20	3.14	.63382	126.76	si
4	-2487.	40.6	20	3.14	.63382	126.76	si
5	-2497.	40.6	20	3.14	.63382	126.76	si
6	-2507.	40.6	20	3.14	.63382	126.76	si
7	-2517.	40.6	20	3.14	.63382	126.76	si
8	-2527.	40.6	20	3.14	.63382	126.76	si
9	-2538.	40.6	20	3.14	.63382	126.76	si
10	-2548.	40.6	20	3.14	.63382	126.76	si
11	-2558.	40.6	20	3.14	.63382	126.76	si
12	-2568.	40.6	20	3.14	.63382	126.76	si
13	-2578.	40.6	20	3.14	.63382	126.76	si
14	-2589.	40.6	20	3.14	.63382	126.76	si
15	-2599.	40.6	20	3.14	.63382	126.76	si
16	-2609.	40.6	20	3.14	.63382	126.76	si
17	-2619.	40.6	20	3.14	.63382	126.76	si
18	-2629.	40.6	20	3.14	.63382	126.76	si
19	-2639.	40.6	20	3.14	.63382	126.76	si
20	-2650.	40.6	20	3.14	.63382	126.76	si
21	-2660.	40.6	20	3.14	.63382	126.76	si
22	-2670.	40.6	20	3.14	.63382	126.76	si
23	-2456.	67.6	20	3.14	1.30154	260.31	si
24	-2466.	67.6	20	3.14	1.30154	260.31	si
25	-2476.	67.6	20	3.14	1.30154	260.31	si
26	-2487.	67.6	20	3.14	1.30154	260.31	si
27	-2497.	67.6	20	3.14	1.30154	260.31	si
28	-2507.	67.6	20	3.14	1.30154	260.31	si
29	-2517.	67.6	20	3.14	1.30154	260.31	si
30	-2527.	67.6	20	3.14	1.30154	260.31	si
31	-2538.	67.6	20	3.14	1.30154	260.31	si
32	-2548.	67.6	20	3.14	1.30154	260.31	si
33	-2558.	67.6	20	3.14	1.30154	260.31	si
34	-2568.	67.6	20	3.14	1.30154	260.31	si
35	-2578.	67.6	20	3.14	1.30154	260.31	si
36	-2589.	67.6	20	3.14	1.30154	260.31	si
37	-2599.	67.6	20	3.14	1.30154	260.31	si
38	-2609.	67.6	20	3.14	1.30154	260.31	si
39	-2619.	67.6	20	3.14	1.30154	260.31	si
40	-2629.	67.6	20	3.14	1.30154	260.31	si
41	-2639.	67.6	20	3.14	1.30154	260.31	si
42	-2650.	67.6	20	3.14	1.30154	260.31	si
43	-2660.	67.6	20	3.14	1.30154	260.31	si
44	-2670.	67.6	20	3.14	1.30154	260.31	si
45	-2456.	-8.4	20	3.14	-.57796	-115.59	si
46	-2473.	-8.4	20	3.14	-.57796	-115.59	si
47	-2489.	-8.4	20	3.14	-.57796	-115.59	si
48	-2505.	-8.4	20	3.14	-.57796	-115.59	si
49	-2522.	-8.4	20	3.14	-.57796	-115.59	si
50	-2538.	-8.4	20	3.14	-.57796	-115.59	si
51	-2555.	-8.4	20	3.14	-.57796	-115.59	si
52	-2571.	-8.4	20	3.14	-.57796	-115.59	si
53	-2588.	-8.4	20	3.14	-.57796	-115.59	si
54	-2604.	-8.4	20	3.14	-.57796	-115.59	si
55	-2621.	-8.4	20	3.14	-.57796	-115.59	si
56	-2637.	-8.4	20	3.14	-.57796	-115.59	si
57	-2654.	-8.4	20	3.14	-.57796	-115.59	si
58	-2670.	-8.4	20	3.14	-.57796	-115.59	si

% ARMAT.: tesa= .77; comp.= .24; tot.= 1.01

Ripristino Ponte-Tubo
VERIFICA PULVINO YZ 5

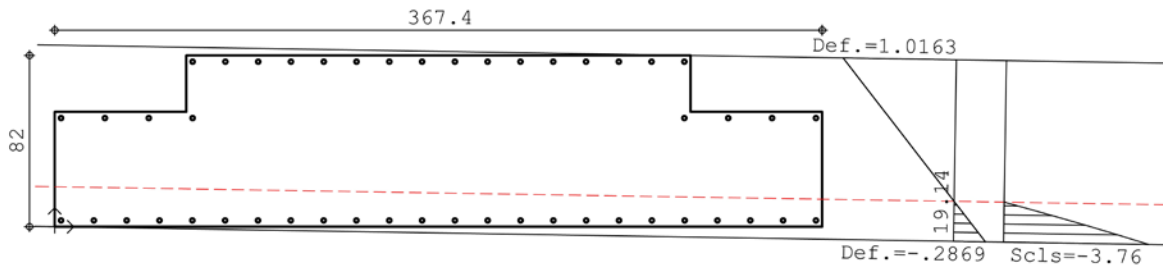
DESCRIZIONI
Tipo sezione : U Pul
Tipo verifica: sTato limite ultimo

CARATTERISTICHE DEI MATERIALI
Calcestruzzo: Rck= 30.
fck= 24.9
fcd= 14.11 (.35%)
Acciaio lento: Tipo= B450C
fyk= 450.
ftk= 540.
ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
eps= muz * y +muy * z + lam
muz= 1.49883410310696E-05
muy= 2.43664606512964E-07
lam=-2.86932530780621E-04

SOLLECITAZIONI AGENTI:
Nd in z= 183.7; y= 37.5 (baricentro CLS)
Nd = -63.86
Mdz = -848.7808
Mdy = -299.8109

UNITA' DI MISURA:
kN; cm; kNm; N/mm2.
Ø in mm; deformazioni*1000.
SIMBOLI:
S=sigma (tensioni sui materiali);
D=deformazioni (epsilon):



TENSIONI NEL CLS:		Dcls	Scls	Vel
ver	z			
1	0.	.53743	0.	si
2	63.	.55278	0.	si
3	63.	.95746	0.	si
4	304.4	1.01628	0.	si
5	304.4	.6116	0.	si
6	367.4	.62695	0.	si
7	367.4	-.19741	-2.65	si
8	0.	-.28693	-3.76	si

TENSIONI NEI FERRI:		Ø (mm)	Af (cm2)	D ferri	S ferri	Vel
fer	z					
1	301.4	79.	20	3.14	.97059	194.12
2	285.7	79.	20	3.14	.96676	193.35
3	270.	79.	20	3.14	.96294	192.59
4	254.3	79.	20	3.14	.95912	191.82
5	238.6	79.	20	3.14	.95529	191.06
6	222.9	79.	20	3.14	.95147	190.29
7	207.2	79.	20	3.14	.94764	189.53
8	191.5	79.	20	3.14	.94382	188.76
9	175.9	79.	20	3.14	.94	188.
10	160.2	79.	20	3.14	.93617	187.23
11	144.5	79.	20	3.14	.93235	186.47
12	128.8	79.	20	3.14	.92852	185.7
13	113.1	79.	20	3.14	.9247	184.94
14	97.4	79.	20	3.14	.92088	184.18
15	81.7	79.	20	3.14	.91705	183.41
16	66.	79.	20	3.14	.91323	182.65
17	66.	52.	20	3.14	.50854	101.71
18	45.	52.	20	3.14	.50343	100.69
19	24.	52.	20	3.14	.49831	99.66
20	3.	52.	20	3.14	.49319	98.64
21	364.4	52.	20	3.14	.58125	116.25
22	343.4	52.	20	3.14	.57614	115.23
23	322.4	52.	20	3.14	.57102	114.2
24	301.4	52.	20	3.14	.5659	113.18
25	364.4	3.	20	3.14	-.15318	-30.64
26	348.7	3.	20	3.14	-.157	-31.4
27	333.	3.	20	3.14	-.16083	-32.17
28	317.3	3.	20	3.14	-.16466	-32.93
29	301.5	3.	20	3.14	-.16849	-33.7
30	285.8	3.	20	3.14	-.17232	-34.46
31	270.1	3.	20	3.14	-.17615	-35.23
32	254.4	3.	20	3.14	-.17998	-36.
33	238.7	3.	20	3.14	-.18381	-36.76
34	223.	3.	20	3.14	-.18763	-37.53
35	207.3	3.	20	3.14	-.19146	-38.29
36	191.6	3.	20	3.14	-.19529	-39.06
37	175.8	3.	20	3.14	-.19912	-39.82
38	160.1	3.	20	3.14	-.20295	-40.59
39	144.4	3.	20	3.14	-.20678	-41.36
40	128.7	3.	20	3.14	-.21061	-42.12
41	113.	3.	20	3.14	-.21444	-42.89
42	97.3	3.	20	3.14	-.21826	-43.65
43	81.6	3.	20	3.14	-.22209	-44.42
44	65.9	3.	20	3.14	-.22592	-45.18
45	50.1	3.	20	3.14	-.22975	-45.95
46	34.4	3.	20	3.14	-.23358	-46.72
47	18.7	3.	20	3.14	-.23741	-47.48
48	3.	3.	20	3.14	-.24124	-48.25

% ARMAT.: tesa= .28; comp.= .28; tot.= .56

Ripristino Ponte-Tubo

VERIFICA PULVINO XZ 6

DESCRIZIONI
 Tipo sezione : RETTANGOLARE
 Tipo verifica: stato limite ultimo

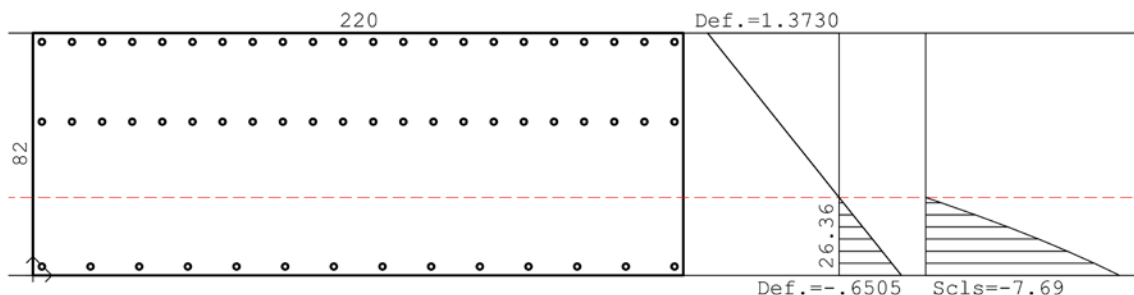
CARATTERISTICHE DEI MATERIALI
 Calcestruzzo: Rck= 30.
 fck= 24.9
 fcd= 14.11 (.35%)
 Acciaio lento: Tipo= B450C
 fyk= 450.
 ftk= 540.
 ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
 eps= muz * y +muy * z + lam
 muz= 2.46772155674196E-05
 muy= 0
 lam=-3.6793824610741E-04

SOLLECITAZIONI AGENTI:
 Nd in y= 29.6 (baricentro CLS)
 Nd = -209.7
 Mdz=-1729.2697
 verifica in pressoflessione retta

UNITA' DI MISURA:
 kN; cm; kNm; N/mm2.
 Ø in mm; deformazioni*1000.

SIMBOLI:
 S=sigma (tensioni sui materiali);
 D=deformazioni (epsilon):



TENSIONI NEL CLS:				
ver	Z	Y	Dcls	Scls Ve
1	-2673.	70.6	1.37304	0. si
2	-2453.	70.6	1.37304	0. si
3	-2453.	-11.4	-65049	-7.69 si
4	-2673.	-11.4	-65049	-7.69 si

TENSIONI NEI FERRI:										
Fer	Z	Y	Ø (mm)	Af (cm2)	D	ferri	S	ferri	Ve	
1	-2456.	40.6	20	3.14		.63272		126.54	si	
3	-2476.	40.6	20	3.14		.63272		126.54	si	
4	-2487.	40.6	20	3.14		.63272		126.54	si	
5	-2497.	40.6	20	3.14		.63272		126.54	si	
6	-2507.	40.6	20	3.14		.63272		126.54	si	
7	-2517.	40.6	20	3.14		.63272		126.54	si	
8	-2527.	40.6	20	3.14		.63272		126.54	si	
9	-2538.	40.6	20	3.14		.63272		126.54	si	
10	-2548.	40.6	20	3.14		.63272		126.54	si	
11	-2558.	40.6	20	3.14		.63272		126.54	si	
12	-2568.	40.6	20	3.14		.63272		126.54	si	
13	-2578.	40.6	20	3.14		.63272		126.54	si	
14	-2589.	40.6	20	3.14		.63272		126.54	si	
15	-2599.	40.6	20	3.14		.63272		126.54	si	
16	-2609.	40.6	20	3.14		.63272		126.54	si	
17	-2619.	40.6	20	3.14		.63272		126.54	si	
18	-2629.	40.6	20	3.14		.63272		126.54	si	
19	-2639.	40.6	20	3.14		.63272		126.54	si	
20	-2650.	40.6	20	3.14		.63272		126.54	si	
21	-2660.	40.6	20	3.14		.63272		126.54	si	
22	-2670.	40.6	20	3.14		.63272		126.54	si	
23	-2456.	67.6	20	3.14	1.29901		259.8	si		
24	-2466.	67.6	20	3.14	1.29901		259.8	si		
25	-2476.	67.6	20	3.14	1.29901		259.8	si		
26	-2487.	67.6	20	3.14	1.29901		259.8	si		
27	-2497.	67.6	20	3.14	1.29901		259.8	si		
28	-2507.	67.6	20	3.14	1.29901		259.8	si		
29	-2517.	67.6	20	3.14	1.29901		259.8	si		
30	-2527.	67.6	20	3.14	1.29901		259.8	si		
31	-2538.	67.6	20	3.14	1.29901		259.8	si		
32	-2548.	67.6	20	3.14	1.29901		259.8	si		
33	-2558.	67.6	20	3.14	1.29901		259.8	si		
34	-2568.	67.6	20	3.14	1.29901		259.8	si		
35	-2578.	67.6	20	3.14	1.29901		259.8	si		
36	-2589.	67.6	20	3.14	1.29901		259.8	si		
37	-2599.	67.6	20	3.14	1.29901		259.8	si		
38	-2609.	67.6	20	3.14	1.29901		259.8	si		
39	-2619.	67.6	20	3.14	1.29901		259.8	si		
40	-2629.	67.6	20	3.14	1.29901		259.8	si		
41	-2639.	67.6	20	3.14	1.29901		259.8	si		
42	-2650.	67.6	20	3.14	1.29901		259.8	si		
43	-2660.	67.6	20	3.14	1.29901		259.8	si		
44	-2670.	67.6	20	3.14	1.29901		259.8	si		
45	-2456.	-8.4	20	3.14		-.57646		-115.29	si	
46	-2473.	-8.4	20	3.14		-.57646		-115.29	si	
47	-2489.	-8.4	20	3.14		-.57646		-115.29	si	
48	-2505.	-8.4	20	3.14		-.57646		-115.29	si	
49	-2522.	-8.4	20	3.14		-.57646		-115.29	si	
50	-2538.	-8.4	20	3.14		-.57646		-115.29	si	
51	-2555.	-8.4	20	3.14		-.57646		-115.29	si	
52	-2571.	-8.4	20	3.14		-.57646		-115.29	si	
53	-2588.	-8.4	20	3.14		-.57646		-115.29	si	
54	-2604.	-8.4	20	3.14		-.57646		-115.29	si	
55	-2621.	-8.4	20	3.14		-.57646		-115.29	si	
56	-2637.	-8.4	20	3.14		-.57646		-115.29	si	
57	-2654.	-8.4	20	3.14		-.57646		-115.29	si	
58	-2670.	-8.4	20	3.14		-.57646		-115.29	si	

% ARMAT.: tesa = .77; comp. = .24; tot. = 1.01

Ripristino Ponte-Tubo

VERIFICA PULVINO YZ 6

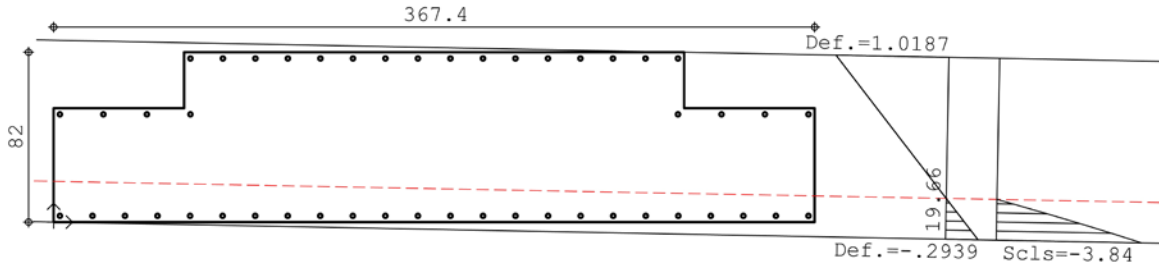
DESCRIZIONI
 Tipo sezione : U Pul
 Tipo verifica: stato limite ultimo

CARATTERISTICHE DEI MATERIALI
 Calcestruzzo: Rck= 30.
 fck= 24.9
 fcd= 14.11 (.35%)
 Acciaio lento: Tipo= B450C
 fyk= 450.
 ftk= 540.
 ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
 eps= muz * y +muy * z + lam
 muz= 1.49460831511411E-05
 muy= 2.85848261164421E-07
 lam=-2.93861200713876E-04

SOLLECITAZIONI AGENTI:
 Nd in z= 183.7; y= 37.5 (baricentro CLS)
 Nd = -66.19
 Mdz= -846.8952
 Mdy= -351.5833

UNITA' DI MISURA:
 kN; cm; kNm; N/mm2.
 Ø in mm; deformazioni*1000.
 SIMBOLI:
 S=sigma (tensioni sui materiali);
 D=deformazioni (epsilon):



TENSIONI NEL CLS:					
ver	Z	Y	Dcls	Scls	Ve
1	0.	55.	.52817	0.	si
2	63.	55.	.54618	0.	si
3	63.	82.	.94973	0.	si
4	304.4	82.	1.01873	0.	si
5	304.4	55.	.61519	0.	si
6	367.4	55.	.63319	0.	si
7	367.4	0.	-.18884	-2.54	si
8	0.	0.	-.29386	-3.84	si

TENSIONI NEI FERRI:									
fer	Z	Y	Ø (mm)	Af (cm2)	D	ferri	S ferri	Ve	
1	301.4	79.	20	3.14	.97303	194.61	si		
2	285.7	79.	20	3.14	.96855	193.71	si		
3	270.	79.	20	3.14	.96406	192.81	si		
4	254.3	79.	20	3.14	.95958	191.92	si		
5	238.6	79.	20	3.14	.95509	191.02	si		
6	222.9	79.	20	3.14	.9506	190.12	si		
7	207.2	79.	20	3.14	.94612	189.22	si		
8	191.5	79.	20	3.14	.94163	188.33	si		
9	175.9	79.	20	3.14	.93715	187.43	si		
10	160.2	79.	20	3.14	.93266	186.53	si		
11	144.5	79.	20	3.14	.92818	185.64	si		
12	128.8	79.	20	3.14	.92369	184.74	si		
13	113.1	79.	20	3.14	.9192	183.84	si		
14	97.4	79.	20	3.14	.91472	182.94	si		
15	81.7	79.	20	3.14	.91023	182.05	si		
16	66.	79.	20	3.14	.90575	181.15	si		
17	66.	52.	20	3.14	.5022	100.44	si		
18	45.	52.	20	3.14	.4962	99.24	si		
19	24.	52.	20	3.14	.4902	98.04	si		
20	3.	52.	20	3.14	.48419	96.84	si		
21	364.4	52.	20	3.14	.5875	117.5	si		
22	343.4	52.	20	3.14	.5815	116.3	si		
23	322.4	52.	20	3.14	.57549	115.1	si		
24	301.4	52.	20	3.14	.56949	113.9	si		
25	364.4	3.	20	3.14	-.14486	-28.97	si		
26	348.7	3.	20	3.14	-.14935	-29.87	si		
27	333.	3.	20	3.14	-.15384	-30.77	si		
28	317.3	3.	20	3.14	-.15833	-31.67	si		
29	301.5	3.	20	3.14	-.16283	-32.57	si		
30	285.8	3.	20	3.14	-.16732	-33.46	si		
31	270.1	3.	20	3.14	-.17181	-34.36	si		
32	254.4	3.	20	3.14	-.1763	-35.26	si		
33	238.7	3.	20	3.14	-.18079	-36.16	si		
34	223.	3.	20	3.14	-.18528	-37.06	si		
35	207.3	3.	20	3.14	-.18978	-37.96	si		
36	191.6	3.	20	3.14	-.19427	-38.85	si		
37	175.8	3.	20	3.14	-.19876	-39.75	si		
38	160.1	3.	20	3.14	-.20325	-40.65	si		
39	144.4	3.	20	3.14	-.20774	-41.55	si		
40	128.7	3.	20	3.14	-.21223	-42.45	si		
41	113.	3.	20	3.14	-.21672	-43.34	si		
42	97.3	3.	20	3.14	-.22122	-44.24	si		
43	81.6	3.	20	3.14	-.22571	-45.14	si		
44	65.9	3.	20	3.14	-.2302	-46.04	si		
45	50.1	3.	20	3.14	-.23469	-46.94	si		
46	34.4	3.	20	3.14	-.23918	-47.84	si		
47	18.7	3.	20	3.14	-.24367	-48.73	si		
48	3.	3.	20	3.14	-.24817	-49.63	si		

% ARMAT.: tesa= .28; comp.= .28; tot.= .56

Ripristino Ponte-Tubo VERIFICA PULVINO XZ 7

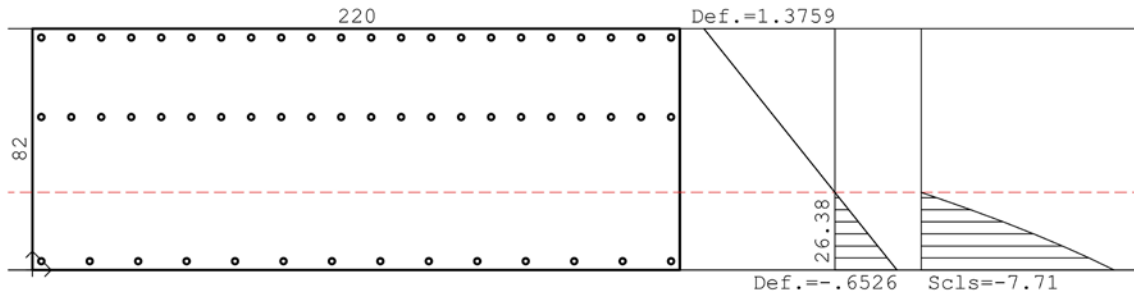
DESCRIZIONI
 Tipo sezione : RETTANGOLARE
 Tipo verifica: stato limite ultimo

CARATTERISTICHE DEI MATERIALI
 Calcestruzzo: Rck= 30.
 fck= 24.9
 fcd= 14.11 (.35%)
 Acciaio lento: Tipo= B450C
 fyk= 450.
 ftk= 540.
 ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
 eps= muz * y + muy * z + lam
 muz= 2.47379223042976E-05
 muy= 0
 lam=-3.69327014237058E-04

SOLLECITAZIONI AGENTI:
 Nd in y= 29.6 (baricentro CLS)
 Nd = -214.58
 Mdz=-1734.0062
 verifica in pressoflessione retta

UNITA' DI MISURA:
 kN; cm; kNm; N/mm2.
 Ø in mm; deformazioni*1000.
 SIMBOLI:
 S=sigma (tensioni sui materiali);
 D=deformazioni (epsilon):



TENSIONI NEL CLS:					
ver	Z	Y	Dcls	Scls	Ve
1	-2673.	70.6	1.37593	0.	si
2	-2453.	70.6	1.37593	0.	si
3	-2453.	-11.4	-.65258	-7.71	si
4	-2673.	-11.4	-.65258	-7.71	si

TENSIONI NEI FERRI:							
Fer	Z	Y	Ø (mm)	Af (cm2)	D ferri	S ferri	Ve
1	-2456.	40.6	20	3.14	.6338	126.76	si
2	-2466.	40.6	20	3.14	.6338	126.76	si
3	-2476.	40.6	20	3.14	.6338	126.76	si
4	-2487.	40.6	20	3.14	.6338	126.76	si
5	-2497.	40.6	20	3.14	.6338	126.76	si
6	-2507.	40.6	20	3.14	.6338	126.76	si
7	-2517.	40.6	20	3.14	.6338	126.76	si
8	-2527.	40.6	20	3.14	.6338	126.76	si
9	-2538.	40.6	20	3.14	.6338	126.76	si
10	-2548.	40.6	20	3.14	.6338	126.76	si
11	-2558.	40.6	20	3.14	.6338	126.76	si
12	-2568.	40.6	20	3.14	.6338	126.76	si
13	-2578.	40.6	20	3.14	.6338	126.76	si
14	-2589.	40.6	20	3.14	.6338	126.76	si
15	-2599.	40.6	20	3.14	.6338	126.76	si
16	-2609.	40.6	20	3.14	.6338	126.76	si
17	-2619.	40.6	20	3.14	.6338	126.76	si
18	-2629.	40.6	20	3.14	.6338	126.76	si
19	-2639.	40.6	20	3.14	.6338	126.76	si
20	-2650.	40.6	20	3.14	.6338	126.76	si
21	-2660.	40.6	20	3.14	.6338	126.76	si
22	-2670.	40.6	20	3.14	.6338	126.76	si
23	-2456.	67.6	20	3.14	1.30172	260.34	si
24	-2466.	67.6	20	3.14	1.30172	260.34	si
25	-2476.	67.6	20	3.14	1.30172	260.34	si
26	-2487.	67.6	20	3.14	1.30172	260.34	si
27	-2497.	67.6	20	3.14	1.30172	260.34	si
28	-2507.	67.6	20	3.14	1.30172	260.34	si
29	-2517.	67.6	20	3.14	1.30172	260.34	si
30	-2527.	67.6	20	3.14	1.30172	260.34	si
31	-2538.	67.6	20	3.14	1.30172	260.34	si
32	-2548.	67.6	20	3.14	1.30172	260.34	si
33	-2558.	67.6	20	3.14	1.30172	260.34	si
34	-2568.	67.6	20	3.14	1.30172	260.34	si
35	-2578.	67.6	20	3.14	1.30172	260.34	si
36	-2589.	67.6	20	3.14	1.30172	260.34	si
37	-2599.	67.6	20	3.14	1.30172	260.34	si
38	-2609.	67.6	20	3.14	1.30172	260.34	si
39	-2619.	67.6	20	3.14	1.30172	260.34	si
40	-2629.	67.6	20	3.14	1.30172	260.34	si
41	-2639.	67.6	20	3.14	1.30172	260.34	si
42	-2650.	67.6	20	3.14	1.30172	260.34	si
43	-2660.	67.6	20	3.14	1.30172	260.34	si
44	-2670.	67.6	20	3.14	1.30172	260.34	si
45	-2456.	-8.4	20	3.14	-.57836	-115.67	si
46	-2473.	-8.4	20	3.14	-.57836	-115.67	si
47	-2489.	-8.4	20	3.14	-.57836	-115.67	si
48	-2505.	-8.4	20	3.14	-.57836	-115.67	si
49	-2522.	-8.4	20	3.14	-.57836	-115.67	si
50	-2538.	-8.4	20	3.14	-.57836	-115.67	si
51	-2555.	-8.4	20	3.14	-.57836	-115.67	si
52	-2571.	-8.4	20	3.14	-.57836	-115.67	si
53	-2588.	-8.4	20	3.14	-.57836	-115.67	si
54	-2604.	-8.4	20	3.14	-.57836	-115.67	si
55	-2621.	-8.4	20	3.14	-.57836	-115.67	si
56	-2637.	-8.4	20	3.14	-.57836	-115.67	si
57	-2654.	-8.4	20	3.14	-.57836	-115.67	si
58	-2670.	-8.4	20	3.14	-.57836	-115.67	si

% ARMAT.: tesa = .77; comp. = .24; tot. = 1.01

Ripristino Ponte-Tubo

VERIFICA PULVINO YZ 7

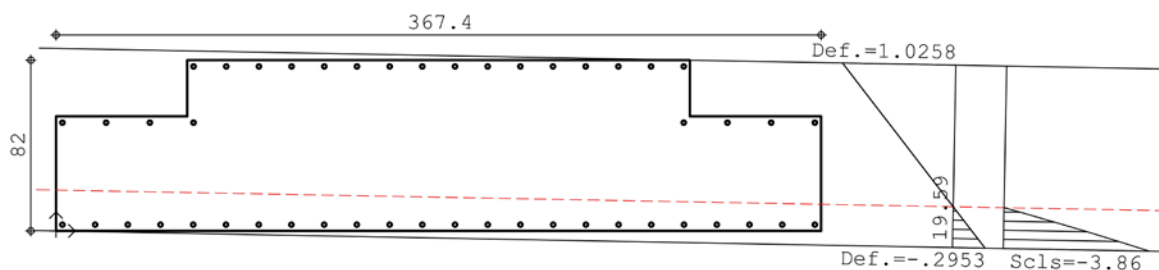
DESCRIZIONI
 Tipo sezione : U Pul
 Tipo verifica: sTato limite ultimo

CARATTERISTICHE DEI MATERIALI
 Calcestruzzo: Rck= 30.
 fck= 24.9
 fcd= 14.11 (.35%)
 Acciaio lento: Tipo= B450C
 fyk= 450.
 ftk= 540.
 ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
 eps= muz * y + muy * z + lam
 muz= 1.50730156515528E-05
 muy= 2.79745848633362E-07
 lam=-2.9533185899873E-04

SOLLECITAZIONI AGENTI:
 Nd in z= 183.7; y= 37.5 (baricentro CLS)
 Nd = -71.46
 Mdz= -855.0569
 Mdy= -344.4652

UNITA' DI MISURA:
 kN; cm; kNm; N/mm2.
 Ø in mm; deformazioni*1000.
 SIMBOLI:
 S=sigma (tensioni sui materiali);
 D=deformazioni (epsilon):



TENSIONI NEL CLS:					
ver	Z	Y	Dcls	Scls	Vel
1	0.	55.	.53368	0.	si
2	63.	55.	.55131	0.	si
3	63.	82.	.95828	0.	si
4	304.4	82.	1.02581	0.	si
5	304.4	55.	.61884	0.	si
6	367.4	55.	.63646	0.	si
7	367.4	0.	-.19255	-2.59	si
8	0.	0.	-.29533	-3.86	si

TENSIONI NEI FERRI:									
fer	Z	Y	Ø (mm)	Af (cm2)	D ferri	S ferri	Vel ferri	Vel	
1	301.4	79.	20	3.14	.97975	.195	.95	si	
2	285.7	79.	20	3.14	.97536	.195	.07	si	
3	270.	79.	20	3.14	.97097	.194	.19	si	
4	254.3	79.	20	3.14	.96658	.193	.32	si	
5	238.6	79.	20	3.14	.96219	.192	.44	si	
6	222.9	79.	20	3.14	.9578	.191	.56	si	
7	207.2	79.	20	3.14	.95341	.190	.68	si	
8	191.5	79.	20	3.14	.94902	.189	.8	si	
9	175.9	79.	20	3.14	.94463	.188	.93	si	
10	160.2	79.	20	3.14	.94024	.188	.05	si	
11	144.5	79.	20	3.14	.93585	.187	.17	si	
12	128.8	79.	20	3.14	.93146	.186	.29	si	
13	113.1	79.	20	3.14	.92707	.185	.41	si	
14	97.4	79.	20	3.14	.92268	.184	.54	si	
15	81.7	79.	20	3.14	.91829	.183	.66	si	
16	66.	79.	20	3.14	.9139	.182	.78	si	
17	66.	52.	20	3.14	.50693	.101	.39	si	
18	45.	52.	20	3.14	.50105	.100	.21	si	
19	24.	52.	20	3.14	.49518	.099	.04	si	
20	3.	52.	20	3.14	.4893	.097	.86	si	
21	364.4	52.	20	3.14	.5904	.118	.08	si	
22	343.4	52.	20	3.14	.58453	.116	.91	si	
23	322.4	52.	20	3.14	.57866	.115	.73	si	
24	301.4	52.	20	3.14	.57278	.114	.56	si	
25	364.4	3.	20	3.14	-.14817	-.29	.63	si	
26	348.7	3.	20	3.14	-.15257	-.30	.51	si	
27	333.	3.	20	3.14	-.15696	-.31	.39	si	
28	317.3	3.	20	3.14	-.16136	-.32	.27	si	
29	301.5	3.	20	3.14	-.16576	-.33	.15	si	
30	285.8	3.	20	3.14	-.17015	-.34	.03	si	
31	270.1	3.	20	3.14	-.17455	-.34	.91	si	
32	254.4	3.	20	3.14	-.17894	-.35	.79	si	
33	238.7	3.	20	3.14	-.18334	-.36	.67	si	
34	223.	3.	20	3.14	-.18773	-.37	.55	si	
35	207.3	3.	20	3.14	-.19213	-.38	.43	si	
36	191.6	3.	20	3.14	-.19653	-.39	.31	si	
37	175.8	3.	20	3.14	-.20092	-.40	.18	si	
38	160.1	3.	20	3.14	-.20532	-.41	.06	si	
39	144.4	3.	20	3.14	-.20971	-.41	.94	si	
40	128.7	3.	20	3.14	-.21411	-.42	.82	si	
41	113.	3.	20	3.14	-.2185	-.43	.7	si	
42	97.3	3.	20	3.14	-.2229	-.44	.58	si	
43	81.6	3.	20	3.14	-.2273	-.45	.46	si	
44	65.9	3.	20	3.14	-.23169	-.46	.34	si	
45	50.1	3.	20	3.14	-.23609	-.47	.22	si	
46	34.4	3.	20	3.14	-.24048	-.48	.1	si	
47	18.7	3.	20	3.14	-.24488	-.48	.98	si	
48	3.	3.	20	3.14	-.24927	-.49	.85	si	

% ARMAT.: tesa= .28; comp.= .28; tot.= .56

Ripristino Ponte-Tubo
VERIFICA PULVINO XZ 8

DESCRIZIONI
Tipo sezione : RETTANGOLARE
Tipo verifica: stato limite ultimo

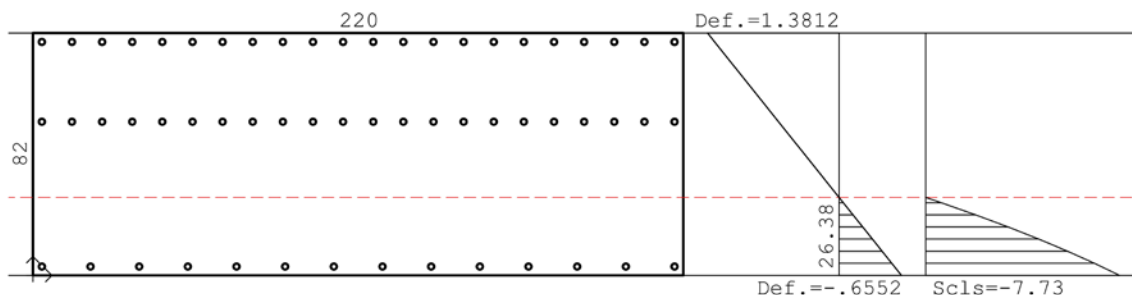
CARATTERISTICHE DEI MATERIALI
Calcestruzzo: Rck= 30.
fck= 24.9
fcd= 14.11 (.35%)
Acciaio lento: Tipo= B450C
fyk= 450.
ftk= 540.
ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
eps= muz * y + muy * z + lam
muz= 2.48342090661304E-05
muy= 0
lam=-3.7080650139684E-04

SOLLECITAZIONI AGENTI:
Nd in y= 29.6 (baricentro CLS)
Nd = -214.72
Mdz=-1740.4278
verifica in pressoflessione retta

UNITA' DI MISURA:
kN; cm; kNm; N/mm2.
Ø in mm; deformazioni*1000.

SIMBOLI:
S=sigma (tensioni sui materiali);
D=deformazioni (epsilon):



TENSIONI NEL CLS:		Dcls	Scls	Ve
ver	Z			
1	-2673.	70.6	1.38125	0.
2	-2453.	70.6	1.38125	0.
3	-2453.	-11.4	-6.5516	-7.73
4	-2673.	-11.4	-6.5516	-7.73

TENSIONI NEI FERRI:		Ø (mm)	Af (cm2)	D	ferri	S	ferri	Ve
Fer	Z							
1	-2456.	40.6	20	3.14	.63622	127.24	si	
37	-2466.	40.6	20	3.14	.63622	127.24	si	
3	-2476.	40.6	20	3.14	.63622	127.24	si	
4	-2487.	40.6	20	3.14	.63622	127.24	si	
5	-2497.	40.6	20	3.14	.63622	127.24	si	
6	-2507.	40.6	20	3.14	.63622	127.24	si	
7	-2517.	40.6	20	3.14	.63622	127.24	si	
8	-2527.	40.6	20	3.14	.63622	127.24	si	
9	-2538.	40.6	20	3.14	.63622	127.24	si	
10	-2548.	40.6	20	3.14	.63622	127.24	si	
11	-2558.	40.6	20	3.14	.63622	127.24	si	
12	-2568.	40.6	20	3.14	.63622	127.24	si	
13	-2578.	40.6	20	3.14	.63622	127.24	si	
14	-2589.	40.6	20	3.14	.63622	127.24	si	
15	-2599.	40.6	20	3.14	.63622	127.24	si	
16	-2609.	40.6	20	3.14	.63622	127.24	si	
17	-2619.	40.6	20	3.14	.63622	127.24	si	
18	-2629.	40.6	20	3.14	.63622	127.24	si	
19	-2639.	40.6	20	3.14	.63622	127.24	si	
20	-2650.	40.6	20	3.14	.63622	127.24	si	
21	-2660.	40.6	20	3.14	.63622	127.24	si	
22	-2670.	40.6	20	3.14	.63622	127.24	si	
23	-2456.	67.6	20	3.14	1.30674	261.35	si	
24	-2466.	67.6	20	3.14	1.30674	261.35	si	
25	-2476.	67.6	20	3.14	1.30674	261.35	si	
26	-2487.	67.6	20	3.14	1.30674	261.35	si	
27	-2497.	67.6	20	3.14	1.30674	261.35	si	
28	-2507.	67.6	20	3.14	1.30674	261.35	si	
29	-2517.	67.6	20	3.14	1.30674	261.35	si	
30	-2527.	67.6	20	3.14	1.30674	261.35	si	
31	-2538.	67.6	20	3.14	1.30674	261.35	si	
32	-2548.	67.6	20	3.14	1.30674	261.35	si	
33	-2558.	67.6	20	3.14	1.30674	261.35	si	
34	-2568.	67.6	20	3.14	1.30674	261.35	si	
35	-2578.	67.6	20	3.14	1.30674	261.35	si	
36	-2589.	67.6	20	3.14	1.30674	261.35	si	
37	-2599.	67.6	20	3.14	1.30674	261.35	si	
38	-2609.	67.6	20	3.14	1.30674	261.35	si	
39	-2619.	67.6	20	3.14	1.30674	261.35	si	
40	-2629.	67.6	20	3.14	1.30674	261.35	si	
41	-2639.	67.6	20	3.14	1.30674	261.35	si	
42	-2650.	67.6	20	3.14	1.30674	261.35	si	
43	-2660.	67.6	20	3.14	1.30674	261.35	si	
44	-2670.	67.6	20	3.14	1.30674	261.35	si	
45	-2456.	-8.4	20	3.14	-.58066	-116.13	si	
46	-2473.	-8.4	20	3.14	-.58066	-116.13	si	
47	-2489.	-8.4	20	3.14	-.58066	-116.13	si	
48	-2505.	-8.4	20	3.14	-.58066	-116.13	si	
49	-2522.	-8.4	20	3.14	-.58066	-116.13	si	
50	-2538.	-8.4	20	3.14	-.58066	-116.13	si	
51	-2555.	-8.4	20	3.14	-.58066	-116.13	si	
52	-2571.	-8.4	20	3.14	-.58066	-116.13	si	
53	-2588.	-8.4	20	3.14	-.58066	-116.13	si	
54	-2604.	-8.4	20	3.14	-.58066	-116.13	si	
55	-2621.	-8.4	20	3.14	-.58066	-116.13	si	
56	-2637.	-8.4	20	3.14	-.58066	-116.13	si	
57	-2654.	-8.4	20	3.14	-.58066	-116.13	si	
58	-2670.	-8.4	20	3.14	-.58066	-116.13	si	

% ARMAT.: tesa = .77; comp. = .24; tot. = 1.01

Ripristino Ponte-Tubo
VERIFICA PULVINO YZ 8

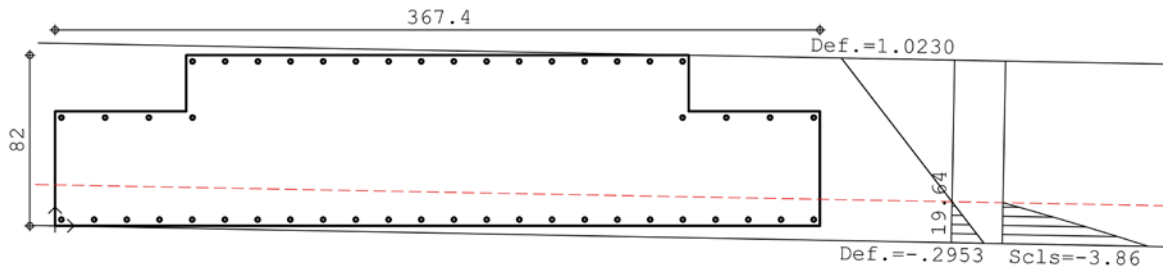
DESCRIZIONI
Tipo sezione : U Pul
Tipo verifica: sEato limite ultimo

CARATTERISTICHE DEI MATERIALI
Calcestruzzo: Rck= 30.
fck= 24.9
fcd= 14.11 (.35%)
Acciaio lento: Tipo= B450C
fyk= 450.
ftk= 540.
ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
eps= muz * y +muy * z + lam
muz= 1.50294173855246E-05
muy= 2.82042130052866E-07
lam=-2.95303743505411E-04

SOLLECITAZIONI AGENTI:
Nd in z= 183.7; y= 37.5 (baricentro CLS)
Nd = -74.46
Mdz = -853.2791
Mdy = -347.5826

UNITA' DI MISURA:
kN; cm; kNm; N/mm2.
Ø in mm; deformazioni*1000.
SIMBOLI:
S=sigma (tensioni sui materiali);
D=deformazioni (epsilon):



TENSIONI NEL CLS:					
ver	z	y	Dcls	Scls	Ve
1	0.	55.	.53131	0.	si
2	63.	55.	.54908	0.	si
3	63.	82.	.95488	0.	si
4	304.4	82.	1.02296	0.	si
5	304.4	55.	.61717	0.	si
6	367.4	55.	.63494	0.	si
7	367.4	0.	-.19168	-2.58	si
8	0.	0.	-.2953	-3.86	si

TENSIONI NEI FERRI:									
fer	z	y	Ø (mm)	Af (cm2)	D ferri	S ferri	Ve		
1	301.4	79.	20	3.14	.97703	195.41	si		
2	285.7	79.	20	3.14	.9726	194.52	si		
3	270.	79.	20	3.14	.96818	193.64	si		
4	254.3	79.	20	3.14	.96375	192.75	si		
5	238.6	79.	20	3.14	.95932	191.86	si		
6	222.9	79.	20	3.14	.9549	190.98	si		
7	207.2	79.	20	3.14	.95047	190.09	si		
8	191.5	79.	20	3.14	.94604	189.21	si		
9	175.9	79.	20	3.14	.94162	188.32	si		
10	160.2	79.	20	3.14	.93719	187.44	si		
11	144.5	79.	20	3.14	.93277	186.55	si		
12	128.8	79.	20	3.14	.92834	185.67	si		
13	113.1	79.	20	3.14	.92391	184.78	si		
14	97.4	79.	20	3.14	.91949	183.9	si		
15	81.7	79.	20	3.14	.91506	183.01	si		
16	66.	79.	20	3.14	.91064	182.13	si		
17	66.	52.	20	3.14	.50484	100.97	si		
18	45.	52.	20	3.14	.49892	99.78	si		
19	24.	52.	20	3.14	.49299	98.6	si		
20	3.	52.	20	3.14	.48707	97.41	si		
21	364.4	52.	20	3.14	.589	117.8	si		
22	343.4	52.	20	3.14	.58308	116.62	si		
23	322.4	52.	20	3.14	.57716	115.43	si		
24	301.4	52.	20	3.14	.57123	114.25	si		
25	364.4	3.	20	3.14	-.14744	-29.49	si		
26	348.7	3.	20	3.14	-.15187	-30.37	si		
27	333.	3.	20	3.14	-.1563	-31.26	si		
28	317.3	3.	20	3.14	-.16073	-32.15	si		
29	301.5	3.	20	3.14	-.16517	-33.03	si		
30	285.8	3.	20	3.14	-.1696	-33.92	si		
31	270.1	3.	20	3.14	-.17403	-34.81	si		
32	254.4	3.	20	3.14	-.17846	-35.69	si		
33	238.7	3.	20	3.14	-.18289	-36.58	si		
34	223.	3.	20	3.14	-.18732	-37.46	si		
35	207.3	3.	20	3.14	-.19176	-38.35	si		
36	191.6	3.	20	3.14	-.19619	-39.24	si		
37	175.8	3.	20	3.14	-.20062	-40.12	si		
38	160.1	3.	20	3.14	-.20505	-41.01	si		
39	144.4	3.	20	3.14	-.20948	-41.9	si		
40	128.7	3.	20	3.14	-.21392	-42.78	si		
41	113.	3.	20	3.14	-.21835	-43.67	si		
42	97.3	3.	20	3.14	-.22278	-44.56	si		
43	81.6	3.	20	3.14	-.22721	-45.44	si		
44	65.9	3.	20	3.14	-.23164	-46.33	si		
45	50.1	3.	20	3.14	-.23607	-47.21	si		
46	34.4	3.	20	3.14	-.24051	-48.1	si		
47	18.7	3.	20	3.14	-.24494	-48.99	si		
48	3.	3.	20	3.14	-.24937	-49.87	si		

% ARMAT.: tesa= .28; comp.= .28; tot.= .56

Ripristino Ponte-Tubo
VERIFICA PULVINO XZ 9

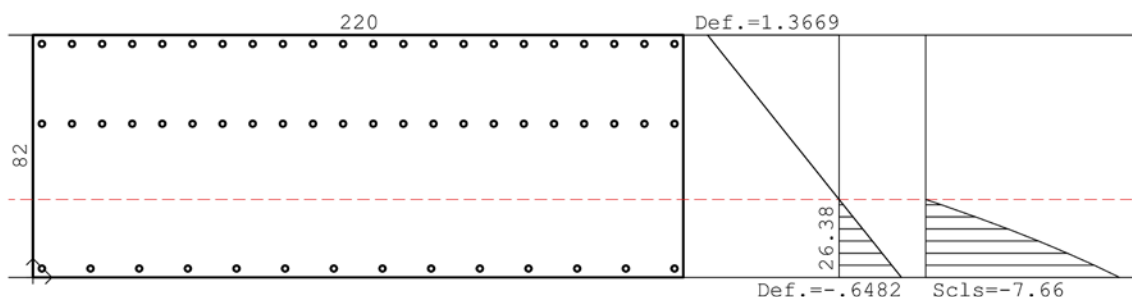
DESCRIZIONI
Tipo sezione : RETTANGOLARE
Tipo verifica: stato limite ultimo

CARATTERISTICHE DEI MATERIALI
Calcestruzzo: Rck= 30.
fck= 24.9
fcd= 14.11 (.35%)
Acciaio lento: Tipo= B450C
fyk= 450.
ftk= 540.
ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
eps= muz * y +muy * z + lam
muz= 2.45741971706001E-05
muy= 0
lam=-3.66825513615846E-04

SOLLECITAZIONI AGENTI:
Nd in y= 29.6 (baricentro CLS)
Nd = -214.47
Mdz=-1723.1011
verifica in pressoflessione retta

UNITA' DI MISURA:
kN; cm; kNm; N/mm2.
Ø in mm; deformazioni*1000.
SIMBOLI:
S=sigma (tensioni sui materiali);
D=deformazioni (epsilon):



TENSIONI NEL CLS:					
ver	Z	Y	Dcls	Scls	Ve
1	-2673.	70.6	1.36688	0.	si
2	-2453.	70.6	1.36688	0.	si
3	-2453.	-11.4	-.6482	-7.66	si
4	-2673.	-11.4	-.6482	-7.66	si

TENSIONI NEI FERRI:										
Fer	Z	Y	Ø (mm)	Af (cm2)	D	ferri	S	ferri	Ve	
1	-2456.	40.6	20	3.14	.62966	125.93	si			
3	-2476.	40.6	20	3.14	.62966	125.93	si			
4	-2487.	40.6	20	3.14	.62966	125.93	si			
5	-2497.	40.6	20	3.14	.62966	125.93	si			
6	-2507.	40.6	20	3.14	.62966	125.93	si			
7	-2517.	40.6	20	3.14	.62966	125.93	si			
8	-2527.	40.6	20	3.14	.62966	125.93	si			
9	-2538.	40.6	20	3.14	.62966	125.93	si			
10	-2548.	40.6	20	3.14	.62966	125.93	si			
11	-2558.	40.6	20	3.14	.62966	125.93	si			
12	-2568.	40.6	20	3.14	.62966	125.93	si			
13	-2578.	40.6	20	3.14	.62966	125.93	si			
14	-2589.	40.6	20	3.14	.62966	125.93	si			
15	-2599.	40.6	20	3.14	.62966	125.93	si			
16	-2609.	40.6	20	3.14	.62966	125.93	si			
17	-2619.	40.6	20	3.14	.62966	125.93	si			
18	-2629.	40.6	20	3.14	.62966	125.93	si			
19	-2639.	40.6	20	3.14	.62966	125.93	si			
20	-2650.	40.6	20	3.14	.62966	125.93	si			
21	-2660.	40.6	20	3.14	.62966	125.93	si			
22	-2670.	40.6	20	3.14	.62966	125.93	si			
23	-2456.	67.6	20	3.14	1.29316	258.63	si			
24	-2466.	67.6	20	3.14	1.29316	258.63	si			
25	-2476.	67.6	20	3.14	1.29316	258.63	si			
26	-2487.	67.6	20	3.14	1.29316	258.63	si			
27	-2497.	67.6	20	3.14	1.29316	258.63	si			
28	-2507.	67.6	20	3.14	1.29316	258.63	si			
29	-2517.	67.6	20	3.14	1.29316	258.63	si			
30	-2527.	67.6	20	3.14	1.29316	258.63	si			
31	-2538.	67.6	20	3.14	1.29316	258.63	si			
32	-2548.	67.6	20	3.14	1.29316	258.63	si			
33	-2558.	67.6	20	3.14	1.29316	258.63	si			
34	-2568.	67.6	20	3.14	1.29316	258.63	si			
35	-2578.	67.6	20	3.14	1.29316	258.63	si			
36	-2589.	67.6	20	3.14	1.29316	258.63	si			
37	-2599.	67.6	20	3.14	1.29316	258.63	si			
38	-2609.	67.6	20	3.14	1.29316	258.63	si			
39	-2619.	67.6	20	3.14	1.29316	258.63	si			
40	-2629.	67.6	20	3.14	1.29316	258.63	si			
41	-2639.	67.6	20	3.14	1.29316	258.63	si			
42	-2650.	67.6	20	3.14	1.29316	258.63	si			
43	-2660.	67.6	20	3.14	1.29316	258.63	si			
44	-2670.	67.6	20	3.14	1.29316	258.63	si			
45	-2456.	-8.4	20	3.14	-.57448	-114.9	si			
46	-2473.	-8.4	20	3.14	-.57448	-114.9	si			
47	-2489.	-8.4	20	3.14	-.57448	-114.9	si			
48	-2505.	-8.4	20	3.14	-.57448	-114.9	si			
49	-2522.	-8.4	20	3.14	-.57448	-114.9	si			
50	-2538.	-8.4	20	3.14	-.57448	-114.9	si			
51	-2555.	-8.4	20	3.14	-.57448	-114.9	si			
52	-2571.	-8.4	20	3.14	-.57448	-114.9	si			
53	-2588.	-8.4	20	3.14	-.57448	-114.9	si			
54	-2604.	-8.4	20	3.14	-.57448	-114.9	si			
55	-2621.	-8.4	20	3.14	-.57448	-114.9	si			
56	-2637.	-8.4	20	3.14	-.57448	-114.9	si			
57	-2654.	-8.4	20	3.14	-.57448	-114.9	si			
58	-2670.	-8.4	20	3.14	-.57448	-114.9	si			

% ARMAT.: tesa = .77; comp. = .24; tot. = 1.01

Ripristino Ponte-Tubo
VERIFICA PULVINO YZ 9

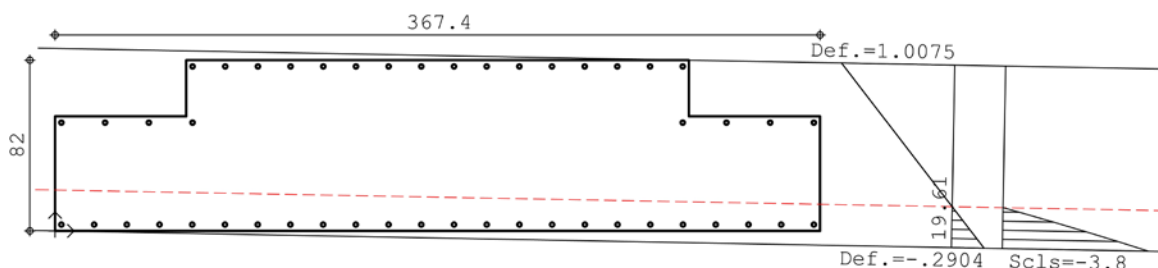
DESCRIZIONI
Tipo sezione : U Pul
Tipo verifica: sEato limite ultimo

CARATTERISTICHE DEI MATERIALI
Calcestruzzo: Rck= 30.
fck= 24.9
fcd= 14.11 (.35%)
Acciaio lento: Tipo= B450C
fyk= 450.
ftk= 540.
ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
eps= muz * y +muy * z + lam
muz= 1.48071664940868E-05
muy= 2.75210748261175E-07
lam=-2.90443914175534E-04

SOLLECITAZIONI AGENTI:
Nd in z= 183.7; y= 37.5 (baricentro CLS)
Nd = -73.69
Mdz= -840.81
Mdy= -339.3986

UNITA' DI MISURA:
kN; cm; kNm; N/mm2.
Ø in mm; deformazioni*1000.
SIMBOLI:
S=sigma (tensioni sui materiali);
D=deformazioni (epsilon):



TENSIONI NEL CLS:					
ver	z	y	Dcls	Scls	Vel
1	0.	55.	.52395	0.	si
2	63.	55.	.54129	0.	si
3	63.	82.	.94108	0.	si
4	304.4	82.	1.00752	0.	si
5	304.4	55.	.60772	0.	si
6	367.4	55.	.62506	0.	si
7	367.4	0.	-.18933	-2.55	si
8	0.	0.	-.29044	-3.8	si

TENSIONI NEI FERRI:										
Fer	z	y	Ø (mm)	Af (cm2)	D ferri	S ferri	Vel			
1	301.4	79.	20	3.14	.96227	192.45	si			
2	285.7	79.	20	3.14	.95795	191.59	si			
3	270.	79.	20	3.14	.95363	190.73	si			
4	254.3	79.	20	3.14	.94931	189.86	si			
5	238.6	79.	20	3.14	.94499	189.	si			
6	222.9	79.	20	3.14	.94068	188.14	si			
7	207.2	79.	20	3.14	.93636	187.27	si			
8	191.5	79.	20	3.14	.93204	186.41	si			
9	175.9	79.	20	3.14	.92772	185.54	si			
10	160.2	79.	20	3.14	.9234	184.68	si			
11	144.5	79.	20	3.14	.91908	183.82	si			
12	128.8	79.	20	3.14	.91476	182.95	si			
13	113.1	79.	20	3.14	.91044	182.09	si			
14	97.4	79.	20	3.14	.90612	181.22	si			
15	81.7	79.	20	3.14	.90181	180.36	si			
16	66.	79.	20	3.14	.89749	179.5	si			
17	66.	52.	20	3.14	.49769	99.54	si			
18	45.	52.	20	3.14	.49191	98.38	si			
19	24.	52.	20	3.14	.48613	97.23	si			
20	3.	52.	20	3.14	.48035	96.07	si			
21	364.4	52.	20	3.14	.57982	115.96	si			
22	343.4	52.	20	3.14	.57404	114.81	si			
23	322.4	52.	20	3.14	.56826	113.65	si			
24	301.4	52.	20	3.14	.56248	112.5	si			
25	364.4	3.	20	3.14	-.14574	-29.15	si			
26	348.7	3.	20	3.14	-.15006	-30.01	si			
27	333.	3.	20	3.14	-.15438	-30.88	si			
28	317.3	3.	20	3.14	-.15871	-31.74	si			
29	301.5	3.	20	3.14	-.16303	-32.61	si			
30	285.8	3.	20	3.14	-.16736	-33.47	si			
31	270.1	3.	20	3.14	-.17168	-34.34	si			
32	254.4	3.	20	3.14	-.17601	-35.2	si			
33	238.7	3.	20	3.14	-.18033	-36.07	si			
34	223.	3.	20	3.14	-.18466	-36.93	si			
35	207.3	3.	20	3.14	-.18898	-37.8	si			
36	191.6	3.	20	3.14	-.1933	-38.66	si			
37	175.8	3.	20	3.14	-.19763	-39.53	si			
38	160.1	3.	20	3.14	-.20195	-40.39	si			
39	144.4	3.	20	3.14	-.20628	-41.26	si			
40	128.7	3.	20	3.14	-.2106	-42.12	si			
41	113.	3.	20	3.14	-.21493	-42.99	si			
42	97.3	3.	20	3.14	-.21925	-43.85	si			
43	81.6	3.	20	3.14	-.22357	-44.71	si			
44	65.9	3.	20	3.14	-.2279	-45.58	si			
45	50.1	3.	20	3.14	-.23222	-46.44	si			
46	34.4	3.	20	3.14	-.23655	-47.31	si			
47	18.7	3.	20	3.14	-.24087	-48.17	si			
48	3.	3.	20	3.14	-.2452	-49.04	si			

% ARMAT.: tesa= .28; comp.= .28; tot.= .56

Ripristino Ponte-Tubo
VERIFICA PULVINO XZ 10

DESCRIZIONI
Tipo sezione : RETTANGOLARE
Tipo verifica: stato limite ultimo

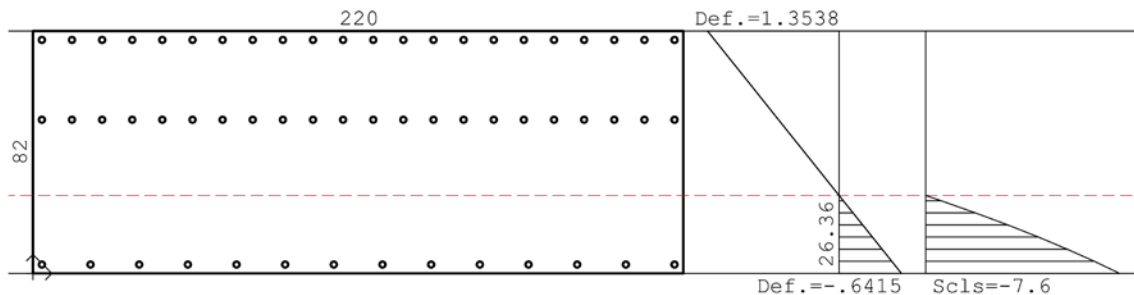
CARATTERISTICHE DEI MATERIALI
Calcestruzzo: Rck= 30.
fck= 24.9
fcd= 14.11 (.35%)
Acciaio lento: Tipo= B450C
fyk= 450.
ftk= 540.
ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
eps= muz * y + muy * z + lam
muz= 2.43337187832632E-05
muy= 0
lam=-3.62911658487999E-04

SOLLECITAZIONI AGENTI:
Nd in y= 29.6 (baricentro CLS)
Nd = -211.74
Mdz=-1706.7052
verifica in pressoflessione retta

UNITA' DI MISURA:
kN; cm; kNm; N/mm2.
Ø in mm; deformazioni*1000.

SIMBOLI:
S=sigma (tensioni sui materiali);
D=deformazioni (epsilon):



TENSIONI NEL CLS:					
ver	Z	Y	Dcls	Scls	Vel
1	-2673.	70.6	1.35383	0.	si
2	-2453.	70.6	1.35383	0.	si
3	-2453.	-11.4	-0.64153	-7.6	si
4	-2673.	-11.4	-0.64153	-7.6	si

TENSIONI NEI FERRI:										
Fer	Z	Y	Ø (mm)	Af (cm2)	D	ferri	S	ferri	Vel	
1	-2456.	40.6	20	3.14		.62382		124.76	si	
3	-2476.	40.6	20	3.14		.62382		124.76	si	
4	-2487.	40.6	20	3.14		.62382		124.76	si	
5	-2497.	40.6	20	3.14		.62382		124.76	si	
6	-2507.	40.6	20	3.14		.62382		124.76	si	
7	-2517.	40.6	20	3.14		.62382		124.76	si	
8	-2527.	40.6	20	3.14		.62382		124.76	si	
9	-2538.	40.6	20	3.14		.62382		124.76	si	
10	-2548.	40.6	20	3.14		.62382		124.76	si	
11	-2558.	40.6	20	3.14		.62382		124.76	si	
12	-2568.	40.6	20	3.14		.62382		124.76	si	
13	-2578.	40.6	20	3.14		.62382		124.76	si	
14	-2589.	40.6	20	3.14		.62382		124.76	si	
15	-2599.	40.6	20	3.14		.62382		124.76	si	
16	-2609.	40.6	20	3.14		.62382		124.76	si	
17	-2619.	40.6	20	3.14		.62382		124.76	si	
18	-2629.	40.6	20	3.14		.62382		124.76	si	
19	-2639.	40.6	20	3.14		.62382		124.76	si	
20	-2650.	40.6	20	3.14		.62382		124.76	si	
21	-2660.	40.6	20	3.14		.62382		124.76	si	
22	-2670.	40.6	20	3.14		.62382		124.76	si	
23	-2456.	67.6	20	3.14	1.28083		256.17	si		
24	-2466.	67.6	20	3.14	1.28083		256.17	si		
25	-2476.	67.6	20	3.14	1.28083		256.17	si		
26	-2487.	67.6	20	3.14	1.28083		256.17	si		
27	-2497.	67.6	20	3.14	1.28083		256.17	si		
28	-2507.	67.6	20	3.14	1.28083		256.17	si		
29	-2517.	67.6	20	3.14	1.28083		256.17	si		
30	-2527.	67.6	20	3.14	1.28083		256.17	si		
31	-2538.	67.6	20	3.14	1.28083		256.17	si		
32	-2548.	67.6	20	3.14	1.28083		256.17	si		
33	-2558.	67.6	20	3.14	1.28083		256.17	si		
34	-2568.	67.6	20	3.14	1.28083		256.17	si		
35	-2578.	67.6	20	3.14	1.28083		256.17	si		
36	-2589.	67.6	20	3.14	1.28083		256.17	si		
37	-2599.	67.6	20	3.14	1.28083		256.17	si		
38	-2609.	67.6	20	3.14	1.28083		256.17	si		
39	-2619.	67.6	20	3.14	1.28083		256.17	si		
40	-2629.	67.6	20	3.14	1.28083		256.17	si		
41	-2639.	67.6	20	3.14	1.28083		256.17	si		
42	-2650.	67.6	20	3.14	1.28083		256.17	si		
43	-2660.	67.6	20	3.14	1.28083		256.17	si		
44	-2670.	67.6	20	3.14	1.28083		256.17	si		
45	-2456.	-8.4	20	3.14	-5.6853		-113.71	si		
46	-2473.	-8.4	20	3.14	-5.6853		-113.71	si		
47	-2489.	-8.4	20	3.14	-5.6853		-113.71	si		
48	-2505.	-8.4	20	3.14	-5.6853		-113.71	si		
49	-2522.	-8.4	20	3.14	-5.6853		-113.71	si		
50	-2538.	-8.4	20	3.14	-5.6853		-113.71	si		
51	-2555.	-8.4	20	3.14	-5.6853		-113.71	si		
52	-2571.	-8.4	20	3.14	-5.6853		-113.71	si		
53	-2588.	-8.4	20	3.14	-5.6853		-113.71	si		
54	-2604.	-8.4	20	3.14	-5.6853		-113.71	si		
55	-2621.	-8.4	20	3.14	-5.6853		-113.71	si		
56	-2637.	-8.4	20	3.14	-5.6853		-113.71	si		
57	-2654.	-8.4	20	3.14	-5.6853		-113.71	si		
58	-2670.	-8.4	20	3.14	-5.6853		-113.71	si		

% ARMAT.: tesa = .77; comp. = .24; tot. = 1.01

Ripristino Ponte-Tubo

VERIFICA PULVINO YZ 10

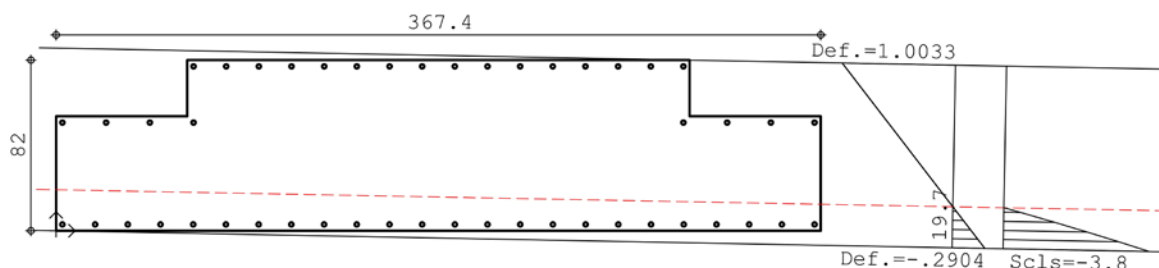
DESCRIZIONI
 Tipo sezione : U Pul
 Tipo verifica: sEato limite ultimo

CARATTERISTICHE DEI MATERIALI
 Calcestruzzo: Rck= 30.
 fck= 24.9
 fcd= 14.11 (.35%)
 Acciaio lento: Tipo= B450C
 fyk= 450.
 ftk= 540.
 ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
 eps= muz * y +muy * z + lam
 muz= 1.4738038642125E-05
 muy= 2.79749856670881E-07
 lam=-2.90423353586248E-04

SOLLECITAZIONI AGENTI:
 Nd in z= 183.7; y= 37.5 (baricentro CLS)
 Nd = -77.
 Mdz= -837.6811
 Mdy= -345.3238

UNITA' DI MISURA:
 kN; cm; kNm; N/mm2.
 Ø in mm; deformazioni*1000.
 SIMBOLI:
 S=sigma (tensioni sui materiali);
 D=deformazioni (epsilon):



TENSIONI NEL CLS:					
ver	z	y	Dcls	Scls	Ve
1	0.	55.	.52017	0.	si
2	63.	55.	.53779	0.	si
3	63.	82.	.93572	0.	si
4	304.4	82.	1.00325	0.	si
5	304.4	55.	.60532	0.	si
6	367.4	55.	.62295	0.	si
7	367.4	0.	-.18764	-2.52	si
8	0.	0.	-.29042	-3.8	si

TENSIONI NEI FERRI:										
Fer	z	y	Ø (mm)	Af (cm2)	D	ferri	S	ferri	Ve	
1	301.4	79.	20	3.14	.9582	191.64	si			
2	285.7	79.	20	3.14	.95381	190.76	si			
3	270.	79.	20	3.14	.94942	189.88	si			
4	254.3	79.	20	3.14	.94503	189.01	si			
5	238.6	79.	20	3.14	.94064	188.13	si			
6	222.9	79.	20	3.14	.93625	187.25	si			
7	207.2	79.	20	3.14	.93186	186.37	si			
8	191.5	79.	20	3.14	.92747	185.49	si			
9	175.9	79.	20	3.14	.92308	184.62	si			
10	160.2	79.	20	3.14	.91869	183.74	si			
11	144.5	79.	20	3.14	.9143	182.86	si			
12	128.8	79.	20	3.14	.90991	181.98	si			
13	113.1	79.	20	3.14	.90552	181.1	si			
14	97.4	79.	20	3.14	.90113	180.23	si			
15	81.7	79.	20	3.14	.89674	179.35	si			
16	66.	79.	20	3.14	.89235	178.47	si			
17	66.	52.	20	3.14	.49442	98.88	si			
18	45.	52.	20	3.14	.48854	97.71	si			
19	24.	52.	20	3.14	.48267	96.53	si			
20	3.	52.	20	3.14	.47679	95.36	si			
21	364.4	52.	20	3.14	.5779	115.58	si			
22	343.4	52.	20	3.14	.57202	114.4	si			
23	322.4	52.	20	3.14	.56615	113.23	si			
24	301.4	52.	20	3.14	.56027	112.05	si			
25	364.4	3.	20	3.14	-.14427	-28.85	si			
26	348.7	3.	20	3.14	-.14866	-29.73	si			
27	333.	3.	20	3.14	-.15306	-30.61	si			
28	317.3	3.	20	3.14	-.15746	-31.49	si			
29	301.5	3.	20	3.14	-.16185	-32.37	si			
30	285.8	3.	20	3.14	-.16625	-33.25	si			
31	270.1	3.	20	3.14	-.17064	-34.13	si			
32	254.4	3.	20	3.14	-.17504	-35.01	si			
33	238.7	3.	20	3.14	-.17943	-35.89	si			
34	223.	3.	20	3.14	-.18383	-36.77	si			
35	207.3	3.	20	3.14	-.18823	-37.65	si			
36	191.6	3.	20	3.14	-.19262	-38.52	si			
37	175.8	3.	20	3.14	-.19702	-39.4	si			
38	160.1	3.	20	3.14	-.20141	-40.28	si			
39	144.4	3.	20	3.14	-.20581	-41.16	si			
40	128.7	3.	20	3.14	-.2102	-42.04	si			
41	113.	3.	20	3.14	-.2146	-42.92	si			
42	97.3	3.	20	3.14	-.219	-43.8	si			
43	81.6	3.	20	3.14	-.22339	-44.68	si			
44	65.9	3.	20	3.14	-.22779	-45.56	si			
45	50.1	3.	20	3.14	-.23218	-46.44	si			
46	34.4	3.	20	3.14	-.23658	-47.32	si			
47	18.7	3.	20	3.14	-.24097	-48.19	si			
48	3.	3.	20	3.14	-.24537	-49.07	si			

% ARMAT.: tesa= .28; comp.= .28; tot.= .56

Ripristino Ponte-Tubo
VERIFICA PULVINO XZ 11

DESCRIZIONI
Tipo sezione : RETTANGOLARE
Tipo verifica: stato limite ultimo

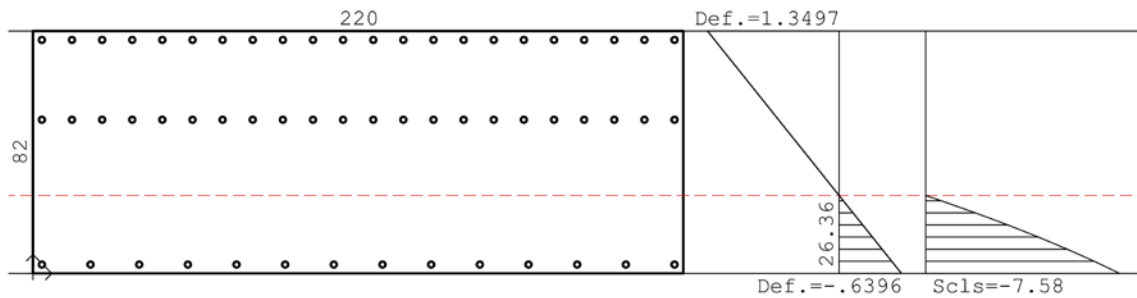
CARATTERISTICHE DEI MATERIALI
Calcestruzzo: Rck= 30.
fck= 24.9
fcd= 14.11 (.35%)
Acciaio lento: Tipo= B450C
fyk= 450.
ftk= 540.
ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
eps= muz * y +muy * z + lam
muz= 2.42592666259486E-05
muy= 0
lam=-3.61820455706771E-04

SOLLECITAZIONI AGENTI:
Nd in y= 29.6 (baricentro CLS)
Nd = -212.15
Mdz=-1701.8069
verifica in pressoflessione retta

UNITA' DI MISURA:
kN; cm; kNm; N/mm2.
Ø in mm; deformazioni*1000.

SIMBOLI:
S=sigma (tensioni sui materiali);
D=deformazioni (epsilon):



TENSIONI NEL CLS:					
ver	Z	Y	Dcls	Scls	Ve
1	-2673.	70.6	1.34967	0.	si
2	-2453.	70.6	1.34967	0.	si
3	-2453.	-11.4	-.63959	-7.58	si
4	-2673.	-11.4	-.63959	-7.58	si

TENSIONI NEI FERRI:											
Fer	Z	Y	Ø (mm)	Af (cm2)	D	ferri	S	ferri	Ve		
1	-2456.	40.6	20	3.14		.62189		124.38	si		
3	-2476.	40.6	20	3.14		.62189		124.38	si		
4	-2487.	40.6	20	3.14		.62189		124.38	si		
5	-2497.	40.6	20	3.14		.62189		124.38	si		
6	-2507.	40.6	20	3.14		.62189		124.38	si		
7	-2517.	40.6	20	3.14		.62189		124.38	si		
8	-2527.	40.6	20	3.14		.62189		124.38	si		
9	-2538.	40.6	20	3.14		.62189		124.38	si		
10	-2548.	40.6	20	3.14		.62189		124.38	si		
11	-2558.	40.6	20	3.14		.62189		124.38	si		
12	-2568.	40.6	20	3.14		.62189		124.38	si		
13	-2578.	40.6	20	3.14		.62189		124.38	si		
14	-2589.	40.6	20	3.14		.62189		124.38	si		
15	-2599.	40.6	20	3.14		.62189		124.38	si		
16	-2609.	40.6	20	3.14		.62189		124.38	si		
17	-2619.	40.6	20	3.14		.62189		124.38	si		
18	-2629.	40.6	20	3.14		.62189		124.38	si		
19	-2639.	40.6	20	3.14		.62189		124.38	si		
20	-2650.	40.6	20	3.14		.62189		124.38	si		
21	-2660.	40.6	20	3.14		.62189		124.38	si		
22	-2670.	40.6	20	3.14		.62189		124.38	si		
23	-2456.	67.6	20	3.14	1.27689	.62189		255.38	si		
24	-2466.	67.6	20	3.14	1.27689	.62189		255.38	si		
25	-2476.	67.6	20	3.14	1.27689	.62189		255.38	si		
26	-2487.	67.6	20	3.14	1.27689	.62189		255.38	si		
27	-2497.	67.6	20	3.14	1.27689	.62189		255.38	si		
28	-2507.	67.6	20	3.14	1.27689	.62189		255.38	si		
29	-2517.	67.6	20	3.14	1.27689	.62189		255.38	si		
30	-2527.	67.6	20	3.14	1.27689	.62189		255.38	si		
31	-2538.	67.6	20	3.14	1.27689	.62189		255.38	si		
32	-2548.	67.6	20	3.14	1.27689	.62189		255.38	si		
33	-2558.	67.6	20	3.14	1.27689	.62189		255.38	si		
34	-2568.	67.6	20	3.14	1.27689	.62189		255.38	si		
35	-2578.	67.6	20	3.14	1.27689	.62189		255.38	si		
36	-2589.	67.6	20	3.14	1.27689	.62189		255.38	si		
37	-2599.	67.6	20	3.14	1.27689	.62189		255.38	si		
38	-2609.	67.6	20	3.14	1.27689	.62189		255.38	si		
39	-2619.	67.6	20	3.14	1.27689	.62189		255.38	si		
40	-2629.	67.6	20	3.14	1.27689	.62189		255.38	si		
41	-2639.	67.6	20	3.14	1.27689	.62189		255.38	si		
42	-2650.	67.6	20	3.14	1.27689	.62189		255.38	si		
43	-2660.	67.6	20	3.14	1.27689	.62189		255.38	si		
44	-2670.	67.6	20	3.14	1.27689	.62189		255.38	si		
45	-2456.	-8.4	20	3.14		-.56681		-113.36	si		
46	-2473.	-8.4	20	3.14		-.56681		-113.36	si		
47	-2489.	-8.4	20	3.14		-.56681		-113.36	si		
48	-2505.	-8.4	20	3.14		-.56681		-113.36	si		
49	-2522.	-8.4	20	3.14		-.56681		-113.36	si		
50	-2538.	-8.4	20	3.14		-.56681		-113.36	si		
51	-2555.	-8.4	20	3.14		-.56681		-113.36	si		
52	-2571.	-8.4	20	3.14		-.56681		-113.36	si		
53	-2588.	-8.4	20	3.14		-.56681		-113.36	si		
54	-2604.	-8.4	20	3.14		-.56681		-113.36	si		
55	-2621.	-8.4	20	3.14		-.56681		-113.36	si		
56	-2637.	-8.4	20	3.14		-.56681		-113.36	si		
57	-2654.	-8.4	20	3.14		-.56681		-113.36	si		
58	-2670.	-8.4	20	3.14		-.56681		-113.36	si		

% ARMAT.: tesa = .77; comp. = .24; tot. = 1.01

Ripristino Ponte-Tubo

VERIFICA PULVINO YZ 11

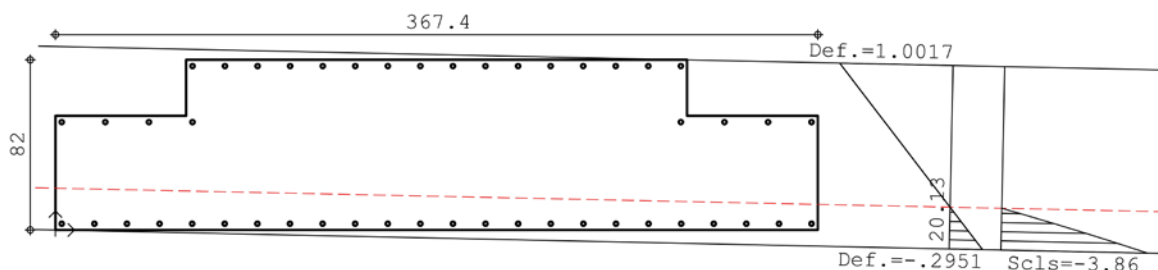
DESCRIZIONI
 Tipo sezione : U Pul
 Tipo verifica: sEato limite ultimo

CARATTERISTICHE DEI MATERIALI
 Calcestruzzo: Rck= 30.
 fck= 24.9
 fcd= 14.11 (.35%)
 Acciaio lento: Tipo= B450C
 fyk= 450.
 ftk= 540.
 ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
 eps= muz * y +muy * z + lam
 muz= 1.46596561901387E-05
 muy= 3.11289009896928E-07
 lam=-2.95115813492964E-04

SOLLECITAZIONI AGENTI:
 Nd in z= 183.7; y= 37.5 (baricentro CLS)
 Nd = -82.08
 Mdz= -834.3843
 Mdy= -384.495

UNITA' DI MISURA:
 kN; cm; kNm; N/mm2.
 Ø in mm; deformazioni*1000.
 SIMBOLI:
 S=sigma (tensioni sui materiali);
 D=deformazioni (epsilon):



TENSIONI NEL CLS:					
ver	z	y	Dcls	Scls	Ve
1	0.	55.	.51117	0.	si
2	63.	55.	.53078	0.	si
3	63.	82.	.92659	0.	si
4	304.4	82.	1.00173	0.	si
5	304.4	55.	.60592	0.	si
6	367.4	55.	.62553	0.	si
7	367.4	0.	-.18075	-2.44	si
8	0.	0.	-.29512	-3.86	si

TENSIONI NEI FERRI:										
Fer	z	y	Ø (mm)	Af (cm2)	D	ferri	S	ferri	Ve	
1	301.4	79.	20	3.14	.95682	191.36	si			
2	285.7	79.	20	3.14	.95193	190.39	si			
3	270.	79.	20	3.14	.94705	189.41	si			
4	254.3	79.	20	3.14	.94216	188.43	si			
5	238.6	79.	20	3.14	.93728	187.46	si			
6	222.9	79.	20	3.14	.93239	186.48	si			
7	207.2	79.	20	3.14	.92751	185.5	si			
8	191.5	79.	20	3.14	.92262	184.52	si			
9	175.9	79.	20	3.14	.91774	183.55	si			
10	160.2	79.	20	3.14	.91285	182.57	si			
11	144.5	79.	20	3.14	.90797	181.59	si			
12	128.8	79.	20	3.14	.90308	180.62	si			
13	113.1	79.	20	3.14	.8982	179.64	si			
14	97.4	79.	20	3.14	.89331	178.66	si			
15	81.7	79.	20	3.14	.88843	177.69	si			
16	66.	79.	20	3.14	.88354	176.71	si			
17	66.	52.	20	3.14	.48773	97.55	si			
18	45.	52.	20	3.14	.48119	96.24	si			
19	24.	52.	20	3.14	.47466	94.93	si			
20	3.	52.	20	3.14	.46812	93.62	si			
21	364.4	52.	20	3.14	.58062	116.12	si			
22	343.4	52.	20	3.14	.57408	114.82	si			
23	322.4	52.	20	3.14	.56755	113.51	si			
24	301.4	52.	20	3.14	.56101	112.2	si			
25	364.4	3.	20	3.14	-.1377	-27.54	si			
26	348.7	3.	20	3.14	-.14259	-28.52	si			
27	333.	3.	20	3.14	-.14749	-29.5	si			
28	317.3	3.	20	3.14	-.15238	-30.48	si			
29	301.5	3.	20	3.14	-.15727	-31.45	si			
30	285.8	3.	20	3.14	-.16216	-32.43	si			
31	270.1	3.	20	3.14	-.16705	-33.41	si			
32	254.4	3.	20	3.14	-.17194	-34.39	si			
33	238.7	3.	20	3.14	-.17683	-35.37	si			
34	223.	3.	20	3.14	-.18172	-36.34	si			
35	207.3	3.	20	3.14	-.18662	-37.32	si			
36	191.6	3.	20	3.14	-.19151	-38.3	si			
37	175.8	3.	20	3.14	-.1964	-39.28	si			
38	160.1	3.	20	3.14	-.20129	-40.26	si			
39	144.4	3.	20	3.14	-.20618	-41.24	si			
40	128.7	3.	20	3.14	-.21107	-42.21	si			
41	113.	3.	20	3.14	-.21596	-43.19	si			
42	97.3	3.	20	3.14	-.22086	-44.17	si			
43	81.6	3.	20	3.14	-.22575	-45.15	si			
44	65.9	3.	20	3.14	-.23064	-46.13	si			
45	50.1	3.	20	3.14	-.23553	-47.11	si			
46	34.4	3.	20	3.14	-.24042	-48.08	si			
47	18.7	3.	20	3.14	-.24531	-49.06	si			
48	3.	3.	20	3.14	-.2502	-50.04	si			

% ARMAT.: tesa= .28; comp.= .28; tot.= .56

Ripristino Ponte-Tubo
VERIFICA PULVINO XZ 12

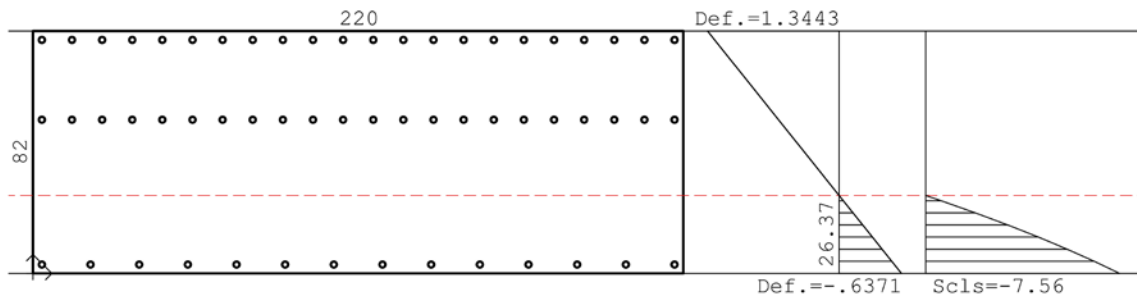
DESCRIZIONI
Tipo sezione : RETTANGOLARE
Tipo verifica: stato limite ultimo

CARATTERISTICHE DEI MATERIALI
Calcestruzzo: Rck= 30.
fck= 24.9
fcd= 14.11 (.35%)
Acciaio lento: Tipo= B450C
fyk= 450.
ftk= 540.
ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
eps= muz * y +muy * z + lam
muz= 2.41631187924551E-05
muy= 0
lam=-3.60397786597235E-04

SOLLECITAZIONI AGENTI:
Nd in y= 29.6 (baricentro CLS)
Nd = -212.53
Mdz=-1695.4582
verifica in pressoflessione retta

UNITA' DI MISURA:
kN; cm; kNm; N/mm2.
Ø in mm; deformazioni*1000.
SIMBOLI:
S=sigma (tensioni sui materiali);
D=deformazioni (epsilon):



TENSIONI NEL CLS:					
ver	Z	Y	Dcls	Scls	Vel
1	-2673.	70.6	1.34431	0.	si
2	-2453.	70.6	1.34431	0.	si
3	-2453.	-11.4	-.63707	-7.56	si
4	-2673.	-11.4	-.63707	-7.56	si

TENSIONI NEI FERRI:										
Fer	Z	Y	Ø (mm)	Af (cm2)	D	ferri	S	ferri	Vel	
1	-2456.	40.6	20	3.14		.61942		123.88	si	
3	-2466.	40.6	20	3.14		.61942		123.88	si	
3	-2476.	40.6	20	3.14		.61942		123.88	si	
4	-2487.	40.6	20	3.14		.61942		123.88	si	
5	-2497.	40.6	20	3.14		.61942		123.88	si	
6	-2507.	40.6	20	3.14		.61942		123.88	si	
7	-2517.	40.6	20	3.14		.61942		123.88	si	
8	-2527.	40.6	20	3.14		.61942		123.88	si	
9	-2538.	40.6	20	3.14		.61942		123.88	si	
10	-2548.	40.6	20	3.14		.61942		123.88	si	
11	-2558.	40.6	20	3.14		.61942		123.88	si	
12	-2568.	40.6	20	3.14		.61942		123.88	si	
13	-2578.	40.6	20	3.14		.61942		123.88	si	
14	-2589.	40.6	20	3.14		.61942		123.88	si	
15	-2599.	40.6	20	3.14		.61942		123.88	si	
16	-2609.	40.6	20	3.14		.61942		123.88	si	
17	-2619.	40.6	20	3.14		.61942		123.88	si	
18	-2629.	40.6	20	3.14		.61942		123.88	si	
19	-2639.	40.6	20	3.14		.61942		123.88	si	
20	-2650.	40.6	20	3.14		.61942		123.88	si	
21	-2660.	40.6	20	3.14		.61942		123.88	si	
22	-2670.	40.6	20	3.14		.61942		123.88	si	
23	-2456.	67.6	20	3.14	1.27182		254.36	si		
24	-2466.	67.6	20	3.14	1.27182		254.36	si		
25	-2476.	67.6	20	3.14	1.27182		254.36	si		
26	-2487.	67.6	20	3.14	1.27182		254.36	si		
27	-2497.	67.6	20	3.14	1.27182		254.36	si		
28	-2507.	67.6	20	3.14	1.27182		254.36	si		
29	-2517.	67.6	20	3.14	1.27182		254.36	si		
30	-2527.	67.6	20	3.14	1.27182		254.36	si		
31	-2538.	67.6	20	3.14	1.27182		254.36	si		
32	-2548.	67.6	20	3.14	1.27182		254.36	si		
33	-2558.	67.6	20	3.14	1.27182		254.36	si		
34	-2568.	67.6	20	3.14	1.27182		254.36	si		
35	-2578.	67.6	20	3.14	1.27182		254.36	si		
36	-2589.	67.6	20	3.14	1.27182		254.36	si		
37	-2599.	67.6	20	3.14	1.27182		254.36	si		
38	-2609.	67.6	20	3.14	1.27182		254.36	si		
39	-2619.	67.6	20	3.14	1.27182		254.36	si		
40	-2629.	67.6	20	3.14	1.27182		254.36	si		
41	-2639.	67.6	20	3.14	1.27182		254.36	si		
42	-2650.	67.6	20	3.14	1.27182		254.36	si		
43	-2660.	67.6	20	3.14	1.27182		254.36	si		
44	-2670.	67.6	20	3.14	1.27182		254.36	si		
45	-2456.	-8.4	20	3.14		-.56458		-112.92	si	
46	-2473.	-8.4	20	3.14		-.56458		-112.92	si	
47	-2489.	-8.4	20	3.14		-.56458		-112.92	si	
48	-2505.	-8.4	20	3.14		-.56458		-112.92	si	
49	-2522.	-8.4	20	3.14		-.56458		-112.92	si	
50	-2538.	-8.4	20	3.14		-.56458		-112.92	si	
51	-2555.	-8.4	20	3.14		-.56458		-112.92	si	
52	-2571.	-8.4	20	3.14		-.56458		-112.92	si	
53	-2588.	-8.4	20	3.14		-.56458		-112.92	si	
54	-2604.	-8.4	20	3.14		-.56458		-112.92	si	
55	-2621.	-8.4	20	3.14		-.56458		-112.92	si	
56	-2637.	-8.4	20	3.14		-.56458		-112.92	si	
57	-2654.	-8.4	20	3.14		-.56458		-112.92	si	
58	-2670.	-8.4	20	3.14		-.56458		-112.92	si	

% ARMAT.: tesa = .77; comp. = .24; tot. = 1.01

Ripristino Ponte-Tubo VERIFICA PULVINO YZ 12

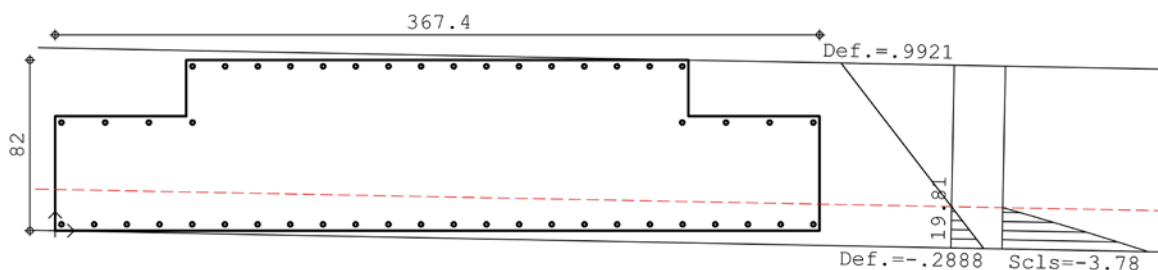
DESCRIZIONI
 Tipo sezione : U Pul
 Tipo verifica: stato limite ultimo

CARATTERISTICHE DEI MATERIALI
 Calcestruzzo: Rck= 30.
 fck= 24.9
 fcd= 14.11 (.35%)
 Acciaio lento: Tipo= B450C
 fyk= 450.
 ftk= 540.
 ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
 eps= muz * y + muy * z + lam
 muz= 1.45806411562549E-05
 muy= 2.80168886655232E-07
 lam=-2.88842562609724E-04

SOLLECITAZIONI AGENTI:
 Nd in z= 183.7; y= 37.5 (baricentro CLS)
 Nd = -86.74
 Mdz= -831.037
 Mdy= -346.8922

UNITA' DI MISURA:
 kN; cm; kNm; N/mm2.
 Ø in mm; deformazioni*1000.
 SIMBOLI:
 S=sigma (tensioni sui materiali);
 D=deformazioni (epsilon):



TENSIONI NEL CLS:			Dcls	Scls	Vel
ver	z	y			
1	0.	55.	.51309	0.	si
2	63.	55.	.53074	0.	si
3	63.	82.	.92442	0.	si
4	304.4	82.	.99205	0.	si
5	304.4	55.	.59838	0.	si
6	367.4	55.	.61603	0.	si
7	367.4	0.	-.18591	-2.5	si
8	0.	0.	-.28884	-3.78	si

TENSIONI NEI FERRI:									
Fer	z	y	Ø (mm)	Af (cm2)	D ferri	S ferri	Vel		
1	301.4	79.	20	3.14	.94747	189.49	si		
2	285.7	79.	20	3.14	.94307	188.61	si		
3	270.	79.	20	3.14	.93868	187.74	si		
4	254.3	79.	20	3.14	.93428	186.86	si		
5	238.6	79.	20	3.14	.92988	185.98	si		
6	222.9	79.	20	3.14	.92549	185.1	si		
7	207.2	79.	20	3.14	.92109	184.22	si		
8	191.5	79.	20	3.14	.91669	183.34	si		
9	175.9	79.	20	3.14	.9123	182.46	si		
10	160.2	79.	20	3.14	.9079	181.58	si		
11	144.5	79.	20	3.14	.9035	180.7	si		
12	128.8	79.	20	3.14	.89911	179.82	si		
13	113.1	79.	20	3.14	.89471	178.94	si		
14	97.4	79.	20	3.14	.89031	178.06	si		
15	81.7	79.	20	3.14	.88592	177.18	si		
16	66.	79.	20	3.14	.88152	176.3	si		
17	66.	52.	20	3.14	.48784	97.57	si		
18	45.	52.	20	3.14	.48196	96.39	si		
19	24.	52.	20	3.14	.47607	95.21	si		
20	3.	52.	20	3.14	.47019	94.04	si		
21	364.4	52.	20	3.14	.57144	114.29	si		
22	343.4	52.	20	3.14	.56556	113.11	si		
23	322.4	52.	20	3.14	.55968	111.94	si		
24	301.4	52.	20	3.14	.55379	110.76	si		
25	364.4	3.	20	3.14	-.14301	-28.6	si		
26	348.7	3.	20	3.14	-.14741	-29.48	si		
27	333.	3.	20	3.14	-.15181	-30.36	si		
28	317.3	3.	20	3.14	-.15621	-31.24	si		
29	301.5	3.	20	3.14	-.16062	-32.12	si		
30	285.8	3.	20	3.14	-.16502	-33.	si		
31	270.1	3.	20	3.14	-.16942	-33.88	si		
32	254.4	3.	20	3.14	-.17382	-34.76	si		
33	238.7	3.	20	3.14	-.17823	-35.65	si		
34	223.	3.	20	3.14	-.18263	-36.53	si		
35	207.3	3.	20	3.14	-.18703	-37.41	si		
36	191.6	3.	20	3.14	-.19143	-38.29	si		
37	175.8	3.	20	3.14	-.19583	-39.17	si		
38	160.1	3.	20	3.14	-.20024	-40.05	si		
39	144.4	3.	20	3.14	-.20464	-40.93	si		
40	128.7	3.	20	3.14	-.20904	-41.81	si		
41	113.	3.	20	3.14	-.21344	-42.69	si		
42	97.3	3.	20	3.14	-.21785	-43.57	si		
43	81.6	3.	20	3.14	-.22225	-44.45	si		
44	65.9	3.	20	3.14	-.22665	-45.33	si		
45	50.1	3.	20	3.14	-.23105	-46.21	si		
46	34.4	3.	20	3.14	-.23546	-47.09	si		
47	18.7	3.	20	3.14	-.23986	-47.97	si		
48	3.	3.	20	3.14	-.24426	-48.85	si		

% ARMAT.: tesa= .28; comp.= .28; tot.= .56

Ripristino Ponte-Tubo

VERIFICA PULVINO XZ 13

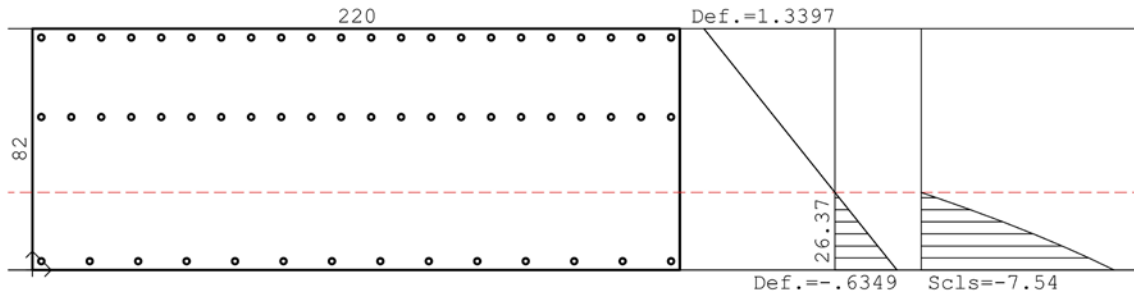
DESCRIZIONI
 Tipo sezione : RETTANGOLARE
 Tipo verifica: stato limite ultimo

CARATTERISTICHE DEI MATERIALI
 Calcestruzzo: Rck= 30.
 fck= 24.9
 fcd= 14.11 (.35%)
 Acciaio lento: Tipo= B450C
 fyk= 450.
 ftk= 540.
 ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
 eps= muz * y + muy * z + lam
 muz= 2.40805945946967E-05
 muy= 0
 lam=-3.59220457932026E-04

SOLLECITAZIONI AGENTI:
 Nd in y= 29.6 (baricentro CLS)
 Nd = -213.31
 Mdz=-1690.073
 verifica in pressoflessione retta

UNITA' DI MISURA:
 kN; cm; kNm; N/mm2.
 Ø in mm; deformazioni*1000.
 SIMBOLI:
 S=sigma (tensioni sui materiali);
 D=deformazioni (epsilon):



TENSIONI NEL CLS:					
ver	Z	Y	Dcls	Scls	Ve
1	-2673.	70.6	1.33967	0.	si
2	-2453.	70.6	1.33967	0.	si
3	-2453.	-11.4	-.63494	-7.54	si
4	-2673.	-11.4	-.63494	-7.54	si

TENSIONI NEI FERRI:									
Fer	Z	Y	Ø (mm)	Af (cm2)	D	ferri	S	ferri	Ve
1	-2456.	40.6	20	3.14		.61725		123.45	si
2	-2466.	40.6	20	3.14		.61725		123.45	si
3	-2476.	40.6	20	3.14		.61725		123.45	si
4	-2487.	40.6	20	3.14		.61725		123.45	si
5	-2497.	40.6	20	3.14		.61725		123.45	si
6	-2507.	40.6	20	3.14		.61725		123.45	si
7	-2517.	40.6	20	3.14		.61725		123.45	si
8	-2527.	40.6	20	3.14		.61725		123.45	si
9	-2538.	40.6	20	3.14		.61725		123.45	si
10	-2548.	40.6	20	3.14		.61725		123.45	si
11	-2558.	40.6	20	3.14		.61725		123.45	si
12	-2568.	40.6	20	3.14		.61725		123.45	si
13	-2578.	40.6	20	3.14		.61725		123.45	si
14	-2589.	40.6	20	3.14		.61725		123.45	si
15	-2599.	40.6	20	3.14		.61725		123.45	si
16	-2609.	40.6	20	3.14		.61725		123.45	si
17	-2619.	40.6	20	3.14		.61725		123.45	si
18	-2629.	40.6	20	3.14		.61725		123.45	si
19	-2639.	40.6	20	3.14		.61725		123.45	si
20	-2650.	40.6	20	3.14		.61725		123.45	si
21	-2660.	40.6	20	3.14		.61725		123.45	si
22	-2670.	40.6	20	3.14		.61725		123.45	si
23	-2456.	67.6	20	3.14	1.26742		253.48	si	si
24	-2466.	67.6	20	3.14	1.26742		253.48	si	si
25	-2476.	67.6	20	3.14	1.26742		253.48	si	si
26	-2487.	67.6	20	3.14	1.26742		253.48	si	si
27	-2497.	67.6	20	3.14	1.26742		253.48	si	si
28	-2507.	67.6	20	3.14	1.26742		253.48	si	si
29	-2517.	67.6	20	3.14	1.26742		253.48	si	si
30	-2527.	67.6	20	3.14	1.26742		253.48	si	si
31	-2538.	67.6	20	3.14	1.26742		253.48	si	si
32	-2548.	67.6	20	3.14	1.26742		253.48	si	si
33	-2558.	67.6	20	3.14	1.26742		253.48	si	si
34	-2568.	67.6	20	3.14	1.26742		253.48	si	si
35	-2578.	67.6	20	3.14	1.26742		253.48	si	si
36	-2589.	67.6	20	3.14	1.26742		253.48	si	si
37	-2599.	67.6	20	3.14	1.26742		253.48	si	si
38	-2609.	67.6	20	3.14	1.26742		253.48	si	si
39	-2619.	67.6	20	3.14	1.26742		253.48	si	si
40	-2629.	67.6	20	3.14	1.26742		253.48	si	si
41	-2639.	67.6	20	3.14	1.26742		253.48	si	si
42	-2650.	67.6	20	3.14	1.26742		253.48	si	si
43	-2660.	67.6	20	3.14	1.26742		253.48	si	si
44	-2670.	67.6	20	3.14	1.26742		253.48	si	si
45	-2456.	-8.4	20	3.14	-.5627		-112.54	si	si
46	-2473.	-8.4	20	3.14	-.5627		-112.54	si	si
47	-2489.	-8.4	20	3.14	-.5627		-112.54	si	si
48	-2505.	-8.4	20	3.14	-.5627		-112.54	si	si
49	-2522.	-8.4	20	3.14	-.5627		-112.54	si	si
50	-2538.	-8.4	20	3.14	-.5627		-112.54	si	si
51	-2555.	-8.4	20	3.14	-.5627		-112.54	si	si
52	-2571.	-8.4	20	3.14	-.5627		-112.54	si	si
53	-2588.	-8.4	20	3.14	-.5627		-112.54	si	si
54	-2604.	-8.4	20	3.14	-.5627		-112.54	si	si
55	-2621.	-8.4	20	3.14	-.5627		-112.54	si	si
56	-2637.	-8.4	20	3.14	-.5627		-112.54	si	si
57	-2654.	-8.4	20	3.14	-.5627		-112.54	si	si
58	-2670.	-8.4	20	3.14	-.5627		-112.54	si	si

% ARMAT.: tesa = .77; comp. = .24; tot. = 1.01

Ripristino Ponte-Tubo

VERIFICA PULVINO YZ 13

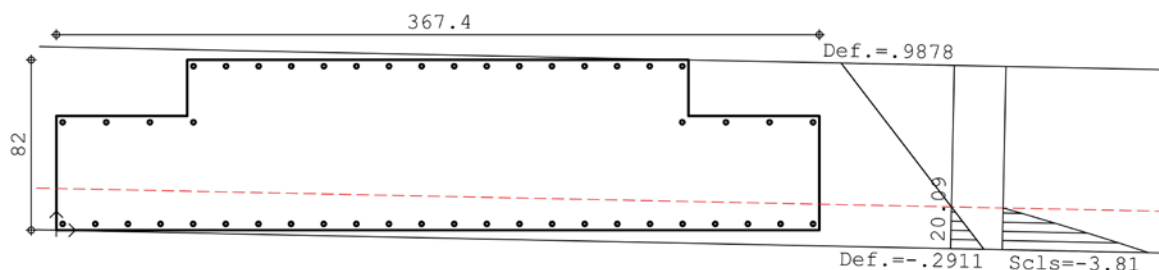
DESCRIZIONI
 Tipo sezione : U Pul
 Tipo verifica: sEato limite ultimo

CARATTERISTICHE DEI MATERIALI
 Calcestruzzo: Rck= 30.
 fck= 24.9
 fcd= 14.11 (.35%)
 Acciaio lento: Tipo= B450C
 fyk= 450.
 ftk= 540.
 ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
 eps= muz * y +muy * z + lam
 muz= 1.44877350946853E-05
 muy= 2.98600908784433E-07
 lam=-2.91067384584012E-04

SOLLECITAZIONI AGENTI:
 Nd in z= 183.7; y= 37.5 (baricentro CLS)
 Nd = -92.37
 Mdz = -827.0667
 Mdy = -370.1709

UNITA' DI MISURA:
 kN; cm; kNm; N/mm2.
 Ø in mm; deformazioni*1000.
 SIMBOLI:
 S=sigma (tensioni sui materiali);
 D=deformazioni (epsilon):



TENSIONI NEL CLS:					
ver	z	y	Dcls	Scls	Ve
1	0.	55.	.50576	0.	si
2	63.	55.	.52457	0.	si
3	63.	82.	.91574	0.	si
4	304.4	82.	.98782	0.	si
5	304.4	55.	.59665	0.	si
6	367.4	55.	.61546	0.	si
7	367.4	0.	-.18136	-2.44	si
8	0.	0.	-.29107	-3.81	si

TENSIONI NEI FERRI:										
fer	z	y	Ø (mm)	Af (cm2)	D ferri	S ferri	Ve ferri			
1	301.4	79.	20	3.14	.94346	188.69	si			
2	285.7	79.	20	3.14	.93878	187.76	si			
3	270.	79.	20	3.14	.93409	186.82	si			
4	254.3	79.	20	3.14	.9294	185.88	si			
5	238.6	79.	20	3.14	.92472	184.94	si			
6	222.9	79.	20	3.14	.92003	184.01	si			
7	207.2	79.	20	3.14	.91535	183.07	si			
8	191.5	79.	20	3.14	.91066	182.13	si			
9	175.9	79.	20	3.14	.90597	181.19	si			
10	160.2	79.	20	3.14	.90129	180.26	si			
11	144.5	79.	20	3.14	.8966	179.32	si			
12	128.8	79.	20	3.14	.89192	178.38	si			
13	113.1	79.	20	3.14	.88723	177.45	si			
14	97.4	79.	20	3.14	.88254	176.51	si			
15	81.7	79.	20	3.14	.87786	175.57	si			
16	66.	79.	20	3.14	.87317	174.63	si			
17	66.	52.	20	3.14	.482	96.4	si			
18	45.	52.	20	3.14	.47573	95.15	si			
19	24.	52.	20	3.14	.46946	93.89	si			
20	3.	52.	20	3.14	.46319	92.64	si			
21	364.4	52.	20	3.14	.57111	114.22	si			
22	343.4	52.	20	3.14	.56483	112.97	si			
23	322.4	52.	20	3.14	.55856	111.71	si			
24	301.4	52.	20	3.14	.55229	110.46	si			
25	364.4	3.	20	3.14	-.13879	-27.76	si			
26	348.7	3.	20	3.14	-.14349	-28.7	si			
27	333.	3.	20	3.14	-.14818	-29.64	si			
28	317.3	3.	20	3.14	-.15287	-30.57	si			
29	301.5	3.	20	3.14	-.15756	-31.51	si			
30	285.8	3.	20	3.14	-.16225	-32.45	si			
31	270.1	3.	20	3.14	-.16695	-33.39	si			
32	254.4	3.	20	3.14	-.17164	-34.33	si			
33	238.7	3.	20	3.14	-.17633	-35.27	si			
34	223.	3.	20	3.14	-.18102	-36.2	si			
35	207.3	3.	20	3.14	-.18571	-37.14	si			
36	191.6	3.	20	3.14	-.19041	-38.08	si			
37	175.8	3.	20	3.14	-.1951	-39.02	si			
38	160.1	3.	20	3.14	-.19979	-39.96	si			
39	144.4	3.	20	3.14	-.20448	-40.9	si			
40	128.7	3.	20	3.14	-.20917	-41.83	si			
41	113.	3.	20	3.14	-.21386	-42.77	si			
42	97.3	3.	20	3.14	-.21856	-43.71	si			
43	81.6	3.	20	3.14	-.22325	-44.65	si			
44	65.9	3.	20	3.14	-.22794	-45.59	si			
45	50.1	3.	20	3.14	-.23263	-46.53	si			
46	34.4	3.	20	3.14	-.23732	-47.46	si			
47	18.7	3.	20	3.14	-.24202	-48.4	si			
48	3.	3.	20	3.14	-.24671	-49.34	si			

% ARMAT.: tesa= .28; comp.= .28; tot.= .56

Ripristino Ponte-Tubo
VERIFICA PULVINO XZ 14

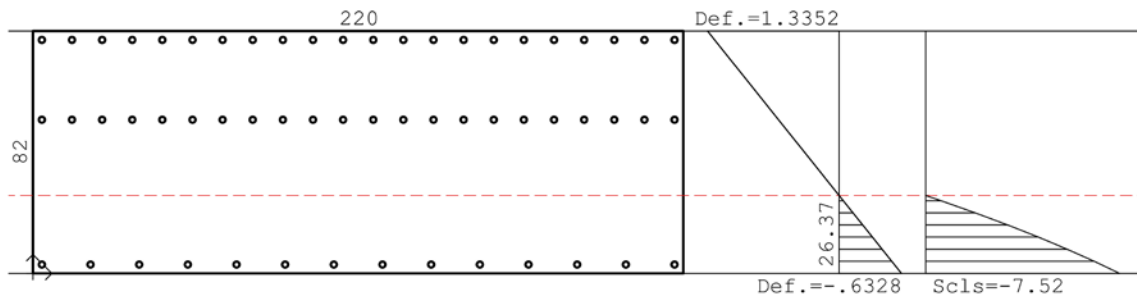
DESCRIZIONI
Tipo sezione : RETTANGOLARE
Tipo verifica: stato limite ultimo

CARATTERISTICHE DEI MATERIALI
Calcestruzzo: Rck= 30.
fck= 24.9
fcd= 14.11 (.35%)
Acciaio lento: Tipo= B450C
fyk= 450.
ftk= 540.
ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
eps= muz * y +muy * z + lam
muz= 2.40004341424946E-05
muy= 0
lam=-3.5798838337447E-04

SOLLECITAZIONI AGENTI:
Nd in y= 29.6 (baricentro CLS)
Nd = -213.13
Mdz=-1684.7059
verifica in pressoflessione retta

UNITA' DI MISURA:
kN; cm; kNm; N/mm2.
Ø in mm; deformazioni*1000.
SIMBOLI:
S=sigma (tensioni sui materiali);
D=deformazioni (epsilon):



TENSIONI NEL CLS:					
ver	Z	Y	Dcls	Scls	Ve
1	-2673.	70.6	1.33524	0.	si
2	-2453.	70.6	1.33524	0.	si
3	-2453.	-11.4	-0.63279	-7.52	si
4	-2673.	-11.4	-0.63279	-7.52	si

TENSIONI NEI FERRI:											
Fer	Z	Y	Ø (mm)	Af (cm2)	D	ferri	S	ferri	Ve		
1	-2456.	40.6	20	3.14		.61523		123.05	si		
3	-2476.	40.6	20	3.14		.61523		123.05	si		
4	-2487.	40.6	20	3.14		.61523		123.05	si		
5	-2497.	40.6	20	3.14		.61523		123.05	si		
6	-2507.	40.6	20	3.14		.61523		123.05	si		
7	-2517.	40.6	20	3.14		.61523		123.05	si		
8	-2527.	40.6	20	3.14		.61523		123.05	si		
9	-2538.	40.6	20	3.14		.61523		123.05	si		
10	-2548.	40.6	20	3.14		.61523		123.05	si		
11	-2558.	40.6	20	3.14		.61523		123.05	si		
12	-2568.	40.6	20	3.14		.61523		123.05	si		
13	-2578.	40.6	20	3.14		.61523		123.05	si		
14	-2589.	40.6	20	3.14		.61523		123.05	si		
15	-2599.	40.6	20	3.14		.61523		123.05	si		
16	-2609.	40.6	20	3.14		.61523		123.05	si		
17	-2619.	40.6	20	3.14		.61523		123.05	si		
18	-2629.	40.6	20	3.14		.61523		123.05	si		
19	-2639.	40.6	20	3.14		.61523		123.05	si		
20	-2650.	40.6	20	3.14		.61523		123.05	si		
21	-2660.	40.6	20	3.14		.61523		123.05	si		
22	-2670.	40.6	20	3.14		.61523		123.05	si		
23	-2456.	67.6	20	3.14	1.26324	252.65		252.65	si		
24	-2466.	67.6	20	3.14	1.26324	252.65		252.65	si		
25	-2476.	67.6	20	3.14	1.26324	252.65		252.65	si		
26	-2487.	67.6	20	3.14	1.26324	252.65		252.65	si		
27	-2497.	67.6	20	3.14	1.26324	252.65		252.65	si		
28	-2507.	67.6	20	3.14	1.26324	252.65		252.65	si		
29	-2517.	67.6	20	3.14	1.26324	252.65		252.65	si		
30	-2527.	67.6	20	3.14	1.26324	252.65		252.65	si		
31	-2538.	67.6	20	3.14	1.26324	252.65		252.65	si		
32	-2548.	67.6	20	3.14	1.26324	252.65		252.65	si		
33	-2558.	67.6	20	3.14	1.26324	252.65		252.65	si		
34	-2568.	67.6	20	3.14	1.26324	252.65		252.65	si		
35	-2578.	67.6	20	3.14	1.26324	252.65		252.65	si		
36	-2589.	67.6	20	3.14	1.26324	252.65		252.65	si		
37	-2599.	67.6	20	3.14	1.26324	252.65		252.65	si		
38	-2609.	67.6	20	3.14	1.26324	252.65		252.65	si		
39	-2619.	67.6	20	3.14	1.26324	252.65		252.65	si		
40	-2629.	67.6	20	3.14	1.26324	252.65		252.65	si		
41	-2639.	67.6	20	3.14	1.26324	252.65		252.65	si		
42	-2650.	67.6	20	3.14	1.26324	252.65		252.65	si		
43	-2660.	67.6	20	3.14	1.26324	252.65		252.65	si		
44	-2670.	67.6	20	3.14	1.26324	252.65		252.65	si		
45	-2456.	-8.4	20	3.14	-56079	-112.16		-112.16	si		
46	-2473.	-8.4	20	3.14	-56079	-112.16		-112.16	si		
47	-2489.	-8.4	20	3.14	-56079	-112.16		-112.16	si		
48	-2505.	-8.4	20	3.14	-56079	-112.16		-112.16	si		
49	-2522.	-8.4	20	3.14	-56079	-112.16		-112.16	si		
50	-2538.	-8.4	20	3.14	-56079	-112.16		-112.16	si		
51	-2555.	-8.4	20	3.14	-56079	-112.16		-112.16	si		
52	-2571.	-8.4	20	3.14	-56079	-112.16		-112.16	si		
53	-2588.	-8.4	20	3.14	-56079	-112.16		-112.16	si		
54	-2604.	-8.4	20	3.14	-56079	-112.16		-112.16	si		
55	-2621.	-8.4	20	3.14	-56079	-112.16		-112.16	si		
56	-2637.	-8.4	20	3.14	-56079	-112.16		-112.16	si		
57	-2654.	-8.4	20	3.14	-56079	-112.16		-112.16	si		
58	-2670.	-8.4	20	3.14	-56079	-112.16		-112.16	si		

% ARMAT.: tesa = .77; comp. = .24; tot. = 1.01

Ripristino Ponte-Tubo

VERIFICA PULVINO YZ 14

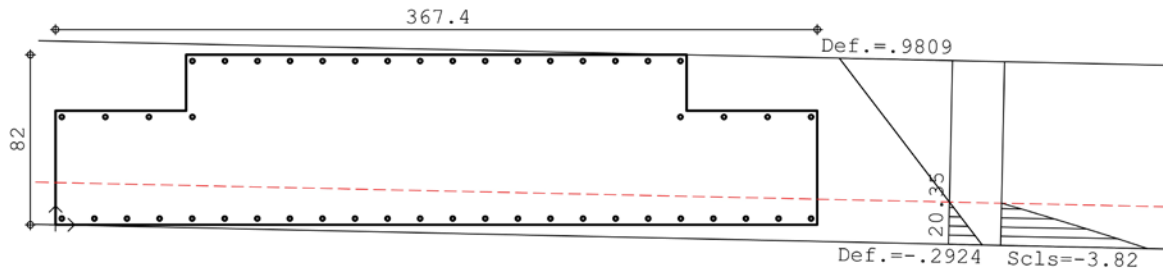
DESCRIZIONI
 Tipo sezione : U Pul
 Tipo verifica: sEato limite ultimo

CARATTERISTICHE DEI MATERIALI
 Calcestruzzo: Rck= 30.
 fck= 24.9
 fcd= 14.11 (.35%)
 Acciaio lento: Tipo= B450C
 fyk= 450.
 ftk= 540.
 ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
 eps= muz * y +muy * z + lam
 muz= 1.43649972079576E-05
 muy= 3.13181609501079E-07
 lam=-2.92369527189875E-04

SOLLECITAZIONI AGENTI:
 Nd in z= 183.7; y= 37.5 (baricentro CLS)
 Nd = -100.66
 Mdz = -822.0123
 Mdy = -389.0758

UNITA' DI MISURA:
 kN; cm; kNm; N/mm2.
 Ø in mm; deformazioni*1000.
 SIMBOLI:
 S=sigma (tensioni sui materiali);
 D=deformazioni (epsilon):



TENSIONI NEL CLS:					
ver	z	y	Dcls	Scls	Ve
1	0.	55.	.49771	0.	si
2	63.	55.	.51744	0.	si
3	63.	82.	.90529	0.	si
4	304.4	82.	.98089	0.	si
5	304.4	55.	.59304	0.	si
6	367.4	55.	.61277	0.	si
7	367.4	0.	-.17731	-2.39	si
8	0.	0.	-.29237	-3.82	si

TENSIONI NEI FERRI:									
Fer	z	y	Ø (mm)	Af (cm2)	D	ferri	S	ferri	Ve
1	301.4	79.	20	3.14	.93686	187.37	si	187.37	si
2	285.7	79.	20	3.14	.93194	186.39	si	186.39	si
3	270.	79.	20	3.14	.92703	185.41	si	185.41	si
4	254.3	79.	20	3.14	.92211	184.42	si	184.42	si
5	238.6	79.	20	3.14	.9172	183.44	si	183.44	si
6	222.9	79.	20	3.14	.91228	182.46	si	182.46	si
7	207.2	79.	20	3.14	.90737	181.47	si	181.47	si
8	191.5	79.	20	3.14	.90245	180.49	si	180.49	si
9	175.9	79.	20	3.14	.89754	179.51	si	179.51	si
10	160.2	79.	20	3.14	.89262	178.52	si	178.52	si
11	144.5	79.	20	3.14	.88771	177.54	si	177.54	si
12	128.8	79.	20	3.14	.88279	176.56	si	176.56	si
13	113.1	79.	20	3.14	.87788	175.58	si	175.58	si
14	97.4	79.	20	3.14	.87297	174.59	si	174.59	si
15	81.7	79.	20	3.14	.86805	173.61	si	173.61	si
16	66.	79.	20	3.14	.86314	172.63	si	172.63	si
17	66.	52.	20	3.14	.47528	95.06	si	95.06	si
18	45.	52.	20	3.14	.4687	93.74	si	93.74	si
19	24.	52.	20	3.14	.46213	92.43	si	92.43	si
20	3.	52.	20	3.14	.45555	91.11	si	91.11	si
21	364.4	52.	20	3.14	.56873	113.75	si	113.75	si
22	343.4	52.	20	3.14	.56216	112.43	si	112.43	si
23	322.4	52.	20	3.14	.55558	111.12	si	111.12	si
24	301.4	52.	20	3.14	.549	109.8	si	109.8	si
25	364.4	3.	20	3.14	-.13515	-27.03	si	-27.03	si
26	348.7	3.	20	3.14	-.14007	-28.01	si	-28.01	si
27	333.	3.	20	3.14	-.14499	-29.	si	-29.	si
28	317.3	3.	20	3.14	-.14991	-29.98	si	-29.98	si
29	301.5	3.	20	3.14	-.15484	-30.97	si	-30.97	si
30	285.8	3.	20	3.14	-.15976	-31.95	si	-31.95	si
31	270.1	3.	20	3.14	-.16468	-32.94	si	-32.94	si
32	254.4	3.	20	3.14	-.1696	-33.92	si	-33.92	si
33	238.7	3.	20	3.14	-.17452	-34.9	si	-34.9	si
34	223.	3.	20	3.14	-.17944	-35.89	si	-35.89	si
35	207.3	3.	20	3.14	-.18436	-36.87	si	-36.87	si
36	191.6	3.	20	3.14	-.18928	-37.86	si	-37.86	si
37	175.8	3.	20	3.14	-.1942	-38.84	si	-38.84	si
38	160.1	3.	20	3.14	-.19912	-39.82	si	-39.82	si
39	144.4	3.	20	3.14	-.20405	-40.81	si	-40.81	si
40	128.7	3.	20	3.14	-.20897	-41.79	si	-41.79	si
41	113.	3.	20	3.14	-.21389	-42.78	si	-42.78	si
42	97.3	3.	20	3.14	-.21881	-43.76	si	-43.76	si
43	81.6	3.	20	3.14	-.22373	-44.75	si	-44.75	si
44	65.9	3.	20	3.14	-.22865	-45.73	si	-45.73	si
45	50.1	3.	20	3.14	-.23357	-46.71	si	-46.71	si
46	34.4	3.	20	3.14	-.23849	-47.7	si	-47.7	si
47	18.7	3.	20	3.14	-.24341	-48.68	si	-48.68	si
48	3.	3.	20	3.14	-.24833	-49.67	si	-49.67	si

% ARMAT.: tesa = .28; comp. = .28; tot. = .56

Ripristino Ponte-Tubo
VERIFICA PULVINO XZ 15

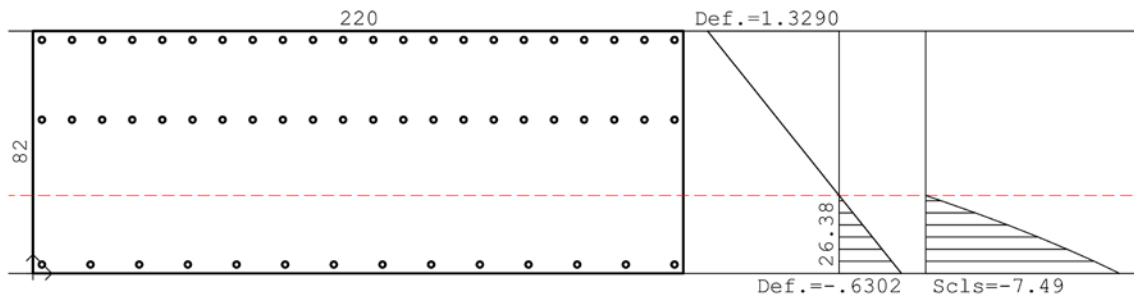
DESCRIZIONI
Tipo sezione : RETTANGOLARE
Tipo verifica: stato limite ultimo

CARATTERISTICHE DEI MATERIALI
Calcestruzzo: Rck= 30.
fck= 24.9
fcd= 14.11 (.35%)
Acciaio lento: Tipo= B450C
fyk= 450.
ftk= 540.
ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
eps= muz * y + muy * z + lam
muz= 2.38933005900338E-05
muy= 0
lam=-3.56652956564046E-04

SOLLECITAZIONI AGENTI:
Nd in y= 29.6 (baricentro CLS)
Nd = -216.16
Mdz=-1678.002
verifica in pressoflessione retta

UNITA' DI MISURA:
kN; cm; kNm; N/mm2.
Ø in mm; deformazioni*1000.
SIMBOLI:
S=sigma (tensioni sui materiali);
D=deformazioni (epsilon):



TENSIONI NEL CLS:				
ver	Z	Y	Dcls	Scls Vel
1	-2673.	70.6	1.32902	0. si
2	-2453.	70.6	1.32902	0. si
3	-2453.	-11.4	-.63023	-7.49 si
4	-2673.	-11.4	-.63023	-7.49 si

TENSIONI NEI FERRI:									
Fer	Z	Y	Ø (mm)	Af (cm2)	D	ferri	S	ferri	Vel
1	-2456.	40.6	20	3.14		.61222		122.44	si
3	-2476.	40.6	20	3.14		.61222		122.44	si
4	-2487.	40.6	20	3.14		.61222		122.44	si
5	-2497.	40.6	20	3.14		.61222		122.44	si
6	-2507.	40.6	20	3.14		.61222		122.44	si
7	-2517.	40.6	20	3.14		.61222		122.44	si
8	-2527.	40.6	20	3.14		.61222		122.44	si
9	-2538.	40.6	20	3.14		.61222		122.44	si
10	-2548.	40.6	20	3.14		.61222		122.44	si
11	-2558.	40.6	20	3.14		.61222		122.44	si
12	-2568.	40.6	20	3.14		.61222		122.44	si
13	-2578.	40.6	20	3.14		.61222		122.44	si
14	-2589.	40.6	20	3.14		.61222		122.44	si
15	-2599.	40.6	20	3.14		.61222		122.44	si
16	-2609.	40.6	20	3.14		.61222		122.44	si
17	-2619.	40.6	20	3.14		.61222		122.44	si
18	-2629.	40.6	20	3.14		.61222		122.44	si
19	-2639.	40.6	20	3.14		.61222		122.44	si
20	-2650.	40.6	20	3.14		.61222		122.44	si
21	-2660.	40.6	20	3.14		.61222		122.44	si
22	-2670.	40.6	20	3.14		.61222		122.44	si
23	-2456.	67.6	20	3.14	1.25734			251.47	si
24	-2466.	67.6	20	3.14	1.25734			251.47	si
25	-2476.	67.6	20	3.14	1.25734			251.47	si
26	-2487.	67.6	20	3.14	1.25734			251.47	si
27	-2497.	67.6	20	3.14	1.25734			251.47	si
28	-2507.	67.6	20	3.14	1.25734			251.47	si
29	-2517.	67.6	20	3.14	1.25734			251.47	si
30	-2527.	67.6	20	3.14	1.25734			251.47	si
31	-2538.	67.6	20	3.14	1.25734			251.47	si
32	-2548.	67.6	20	3.14	1.25734			251.47	si
33	-2558.	67.6	20	3.14	1.25734			251.47	si
34	-2568.	67.6	20	3.14	1.25734			251.47	si
35	-2578.	67.6	20	3.14	1.25734			251.47	si
36	-2589.	67.6	20	3.14	1.25734			251.47	si
37	-2599.	67.6	20	3.14	1.25734			251.47	si
38	-2609.	67.6	20	3.14	1.25734			251.47	si
39	-2619.	67.6	20	3.14	1.25734			251.47	si
40	-2629.	67.6	20	3.14	1.25734			251.47	si
41	-2639.	67.6	20	3.14	1.25734			251.47	si
42	-2650.	67.6	20	3.14	1.25734			251.47	si
43	-2660.	67.6	20	3.14	1.25734			251.47	si
44	-2670.	67.6	20	3.14	1.25734			251.47	si
45	-2456.	-8.4	20	3.14		-.55855		-111.71	si
46	-2473.	-8.4	20	3.14		-.55855		-111.71	si
47	-2489.	-8.4	20	3.14		-.55855		-111.71	si
48	-2505.	-8.4	20	3.14		-.55855		-111.71	si
49	-2522.	-8.4	20	3.14		-.55855		-111.71	si
50	-2538.	-8.4	20	3.14		-.55855		-111.71	si
51	-2555.	-8.4	20	3.14		-.55855		-111.71	si
52	-2571.	-8.4	20	3.14		-.55855		-111.71	si
53	-2588.	-8.4	20	3.14		-.55855		-111.71	si
54	-2604.	-8.4	20	3.14		-.55855		-111.71	si
55	-2621.	-8.4	20	3.14		-.55855		-111.71	si
56	-2637.	-8.4	20	3.14		-.55855		-111.71	si
57	-2654.	-8.4	20	3.14		-.55855		-111.71	si
58	-2670.	-8.4	20	3.14		-.55855		-111.71	si

% ARMAT.: tesa = .77; comp. = .24; tot. = 1.01

Ripristino Ponte-Tubo

VERIFICA PULVINO YZ 15

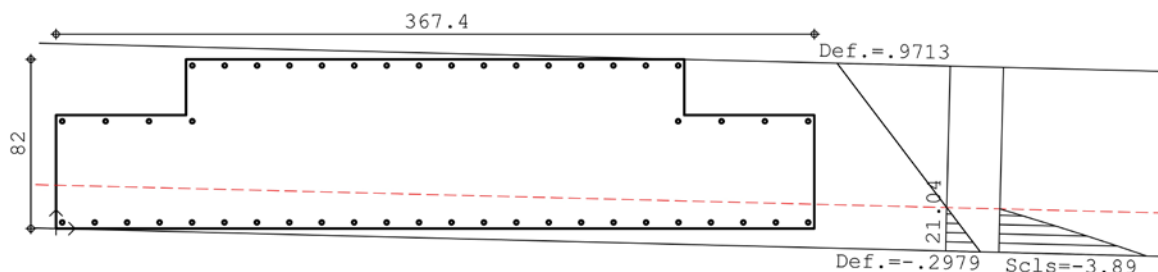
DESCRIZIONI
 Tipo sezione : U Pul
 Tipo verifica: sTato limite ultimo

CARATTERISTICHE DEI MATERIALI
 Calcestruzzo: Rck= 30.
 fck= 24.9
 fcd= 14.11 (.35%)
 Acciaio lento: Tipo= B450C
 fyk= 450.
 ftk= 540.
 ftd= 469.57 (6.75%)

PIANO DI EQUILIBRIO:
 eps= muz * y +muy * z + lam
 muz= 1.415474508051444E-05
 muy= 3.56286505521731E-07
 lam=-2.9785876301837E-04

SOLLECITAZIONI AGENTI:
 Nd in z= 183.7; y= 37.5 (baricentro CLS)
 Nd = -116.65
 Mdz = -813.6984
 Mdy = -444.1513

UNITA' DI MISURA:
 kN; cm; kNm; N/mm2.
 Ø in mm; deformazioni*1000.
 SIMBOLI:
 S=sigma (tensioni sui materiali);
 D=deformazioni (epsilon):



TENSIONI NEL CLS:			Dcls	Scls	Vel
ver	z	y			
1	0.	55.	.48065	0.	si
2	63.	55.	.5031	0.	si
3	63.	82.	.88528	0.	si
4	304.4	82.	.97128	0.	si
5	304.4	55.	.58911	0.	si
6	367.4	55.	.61155	0.	si
7	367.4	0.	-.16696	-2.26	si
8	0.	0.	-.29786	-3.89	si

TENSIONI NEI FERRI:									
Fer	z	y	Ø (mm)	Af (cm2)	D	ferri	S	ferri	Vel
1	301.4	79.	20	3.14	3.14	.92775		185.45	si
2	285.7	79.	20	3.14	3.14	.92216		184.43	si
3	270.	79.	20	3.14	3.14	.91657		183.31	si
4	254.3	79.	20	3.14	3.14	.91098		182.2	si
5	238.6	79.	20	3.14	3.14	.90539		181.08	si
6	222.9	79.	20	3.14	3.14	.89979		179.96	si
7	207.2	79.	20	3.14	3.14	.8942		178.84	si
8	191.5	79.	20	3.14	3.14	.88861		177.72	si
9	175.9	79.	20	3.14	3.14	.88302		176.6	si
10	160.2	79.	20	3.14	3.14	.87743		175.49	si
11	144.5	79.	20	3.14	3.14	.87184		174.37	si
12	128.8	79.	20	3.14	3.14	.86625		173.25	si
13	113.1	79.	20	3.14	3.14	.86065		172.13	si
14	97.4	79.	20	3.14	3.14	.85506		171.01	si
15	81.7	79.	20	3.14	3.14	.84947		169.89	si
16	66.	79.	20	3.14	3.14	.84388		168.78	si
17	66.	52.	20	3.14	3.14	.4617		92.34	si
18	45.	52.	20	3.14	3.14	.45422		90.84	si
19	24.	52.	20	3.14	3.14	.44674		89.35	si
20	3.	52.	20	3.14	3.14	.43926		87.85	si
21	364.4	52.	20	3.14	3.14	.56802		113.6	si
22	343.4	52.	20	3.14	3.14	.56054		112.11	si
23	322.4	52.	20	3.14	3.14	.55305		110.61	si
24	301.4	52.	20	3.14	3.14	.54557		109.11	si
25	364.4	3.	20	3.14	3.14	-.12556		-25.11	si
26	348.7	3.	20	3.14	3.14	-.13116		-26.23	si
27	333.	3.	20	3.14	3.14	-.13676		-27.35	si
28	317.3	3.	20	3.14	3.14	-.14236		-28.47	si
29	301.5	3.	20	3.14	3.14	-.14796		-29.59	si
30	285.8	3.	20	3.14	3.14	-.15356		-30.71	si
31	270.1	3.	20	3.14	3.14	-.15915		-31.83	si
32	254.4	3.	20	3.14	3.14	-.16475		-32.95	si
33	238.7	3.	20	3.14	3.14	-.17035		-34.07	si
34	223.	3.	20	3.14	3.14	-.17595		-35.19	si
35	207.3	3.	20	3.14	3.14	-.18155		-36.31	si
36	191.6	3.	20	3.14	3.14	-.18715		-37.43	si
37	175.8	3.	20	3.14	3.14	-.19274		-38.55	si
38	160.1	3.	20	3.14	3.14	-.19834		-39.67	si
39	144.4	3.	20	3.14	3.14	-.20394		-40.79	si
40	128.7	3.	20	3.14	3.14	-.20954		-41.91	si
41	113.	3.	20	3.14	3.14	-.21514		-43.03	si
42	97.3	3.	20	3.14	3.14	-.22074		-44.15	si
43	81.6	3.	20	3.14	3.14	-.22633		-45.27	si
44	65.9	3.	20	3.14	3.14	-.23193		-46.39	si
45	50.1	3.	20	3.14	3.14	-.23753		-47.51	si
46	34.4	3.	20	3.14	3.14	-.24313		-48.63	si
47	18.7	3.	20	3.14	3.14	-.24873		-49.75	si
48	3.	3.	20	3.14	3.14	-.25433		-50.87	si

% ARMAT.: tesa= .28; comp.= .28; tot.= .56